

New Quincy Courthouse

Draft Environmental Impact Report

APPENDICES
Volume 1

Prepared for:
Judicial Council of California

NOVEMBER 2026

NEW QUINCY COURTHOUSE PROJECT

Draft Environmental Impact Report

Appendices (Volume 1)

Prepared for:

Judicial Council of California
2860 Gateway Oaks, Suite 400
Sacramento, CA 95833-3509

Contact:

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Prepared by:

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INTRODUCTION

The technical appendices for the New Quincy Courthouse Draft Environmental Impact Report (EIR) are presented in two volumes. This document is Appendices Volume 1 of the Draft EIR.

Volume 1 presents the following appendices:

Appendix A. Notice of Preparation and Public Scoping Comments

Appendix B. Air Quality and GHG Emissions Calculations

Appendix C. Biological Resources Report

Appendix D. Historical Resources Study & Archaeological Resources Report

Appendix E. Geotechnical Engineering and Geohazard Study

Volume 2 presents the following appendices:

Appendix F. Phase I Environmental Site Assessment

Appendix G. Hazardous Building Material Survey

Appendix H. CEQA Transportation Analysis Memo

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APPENDIX A

Notice of Preparation and Public Scoping Comments

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NOTICE OF PREPARATION

OF AN ENVIRONMENTAL IMPACT REPORT

NEW QUINCY COURTHOUSE

DATE: October 15, 2025

TO: Responsible and Trustee Agencies, Interested Parties, and Organizations

SUBJECT: Notice of Preparation of an Environmental Impact Report for the New Quincy Courthouse

The Judicial Council of California (Judicial Council) is the lead agency and will prepare an Environmental Impact Report ("EIR") compliant with the California Environmental Quality Act ("CEQA") for the proposed New Quincy Courthouse (the "Project"). No Initial Study was prepared as the Judicial Council has determined that an EIR is clearly required for the Project. In accordance with Section 15082 of the CEQA Guidelines, this Notice of Preparation ("NOP") provides the Project location, a brief Project description, and a summary of the potential environmental impacts of the proposed Project.

The purpose of this NOP is to provide an opportunity to comment on the scope and proposed content of the EIR. In accordance with Public Resources Code sections 21092(b)(1) and 21083.9, this NOP is public notice that the Judicial Council will hold a public scoping meeting as described below. As provided in CEQA Guidelines section 15082, the Judicial Council invites responsible and trustee agencies to provide information relevant to the analysis of environmental resources falling within the jurisdiction of such agencies. Specifically, input is requested on:

1. **Scope and Content of Environmental Analysis**—guidance on the scope and content of analysis for this EIR within the agency's area of statutory responsibility, including identification of specific significant environmental issues that will require closer study due to the location, scale, and character of the Project, and whether the agency will be a responsible agency or trustee agency for the Project;

2. **Mitigation Measures**—proposals for feasible mitigation, including mitigation that would avoid or reduce potentially significant or significant impacts to environmental resources; and

3. **Alternatives**—proposals for alternatives to the proposed Project that could reduce or avoid potentially significant or significant impacts.

As outlined in CEQA Guidelines Section 15082(b), each responsible and trustee agency must identify specific environmental issues, alternatives, and mitigation measures that should be explored in the EIR. If there is no response within 30 days, the Judicial Council will presume

that there are no specific environmental issues, alternatives, or mitigation measures that the responsible and trustee agencies believe should be incorporated into the EIR.

WRITTEN COMMENTS ON THE NOTICE OF PREPARATION

Please provide your written comments by **November 17, 2025**. Comments, along with the name and contact information of the appropriate person in your organization, should be addressed to:

> Alex Cervantes, Senior Facilities Analyst
> Judicial Council of California, Facilities Services
> 2860 Gateway Oaks Drive, Suite 400, Sacramento, CA 95833-3509
>
> newquincycourthouseproject@jud.ca.gov (enter "New Quincy Courthouse NOP in the 'Subject' line)

The Judicial Council will hold a public scoping meeting on **Thursday, October 23, 2025, from 6:00 p.m. to 7:00 p.m**. at the following location:

> Plumas County Fairgrounds
> Mineral Building
> 204 Fairgrounds Road
> Quincy, CA 93433

Parking: Available in and around the Fairground Mineral Building.

Information related to the proposed Project, including how to access the Project documents and how to participate in the public review process will be provided at the scoping meeting. Information related to this Project is available for review on the Judicial Council's website at: https://courts.ca.gov/facilities/plumas-county-new-quincy-courthouse.

PROJECT LOCATION AND SURROUNDING LAND USES

The Judicial Council proposes to construct a new courthouse to relocate Superior Court operations that are currently housed in the Plumas County Courthouse located at 520 Main Street in Quincy, California.

The 2.86-acre Project site consists of three contiguous, privately-owned parcels in the unincorporated town of Quincy in Plumas County (Figure 1). Site addresses include 253 Lawrence Street (APN 115-031-055), 287 Lawrence Street (APN 115-031-052), and 293 Lawrence Street (APN 115-031-054). The Project site is currently developed with three commercial buildings—Feather Publishing Co., Inc. at 287 Lawrence Street, a storage facility for boats and recreational trailers at 253 Lawrence Street, and the Quincy Paint Center and The2Mic (amplification supplies for guitars) at 293 Lawrence Street, which was previously occupied by Quincy Lumber & Supply. There are paved parking areas around the structures in the southern and central portions of the Site, with the northwestern and northern portions consisting of an unpaved gravel surface.

Lawrence Street in this location in downtown Quincy serves as State Routes (SR) 70/89. The Project site is bounded by Lawrence Street/SR 70/89 to the south, multi-family and single-family residential land uses to the west, a bike path along a former railroad alignment and a defunct, former wastewater treatment plant to the north, and multi-family residential and commercial land uses to the east (Figure 2).

The Plumas County General Plan designates the Project site parcels for Commercial land use. The Commercial land use designation identifies locations that are appropriate for a wide range of commercial operations, including retail, offices, and services and allows for residential use in conjunction with commercial uses. The County zoning district for this site is Periphery Commercial (C-2), which includes a broad assortment of commercial uses, parking lots, and dwelling units.

The Project's proposed use of the property is consistent with the commercial land use designation by the Plumas County General Plan and the Periphery Commercial (C-2) zoning district that allow for the construction, use and occupancy of business office buildings and facilities. The Judicial Council, acting as the judicial branch of State government, is not subject to local land use regulations; however, the Judicial Council, as appropriate, considers local policies in evaluating whether the Project's impacts would be significant and the above information regarding the County's General Plan and zoning is presented for context.

This Project site location was selected by the Judicial Council's Court Facilities Advisory Committee (CFAC) after research and evaluation of ten potential project sites.

PROPOSED PROJECT

The existing Plumas County Courthouse is owned by Plumas County. The County's plans for repurposing the existing Plumas County Courthouse are not currently available and are not part of the Project.

The Project would provide a new permanent state-owned courthouse facility that is accessible to the public and can provide enhanced services to the public. The Project would include construction of courtrooms with support spaces, administrative and operations areas, and an entry plaza. The Project also includes site improvements, including new on-site surface parking lots and drive aisles, and rerouted utility connections to serve the new building. The Project will include demolition of the existing structures on the Project site.

PROPOSED FACILITIES

The Project would be an approximately 23,000 square-foot, 1-story courthouse building. The Project does not propose any subterranean building area.

High volume public functions, court, and court support functions would all take place on the single ground floor level of the new courthouse. The new courthouse building would include the following features and areas:

- Two courtrooms
- Multipurpose room
- Public lobby and security screening area
- Chambers and courtroom support areas
- Court operations area
- Clerk's office

- Family court services area
- Self-help area
- Space for administration and information technology
- Jury Services area
- Sheriff area
- Central in-custody holding area
- Space for staff and building support
- Secured loading zone and sallyport

The new courthouse building would be set back a minimum of 25 feet from the nearest property lines (i.e., the western and southern site boundaries). The Conceptual Site Plan is shown in Figure 3. The Project will be designed and constructed according to the 2023 Judicial Council of California Trial Court Facility Standards.

Access and Utilities

The existing vehicle entrance to the Project site is established off Lawrence Street/SR-70/89 along the southern property boundary. The Project proposes to use this existing public access. A second access for emergency vehicles only would be provided at the northeast end of the property from the Summerfield Lane cul-de-sac.

The Project site is served by American Valley Community Services District for water and wastewater service, Plumas County Public Works Department for stormwater drainage and solid waste collection and disposal, and Pacific Gas and Electric (PG&E) for electricity and natural gas. Utility service connections would be modified as needed to support the operation of the Project.

Construction

All construction equipment and vehicles would be staged on the 2.86-acre Project site. Construction will be phased in alignment with the Office of the State Fire Marshal's permitting. Construction is anticipated to begin in December 2029 and be completed in January 2032.

PROJECT OBJECTIVES

The Judicial Council has identified the following Project Objectives to guide planning for the Project site, as well as the analysis included within the EIR:

- Provide a permanent, sustainable, safe, and accessible courthouse that improves the public's access to justice and enhances public services
- Enhance the public's access to justice by offering basic services such as self-help not currently provided to county residents due to overcrowding and lack of space
- Align courthouse spaces and organization with Judicial Council's California Trial Court Facilities Standards
- Improve security, relieve current space shortfall, and improve operational efficiency and customer service

ENVIRONMENTAL REVIEW

As required by CEQA, the EIR will describe existing conditions and evaluate the potential environmental effects of the Project, and a reasonable range of alternatives including the no-project alternative. It will address reasonably foreseeable direct, indirect, cumulative, and

growth-inducing effects. The EIR will identify feasible mitigation measures, if available, to reduce significant and potentially significant impacts to environmental resources.

POTENTIAL ENVIRONMENTAL IMPACTS

Based on the Project characteristics and site conditions, the EIR will evaluate, at a minimum, the following issue areas:

- Aesthetics/Visual
- Agriculture and Forestry Resources
- Air Quality
- Biological Resources
- Cultural Resources
- Energy
- Geology and Soils
- Greenhouse Gas Emissions
- Hazards and Hazardous Materials
- Hydrology and Water Quality
- Land Use and Planning
- Mineral Resources
- Noise
- Population and Housing
- Public Services
- Recreation
- Transportation
- Tribal Cultural Resources
- Utilities and Service Systems
- Wildfire
- Cumulative Effects
- Growth Inducing Effects

For each of these areas, the EIR will identify whether the Proposed Project would cause significant or potentially significant impacts. Where impacts are identified, the EIR will recommend feasible mitigation measures designed to avoid, minimize, or offset those impacts. The alternatives analysis will evaluate a reasonable range of project alternatives that, consistent with CEQA, meet most of the project objectives and reduce or avoid any significant environmental effects of the project, including a required No Project Alternative. The EIR will therefore serve as the primary disclosure document for decision-makers, agencies, and the public, ensuring that environmental considerations are fully integrated into the planning and approval process for the Project.

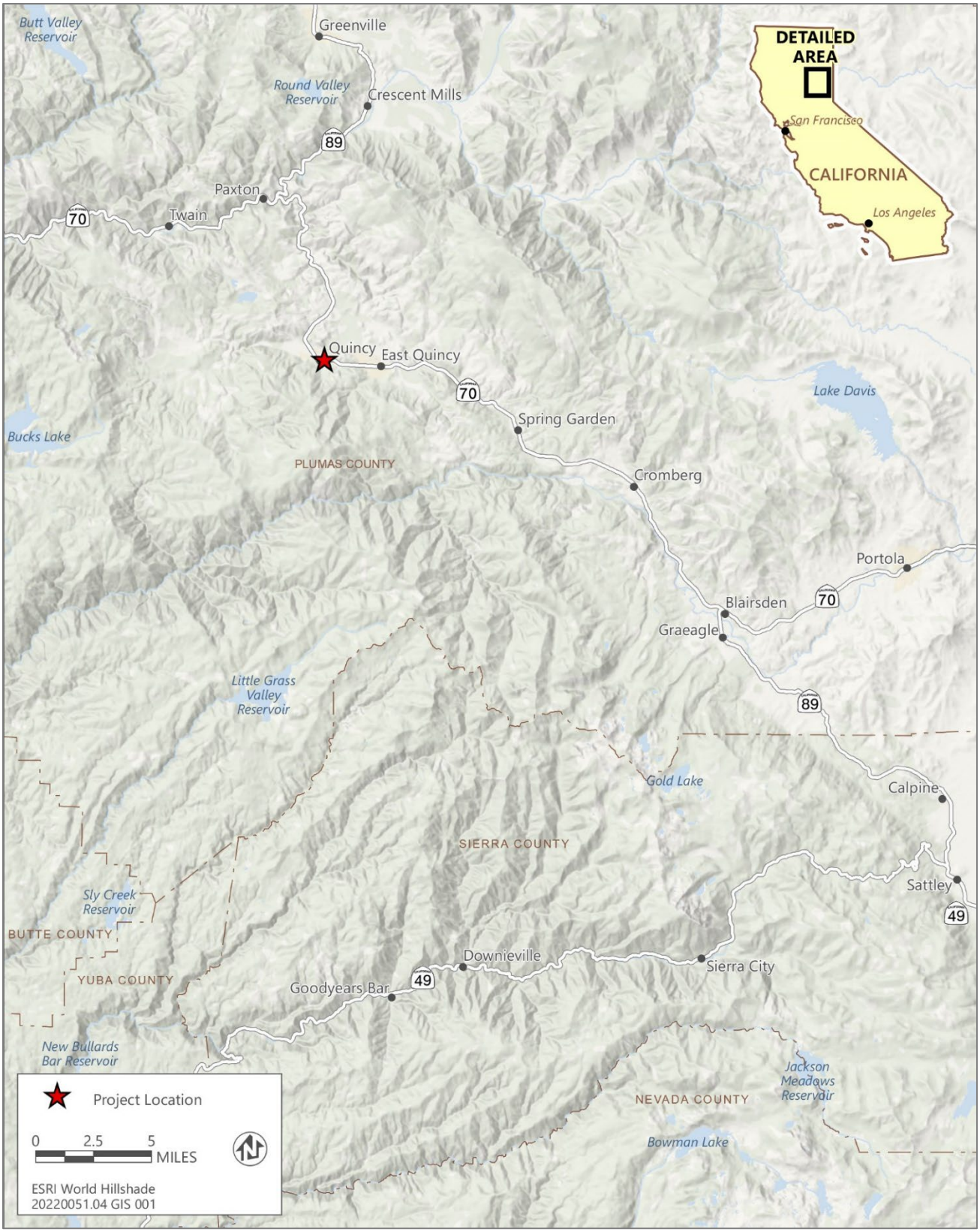


Figure 1 Regional Location



Figure 2 Project Location

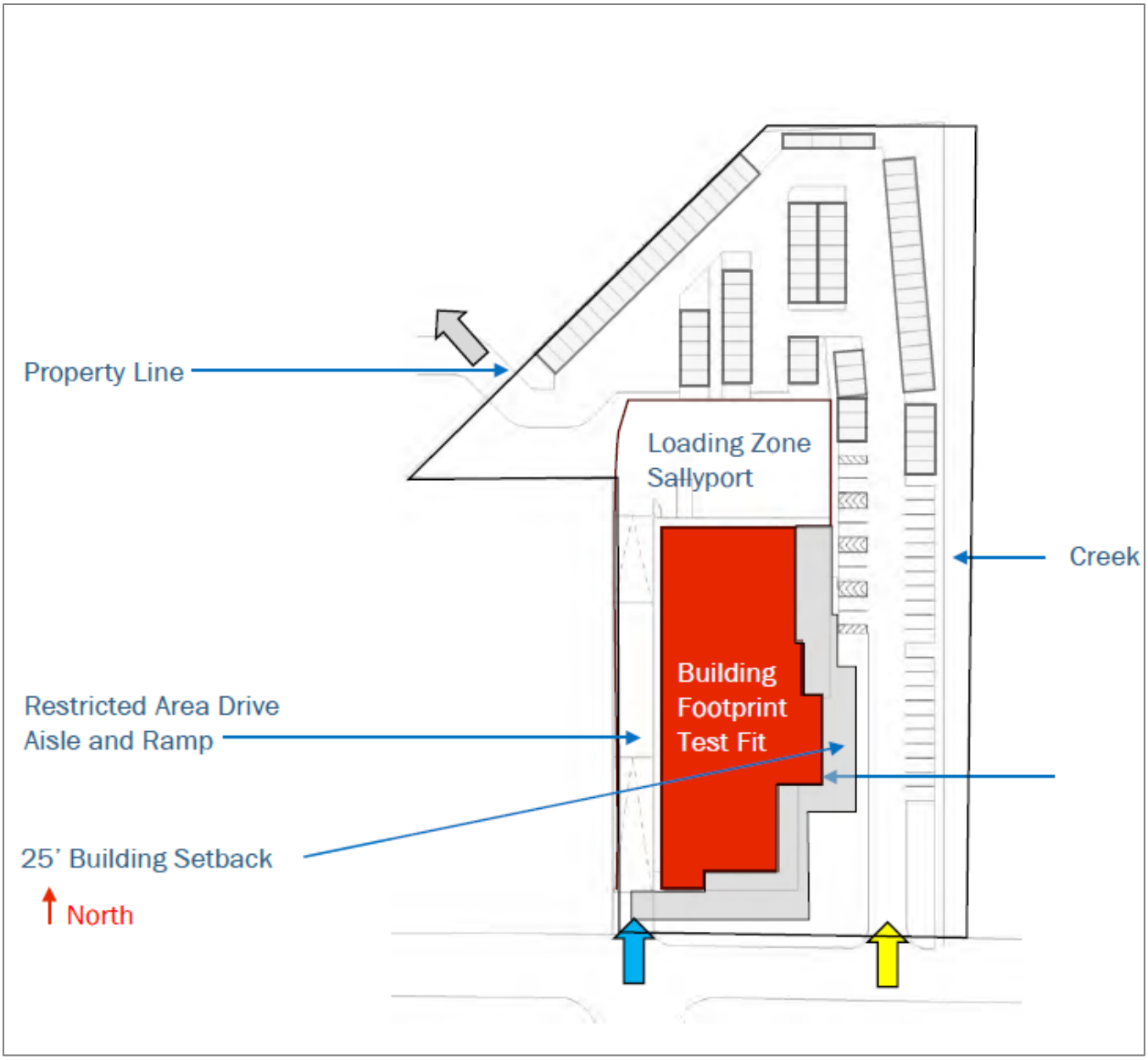


Figure 3 Conceptual Site Plan

Cervantes, Alexandra

From: Wildlife R2 CEQA <R2CEQA@wildlife.ca.gov>
Sent: Monday, November 17, 2025 9:34 AM
To: New Quincy Courthouse Project
Cc: Bryant, Claire@Wildlife; Sheya, Tanya@Wildlife; Kilgour, Morgan@Wildlife; Stanfield, Melissa@Wildlife; OPR State Clearinghouse
Subject: CDFW Comments - New Quincy Courthouse (SCH No. 2025100787)
Attachments: R2_CEQA_Comment_New Quincy Courthouse _NOP_EIR.docx.pdf

EXTERNAL EMAIL

Hello Alex Cervantes,

Attached you will find a completely executed copy of the above referenced document. Please reply verifying you can open this email and the attachment.

Thank you,
Nicole Haggerty
Staff Services Analyst
California Department of Fish & Wildlife
North Central Region – Region 2
916.907.3438

CALIFORNIA DEPARTMENT OF FISH and WILDLIFE

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State of California – Natural Resources Agency
DEPARTMENT OF FISH AND WILDLIFE
North Central Region
1701 Nimbus Road, Suite A
Rancho Cordova, CA 95670-4599
(916) 358-2900
www.wildlife.ca.gov

GAVIN NEWSOM, Governor
CHARLTON H. BONHAM, Director

November 17, 2025

Alex Cervantes
Senior Facilities Analyst
Judicial Council of California
2860 Gateway Oaks Drive, Suite 400
Sacramento, CA 95833-3509
newquincycourthouseproject@jud.ca.gov

Subject: New Quincy Courthouse
Notice of Preparation of an Environmental Impact Report
SCH No. 2025100787

Dear Alex Cervantes:

The California Department of Fish and Wildlife (CDFW) received and reviewed the Notice of Preparation of an Environmental Impact Report (EIR) from the Judicial Council of California for the New Quincy Courthouse (Project) in Plumas County pursuant to the California Environmental Quality Act (CEQA) statute and guidelines.[1]

Thank you for the opportunity to provide comments and recommendations regarding those activities involved in the Project that may affect California fish, wildlife, plants and their habitats. Likewise, CDFW appreciates the opportunity to provide comments regarding those aspects of the Project that it, by law, may need to exercise its own regulatory authority under the Fish and Game Code (Fish & G. Code).

CDFW ROLE

CDFW is California's Trustee Agency for fish and wildlife resources and holds those resources in trust by statute for all the people of the State (Fish & G. Code, §§ 711.7, subd. (a) & 1802; Pub. Resources Code, § 21070; CEQA Guidelines § 15386, subd. (a).). CDFW, in its trustee capacity, has jurisdiction over the conservation, protection, and management of fish, wildlife, native plants, and habitat necessary for biologically sustainable populations of those species (Fish & G. Code, § 1802.). Similarly, for purposes of CEQA, CDFW provides, as available, biological expertise during public agency environmental review efforts, focusing specifically on projects and related activities that have the potential to adversely affect fish and wildlife resources.

1 CEQA is codified in the California Public Resources Code in section 21000 et seq. The "CEQA Guidelines" are found in Title 14 of the California Code of Regulations, commencing with section 15000.

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CDFW may also act as a Responsible Agency under CEQA. (Pub. Resources Code, § 21069; CEQA Guidelines, § 15381.) CDFW expects that it may need to exercise regulatory authority as provided by the Fish and Game Code. As proposed, for example, the Project may be subject to CDFW's lake and streambed alteration regulatory authority. (Fish & G. Code, § 1600 et seq.) Likewise, to the extent implementation of the Project as proposed may result in "take" as defined by State law of any species protected under the California Endangered Species Act (CESA) (Fish & G. Code, § 2050 et seq.), the project proponent may seek related take authorization as provided by the Fish and Game Code.

PROJECT DESCRIPTION SUMMARY

The Project site is located at 287 Lawrence St, Quincy, California 95971; Assessor Parcel Numbers 115-031-055, 115-031-054, 115-031-052.The Project consists of the demolition of three existing structures, and the construction of a new approximately 23.000 square foot, 1 story, courthouse. The Project also includes improvements to onsite surface parking lots, developing drive aisles, and rerouting utility connections.

COMMENTS AND RECOMMENDATIONS

CDFW offers the comments and recommendations presented below to assist the Judicial Council of California in adequately identifying and/or mitigating the Project's significant, or potentially significant, impacts on biological resources. The comments and recommendations are also offered to enable CDFW to adequately review and comment on the proposed Project with respect to impacts on biological resources. CDFW recommends that the forthcoming EIR address the following:

Project Description

The Project description should include the whole action as defined in the CEQA Guidelines § 15378 and should include appropriate detailed exhibits disclosing the Project area including temporary impacted areas such as equipment stage area, spoils areas, adjacent infrastructure development, staging areas and access and haul roads if applicable.

As required by § 15126.6 of the CEQA Guidelines, the EIR should include an appropriate range of reasonable and feasible alternatives that would attain most of the basic Project objectives and avoid or minimize significant impacts to resources under CDFW's jurisdiction.

Assessment of Biological Resources

Section 15125(c) of the CEQA Guidelines states that knowledge of the regional setting of a project is critical to the assessment of environmental impacts and that special emphasis should be placed on environmental resources that are rare or unique to the region. To enable CDFW staff to adequately review and comment on the Project, the EIR should include a complete assessment of the flora and fauna within and adjacent to the Project footprint, with emphasis on identifying rare, threatened, endangered, and

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other sensitive species and their associated habitats. CDFW recommends the EIR specifically include:

1. An assessment of all habitat types located within the Project footprint, and a map that identifies the location of each habitat type. CDFW recommends that floristic, alliance- and/or association-based mapping and assessment be completed following, *The Manual of California Vegetation*, second edition (Sawyer 2009). Adjoining habitat areas should also be included in this assessment where site activities could lead to direct or indirect impacts offsite. Habitat mapping at the alliance level will help establish baseline vegetation conditions.

2. A general biological inventory of the fish, amphibian, reptile, bird, and mammal species that are present or have the potential to be present within each habitat type onsite and within adjacent areas that could be affected by the Project. CDFW recommends that the California Natural Diversity Database (CNDDB), as well as previous studies performed in the area, be consulted to assess the potential presence of sensitive species and habitats. A nine United States Geologic Survey 7.5-minute quadrangle search is recommended to determine what may occur in the region, larger if the Project area extends past one quad (see *Data Use Guidelines* on the CDFW webpage www.wildlife.ca.gov/Data/CNDDB/Maps-and-Data). Please review the webpage for information on how to access the database to obtain current information on any previously reported sensitive species and habitat, including Significant Natural Areas identified under Chapter 12 of the Fish and Game Code, in the vicinity of the Project. CDFW recommends that CNDDB Field Survey Forms be completed and submitted to CNDDB to document survey results. Online forms can be obtained and submitted at: https://www.wildlife.ca.gov/Data/CNDDB/Submitting-Data.

   Please note that CDFW's CNDDB is not exhaustive in terms of the data it houses, nor is it an absence database. CDFW recommends that it be used as a starting point in gathering information about the *potential presence* of species within the general area of the Project site. Other sources for identification of species and habitats near or adjacent to the Project area should include, but may not be limited to, State and federal resource agency lists, California Wildlife Habitat Relationship System, California Native Plant Society Inventory, agency contacts, environmental documents for other projects in the vicinity, academics, and professional or scientific organizations.

3. A complete and recent inventory of rare, threatened, endangered, and other sensitive species located within the Project footprint and within offsite areas with the potential to be affected, including California Species of Special Concern and California Fully Protected Species (Fish & G. Code § § 3511, 4700, 5050, and 5515). Species to be addressed should include all those which meet the CEQA definition (CEQA Guidelines § 15380). The inventory should address seasonal variations in use of the Project area and should not be limited to resident species. The EIR should include the results of focused species-specific surveys, completed by a qualified biologist and conducted at the appropriate time of year

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and time of day when the sensitive species are active or otherwise identifiable. Species-specific surveys should be conducted in order to ascertain the presence of species with the potential to be directly, indirectly, on or within a reasonable distance of the Project activities. CDFW recommends the Judicial Council of California rely on survey and monitoring protocols and guidelines available at: www.wildlife.ca.gov/Conservation/Survey-Protocols. Alternative survey protocols may be warranted; justification should be provided to substantiate why an alternative protocol is necessary. Acceptable species-specific survey procedures should be developed in consultation with CDFW and the U.S. Fish and Wildlife Service, where necessary. Some aspects of the Project may warrant periodic updated surveys for certain sensitive taxa, particularly if the Project is proposed to occur over a protracted time frame, or in phases, or if surveys are completed during periods of drought or deluge.

4. A thorough, recent (within the last two years), floristic-based assessment of special-status plants and natural communities, following CDFW's *Protocols for Surveying and Evaluating Impacts to Special Status Native Plant Populations and Natural Communities* (see www.wildlife.ca.gov/Conservation/Plants).

5. Information on the regional setting that is critical to an assessment of environmental impacts, with special emphasis on resources that are rare or unique to the region (CEQA Guidelines § 15125[c]).

Analysis of Direct, Indirect, and Cumulative Impacts to Biological Resources

The EIR should provide a thorough discussion of the Project's potential direct, indirect, and cumulative impacts on biological resources. To ensure that Project impacts on biological resources are fully analyzed, the following information should be included in the EIR:

1. The EIR should define the threshold of significance for each impact and describe the criteria used to determine whether the impacts are significant (CEQA Guidelines, § 15064, subd. (f)). The EIR must demonstrate that the significant environmental impacts of the Project were adequately investigated and discussed, and it must permit the significant effects of the Project to be considered in the full environmental context.

2. A discussion of potential impacts from lighting, noise, human activity, and wildlife-human interactions created by Project activities especially those adjacent to natural areas, exotic and/or invasive species occurrences, and drainages. The EIR should address Project-related changes to drainage patterns and water quality within, upstream, and downstream of the Project site, including: volume, velocity, and frequency of existing and post-Project surface flows; polluted runoff; soil erosion and/or sedimentation in streams and water bodies; and post-Project fate of runoff from the Project site.

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3. A discussion of potential indirect Project impacts on biological resources, including resources in areas adjacent to the Project footprint, such as nearby public lands (e.g., National Forests, State Parks, etc.), open space, adjacent natural habitats, riparian ecosystems, wildlife corridors, and any designated and/or proposed reserve or mitigation lands (e.g., preserved lands associated with a Conservation or Recovery Plan, or other conserved lands).

4. A cumulative effects analysis developed as described under CEQA Guidelines section 15130. The EIR should discuss the Project's cumulative impacts to natural resources and determine if that contribution would result in a significant impact. The EIR should include a list of present, past, and probable future projects producing related impacts to biological resources or shall include a summary of the projections contained in an adopted local, regional, or statewide plan, that consider conditions contributing to a cumulative effect. The cumulative analysis shall include impact analysis of vegetation and habitat reductions within the area and their potential cumulative effects. Please include all potential direct and indirect Project-related impacts to riparian areas, wetlands, wildlife corridors or wildlife movement areas, aquatic habitats, sensitive species and/or special-status species, open space, and adjacent natural habitats in the cumulative effects analysis.

Mitigation Measures for Project Impacts to Biological Resources

The EIR should include appropriate and adequate avoidance, minimization, and/or mitigation measures for all direct, indirect, and cumulative impacts that are expected to occur as a result of the construction and long-term operation and maintenance of the Project. CDFW also recommends the environmental documentation provide scientifically supported discussion regarding adequate avoidance, minimization, and/or mitigation measures to address the Project's significant impacts upon fish and wildlife and their habitat. For individual projects, mitigation must be roughly proportional to the level of impacts, including cumulative impacts, in accordance with the provisions of CEQA (Guidelines § § 15126.4(a)(4)(B), 15064, 15065, and 16355). In order for mitigation measures to be effective, they must be specific, enforceable, and feasible actions that will improve environmental conditions. When proposing measures to avoid, minimize, or mitigate impacts, CDFW recommends consideration of the following:

1. *Fully Protected Species*: Fully Protected Species (Fish & G. Code § 3511) have the potential to occur within or adjacent to the Project area, including Bald Eagle (*Haliaeetus leucocephalus*) . Project activities described in the EIR should be designed to completely avoid any fully protected species that have the potential to be present within or adjacent to the Project area. If fully protected species cannot be completely avoided, the Project should obtain incidental take coverage for all species that have the potential to be present within or adjacent to the

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Project Area[2]. CDFW also recommends the EIR fully analyze potential adverse impacts to fully protected species due to habitat modification, loss of foraging habitat, and/or interruption of migratory and breeding behaviors. CDFW recommends that the Judicial Council of California include in the analysis how appropriate avoidance, minimization and mitigation measures will reduce indirect impacts to fully protected species.

2. *Species of Special Concern*: Several Species of Special Concern (SSC) have the potential to occur within or adjacent to the Project area, including, but not limited to: Townsend's big eared bat (*Corynorhinus townsendii),* pallid bat (*Antrosous pallidus*), western red bat (*Lasiurus frantzii*), and American Goshawk (*Astur atricapillus*). Project activities described in the EIR should be designed to avoid any SSC that has the potential to be present within or adjacent to the Project area. CDFW also recommends that the EIR fully analyze potential adverse impacts to SSC due to habitat modification, loss of foraging habitat, and/or interruption of migratory and breeding behaviors. CDFW recommends the Judicial Council of California include in the analysis how appropriate avoidance, minimization and mitigation measures will reduce impacts to SSC.

3. *Sensitive Plant Communities*: CDFW considers sensitive plant communities to be imperiled habitats having both local and regional significance. Plant communities, alliances, and associations with a statewide ranking of S-1, S-2, S-3, and S-4 should be considered sensitive and declining at the local and regional level. These ranks can be obtained by querying the CNDDB and are included in *The Manual of California Vegetation* (Sawyer 2009). The EIR should include measures to fully avoid and otherwise protect sensitive plant communities from Project-related direct and indirect impacts.

4. *Native Wildlife Nursery Sites*: CDFW recommends the EIR fully analyze potential adverse impacts to native wildlife nursery sites, including but not limited to bat maternity roosts. Based on review of Project materials and aerial photography, the Project site contains potential nursery site habitat for structure and tree roosting bats, and is near potential foraging habitat. Bats are considered non-game mammals and are afforded protection by state law from take and/or harassment, (Fish & G. Code, § 4150; Cal. Code of Regs, § 251.1). CDFW recommends that the EIR fully identify the Project's potential impacts to native wildlife nursery sites, and include appropriate avoidance, minimization and mitigation measures to reduce impacts or mitigate any potential significant impacts to bat nursery sites.

5. *Mitigation*: CDFW considers adverse Project-related impacts to sensitive species and habitats to be significant to both local and regional ecosystems, and the EIR should include mitigation measures for adverse Project-related impacts to these

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2 CDFW may only issue incidental take permits for specified projects if certain conditions are satisfied per SB 147.

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resources. Mitigation measures should emphasize avoidance and reduction of Project impacts. For unavoidable impacts, onsite habitat restoration, enhancement, or permanent protection should be evaluated and discussed in detail. If onsite mitigation is not feasible or would not be biologically viable and therefore not adequately mitigate the loss of biological functions and values, offsite mitigation through habitat creation and/or acquisition and preservation in perpetuity should be addressed.

The EIR should include measures to perpetually protect the targeted habitat values within mitigation areas from direct and indirect adverse impacts in order to meet mitigation objectives to offset Project-induced qualitative and quantitative losses of biological values. Specific issues that should be addressed include restrictions on access, proposed land dedications, long-term monitoring and management programs, control of illegal dumping, water pollution, increased human intrusion, etc.

6. *Habitat Revegetation/Restoration Plans*: Plans for restoration and revegetation should be prepared by persons with expertise in the regional ecosystems and native plant restoration techniques. Plans should identify the assumptions used to develop the proposed restoration strategy. Each plan should include, at a minimum: (a) the location of restoration sites and assessment of appropriate reference sites; (b) the plant species to be used, sources of local propagules, container sizes, and seeding rates; (c) a schematic depicting the mitigation area; (d) a local seed and cuttings and planting schedule; (e) a description of the irrigation methodology; (f) measures to control exotic vegetation on site; (g) specific success criteria; (h) a detailed monitoring program; (i) contingency measures should the success criteria not be met; and (j) identification of the party responsible for meeting the success criteria and providing for conservation of the mitigation site in perpetuity. Monitoring of restoration areas should extend across a sufficient time frame to ensure that the new habitat is established, self-sustaining, and capable of surviving drought.

   CDFW recommends that local onsite propagules from the Project area and nearby vicinity be collected and used for restoration purposes. Onsite seed collection should be appropriately timed to ensure the viability of the seeds when planted. Onsite vegetation mapping at the alliance and/or association level should be used to develop appropriate restoration goals and local plant palettes. Reference areas should be identified to help guide restoration efforts. Specific restoration plans should be developed for various Project components as appropriate. Restoration objectives should include protecting special habitat elements or re-creating them in areas affected by the Project. Examples may include retention of woody material, logs, snags, rocks, and brush piles. Fish and Game Code sections 1002, 1002.5 and 1003 authorize CDFW to issue permits for the take or possession of plants and wildlife for scientific, educational, and propagation purposes. Please see our website for more information on Scientific Collecting Permits at www.wildlife.ca.gov/Licensing/Scientific-Collecting#53949678-regulations-.

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7. *Nesting Birds*: Please note that it is the Project proponent's responsibility to comply with all applicable laws related to nesting birds and birds of prey. Migratory non-game native bird species are protected by international treaty under the federal Migratory Bird Treaty Act (MBTA) of 1918, as amended (16 U.S.C. 703 *et seq.*). CDFW implemented the MBTA by adopting the Fish and Game Code section 3513. Fish and Game Code sections 3503, 3503.5 and 3800 provide additional protection to nongame birds, birds of prey, their nests and eggs. Sections 3503, 3503.5, and 3513 of the Fish and Game Code afford protective measures as follows: section 3503 states that it is unlawful to take, possess, or needlessly destroy the nest or eggs of any bird, except as otherwise provided by the Fish and Game Code or any regulation made pursuant thereto; section 3503.5 states that is it unlawful to take, possess, or destroy any birds in the orders Falconiformes or Strigiformes (birds-of-prey) or to take, possess, or destroy the nest or eggs of any such bird except as otherwise provided by the Fish and Game Code or any regulation adopted pursuant thereto; and section 3513 states that it is unlawful to take or possess any migratory nongame bird as designated in the MBTA or any part of such migratory nongame bird except as provided by rules and regulations adopted by the Secretary of the Interior under provisions of the MBTA.

   Potential habitat for nesting birds and birds of prey is present within the Project area. The Project should disclose all potential activities that may incur a direct or indirect take to nongame nesting birds within the Project footprint and its vicinity. Appropriate avoidance, minimization, and/or mitigation measures to avoid take must be included in the EIR.

   CDFW recommends the EIR include specific avoidance and minimization measures to ensure that impacts to nesting birds or their nests do not occur. Project-specific avoidance and minimization measures may include, but not be limited to: Project phasing and timing, monitoring of Project-related noise (where applicable), sound walls, and buffers, where appropriate. The EIR should also include specific avoidance and minimization measures that will be implemented should a nest be located within the Project site. In addition to larger, protocol level survey efforts (e.g., Swainson's hawk surveys) and scientific assessments, CDFW recommends a final preconstruction survey be required no more than three (3) days prior to vegetation clearing or ground disturbance activities, as instances of nesting could be missed if surveys are conducted earlier.

8. *Moving out of Harm's Way*: The Project is anticipated to result in the clearing of natural habitats that support native species. To avoid direct mortality, the Judicial Council of California should state in the EIR a requirement for a qualified biologist with the proper handling permits, will be retained to be onsite prior to and during all ground- and habitat-disturbing activities. Furthermore, the EIR should describe that the qualified biologist with the proper permits may move out of harm's way special-status species or other wildlife of low or limited mobility that would otherwise be injured or killed from Project-related activities, as needed. The EIR should also describe qualified biologist qualifications and authorities to stop work to prevent direct mortality of special-status species. CDFW recommends fish and wildlife species be allowed to

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move out of harm's way on their own volition, if possible, and to assist their relocation as a last resort. It should be noted that the temporary relocation of onsite wildlife does not constitute effective mitigation for habitat loss.

9. *Translocation of Species*: CDFW generally does not support the use of relocation, salvage, and/or transplantation as the sole mitigation for impacts to rare, threatened, or endangered species as these efforts are generally experimental in nature and largely unsuccessful. Therefore, the EIR should describe additional mitigation measures utilizing habitat restoration, conservation, and/or preservation, in addition to avoidance and minimization measures, if it is determined that there may be impacts to rare, threatened, or endangered species.

The EIR should incorporate mitigation performance standards that would ensure that impacts are reduced to a less-than-significant level. Mitigation measures proposed in the EIR should be made a condition of approval of the Project. Please note that obtaining a permit from CDFW by itself with no other mitigation proposal may constitute mitigation deferral. CEQA Guidelines section 15126.4, subdivision (a)(1)(B) states that formulation of mitigation measures should not be deferred until some future time. To avoid deferring mitigation in this way, the EIR should describe avoidance, minimization and mitigation measures that would be implemented should the impact occur.

California Endangered Species Act

CDFW is responsible for ensuring appropriate conservation of fish and wildlife resources including threatened, endangered, and/or candidate plant and animal species, pursuant to CESA. CDFW recommends that a CESA Incidental Take Permit (ITP) be obtained if the Project has the potential to result in "take" (Fish & G. Code § 86 defines "take" as "hunt, pursue, catch, capture, or kill, or attempt to hunt, pursue, catch, capture, or kill") of State-listed CESA species, either through construction or over the life of the Project.

The EIR should disclose the potential of the Project to take State-listed species and how the impacts will be avoided, minimized, and mitigated. Please note that mitigation measures that are adequate to reduce impacts to a less-than significant level to meet CEQA requirements may not be enough for the issuance of an ITP. To facilitate the issuance of an ITP, if applicable, CDFW recommends the EIR include measures to minimize and fully mitigate the impacts to any State-listed species the Project has potential to take. CDFW encourages early consultation with staff to determine appropriate measures to facilitate future permitting processes and to engage with the U.S. Fish and Wildlife Service and/or National Marine Fisheries Service to coordinate specific measures if both State and federally listed species may be present within the Project vicinity.

Native Plant Protection Act

The Native Plant Protection Act (Fish & G. Code §1900 *et seq.*) prohibits the take or possession of State-listed rare and endangered plants, including any part or product thereof, unless authorized by CDFW or in certain limited circumstances. Take of State-

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listed rare and/or endangered plants due to Project activities may only be permitted through an ITP or other authorization issued by CDFW pursuant to California Code of Regulations, Title 14, section 786.9 subdivision (b).

Lake and Streambed Alteration Program

The EIR should identify all perennial, intermittent, and ephemeral rivers, streams, lakes, other hydrologically connected aquatic features, and any associated biological resources/habitats present within the entire Project footprint (including utilities, access and staging areas). The environmental document should analyze all potential temporary, permanent, direct, indirect and/or cumulative impacts to the above-mentioned features and associated biological resources/habitats that may occur because of the Project. If it is determined the Project will result in significant impacts to these resources the EIR shall propose appropriate avoidance, minimization and/or mitigation measures to reduce impacts to a less-than-significant level.

Section 1602 of the Fish and Game Code requires an entity to notify CDFW prior to commencing any activity that may do one or more of the following:

1. Substantially divert or obstruct the natural flow of any river, stream or lake;

2. Substantially change or use any material from the bed, channel or bank of any river, stream, or lake; or

3. Deposit debris, waste or other materials where it may pass into any river, stream or lake.

Please note that "any river, stream or lake" includes those that are episodic (i.e., those that are dry for periods of time) as well as those that are perennial (i.e., those that flow year-round). This includes ephemeral streams and watercourses with a subsurface flow. It may also apply to work undertaken within the flood plain of a body of water.

If upon review of an entity's notification, CDFW determines that the Project activities may substantially adversely affect an existing fish or wildlife resource, a Lake and Streambed Alteration (LSA) Agreement will be issued which will include reasonable measures necessary to protect the resource. CDFW's issuance of an LSA Agreement is a "project" subject to CEQA (see Pub. Resources Code 21065). To facilitate issuance of an LSA Agreement, if one is necessary, the EIR should fully identify the potential impacts to the lake, stream, or riparian resources, and provide adequate avoidance, mitigation, and monitoring and reporting commitments. Early consultation with CDFW is recommended, since modification of the Project may avoid or reduce impacts to fish and wildlife resources. All LSA Notification types must be submitted online through CDFW's Environmental Permit Information Management System (EPIMS). For more information about EPIMS, please visit https://wildlife.ca.gov/Conservation/Environmental-Review/EPIMS. More information about LSA Notifications, paper forms and fees may be found at https://www.wildlife.ca.gov/Conservation/Environmental-Review/LSA.

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Please note that other agencies may use specific methods and definitions to determine impacts to areas subject to their authorities. These methods and definitions often do not include all needed information for CDFW to determine the extent of fish and wildlife resources affected by activities subject to Notification under Fish and Game Code section 1602. Therefore, CDFW does not recommend relying solely on methods developed specifically for delineating areas subject to other agencies' jurisdiction (such as United States Army Corps of Engineers) when mapping lakes, streams, wetlands, floodplains, riparian areas, etc. in preparation for submitting a Notification of an LSA.

CDFW relies on the lead agency environmental document analysis when acting as a responsible agency issuing an LSA Agreement. CDFW recommends lead agencies coordinate with us as early as possible, since potential modification of the proposed Project may avoid or reduce impacts to fish and wildlife resources and expedite the Project approval process.

The following information will be required for the processing of an LSA Notification and CDFW recommends incorporating this information into any forthcoming CEQA document(s) to avoid subsequent documentation and Project delays:

1. Mapping and quantification of lakes, streams, and associated fish and wildlife habitat (e.g., riparian habitat, freshwater wetlands, etc.) that will be temporarily and/or permanently impacted by the Project, including impacts from access and staging areas. Please include an estimate of impact to each habitat type.

2. Discussion of specific avoidance, minimization, and mitigation measures to reduce Project impacts to fish and wildlife resources to a less-than-significant level. Please refer to section 15370 of the CEQA Guidelines.

ENVIRONMENTAL DATA

CEQA requires that information developed in environmental impact reports and negative declarations be incorporated into a database, which may be used to make subsequent or supplemental environmental determinations (Pub. Resources Code, § 21003, subd. (e)). Accordingly, please report any special-status species and natural communities detected during Project surveys to CNDDB. The CNNDB field survey form can be found at the following link: https://www.wildlife.ca.gov/Data/CNDDB/Submitting-Data. The completed form can be submitted online or mailed electronically to CNDDB at the following email address: CNDDB@wildlife.ca.gov.

FILING FEES

The Project, as proposed, would have an effect on fish and wildlife, and assessment of filing fees is necessary. Fees are payable upon filing of the Notice of Determination by the Judicial Council of California and serve to help defray the cost of environmental review by CDFW. Payment of the fee is required in order for the underlying project approval to be operative, vested, and final. (Cal. Code Regs, tit. 14, § 753.5; Fish & G. Code § 711.4; Pub. Resources Code, § 21089.)

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CONCLUSION

Pursuant to Public Resources Code sections 21092 and 21092.2, CDFW requests written notification of proposed actions and pending decisions regarding the Project. Written notifications shall be directed to: California Department of Fish and Wildlife North Central Region, 1701 Nimbus Road, Rancho Cordova, CA 95670 or emailed to R2CEQA@wildlife.ca.gov.

CDFW appreciates the opportunity to comment on the Notice of Preparation of the EIR for the New Quincy Courthouse and recommends that the Judicial Council of California address CDFW's comments and concerns in the forthcoming EIR. CDFW personnel are available for consultation regarding biological resources and strategies to minimize impacts.

If you have any questions regarding the comments provided in this letter, or wish to schedule a meeting and/or site visit, please contact Claire Bryant, Environmental Scientist, at (530) 333-7748 or claire.bryant@wildlife.ca.gov.

Sincerely,

DocuSigned by:
Tanya Sheya
1ABC45303752499...

Tanya Sheya
Environmental Program Manager

ec: Melissa Stanfield, Senior Environmental Scientist (Supervisory)
Claire Bryant, Environmental Scientist
Department of Fish and Wildlife

Office of Land Use and Climate Innovation, State Clearinghouse, Sacramento

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REFERENCES

Sawyer, J. O., T. Keeler-Wolf, and J. M. Evens. 2009. A Manual of California Vegetation, 2nd ed. California Native Plant Society Press, Sacramento, California. http://vegetation.cnps.org/

Cervantes, Alexandra

From: Melissa Klundby <melissak@myairdistrict.com>
Sent: Friday, November 21, 2025 4:05 PM
To: New Quincy Courthouse Project
Subject: Quincy Courthouse Project NOP
Attachments: Comments and Dust Plan Request NSAQMD.pdf

EXTERNAL EMAIL

Please find the attached comments

--
Melissa Klundby
Air Pollution Control Specialist
Northern Sierra Air Quality Management District
www.myairdistrict.com
530-832-0102 ext. 4
P.O. Box 2227
Portola, CA 96122

Northern Sierra Air Quality Management District

PO Box 2227
Portola, CA 96122
(530) 832-0102
office@myairdistrict.com
melissak@myairdistrict.com

November 11, 2025

Plumas County Planning Department

Re: NOP, New Quincy Courthouse Project

Due to the size of the development (over 1 acre) NSAQMD requires the applicant submit a Dust Mitigation Plan to the District if the project moves forward. The applicant must also confirm that there is no Asbestos containing soils on the property. If a project is in an area mapped as having ultramafic rock or serpentine, or if these rock types are discovered on site, the statewide Asbestos Airborne Toxic Control Measure (ATCM) for Construction, Grading, Quarrying, and Surface Mining Operations (Section 93105 of Title 17 of the California Code of Regulations) applies and specifies more stringent conditions than those listed below. If ultramafic or Asbestos containing soils are at the site the applicant will be required to submit an Asbestos Mitigation plan to the District, and we will provide additional guidance if that is the case.

District Rule 226 states, “A dust control plan must be submitted to and approved by the Air Pollution Control Officer before topsoil is disturbed on any project where more than one (1) acre of natural surface area is to be altered or where the natural ground cover is removed.” This applies to any clearing or grading.

Typically, the Dust Control Plan requirement is fulfilled by clearly phrased and enforceable conditions included on the project grading plans, preferably under its own heading. This should also include accurate contact information for a project manager in charge of enforcing dust control measures during the project.

Following is a set of standard minimum Dust Control measures recommended for inclusion in the Plan:

- Identify on the grading plan and in a dust mitigation plan the person responsible for ensuring that all adequate dust control measures are implemented in a timely and effective manner, include name and contact information.
- Specify that all material excavated, stockpiled, or graded shall be sufficiently watered, treated, or covered to prevent fugitive dust from leaving the property boundaries and/or causing a public nuisance. Watering during summer months should occur at least twice daily, with complete coverage of disturbed areas.
- Require that all areas with vehicle traffic shall be watered or have dust palliative applied as necessary to minimize dust emissions.
- Require that all on-site vehicle traffic shall be limited to a speed of 15 mph on unpaved roads.

Northern Sierra Air Quality Management District

PO Box 2227
Portola, CA 96122
(530) 832-0102
office@myairdistrict.com
melissak@myairdistrict.com

- Specify that all land clearing, grading, earth moving, or excavation activities on a project shall be suspended as necessary to prevent excessive windblown dust when winds are expected to exceed 20 mph.
- Specify that all disturbed inactive portions of the development site shall be covered, seeded, or watered or otherwise stabilized until a suitable cover is established.
- Specify that all material transported off-site shall be either sufficiently watered or securely covered to prevent it being entrained in the air, and there must be a minimum of six (6) inches of freeboard in the bed of the transport vehicle.
- Specify that all that paved streets adjacent to the project shall be swept or washed at the end of each day, or more frequently, if necessary, to remove excessive accumulations or visibly raised areas of soil which may have resulted from activities at the project site.
- Notes that prior to final occupancy, the applicant shall re-establish ground cover on disturbed ground on the site through seeding and watering or with ground cover such as gravel or pavement.

Please also note any portable generators that are above 50 horsepower and are diesel must also be reported to the District and will be required to be permitted.

Also due to the proposed location, the District would request that we receive all details regarding site construction timelines. The District maintains a PM 2.5 monitor on the parcel located behind the proposed location. This monitor is used to determine the areas compliance with State allowable PM 2.5 pollution levels. If this project moves forward at the proposed location, the District will provide additional comments regarding this issue.

Further, the District would recommend that any ground cover removed not be burned on site, but be transferred to the local green waste facility as available. If materials are to be burned on site, the applicant must contact the District to obtain an Air Pollution permit.

Sincerely,

Melissa Klundby

Melissa Klundby
Air Pollution Control Specialist II

Cervantes, Alexandra

From: littledove <glittledove@gmail.com>
Sent: Wednesday, October 15, 2025 5:20 PM
To: New Quincy Courthouse Project
Subject: Please choose an undeveloped site

EXTERNAL EMAIL

There are so many open lots available why destroy the potential for the Stonehouse to come back into use or remove the once fully functioning newspaper printing facility?
Both of these have future potential.
In a town this small, the tearing asunder does not help morale.
Thanks,
Littledove

Cervantes, Alexandra

From: littledove <glittledove@gmail.com>
Sent: Wednesday, October 15, 2025 5:25 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

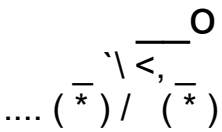
Please make a more civil and wise choice for a spot, like the hill between East and West Quincy and setting aside a memorial marker for the Harlem Club?
Removing the future potential use of both the Publishing Company and the Stonehouse is an affront to the roots of the community.
Try again.
Truly,
Littledove

Cervantes, Alexandra

From: Kevin Danaher <kevindanaher1519@gmail.com>
Sent: Tuesday, October 21, 2025 8:22 AM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

I would like to know the plan for disposal of the lumber and other building materials of the Quincy Lumber building that will be demolished to make room for the new courthouse.
thanks,
Kevin Danaher



A number of my video lectures and my latest book can be seen at https://www.kevindanaher.org/

Kevin Danaher, PhD

Co-Founder, Global Exchange, Green Festival, Fair Trade USA

415-902-9796

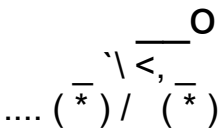
www.globalexchange.org

Cervantes, Alexandra

From: Kevin Danaher <kevindanaher1519@gmail.com>
Sent: Thursday, October 23, 2025 10:30 AM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

Friends,
I would like to know what the plan is for reusing the awesome historic materials in the Quincy Lumber building when its disassembled.
thank you,
Dr. Kevin Danaher



A number of my video lectures and my latest book can be seen at
https://www.kevindanaher.org/

Kevin Danaher, PhD

Co-Founder, Global Exchange, Green Festival, Fair Trade USA

415-902-9796

www.globalexchange.org

Cervantes, Alexandra

From: Shelley Hunter <quincyfeatherbedinn@gmail.com>
Sent: Tuesday, October 28, 2025 7:58 AM
To: New Quincy Courthouse Project
Subject: Approve of new site

EXTERNAL EMAIL

Dear Alex Cervantes,
Senior Facilities Analyst,
Judicial Council of California,
Facilities Services

I approve of the new location for the new Quincy Courthouse. Its proximity to the old Courthouse, and downtown eateries is perfect.

Please proceed.

Sincerely,

Shelley Hunter

--
Shelley Hunter
Quincy Feather Bed Inn
542 Jackson Street
Quincy, CA 95971

530-283-3000
quincyfeatherbed.com

Cervantes, Alexandra

From: Eva Small <evasmll@yahoo.com>
Sent: Tuesday, October 28, 2025 6:47 PM
To: New Quincy Courthouse Project
Subject: New Quincy courthouse NOP

EXTERNAL EMAIL

I have been a Quincy California resident for 45 years. My husband was an employee of the Plumas County sheriff's department for 40 years. Most of his time, he was a security / bailiff in the courthouse. I have been in the current courthouse in Quincy many times. I am currently an employee of Feather Publishing, with a desk in the building that the state wants to buy.
I agree wholeheartedly that the Feather Publishing property is the best place for the state to build a new courthouse. (I am not getting money from the sale of the property.).
A few people are upset about the Quincy Lumber building being torn down—that thing is falling apart and isn't that "historically" precious. It could burn down tomorrow and most people wouldn't care.
You might not hear from very many people who are in favor of the new building. You will probably get more feedback from the local idiots who hate any kind of change. These same people will complain about every new cell tower to go up, and then they complain about "dead spots" where their cell phones won't work or wonder why it takes an hour for an ambulance to get to their backwoods home.
Thank you for letting me express my opinion.
Eva Small
Evasmll@yahoo.com
Quincy, California.

Sent from my iPhone

Cervantes, Alexandra

From: Janet Crain <janetc@hughes.net>
Sent: Friday, October 31, 2025 4:33 PM
To: New Quincy Courthouse Project
Cc: editor@plumassun.org
Subject: New Quincy Courthouse NOPE

EXTERNAL EMAIL

As you know, many Plumas County residents, including myself, opposed locating the new courthouse on the site of Dame Shirley park, the only park existing in Downtown Quincy. Thanks to the organized community opposition, our Board of Supervisors voted against selling it to the State. The current site is much preferred. However I am opposed to the demolition of the the Red Barn building. And I think once the community realizes that that is part of your proposed plan, there will be many more opposed to that. There is no justification for needing the parcel that the Barn sits on. You were planning on making the new courthouse fit at the Shirley location on 1.37 acres vs the 2.86 acres in your current proposal which more than doubles the available land. Presumably the building on the Shirley would have needed at least 2 stories if you now plan to need all of the land in your current proposal . You could make the new courthouse two stories. That would save the barn plus eliminate the need for such a big building footprint.

Quincy town is unique. We don't want nor is there a need for a big, ugly, sprawling building. Keeping the Red Barn, making the new courthouse 2 (or more) stories high and setting it back from the street would reduce its visual and environmental impacts significantly plus a 2 story building would be less expensive for heating and air conditioning. I am appalled at your lack of following good planning principals.

Cervantes, Alexandra

From: Leslie Mink <lesliemink@gmail.com>
Sent: Saturday, November 1, 2025 10:02 AM
To: New Quincy Courthouse Project
Subject: new quincy courthouse nop

EXTERNAL EMAIL

I support investigating the location of the new courthouse at the Feather Publishing site. Portions of the Quincy Lumber building should be preserved (storage?, covered parking?). The size of the new courthouse seems excessive. Does it really need to be that big? Heating and cooling costs must be factored into the design, with as much passive heating and cooling as possible. The building should have plenty of natural light. Quincy continues to have a flooding problem downstream of the proposed location. Infiltration in downtown Quincy needs to be improved. Permeable pavers should be used for all parking areas, and parking areas should not be excessively large.
-Leslie Mink

Cervantes, Alexandra

From: Paul Stancheff <paulstancheff@gmail.com>
Sent: Sunday, November 2, 2025 5:03 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

The Quincy Lumber Barn is an Iconic Historic and cultural Landmark of Plumas County. This building is over 125 years old and in sound structural condition. This is one of the few remaining buildings present at the founding of Quincy and the last large wooden barn left in Quincy illustrating this irreplaceable Iconic historical architecture. There are photographs of Quincy from 1900 illustrating this structure during the horse and wagon transportation era depicting the earliest development of this historic community. This beloved landmark should be designated as a historic site and preserved in its present condition and location.

Cervantes, Alexandra

From: Paul Stancheff <paulstancheff@gmail.com>
Sent: Sunday, November 2, 2025 9:00 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

There are numerous ALTERNATIVES that have not been considered nor explored in the new courthouse proposal. These ALTERNATIVES may be less expensive to develop and would not destroy the beloved landmarks of the Quincy Lumber barn nor the Stone House.
Alternatives analyzed in the EIR should include: 1a)Preservation of the historic barn, utilizing the existing superior courtroom for less serious cases and building just one new courtroom within the existing Feather River Publishing Bldg. The inside of the barn could be remodeled for office space or parking. This would substantially reduce construction, maintenance, and energy costs while preserving the historic landmark. 1b)Preserve the historic barn, utilize, remodel and/or add a 2nd story to the existing Feather River Bulletin Bldg. If needed, additional parking could be included on part of the adjoining abandoned water treatment property located behind.

2) Analyze other sites not originally considered that are now for sale including 1)Quincy Motor Supply at 85 Lawrence st.(2.2 acres,· listed $799,000), 2)390 E Main (8.27 ac, listed $299,000), 3)1097 Lee rd (6ac, listed $522,500). 4)These sites· would dramatically reduce demolition costs and provide easier public access than the proposed alternatives.
3) Consider properties not listed for sale but currently vacant or potentially open to sale in which the owner could be approached to consider sale. These properties could include 1)the empty armory at 20 Redburg plus part the adjoining County waste management site or Skips Repair, adjacent to the county jail. 2)1986 East Main, closed Little Lots and adjoining auto lot. 3)380 East Main, the burned Harlem Club.4)388 Crescent St, previously Willits Motors. 5)550 Orion Way, previously American Valley Aviation.

6)remodel the unused courthouse buildt in Portola to meet minimum current standards.
Each of these alternatives would improve the aesthectics of Quincy without demolishing historical or unique architectural landmarks while dramatically reducing public controversy over the 2 proposed sites in the current NOP.

Cervantes, Alexandra

From: Paul Stancheff <paulstancheff@gmail.com>
Sent: Wednesday, November 5, 2025 1:37 PM
To: New Quincy Courthouse Project
Subject: New quincy courthouse project NOP

EXTERNAL EMAIL

The new Quincy Courthouse Public Scoping meeting on 10/23/25 was not sufficiently announced to inform the Plumas County communities of the meeting and therfore should be rescheduled and the comment time extended.
There was no press release of this event to the Plumas Sun, (local internet newspaper) nor local radio stations, nor the local Bulletin boards at the Post Offices, Libraries, County Court House, the HUB, etc. The public were unaware of this meeting and therefore did not attend. A previous meeting was attended by 100's of concerned citizens regarding this subject who are still extremely interested in the project site location and design.
This meeting was held in a very small county building located behind the locked front gates of the Fairgrounds which would lead attendees to believe the meeting was canceled. Access was only available thru a maintenance side gate with an indirect route only navigatable by someone familiar with the Fairgrounds layout.
The presentation was insufficient, without a description of the alternatives nor list of sites considered and posted on a screen too small to be visible by all. There was no handout of the information presented and no mailing address on the comment sheet. This was not a viable public comment meeting designed for inclusive, thoughtful, input and should be rescheduled with appropriate announcements.

Cervantes, Alexandra

From: Paul Stancheff <paulstancheff@gmail.com>
Sent: Wednesday, November 5, 2025 3:35 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

The new Quincy Courthouse Scoping process has excluded public input from the development of site selection criteria and site selection proposals. The chosen site selection committee consisted of only business owners and government employees excluding anyone from the general public that the proposal is supposed to represent. Some of these appointees may have personal economic interests that have possibly influenced the site selection process. This process did not permit any public input on site selection criteria nor site selection ranking. The site selection criteria should include historical, esthetical, and architectural significance of existing and proposed structures.
A new site selection review team should be chosen who do not have personal political or economic interests in this decision and should include members from the general public. All possible sites should be reevaluated and reranked based on selection criteria that includes public input. Only then should a new comprehensive Environmental Impact Statement be initiated.

Cervantes, Alexandra

From: Bianca Harrison <dragonfly54b@gmail.com>
Sent: Friday, November 7, 2025 10:58 AM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

Hello,
Here are my thoughts on this major change to our city and county. I am very concerned that this project was not openly discussed with the public after the judicial council could not purchase Dame Shirley Plaza. The second meeting was not announced on accessible media. I learned about this meeting via the article in Plumas Sun after it happened. That is not a public meeting, but a meeting engineered to meet the minimum legal requirements and to push through the purchase of the Feather Publishing building and the historic Quincy Lumber building as well as an adjacent business.

It is unclear to me how the local selection committee was assembled. There was no

public announcement that this committee was convened or who would be selected for it. At the initial meeting I did not see any stakeholders of the public on this committee, only business owners, property owners and state employees.

There are other parcels for sale in Quincy that would meet the requirements for a new courthouse. I feel that a new search needs to beP initiated with intensive public outreach. Such a state facility in a residential neighborhood must be accepted by the neighbors and the community at large before it is started. I look forwardto seeing an open disclosure of all publiccomments and responses from the judicial counsel in the near future.

Sincerely,
Bianca Harrison, CMA
Retired Assistant Auditor, Plumas County

To: Mr. Alex Cervantes, Senior Facilities Analyst,
Judicial Council of California Facilities Services

From: Bill Martin, Quincy, California

Subj: New Quincy Courthouse NOP

Date: November 8, 2025.

==========

Your project is early enough in its development to consider all approaches to maximize its goals, both environmental and financial.

The purpose of this message is to boost consideration of geothermal heat pump technology (geo) to handle the new courthouse's heating, cooling, and hot water needs. It contains references to successful projects elsewhere that use geo, and an explanation of the basic functions of this technology.

In terms of efficiency, if one is familiar with Coefficient of Performance (COP) where an electric resistance water heater equals a COP of 1.0, residential geo systems have now broken above 5.0. But commercial systems **for larger buildings now stand at 8.0**. In an era where electricity prices are destined to rise, this thermal leverage should not be ignored.

Thank you for your consideration.

—Bill M.

Dear Mr. Cervantes,

I am writing to share a recommendation for the heating and cooling system of the New Quincy Courthouse. I hope that your eventual design/build agent will help you to consider geothermal heat pump (GHP) technology for this project. Your building could minimize its environmental footprint and keep operational expenses lower than with any other HVAC system. When public ownership is involved, the energy costs supporting this building will continue for its life.

The 10/15/25 Notice of Preparation of an Environmental Impact Report states that the EIR will contain 22 issue areas for consideration. Of that total, I have identified five that would be rendered neutral or positive if you opt for all-electric services and geothermal heat pump technology. They are:

(1) Air quality,
(2) Greenhouse gas emissions,
(3) Noise
(4) Energy,
(5) Hazards and hazardous materials,

1. GHPs are air quality neutral and their use displaces other buildings' negative air quality when such fuels are used for combustion.

2. Since GHPs have no combustion or back-up combustion, there are no greenhouse gas emissions.

3. Other than some pumps and a compressor in a mechanical room and small fans throughout the interior, GHPs are quiet. They heat and cool without ANY outside equipment exposed to weather or vandals. Their pumped fluid heat exchangers are publicly inaccessible and silent.

4. GHPs were proven by the EPA in the mid-1980s to consume less electricity per unit of heat or cool delivered than any other conventional HVAC method. This results in less overall consumption and less instantaneous demand—an increasingly present utility charge forced by grid capacity limits. GHPs can incorporate chilled or hot water storage easily to help displace Time-of-Day premium pricing. GHP installations will keep flat roof areas available for solar PV deployment to reduce electricity consumption. Air-source heat pumps or conventional air conditioning equipment cannot do that.

5. All occupied buildings utilize electricity. No stored gas or oil need be trucked or pumped to the site, and electricity pricing is better regulated to favor the consumer than imported fuels are.

I am a 54 year resident of Quincy and I have no financial interest in equipment, installer contracts, or any partnerships whose selection for your project might provide benefit to me. I am simply a strong and consistent advocate for this technology and am very experienced with its use in all sizes of buildings. After 35 years of teaching at Feather River Community College, I became affiliated with the **California Geothermal Heat Pump Association**, I served on its Board of Directors, and then as President for nine years.

I am now Past President. Our non-profit trade association supports **professional members** who are manufacturers, distributors, installers, drillers, mechanical engineers, and geo "utilities," (of which we have two, and they can postpone the up front cost of installing the ground loop on which all geo heat pumps depend). Like all heat pumps, geo heat pumps concentrate and move heat—they do not create it. The refrigerant-compression cycle is what makes this possible to both heat and cool.

I have experienced every kind of heating system: electrical resistance; propane; kerosene; wood, and a ducted central air-source heat pump back in 1977. **My current home was completed in 2014** and features a relatively small geo heat pump for its 3,265 sf of conditioned space. Solar PV on my roof helped me achieve outstanding results. In 10 full years of operation, this all-electric home has achieved annual **zero net energy** five times, **zero energy cost** eight times, and in the remaining two years averaged out to a monthly PG&E bill of under $4. By calculation, 80% of the heat delivered at my registers is from underground by the interaction of my ground loop with soil and with my GHP's main heat exchanger. The rest comes from my compressor raising the temperature of vaporized refrigerant gas by up to 100°.

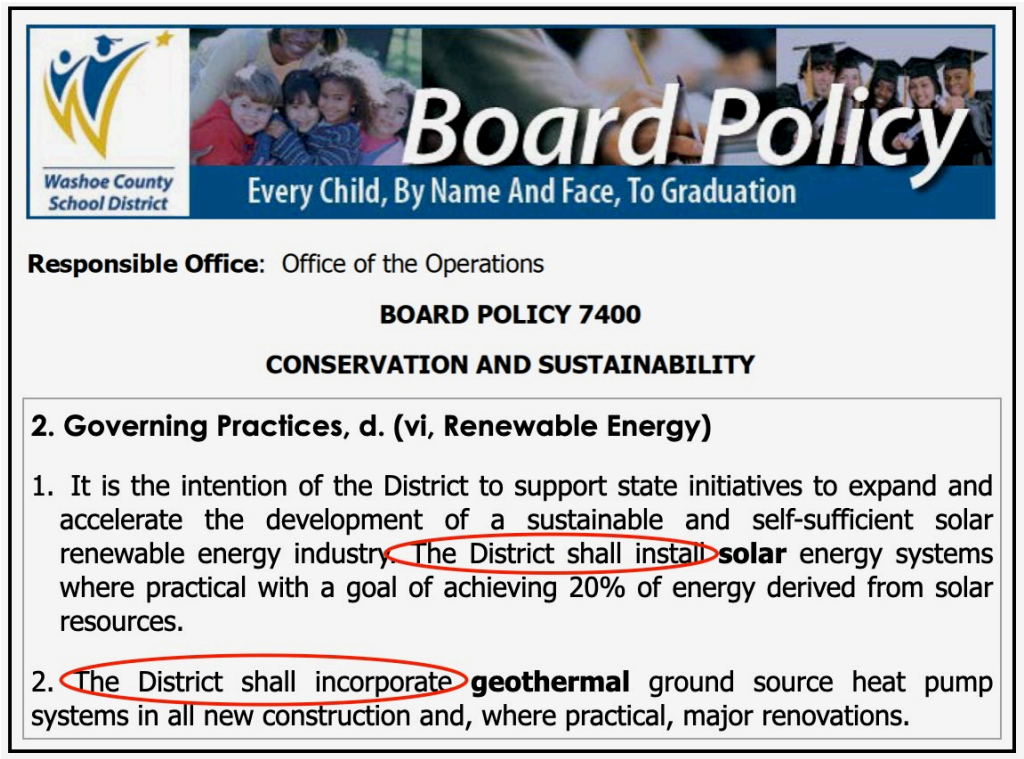
My geo heat pump is in its 13th year of operation. I am a Director for the local water and sewer district and our office unit was just replaced last week after 36 years of service. Nearby Feather River College installed its first geo systems in 1989 which continue in their 37th year. 93% of the campus' buildings are served by geo.



A Strong Commercial Performance Example

*A new 60,000 ft² Pueblo, Colorado Health Department clinic was **designed and built with Geo technology**. Its first month's total utility bill – lights, HVAC, hot water, etc. totaled $3,000, or $0.05 per ft² for the month. This owner also has a 2012-built 40,000 ft² clinic nearby with a very efficient, conventional HVAC system. That total utility bill for the same month was $7,000, or about $0.175 per ft² **(3.5 times more than the newer Geo-equipped facility).*** Their next facility constructed will be Geo!

This is an outstanding larger building served with a geo heat pump system.



Washoe County School District

Board Policy

Every Child, By Name And Face, To Graduation

Responsible Office: Office of the Operations

BOARD POLICY 7400

CONSERVATION AND SUSTAINABILITY

2. Governing Practices, d. (vi, Renewable Energy)

1. It is the intention of the District to support state initiatives to expand and accelerate the development of a sustainable and self-sufficient solar renewable energy industry. The District shall install **solar** energy systems where practical with a goal of achieving 20% of energy derived from solar resources.

2. The District shall incorporate **geothermal** ground source heat pump systems in all new construction and, where practical, major renovations.

Even with access to cheap natural gas, this Reno school district has prioritized solar PV and geo as a matter of policy.

They currently have **nine schools** equipped with geo. This fuel is free.

New York City has a number of all-geo projects like the one below. Please note that this complex fits on only 1.5 acres and that the total geo system throughout was only 1% of the construction budget.



In being a long-time advocate for GHPs in larger projects, I've found a common denominator related to human psychology. Too many projects won't consider geo and prefer conventional systems. The

architects and mechanical engineers are risk averse to consider alternative systems, even though there are examples of success elsewhere. In residential-sized projects I've seen too many "cookie cutter contractors" who do the same thing 500 times over because that is where they are comfortable and are likely to reduce construction costs. But their methods don't always do much to lower energy bills for their customers. My first contractor contact in '73 insisted on single-pane windows in my next house.

For many years, the largest hurdle for projects considering geo was the ground loop, a very necessary but poorly understood piece of the puzzle. It was a significant extra first cost that soured many against geo's use. The phrase "I hear it's expensive" quickly kills interest.

Fortunately, we now have "geo utilities," who, once the heating and cooling loads of the building(s) are known, they provide loop design, installation, guaranteed performance, and any maintenance or repair needs that might pop up. This adds no up-front construction cost and the owner pays a monthly bill structured in various ways afterward.

There are a number of projects whose details I could share if needed and I would be happy to consult with you or members of your design construction team at no expense to them, or you.

Thank you for your consideration,

Bill Martin, Quincy, CA
willycliff@gmail.com
cell = 530-394-8224





Cervantes, Alexandra

From: Ralph koehne <r.koe@hotmail.com>
Sent: Wednesday, November 12, 2025 1:32 PM
To: New Quincy Courthouse Project
Cc: Ralph koehne; Paul Stancheff
Subject: New Quincy Courthouse - Extension of Time

EXTERNAL EMAIL

Thank you for accepting my comments on the proposed new courthouse.

I realize the closing date for optional sites was in June, Therefor I'm requesting an extension of time in order to include more options.

My preferred site is the old Plumas Motor Parts store (HUT) lots, APN's 115-042-024, 025, 037, located across the street from the shopping center. This site is 2.2 acres and has been For Sale since July, over 4 months now. I'm sure the entire committee has seen the For Sale Sign and knows the location.

The HUT location has many advantages over your preferred locations of the old Feather River Publishing (FRP) site which is 2.8 ac., or the Stone House which is 2.3 ac., another iconic building to Quincy's landscape

Some of the advantages of the HUT site are as follows:

1. Save the old Quincy Lumber Red Barn (RB): The Red Barn was built by Diamond Match Lumber in 1937. It's a well-known landmark and has a unique barn setting, although never housing a horse or cow. This 88-year-old building has a concrete foundation, designed by designers and was built with milled dimensional lumber. It has had three business sites within, the old paint store, computer repair and large storage covering.
2. Lower property costs for acquisition: The HUT asking price is much lower than FRP. It's owned by one owner, whereas FRP is owned by three owners which makes negation harder.
3. Saves property taxes to Plumas County: The FRP property taxes paid to Plumas County are much higher than the HUT. The FRP, approx. 16000 sf building is a newer building and any business can move in with little remodeling. It is solar equipped.
4. Improvers the Skyline of Quincy: The Hut is located in a very visual corridor and not very attractive metal hut building, whereas the Barn adds to Quincy's skyline.
5. Less disturbance to the neighbors during demolition and construction: The Hut is located in the middle of the three lots and has room for equipment to move around and has less neighbors than the FRP, which 3 structures are closer to the neighbors boundaries.

Please extend the time so the Plumas Moter Site can be analyzed. It is in the best interest of Plumas County to analyze this property

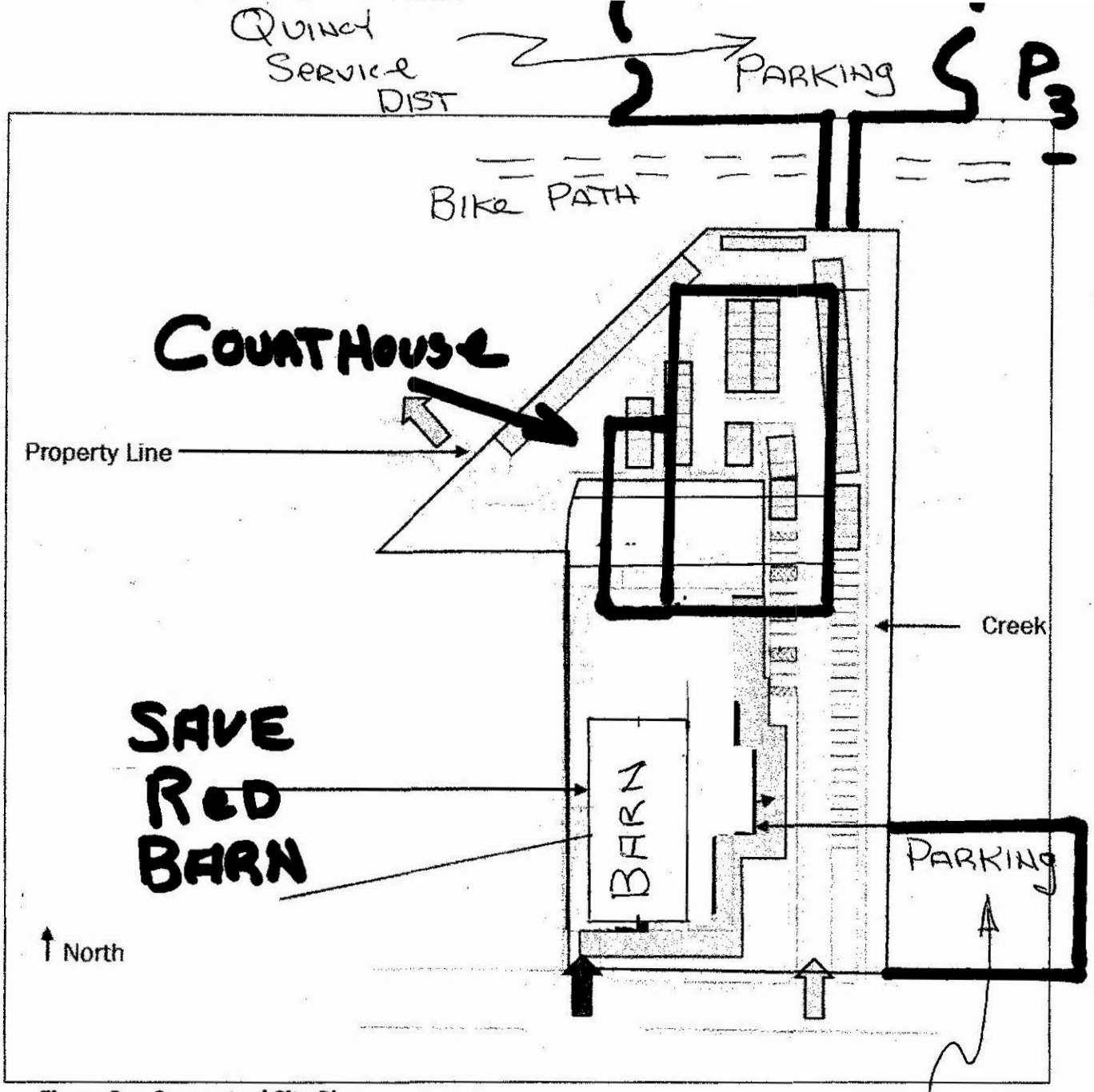


Figure 3 Conceptual Site Plan


5. -047
13
17
SOUTH LINE OLD QUINCY R.R. R/W
ASSESSOR M.P. LEGEND
U.S.T.S.
P.N.F.
HDQ TRS.
FOREST SERVICE
042
HUT
25
37
2.2 AC.
041
12
0.80Ac.
LINDAN
QUINCY JUNCTION ROAD
HIGH SCHOOL
LAWRENCE STREET
(HWY. 70)
MAIN STREET
AVENUE
03
29
SHOPPING CENTER
PLUMAS AUTO
95 MAIN ST.
FOR SALE
ASSESSOR'S PLATS ARE FOR GENERAL PROPERTY LOCATION AND TAX PURPOSES ONLY. THEY MAY NOT BE USED AS A BASIS FOR LEGAL PROPERTY DESCRIPTIONS.

Cervantes, Alexandra

From: Bill Martin <willycliff@gmail.com>
Sent: Saturday, November 8, 2025 12:26 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP
Attachments: aCervantes @Judicial Facilities 11425.pdf

EXTERNAL EMAIL

To: Mr. Alex Cervantes, Senior Facilities Analyst,
Judicial Council of California Facilities Services

From: Bill Martin, Quincy, California

Subj: New Quincy Courthouse NOP

Date: November 8, 2025.

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Your project is early enough in its development to consider all approaches to maximize its goals, both environmental and financial.

The purpose of this message is to boost consideration of geothermal heat pump technology (geo) to handle the new courthouse's heating, cooling, and hot water needs. It contains references to successful projects elsewhere that use geo, and an explanation of the basic functions of this technology.

In terms of efficiency, if one is familiar with Coefficient of Performance (COP) where an electric resistance water heater equals a COP of 1.0, residential geo systems have now broken above 5.0. But commercial systems **for larger buildings now stand at 8.0**. In an era where electricity prices are destined to rise, this thermal leverage should not be ignored.

Thank you for your consideration.
(A 5-page PDF document is attached and a hard copy w/o hot links is in the mail)

--Bill M

Cervantes, Alexandra

From: Bianca Harrison <dragonfly54b@gmail.com>
Sent: Tuesday, November 11, 2025 9:01 AM
To: New Quincy Courthouse Project
Subject: Quincy new courthouse

EXTERNAL EMAIL

Hi,
The red barn that is part of the considered parcel is a historic landmark in Quincy and beloved by the community. The local merchants and business owners rely on tourists for their income. The red barn is the last large barn in the Quincy area and should be preserved as part of the character of Quincy as a historic town.
A viable alternative is the Plumas Motor parcel that is on the market. It is an eyesore with the empty metal building, will not need a lot of demolition and it will be well situated for traffiflowc. There are no residential houses directly adjacent and the owner is willing to sell. This is the preferred choice and will not disrupt Quincy business for several years. These impacts need to be considered by the judicial council and the selection committee.

If FRP remains the preferred alternative, you can still save the old Quincy Lumber Red Barn. If replacement area is needed by saving the barns 0.5 ac., buy the property to the East, green shop, APN 115-031-047, 0.11 ac., which was For Sale all summer. Another option is to neigiate with Quincy Services Dist., part of their property to the North, across the bike path. This level property is 4.18 ac. and has not been used for years. The bike path can be relocated to make contiguous parking, if needed.

Thank you

Ralph Koehne Sent 11-12-2025 @ 1:30 pm
PO Box 214
Quincy, Ca,. 95971 Phone-530-283-0677

Cervantes, Alexandra

From: Rose Buzzetta <rbuzzetta18@gmail.com>
Sent: Thursday, November 13, 2025 12:58 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

I have been a resident of Plumas County for 49 years. The County and Quincy itself, is declining in population and that population is aging. Crime is comparatively minimal, as opposed to more urban areas and a new 23,000 square foot courthouse with 110 parking spaces is excessive for the area. This is "urban sprawl" at it's worst.

The proposal to demolish the existing buildings on the lot off Lawrence St will destroy a landmark building, Quincy Lumber. This building is in good repair and paint and is being utilized by locals for business purposes.

I am opposed to the waste of the land and the construction of a one story expansive building.

Plumas county just built a new jail and the old jail and the ancient Armory building are right next to the new facility. I would like to see the State utilize those areas that are already in disrepair and could be demolished with a benefit to the town. INstead of purchasing land, perhaps the County would give the properties to the State for a courthouse complex and money could be spent on demolition and construction on those sites.

At that location, inmates could be walked to the courthouse from the new jail.

Also, wherever the new facility is built, please consider a multi level building to keep the footprint of the new courthouse to a minimum.

Esthetics of any new facility needs to align with the rural, agricultural history of the county.

Rose Buzzetta
rbuzzetta18@gmail.com

Cervantes, Alexandra

From: Rose Buzzetta <rbuzzetta18@gmail.com>
Sent: Monday, November 17, 2025 2:15 PM
To: New Quincy Courthouse Project
Subject: new quincy courthouseNOP

EXTERNAL EMAIL

I have given a response to the proposed courthouse plan previously. I would like to reiterate that I feel a one level, expansive building is unnecessary and a waste of taxpayer money.
Please consider purchasing the bulletin building and the storage area by Lawrence St only, and leave the quaint Quincy Lumber building. put parking in the front--you DO NOT need 120 spaces and keep the building footprint smaller and taller. Build a two story building.
Rose Buzzetta

Cervantes, Alexandra

From: Len Fernandes <len.fernandes.writes@gmail.com>
Sent: Thursday, November 13, 2025 3:23 PM
To: New Quincy Courthouse Project
Cc: Senator.Dahle@outreach.senate.ca.gov
Subject: New Quincy Courthouse NOP

EXTERNAL EMAIL

In response to Sen. Dahle's email, has the already built facility in Portola even been considered?

This is a beautiful building that has sat vacant for years and is just rotting away. Taxpayer dollars down the toilet.

https://capital-engineering.com/projects/civic/criminal-justice/plumas-sierra-courthouse/



---------- Forwarded message---------
From: <Senator.Dahle@outreach.senate.ca.gov>
Date: Thu, Nov 13, 2025 at 2:00 PM
Subject: Help shape the future of Plumas County courthouse
To:

Display errors? Click here to view in browser.

Help shape the future of Plumas courthouse

A new courthouse can shape a community for a very long time, as residents of Plumas County know well. The courthouse in Quincy, the county seat, has been a landmark for more than a century.

The courthouse remains a beauty, but its age is showing. It doesn't meet modern security or access standards, and it has the various troubles of a century-old building. Because of those needs, Plumas County has reached the top of the list for the state Judicial Council to invest in a new courthouse.

The roughly $100 million new courthouse will be a major investment in Quincy and a big change to its downtown. As with any project this size, the state has an obligation to review the impacts. It recently launched that process and is taking community input on what the public thinks are the critical factors to study. It's important to know that early plans to build on Quincy's Dame Shirley Plaza have been abandoned, and the courts are now exploring other sites. The new preferred location is the old Feather Publishing property.

Many more details about the proposal are on the courts' website here.

The courts are taking written comments by Monday, November 17, 2025.

Alex Cervantes, Senior Facilities Analyst
Judicial Council of California, Facilities Services
2860 Gateway Oaks Drive, Suite 400
Sacramento, CA 95833-3509

Email: newquincycourthouseproject@jud.ca.gov (Use "New Quincy Courthouse NOP" in the Subject line.)

Make sure your voice is heard early to shape this important project so it best meets the community's needs.

– Senator Megan Dahle

Click here to unsubscribe or update your email address.

Cervantes, Alexandra

From: Dawn <dawnlaborde@gmail.com>
Sent: Thursday, November 13, 2025 4:11 PM
To: New Quincy Courthouse Project
Subject: Comment

EXTERNAL EMAIL

Hello,
Modern is not more beautiful. The courthouse in Quincy is so beautiful, please do not destroy it with a hideous modern building.
Let America's history remain!
Repair reinforce if needed but please leave it alone.
Dawn LaBorde

Cervantes, Alexandra

From: Dawn <dawnlaborde@gmail.com>
Sent: Thursday, November 13, 2025 4:12 PM
To: New Quincy Courthouse Project
Subject: Inquiry

EXTERNAL EMAIL

Who's idea is this to destroy that beautiful courthouse.
I imagine it's not a local!
Dawn

Cervantes, Alexandra

From: Sandy Fitzpatrick <sandyfitz70@gmail.com>
Sent: Friday, November 14, 2025 1:14 PM
To: New Quincy Courthouse Project
Subject: New Quincy Courthouse

EXTERNAL EMAIL

Gentlemen,
Thank you for opportunity to voice concerns re new courthouse.

Sadly, the recent public meeting was not well advertised, as you must have discerned from poor public attendance.

For we folks who have lived here more than 60 years, we feel we have more common-sense re our community needs than state mandated square-footage buildings. As was stated at the original meeting, space for 160 parking places is required. This is such overkill!
Reading in Plumas Sun, it appears there are still other sites to consider.
I have no opposition to the Feather River Bulletin site; however object to the removal of one of our town's historical sites, Quincy Lumber, and the amount of required parking.
Thanks again…knowing my comments are worthless in the long run…too bad city folks won't reconsider input from folks living here.

Sandra Fitzpatrick
2349 Ponderosa St
Quincy, Ca 95971

APPENDIX B

Air Quality and GHG Emissions Calculations

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New Quincy Courthouse Detailed Report

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1. Basic Project Information

1.1. Basic Project Information

Data Field	Value
Project Name	New Quincy Courthouse
Construction Start Date	10/1/2028
Operational Year	2030
Lead Agency	—
Land Use Scale	Project/site
Analysis Level for Defaults	County
Windspeed (m/s)	2.90000
Precipitation (days)	61.6000
Location	287 Lawrence St, Quincy, CA 95971, USA
County	Plumas
City	Unincorporated
Air District	Northern Sierra AQMD
Air Basin	Mountain Counties
TAZ	273
EDFZ	3
Electric Utility	Plumas-Sierra Rural Electric Cooperative
Gas Utility	Pacific Gas & Electric
App Version	2022.1.1.43

1.2. Land Use Types

Land Use Subtype	Size	Unit	Lot Acreage	Building Area (sq ft)	Landscape Area (sq ft)	Special Landscape Area (sq ft)	Population	Description
General Office Building	23.1000	1000sqft	0.75069	23,100.0	5,000.00	—	—	—

Parking Lot	120.000	Space	2.10931	0.00000	0.00000	—	—	—

1.3. User-Selected Emission Reduction Measures by Emissions Sector

No measures selected

2. Emissions Summary

2.1. Construction Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	1.35862	1.23291	9.12109	12.1176	0.02401	0.26092	0.13544	0.36247	0.24019	0.03175	0.26520	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	12.1202	12.0976	14.4585	15.4766	0.03799	0.51580	2.85250	3.36830	0.47453	1.35681	1.83135	—	3,728.68	3,728.68	0.11458	0.19970	0.05833	3,790.97
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	1.02857	0.91538	4.81965	6.42128	0.01259	0.13830	0.15752	0.22220	0.12731	0.04214	0.14048	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.18771	0.16706	0.87959	1.17188	0.00230	0.02524	0.02875	0.04055	0.02323	0.00769	0.02564	—	208.706	208.706	0.00818	0.00329	0.01754	209.908

2.2. Construction Emissions by Year

2.2.1. Total Construction Emissions by Year, Unmitigated

Includes both onsite and offsite emissions.

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	1.35862	1.23291	9.12109	12.1176	0.02401	0.26092	0.13544	0.36247	0.24019	0.03175	0.26520	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	1.69461	1.42554	14.4585	15.4766	0.03799	0.51580	2.85250	3.36830	0.47453	1.35681	1.83135	—	3,728.68	3,728.68	0.11458	0.19970	0.05833	3,790.97
2029	12.1202	12.0976	9.14121	12.0830	0.02401	0.26100	0.13544	0.36256	0.24019	0.03175	0.26520	—	2,394.20	2,394.20	0.09374	0.03820	0.01185	2,407.93
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.25972	0.21792	1.96542	2.34471	0.00496	0.06467	0.15752	0.22220	0.05960	0.04214	0.10174	—	499.384	499.384	0.01766	0.01528	0.07716	504.455
2029	1.02857	0.91538	4.81965	6.42128	0.01259	0.13830	0.05367	0.19197	0.12731	0.01316	0.14048	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.04740	0.03977	0.35869	0.42791	0.00091	0.01180	0.02875	0.04055	0.01088	0.00769	0.01857	—	82.6788	82.6788	0.00292	0.00253	0.01277	83.5183
2029	0.18771	0.16706	0.87959	1.17188	0.00230	0.02524	0.00979	0.03504	0.02323	0.00240	0.02564	—	208.706	208.706	0.00818	0.00329	0.01754	209.908

2.2.2. Onsite Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	1.27069	1.15509	8.88672	11.6062	0.02312	0.25913	0.00000	0.25913	0.23840	0.00000	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	1.60969	1.35258	12.1706	14.4591	0.02508	0.51580	2.76221	3.27801	0.47453	1.33565	1.81018	—	2,715.59	2,715.59	0.11016	0.02203	0.00000	2,724.91
2029	12.1118	12.0903	8.88672	11.6062	0.02312	0.25913	0.00000	0.25913	0.23840	0.00000	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.24755	0.20699	1.81477	2.22805	0.00411	0.06336	0.12493	0.18828	0.05829	0.03378	0.09206	—	410.478	410.478	0.01665	0.00333	0.00000	411.886

2029	1.00193	0.89225	4.69184	6.16011	0.01213	0.13740	0.00000	0.13740	0.12641	0.00000	0.12641	—	1,157.63	1,157.63	0.04696	0.00939	0.00000	1,161.60
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.04518	0.03778	0.33120	0.40662	0.00075	0.01156	0.02280	0.03436	0.01064	0.00616	0.01680	—	67.9592	67.9592	0.00276	0.00055	0.00000	68.1925
2029	0.18285	0.16283	0.85626	1.12422	0.00221	0.02507	0.00000	0.02507	0.02307	0.00000	0.02307	—	191.659	191.659	0.00777	0.00155	0.00000	192.316

2.2.3. Offsite Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	0.08793	0.07783	0.23438	0.94486	0.00089	0.00178	0.13544	0.13544	0.00178	0.03175	0.03175	—	198.224	198.224	0.00720	0.02009	0.45629	204.784
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.11168	0.09807	2.28798	1.01743	0.01406	0.02091	0.40117	0.42208	0.02091	0.10539	0.12630	—	1,234.15	1,234.15	0.00772	0.17946	0.05833	1,287.89
2029	0.08562	0.07485	0.25449	0.86902	0.00089	0.00187	0.13544	0.13544	0.00178	0.03175	0.03175	—	193.153	193.153	0.00853	0.02034	0.01185	199.337
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.01216	0.01092	0.15065	0.11666	0.00086	0.00132	0.03260	0.03391	0.00132	0.00836	0.00968	—	88.9067	88.9067	0.00101	0.01195	0.07716	92.5688
2029	0.02664	0.02313	0.12781	0.26117	0.00045	0.00091	0.05367	0.05458	0.00091	0.01316	0.01407	—	102.968	102.968	0.00243	0.01047	0.10592	106.256
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.00222	0.00199	0.02749	0.02129	0.00016	0.00024	0.00595	0.00619	0.00024	0.00153	0.00177	—	14.7195	14.7195	0.00017	0.00198	0.01277	15.3258
2029	0.00486	0.00422	0.02333	0.04766	0.00008	0.00017	0.00979	0.00996	0.00017	0.00240	0.00257	—	17.0475	17.0475	0.00040	0.00173	0.01754	17.5918

2.3. Operations Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	4.71954	4.21086	4.96395	42.4915	0.08893	0.09556	7.62802	7.72358	0.08969	1.94540	2.03510	19.4454	10,149.1	10,168.5	2.39121	0.37406	24.6180	10,364.4
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	4.48567	3.98224	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	19.4454	9,681.07	9,700.51	2.41999	0.41787	0.69308	9,886.23
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	3.58313	3.19952	4.20445	29.3411	0.06443	0.07187	5.54898	5.62085	0.06754	1.41631	1.48386	19.4454	7,660.25	7,679.70	2.31902	0.31145	8.08428	7,838.57
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.65392	0.58391	0.76731	5.35474	0.01176	0.01312	1.01269	1.02580	0.01233	0.25848	0.27080	3.21941	1,268.24	1,271.46	0.38394	0.05156	1.33844	1,297.76

2.4. Operations Emissions by Sector, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Sector	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Area	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.71954	4.21086	4.96395	42.4915	0.08893	0.09556	7.62802	7.72358	0.08969	1.94540	2.03510	19.4454	10,149.1	10,168.5	2.39121	0.37406	24.6180	10,364.4
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Mobile	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Area	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.48567	3.98224	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	19.4454	9,681.07	9,700.51	2.41999	0.41787	0.69308	9,886.23
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.96050	2.58369	4.20028	28.8456	0.06440	0.07099	5.54898	5.61997	0.06688	1.41631	1.48319	—	6,549.40	6,549.40	0.27430	0.28248	8.02810	6,648.47
Area	0.62262	0.61582	0.00417	0.49546	0.00003	0.00088	—	0.00088	0.00067	—	0.00067	—	2.03738	2.03738	0.00009	0.00002	—	2.04473
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	3.58313	3.19952	4.20445	29.3411	0.06443	0.07187	5.54898	5.62085	0.06754	1.41631	1.48386	19.4454	7,660.25	7,679.70	2.31902	0.31145	8.08428	7,838.57
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Area	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	180.917	180.917	0.01317	0.00160	—	181.722
Water	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808
Waste	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	0.65392	0.58391	0.76731	5.35474	0.01176	0.01312	1.01269	1.02580	0.01233	0.25848	0.27080	3.21941	1,268.24	1,271.46	0.38394	0.05156	1.33844	1,297.76

3. Construction Emissions Details

3.1. Demolition (2028)

3.1.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.58294	1.32747	12.1706	14.4591	0.02393	0.44950	—	0.44950	0.41354	—	0.41354	—	2,494.52	2,494.52	0.10119	0.02024	—	2,503.08
Demolition	—	—	—	—	—	—	1.35820	1.35820	—	0.20567	0.20567	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.08674	0.07274	0.66688	0.79228	0.00131	0.02463	—	0.02463	0.02266	—	0.02266	—	136.686	136.686	0.00554	0.00111	—	137.155
Demolition	—	—	—	—	—	—	0.07442	0.07442	—	0.01127	0.01127	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01583	0.01327	0.12171	0.14459	0.00024	0.00450	—	0.00450	0.00414	—	0.00414	—	22.6299	22.6299	0.00092	0.00018	—	22.7076
Demolition	—	—	—	—	—	—	0.01358	0.01358	—	0.00206	0.00206	—	—	—	—	—	—	—

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.1.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.07465	0.06893	0.07338	0.78706	0.00000	0.00000	0.11287	0.11287	0.00000	0.02646	0.02646	—	118.201	118.201	0.00738	0.00462	0.01068	119.774
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.03702	0.02914	2.21461	0.23037	0.01406	0.02091	0.28830	0.30921	0.02091	0.07893	0.09984	—	1,115.95	1,115.95	0.00034	0.17484	0.04765	1,168.11
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00403	0.00375	0.00356	0.04206	0.00000	0.00000	0.00594	0.00594	0.00000	0.00139	0.00139	—	6.55810	6.55810	0.00037	0.00025	0.00977	6.65273
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00207	0.00162	0.12047	0.01240	0.00077	0.00115	0.01532	0.01647	0.00115	0.00421	0.00535	—	61.1522	61.1522	0.00002	0.00958	0.04341	64.0509
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00074	0.00068	0.00065	0.00768	0.00000	0.00000	0.00108	0.00108	0.00000	0.00025	0.00025	—	1.08577	1.08577	0.00006	0.00004	0.00162	1.10144
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00038	0.00029	0.02198	0.00226	0.00014	0.00021	0.00280	0.00301	0.00021	0.00077	0.00098	—	10.1244	10.1244	< 0.000005	0.00159	0.00719	10.6044

3.2. Site Preparation (2028)

3.2.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24548	1.04655	8.41892	10.7072	0.02508	0.35834	—	0.35834	0.32967	—	0.32967	—	2,715.59	2,715.59	0.11016	0.02203	—	2,724.91
Dust From Material Movement	—	—	—	—	—	—	0.62039	0.62039	—	0.06699	0.06699	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01024	0.00860	0.06920	0.08800	0.00021	0.00295	—	0.00295	0.00271	—	0.00271	—	22.3199	22.3199	0.00091	0.00018	—	22.3965
Dust From Material Movement	—	—	—	—	—	—	0.00510	0.00510	—	0.00055	0.00055	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00187	0.00157	0.01263	0.01606	0.00004	0.00054	—	0.00054	0.00049	—	0.00049	—	3.69532	3.69532	0.00015	0.00003	—	3.70800
Dust From Material Movement	—	—	—	—	—	—	0.00093	0.00093	—	0.00010	0.00010	—	—	—	—	—	—	—

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.2.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04479	0.04136	0.04403	0.47223	0.00000	0.00000	0.06772	0.06772	0.00000	0.01587	0.01587	—	70.9208	70.9208	0.00443	0.00277	0.00641	71.8647
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00036	0.00034	0.00032	0.00379	0.00000	0.00000	0.00053	0.00053	0.00000	0.00012	0.00012	—	0.59023	0.59023	0.00003	0.00002	0.00088	0.59875
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00007	0.00006	0.00006	0.00069	0.00000	0.00000	0.00010	0.00010	0.00000	0.00002	0.00002	—	0.09772	0.09772	0.00001	< 0.000005	0.00015	0.09913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3. Grading (2028)

3.3.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.60969	1.35258	11.7838	13.9071	0.02268	0.51580	—	0.51580	0.47453	—	0.47453	—	2,456.26	2,456.26	0.09964	0.01993	—	2,464.69
Dust From Material Movement	—	—	—	—	—	—	2.76221	2.76221	—	1.33565	1.33565	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02646	0.02223	0.19371	0.22861	0.00037	0.00848	—	0.00848	0.00780	—	0.00780	—	40.3769	40.3769	0.00164	0.00033	—	40.5155
Dust From Material Movement	—	—	—	—	—	—	0.04541	0.04541	—	0.02196	0.02196	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00483	0.00406	0.03535	0.04172	0.00007	0.00155	—	0.00155	0.00142	—	0.00142	—	6.68486	6.68486	0.00027	0.00005	—	6.70781
Dust From Material Movement	—	—	—	—	—	—	0.00829	0.00829	—	0.00401	0.00401	—	—	—	—	—	—	—

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.05972	0.05514	0.05870	0.62964	0.00000	0.00000	0.09030	0.09030	0.00000	0.02117	0.02117	—	94.5610	94.5610	0.00590	0.00370	0.00854	95.8196
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00097	0.00090	0.00085	0.01010	0.00000	0.00000	0.00143	0.00143	0.00000	0.00033	0.00033	—	1.57394	1.57394	0.00009	0.00006	0.00234	1.59666
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00018	0.00016	0.00016	0.00184	0.00000	0.00000	0.00026	0.00026	0.00000	0.00006	0.00006	—	0.26058	0.26058	0.00001	0.00001	0.00039	0.26434
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4. Building Construction (2028)

3.4.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.29438	1.07850	9.22917	11.6712	0.02312	0.28471	—	0.28471	0.26194	—	0.26194	—	2,201.41	2,201.41	0.08930	0.01786	—	2,208.97
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.12412	0.10342	0.88499	1.11915	0.00222	0.02730	—	0.02730	0.02512	—	0.02512	—	211.095	211.095	0.00856	0.00171	—	211.819
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02265	0.01887	0.16151	0.20425	0.00040	0.00498	—	0.00498	0.00458	—	0.00458	—	34.9491	34.9491	0.00142	0.00028	—	35.0691
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04415	0.04076	0.04339	0.46543	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	69.8995	69.8995	0.00436	0.00273	0.00631	70.8298
Vendor	0.00565	0.00451	0.22924	0.05092	0.00089	0.00187	0.03481	0.03668	0.00187	0.00937	0.01124	—	127.691	127.691	0.00106	0.01850	0.00667	133.236
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00417	0.00388	0.00368	0.04353	0.00000	0.00000	0.00615	0.00615	0.00000	0.00144	0.00144	—	6.78685	6.78685	0.00039	0.00026	0.01011	6.88478
Vendor	0.00057	0.00045	0.02176	0.00478	0.00009	0.00017	0.00323	0.00340	0.00017	0.00087	0.00104	—	12.2455	12.2455	0.00011	0.00177	0.01065	12.7850
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00076	0.00071	0.00067	0.00794	0.00000	0.00000	0.00112	0.00112	0.00000	0.00026	0.00026	—	1.12364	1.12364	0.00006	0.00004	0.00167	1.13985
Vendor	0.00010	0.00008	0.00397	0.00087	0.00002	0.00003	0.00059	0.00062	0.00003	0.00016	0.00019	—	2.02737	2.02737	0.00002	0.00029	0.00176	2.11670
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5. Building Construction (2029)

3.5.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24858	1.04039	8.88672	11.6062	0.02312	0.25913	—	0.25913	0.23840	—	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24858	1.04039	8.88672	11.6062	0.02312	0.25913	—	0.25913	0.23840	—	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.63528	0.52936	4.52162	5.90532	0.01176	0.13185	—	0.13185	0.12130	—	0.12130	—	1,119.90	1,119.90	0.04543	0.00909	—	1,123.75
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.11594	0.09661	0.82520	1.07772	0.00215	0.02406	—	0.02406	0.02214	—	0.02214	—	185.413	185.413	0.00752	0.00150	—	186.049
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04333	0.03835	0.02845	0.46563	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	73.7827	73.7827	0.00355	0.00257	0.22486	74.8626
Vendor	0.00582	0.00468	0.20592	0.04577	0.00089	0.00178	0.03481	0.03659	0.00178	0.00937	0.01115	—	124.441	124.441	0.00114	0.01752	0.23073	129.922
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04219	0.03689	0.03874	0.42825	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	68.7193	68.7193	0.00420	0.00273	0.00584	69.6450
Vendor	0.00565	0.00443	0.21576	0.04855	0.00089	0.00187	0.03481	0.03668	0.00178	0.00937	0.01115	—	124.433	124.433	0.00025	0.01761	0.00598	129.692
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02122	0.01860	0.01718	0.21192	0.00000	0.00000	0.03262	0.03262	0.00000	0.00762	0.00762	—	35.4036	35.4036	0.00205	0.00139	0.04940	35.9190
Vendor	0.00288	0.00230	0.10857	0.02381	0.00045	0.00091	0.01714	0.01804	0.00091	0.00462	0.00553	—	63.3146	63.3146	0.00013	0.00892	0.05059	66.0251
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00387	0.00339	0.00313	0.03868	0.00000	0.00000	0.00595	0.00595	0.00000	0.00139	0.00139	—	5.86148	5.86148	0.00034	0.00023	0.00818	5.94681
Vendor	0.00052	0.00042	0.01981	0.00435	0.00008	0.00017	0.00313	0.00329	0.00017	0.00084	0.00101	—	10.4825	10.4825	0.00002	0.00148	0.00838	10.9312
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6. Paving (2029)

3.6.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.71805	0.60245	5.41905	8.18783	0.01181	0.18968	—	0.18968	0.17450	—	0.17450	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.71805	0.60245	5.41905	8.18783	0.01181	0.18968	—	0.18968	0.17450	—	0.17450	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01967	0.01651	0.14847	0.22432	0.00032	0.00520	—	0.00520	0.00478	—	0.00478	—	34.0659	34.0659	0.00138	0.00028	—	34.1828
Paving	0.01514	0.01514	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00359	0.00301	0.02710	0.04094	0.00006	0.00095	—	0.00095	0.00087	—	0.00087	—	5.64000	5.64000	0.00023	0.00005	—	5.65936
Paving	0.00276	0.00276	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Worker	0.08793	0.07783	0.05773	0.94486	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	149.721	149.721	0.00720	0.00522	0.45629	151.913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.08562	0.07485	0.07861	0.86902	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	139.447	139.447	0.00853	0.00555	0.01185	141.325
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00232	0.00203	0.00188	0.02316	0.00000	0.00000	0.00356	0.00356	0.00000	0.00083	0.00083	—	3.86840	3.86840	0.00022	0.00015	0.00540	3.92472
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00042	0.00037	0.00034	0.00423	0.00000	0.00000	0.00065	0.00065	0.00000	0.00015	0.00015	—	0.64046	0.64046	0.00004	0.00003	0.00089	0.64978
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7. Architectural Coating (2029)

3.7.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road	0.12385	0.10236	0.79416	1.11216	0.00173	0.01284	—	0.01284	0.01181	—	0.01181	—	133.510	133.510	0.00542	0.00108	—	133.968
Architectural Coatings	11.9879	11.9879	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00339	0.00280	0.02176	0.03047	0.00005	0.00035	—	0.00035	0.00032	—	0.00032	—	3.65780	3.65780	0.00015	0.00003	—	3.67035
Architectural Coatings	0.32844	0.32844	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00062	0.00051	0.00397	0.00556	0.00001	0.00006	—	0.00006	0.00006	—	0.00006	—	0.60559	0.60559	0.00002	< 0.000005	—	0.60767
Architectural Coatings	0.05994	0.05994	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00844	0.00738	0.00775	0.08565	0.00000	0.00000	0.01335	0.01335	0.00000	0.00313	0.00313	—	13.7439	13.7439	0.00084	0.00055	0.00117	13.9290
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00023	0.00020	0.00018	0.00228	0.00000	0.00000	0.00035	0.00035	0.00000	0.00008	0.00008	—	0.38127	0.38127	0.00002	0.00001	0.00053	0.38682
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00004	0.00004	0.00003	0.00042	0.00000	0.00000	0.00006	0.00006	0.00000	0.00001	0.00001	—	0.06312	0.06312	< 0.000005	< 0.000005	0.00009	0.06404
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

4. Operations Emissions Details

4.1. Mobile Emissions by Land Use

4.1.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

General Office Building	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73

4.2. Energy

4.2.1. Electricity Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	164.371	164.371	0.01197	0.00145	—	165.103
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	16.5462	16.5462	0.00120	0.00015	—	16.6198
Total	—	—	—	—	—	—	—	—	—	—	—	—	180.917	180.917	0.01317	0.00160	—	181.722

4.2.3. Natural Gas Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

4.3. Area Emissions by Source

4.3.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Source	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Architectural Coating	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscape Equipment	0.17888	0.16509	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Total	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.09154	0.09154	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.00599	0.00599	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscape Equipment	0.01610	0.01486	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Total	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853

4.4. Water Emissions by Land Use

4.4.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808

4.5. Waste Emissions by Land Use

4.5.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649

4.6. Refrigerant Emissions by Land Use

4.6.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930

4.7. Offroad Emissions By Equipment Type

4.7.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.8. Stationary Emissions By Equipment Type

4.8.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.9. User Defined Emissions By Equipment Type

4.9.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10. Soil Carbon Accumulation By Vegetation Type

4.10.1. Soil Carbon Accumulation By Vegetation Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Vegetation	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.2. Above and Belowground Carbon Accumulation by Land Use Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.3. Avoided and Sequestered Emissions by Species - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Species	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

5. Activity Data

5.1. Construction Schedule

Phase Name	Phase Type	Start Date	End Date	Days Per Week	Work Days per Phase	Phase Description
Demolition	Demolition	10/1/2028	10/29/2028	5.00000	20.0000	—
Site Preparation	Site Preparation	10/30/2028	11/3/2028	5.00000	3.00000	—
Grading	Grading	11/4/2028	11/12/2028	5.00000	6.00000	—
Building Construction	Building Construction	11/13/2028	9/17/2029	5.00000	220.000	—
Paving	Paving	9/18/2029	10/2/2029	5.00000	10.00000	—
Architectural Coating	Architectural Coating	10/3/2029	10/17/2029	5.00000	10.00000	—

5.2. Off-Road Equipment

5.2.1. Unmitigated

Phase Name	Equipment Type	Fuel Type	Engine Tier	Number per Day	Hours Per Day	Horsepower	Load Factor
Demolition	Concrete/Industrial Saws	Diesel	Average	1.000000	8.00000	33.0000	0.73000
Demolition	Rubber Tired Dozers	Diesel	Average	1.000000	8.00000	367.000	0.40000
Demolition	Tractors/Loaders/Backhoes	Diesel	Average	3.00000	8.00000	84.0000	0.37000
Site Preparation	Graders	Diesel	Average	1.000000	8.00000	148.000	0.41000
Site Preparation	Scrapers	Diesel	Average	1.000000	8.00000	423.000	0.48000
Site Preparation	Tractors/Loaders/Backhoes	Diesel	Average	1.000000	7.00000	84.0000	0.37000
Grading	Graders	Diesel	Average	1.000000	8.00000	148.000	0.41000
Grading	Rubber Tired Dozers	Diesel	Average	1.000000	8.00000	367.000	0.40000
Grading	Tractors/Loaders/Backhoes	Diesel	Average	2.00000	7.00000	84.0000	0.37000
Building Construction	Cranes	Diesel	Average	1.000000	8.00000	367.000	0.29000
Building Construction	Forklifts	Diesel	Average	2.00000	7.00000	82.0000	0.20000
Building Construction	Generator Sets	Diesel	Average	1.000000	8.00000	14.0000	0.74000
Building Construction	Tractors/Loaders/Backhoes	Diesel	Average	1.000000	6.00000	84.0000	0.37000
Building Construction	Welders	Diesel	Average	3.00000	8.00000	46.0000	0.45000
Paving	Cement and Mortar Mixers	Diesel	Average	1.000000	8.00000	10.00000	0.56000
Paving	Pavers	Diesel	Average	1.000000	8.00000	81.0000	0.42000
Paving	Paving Equipment	Diesel	Average	1.000000	8.00000	89.0000	0.36000
Paving	Rollers	Diesel	Average	2.00000	8.00000	36.0000	0.38000
Paving	Tractors/Loaders/Backhoes	Diesel	Average	1.000000	8.00000	84.0000	0.37000
Architectural Coating	Air Compressors	Diesel	Average	1.000000	6.00000	37.0000	0.48000

5.3. Construction Vehicles

5.3.1. Unmitigated

Phase Name	Trip Type	One-Way Trips per Day	Miles per Trip	Vehicle Mix
Demolition	Worker	12.5000	12.7800	LDA,LDT1,LDT2
Demolition	Vendor	—	10.6800	HHDT,MHDT
Demolition	Hauling	15.5500	20.0000	HHDT
Demolition	Onsite truck	—	—	HHDT
Site Preparation	Worker	7.50000	12.7800	LDA,LDT1,LDT2
Site Preparation	Vendor	—	10.6800	HHDT,MHDT
Site Preparation	Hauling	0.00000	20.0000	HHDT
Site Preparation	Onsite truck	—	—	HHDT
Grading	Worker	10.00000	12.7800	LDA,LDT1,LDT2
Grading	Vendor	—	10.6800	HHDT,MHDT
Grading	Hauling	0.00000	20.0000	HHDT
Grading	Onsite truck	—	—	HHDT
Building Construction	Worker	7.39200	12.7800	LDA,LDT1,LDT2
Building Construction	Vendor	3.78609	10.6800	HHDT,MHDT
Building Construction	Hauling	0.00000	20.0000	HHDT
Building Construction	Onsite truck	—	—	HHDT
Paving	Worker	15.0000	12.7800	LDA,LDT1,LDT2
Paving	Vendor	—	10.6800	HHDT,MHDT
Paving	Hauling	0.00000	20.0000	HHDT
Paving	Onsite truck	—	—	HHDT
Architectural Coating	Worker	1.47840	12.7800	LDA,LDT1,LDT2
Architectural Coating	Vendor	—	10.6800	HHDT,MHDT
Architectural Coating	Hauling	0.00000	20.0000	HHDT
Architectural Coating	Onsite truck	—	—	HHDT

5.4. Vehicles

5.4.1. Construction Vehicle Control Strategies

Non-applicable. No control strategies activated by user.

5.5. Architectural Coatings

Phase Name	Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)
Architectural Coating	0.00000	0.00000	34,650.0	11,550.0	5,512.90

5.6. Dust Mitigation

5.6.1. Construction Earthmoving Activities

Phase Name	Material Imported (Ton of Debris)	Material Exported (Ton of Debris)	Acres Graded (acres)	Material Demolished (Building Square Footage)	Acres Paved (acres)
Demolition	0.00000	0.00000	0.00000	27,000.0	0.00000
Site Preparation	0.00000	0.00000	4.50000	0.00000	0.00000
Grading	0.00000	0.00000	6.00000	0.00000	0.00000
Paving	0.00000	0.00000	0.00000	0.00000	2.10931

5.6.2. Construction Earthmoving Control Strategies

Control Strategies Applied	Frequency (per day)	PM10 Reduction	PM2.5 Reduction
Water Exposed Area	2	61%	61%

5.7. Construction Paving

Phase Name	Land Use	Area Paved (acres)	% Asphalt
Paving	General Office Building	0.00000	0%
Paving	Parking Lot	2.10931	100%

5.8. Construction Electricity Consumption and Emissions Factors

kWh per Year and Emission Factor (lb/MWh)

Year	kWh per Year	CO2	CH4	N2O
2028	0.00000	453.209	0.03300	0.00400
2029	0.00000	453.209	0.03300	0.00400

5.9. Operational Mobile Sources

5.9.1. Unmitigated

Land Use Type	Trips/Weekday	Trips/Saturday	Trips/Sunday	Trips/Year	VMT/Weekday	VMT/Saturday	VMT/Sunday	VMT/Year
General Office Building	435.950	98.9169	31.3311	120,450	10,643.2	2,414.94	764.914	2,940,651
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

5.10. Operational Area Sources

5.10.1. Hearths

Land Use	Hearth Type	Unmitigated (number)	Mitigated (number)
General Office Building	Wood Fireplaces	0	0
General Office Building	Gas Fireplaces	0	0
General Office Building	Propane Fireplaces	0	0
General Office Building	Electric Fireplaces	0	0
General Office Building	No Fireplaces	0	0
General Office Building	Conventional Wood Stoves	0	0
General Office Building	Catalytic Wood Stoves	0	0
General Office Building	Non-Catalytic Wood Stoves	0	0
General Office Building	Pellet Wood Stoves	0	0
Parking Lot	Wood Fireplaces	0	0

Parking Lot	Gas Fireplaces	0	0
Parking Lot	Propane Fireplaces	0	0
Parking Lot	Electric Fireplaces	0	0
Parking Lot	No Fireplaces	0	0
Parking Lot	Conventional Wood Stoves	0	0
Parking Lot	Catalytic Wood Stoves	0	0
Parking Lot	Non-Catalytic Wood Stoves	0	0
Parking Lot	Pellet Wood Stoves	0	0

5.10.2. Architectural Coatings

Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)
0.00000	0.00000	34,650.0	11,550.0	5,512.90

5.10.3. Landscape Equipment

Season	Unit	Value
Snow Days	day/yr	0.00000
Summer Days	day/yr	180.000

5.11. Operational Energy Consumption

5.11.1. Unmitigated

Electricity (kWh/yr) and CO2 and CH4 and N2O and Natural Gas (kBTU/yr)

Land Use	Electricity (kWh/yr)	CO2	CH4	N2O	Natural Gas (kBTU/yr)
General Office Building	799,577	453.209	0.0330	0.0040	0.00000
Parking Lot	80,488.3	453.209	0.0330	0.0040	0.00000

5.12. Operational Water and Wastewater Consumption

5.12.1. Unmitigated

Land Use	Indoor Water (gal/year)	Outdoor Water (gal/year)
General Office Building	4,105,650	47,553.0
Parking Lot	0.00000	0.00000

5.13. Operational Waste Generation

5.13.1. Unmitigated

Land Use	Waste (ton/year)	Cogeneration (kWh/year)
General Office Building	21.4830	0.00000
Parking Lot	0.00000	0.00000

5.14. Operational Refrigeration and Air Conditioning Equipment

5.14.1. Unmitigated

Land Use	Equipment Type	Refrigerant	GWP	Quantity (kg)	Operations Leak Rate	Service Leak Rate	Times Serviced
General Office Building	Household refrigerators and/or freezers	R-134a	1,430.00	0.01679	0.60000	0.00000	1.000000
General Office Building	Other commercial A/C and heat pumps	R-410A	2,088.00	0.00180	4.00000	4.00000	18.0000

5.15. Operational Off-Road Equipment

5.15.1. Unmitigated

5.16. Stationary Sources

5.16.1. Emergency Generators and Fire Pumps

5.16.2. Process Boilers

5.17. User Defined

5.18. Vegetation

5.18.1. Land Use Change

5.18.1.1. Unmitigated

Vegetation Land Use Type	Vegetation Soil Type	Initial Acres	Final Acres

5.18.1. Biomass Cover Type

5.18.1.1. Unmitigated

Biomass Cover Type	Initial Acres	Final Acres

5.18.2. Sequestration

5.18.2.1. Unmitigated

Tree Type	Number	Electricity Saved (kWh/year)	Natural Gas Saved (btu/year)

6. Climate Risk Detailed Report

6.1. Climate Risk Summary

Cal-Adapt midcentury 2040–2059 average projections for four hazards are reported below for your project location. These are under Representation Concentration Pathway (RCP) 8.5 which assumes GHG emissions will continue to rise strongly through 2050 and then plateau around 2100.

Climate Hazard	Result for Project Location	Unit
Temperature and Extreme Heat	25.8300	annual days of extreme heat

Extreme Precipitation	14.2000	annual days with precipitation above 20 mm
Sea Level Rise	—	meters of inundation depth
Wildfire	58.0900	annual hectares burned

Temperature and Extreme Heat data are for grid cell in which your project are located. The projection is based on the 98th historical percentile of daily maximum/minimum temperatures from observed historical data (32 climate model ensemble from Cal-Adapt, 2040–2059 average under RCP 8.5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.
Extreme Precipitation data are for the grid cell in which your project are located. The threshold of 20 mm is equivalent to about ¾ an inch of rain, which would be light to moderate rainfall if received over a full day or heavy rain if received over a period of 2 to 4 hours. Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.
Sea Level Rise data are for the grid cell in which your project are located. The projections are from Radke et al. (2017), as reported in Cal-Adapt (Radke et al., 2017, CEC-500-2017-008), and consider inundation location and depth for the San Francisco Bay, the Sacramento-San Joaquin River Delta and California coast resulting different increments of sea level rise coupled with extreme storm events. Users may select from four scenarios to view the range in potential inundation depth for the grid cell. The four scenarios are: No rise, 0.5 meter, 1.0 meter, 1.41 meters
Wildfire data are for the grid cell in which your project are located. The projections are from UC Davis, as reported in Cal-Adapt (2040–2059 average under RCP 8.5), and consider historical data of climate, vegetation, population density, and large (> 400 ha) fire history. Users may select from four model simulations to view the range in potential wildfire probabilities for the grid cell. The four simulations make different assumptions about expected rainfall and temperature are: Warmer/drier (HadGEM2-ES), Cooler/wetter (CNRM-CM5), Average conditions (CanESM2), Range of different rainfall and temperature possibilities (MIROC5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.

6.2. Initial Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score
Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	2	0	0	N/A
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	1	0	0	N/A
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	0	0	0	N/A
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.
The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.
The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores do not include implementation of climate risk reduction measures.

6.3. Adjusted Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score

Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	2	1	1	3
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	1	1	1	2
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	1	1	1	2
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.
The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.
The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores include implementation of climate risk reduction measures.

6.4. Climate Risk Reduction Measures

7. Health and Equity Details

7.1. CalEnviroScreen 4.0 Scores

The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.

Indicator	Result for Project Census Tract
Exposure Indicators	—
AQ-Ozone	72.5451
AQ-PM	40.0124
AQ-DPM	3.97013
Drinking Water	8.77982
Lead Risk Housing	47.6497
Pesticides	28.7586
Toxic Releases	3.37584
Traffic	6.03750

Effect Indicators	—
CleanUp Sites	0.00000
Groundwater	63.3737
Haz Waste Facilities/Generators	50.1390
Impaired Water Bodies	12.4528
Solid Waste	88.9347
Sensitive Population	—
Asthma	58.4247
Cardio-vascular	65.3166
Low Birth Weights	16.7693
Socioeconomic Factor Indicators	—
Education	28.0815
Housing	31.7364
Linguistic	12.2750
Poverty	51.0930
Unemployment	17.1135

7.2. Healthy Places Index Scores

The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

Indicator	Result for Project Census Tract
Economic	—
Above Poverty	40.54921083
Employed	20.45425382
Median HI	34.74913384
Education	—
Bachelor's or higher	37.46952393
High school enrollment	100
Preschool enrollment	9.713845759

Transportation	—
Auto Access	27.83267035
Active commuting	68.45887335
Social	—
2-parent households	32.0544078
Voting	70.19119723
Neighborhood	—
Alcohol availability	62.49197998
Park access	29.33401771
Retail density	10.97138458
Supermarket access	62.94110099
Tree canopy	96.09906326
Housing	—
Homeownership	65.75131528
Housing habitability	72.97574747
Low-inc homeowner severe housing cost burden	24.72731939
Low-inc renter severe housing cost burden	70.92262287
Uncrowded housing	84.29359682
Health Outcomes	—
Insured adults	79.19928141
Arthritis	0.0
Asthma ER Admissions	40.0
High Blood Pressure	0.0
Cancer (excluding skin)	0.0
Asthma	0.0
Coronary Heart Disease	0.0
Chronic Obstructive Pulmonary Disease	0.0
Diagnosed Diabetes	0.0

Life Expectancy at Birth	39.1
Cognitively Disabled	0.5
Physically Disabled	1.3
Heart Attack ER Admissions	29.4
Mental Health Not Good	0.0
Chronic Kidney Disease	0.0
Obesity	0.0
Pedestrian Injuries	48.7
Physical Health Not Good	0.0
Stroke	0.0
Health Risk Behaviors	—
Binge Drinking	0.0
Current Smoker	0.0
No Leisure Time for Physical Activity	0.0
Climate Change Exposures	—
Wildfire Risk	49.2
SLR Inundation Area	0.0
Children	72.4
Elderly	8.9
English Speaking	92.4
Foreign-born	1.1
Outdoor Workers	24.1
Climate Change Adaptive Capacity	—
Impervious Surface Cover	90.5
Traffic Density	10.7
Traffic Access	0.0
Other Indices	—
Hardship	52.4

Other Decision Support	—
2016 Voting	76.8

7.3. Overall Health & Equity Scores

Metric	Result for Project Census Tract
CalEnviroScreen 4.0 Score for Project Location (a)	26.0000
Healthy Places Index Score for Project Location (b)	43.0000
Project Located in a Designated Disadvantaged Community (Senate Bill 535)	No
Project Located in a Low-Income Community (Assembly Bill 1550)	No
Project Located in a Community Air Protection Program Community (Assembly Bill 617)	No

a: The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.
b: The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

7.4. Health & Equity Measures

No Health & Equity Measures selected.

7.5. Evaluation Scorecard

Health & Equity Evaluation Scorecard not completed.

7.6. Health & Equity Custom Measures

No Health & Equity Custom Measures created.

8. User Changes to Default Data

8.1. Justifications

Screen	Justification
Land Use	Updated land use lot acreage and landscape square footage based on project specific details
Construction: Architectural Coatings	Updated VOC content to 50 g/L per NSAQMD Rule 230.
Operations: Vehicle Data	Updated Government Office Building vehicle trip rates and trip lengths consistent with the Quincy Courthouse Transportation Analysis Draft Memo prepared by Fehr and Peers 11/14/25.

Operations: Architectural Coatings	Updated VOC content to 50 g/L per NSAQMD Rule 230.
Operations: Energy Use	Updated total annual consumption for Government Office Building (Courthouse) land use based on all-electric building design.

8.3. Land Use

Model Parameter	Units	Default Value	New Value
Lot Area	acre	0.53030	0.75069
Landscape Area	sq. ft	—	5,000.00
Lot Area	acre	1.08000	2.10931
Landscape Area	sq. ft	—	0.00000

8.4. Construction

8.4.8. Architectural Coatings

Phase Name	Model Parameter	Units	Default Value	New Value
Architectural Coating	Residential Interior VOC	g/L	250.000	50.0000
Architectural Coating	Non-Residential Interior VOC	g/L	250.000	50.0000
Architectural Coating	Residential Exterior VOC	g/L	250.000	50.0000
Architectural Coating	Non-Residential Exterior VOC	g/L	250.000	50.0000
Architectural Coating	VOC for Parking Paint	g/L	250.000	50.0000

8.5. Operations

8.5.1. Mobile Sources

8.5.1.1. Vehicle Data

Land Use	Model Parameter	Units	Default Value	New Value
General Office Building	Weekday Trip Rate	size/day	9.74000	18.8723

General Office Building	Saturday Trip Rate	size/day	2.21000	4.28212
General Office Building	Sunday Trip Rate	size/day	0.70000	1.35633
General Office Building	Non-Res H-W Trip Length	miles	13.4405	28.2403
General Office Building	Non-Res W-O Trip Length	miles	11.3555	23.8594
General Office Building	Non-Res O-O Trip Length	miles	11.0835	23.2879

8.5.2. Area Sources

8.5.2.3. Architectural Coatings

Model Parameter	Units	Default Value	New Value
Residential Interior VOC	g/L	250.000	50.0000
Non-Residential Interior VOC	g/L	250.000	50.0000
Residential Exterior VOC	g/L	250.000	50.0000
Non-Residential Exterior VOC	g/L	250.000	50.0000
VOC for Parking Paint	g/L	250.000	50.0000

8.5.3. Energy Usage

Land Use	Model Parameter	Units	Default Value	New Value
General Office Building	Electricity	kWh/yr	535,217	799,577
General Office Building	Electricity (Subject to Title 24)	kWh/yr	369,153	600,257
General Office Building	Electricity (Not Subject to Title 24)	kWh/yr	166,064	199,320
General Office Building	Natural Gas	kBTU/yr	901,997	0.00000
General Office Building	Natural Gas (Subject to Title 24)	kBTU/yr	788,529	0.00000
General Office Building	Natural Gas (Not Subject to Title 24)	kBTU/yr	113,469	0.00000

New Quincy Courthouse - Mitigated Detailed Report

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1. Basic Project Information

1.1. Basic Project Information

Data Field	Value
Project Name	New Quincy Courthouse - Mitigated
Construction Start Date	10/1/2028
Operational Year	2030
Lead Agency	—
Land Use Scale	Project/site
Analysis Level for Defaults	County
Windspeed (m/s)	2.90000
Precipitation (days)	61.6000
Location	287 Lawrence St, Quincy, CA 95971, USA
County	Plumas
City	Unincorporated
Air District	Northern Sierra AQMD
Air Basin	Mountain Counties
TAZ	273
EDFZ	3
Electric Utility	Plumas-Sierra Rural Electric Cooperative
Gas Utility	Pacific Gas & Electric
App Version	2022.1.1.43

1.2. Land Use Types

Land Use Subtype	Size	Unit	Lot Acreage	Building Area (sq ft)	Landscape Area (sq ft)	Special Landscape Area (sq ft)	Population	Description
General Office Building	23.1000	1000sqft	0.75069	23,100.0	5,000.00	—	—	—

Parking Lot	120.000	Space	2.10931	0.00000	0.00000	—	—	—

1.3. User-Selected Emission Reduction Measures by Emissions Sector

Sector	#	Measure Title
Construction	C-5	Use Advanced Engine Tiers

2. Emissions Summary

2.1. Construction Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	1.35862	1.23291	9.12109	12.1176	0.02401	0.26092	0.13544	0.36247	0.24019	0.03175	0.26520	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
Mit.	1.07326	1.00682	5.37048	14.1318	0.02401	0.11885	0.13544	0.22912	0.11172	0.03175	0.13673	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
% Reduced	21%	18%	41%	-17%	—	54%	—	37%	53%	—	48%	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	12.1202	12.0976	14.4585	15.4766	0.03799	0.51580	2.85250	3.36830	0.47453	1.35681	1.83135	—	3,728.68	3,728.68	0.11458	0.19970	0.05833	3,790.97
Mit.	12.1202	12.0976	5.47473	15.6485	0.03799	0.13072	2.85250	2.89869	0.12265	1.35681	1.40300	—	3,728.68	3,728.68	0.11444	0.19970	0.05833	3,790.97
% Reduced	—	—	62%	-1%	—	75%	—	14%	74%	—	23%	—	—	—	—	—	—	—
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	1.02857	0.91538	4.81965	6.42128	0.01259	0.13830	0.15752	0.22220	0.12731	0.04214	0.14048	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86
Mit.	0.77864	0.71709	2.83242	7.45838	0.01259	0.06339	0.15752	0.17604	0.05956	0.04214	0.07273	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86

% Reduced	24%	22%	41%	-16%	—	54%	—	21%	53%	—	48%	—	—	—	—	—	—	—
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.18771	0.16706	0.87959	1.17188	0.00230	0.02524	0.02875	0.04055	0.02323	0.00769	0.02564	—	208.706	208.706	0.00818	0.00329	0.01754	209.908
Mit.	0.14210	0.13087	0.51692	1.36116	0.00230	0.01157	0.02875	0.03213	0.01087	0.00769	0.01327	—	208.706	208.706	0.00818	0.00329	0.01754	209.908
% Reduced	24%	22%	41%	-16%	—	54%	—	21%	53%	—	48%	—	—	—	—	—	—	—

2.2. Construction Emissions by Year

2.2.1. Total Construction Emissions by Year, Unmitigated

Includes both onsite and offsite emissions.

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	1.35862	1.23291	9.12109	12.1176	0.02401	0.26092	0.13544	0.36247	0.24019	0.03175	0.26520	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	1.69461	1.42554	14.4585	15.4766	0.03799	0.51580	2.85250	3.36830	0.47453	1.35681	1.83135	—	3,728.68	3,728.68	0.11458	0.19970	0.05833	3,790.97
2029	12.1202	12.0976	9.14121	12.0830	0.02401	0.26100	0.13544	0.36256	0.24019	0.03175	0.26520	—	2,394.20	2,394.20	0.09374	0.03820	0.01185	2,407.93
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.25972	0.21792	1.96542	2.34471	0.00496	0.06467	0.15752	0.22220	0.05960	0.04214	0.10174	—	499.384	499.384	0.01766	0.01528	0.07716	504.455
2029	1.02857	0.91538	4.81965	6.42128	0.01259	0.13830	0.05367	0.19197	0.12731	0.01316	0.14048	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.04740	0.03977	0.35869	0.42791	0.00091	0.01180	0.02875	0.04055	0.01088	0.00769	0.01857	—	82.6788	82.6788	0.00292	0.00253	0.01277	83.5183
2029	0.18771	0.16706	0.87959	1.17188	0.00230	0.02524	0.00979	0.03504	0.02323	0.00240	0.02564	—	208.706	208.706	0.00818	0.00329	0.01754	209.908

2.2.2. Onsite Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	1.27069	1.15509	8.88672	11.6062	0.02312	0.25913	0.00000	0.25913	0.23840	0.00000	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	1.60969	1.35258	12.1706	14.4591	0.02508	0.51580	2.76221	3.27801	0.47453	1.33565	1.81018	—	2,715.59	2,715.59	0.11016	0.02203	0.00000	2,724.91
2029	12.1118	12.0903	8.88672	11.6062	0.02312	0.25913	0.00000	0.25913	0.23840	0.00000	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.24755	0.20699	1.81477	2.22805	0.00411	0.06336	0.12493	0.18828	0.05829	0.03378	0.09206	—	410.478	410.478	0.01665	0.00333	0.00000	411.886
2029	1.00193	0.89225	4.69184	6.16011	0.01213	0.13740	0.00000	0.13740	0.12641	0.00000	0.12641	—	1,157.63	1,157.63	0.04696	0.00939	0.00000	1,161.60
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.04518	0.03778	0.33120	0.40662	0.00075	0.01156	0.02280	0.03436	0.01064	0.00616	0.01680	—	67.9592	67.9592	0.00276	0.00055	0.00000	68.1925
2029	0.18285	0.16283	0.85626	1.12422	0.00221	0.02507	0.00000	0.02507	0.02307	0.00000	0.02307	—	191.659	191.659	0.00777	0.00155	0.00000	192.316

2.2.3. Offsite Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	0.08793	0.07783	0.23438	0.94486	0.00089	0.00178	0.13544	0.13544	0.00178	0.03175	0.03175	—	198.224	198.224	0.00720	0.02009	0.45629	204.784
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.11168	0.09807	2.28798	1.01743	0.01406	0.02091	0.40117	0.42208	0.02091	0.10539	0.12630	—	1,234.15	1,234.15	0.00772	0.17946	0.05833	1,287.89

2029	0.08562	0.07485	0.25449	0.86902	0.00089	0.00187	0.13544	0.13544	0.00178	0.03175	0.03175	—	193.153	193.153	0.00853	0.02034	0.01185	199.337
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.01216	0.01092	0.15065	0.11666	0.00086	0.00132	0.03260	0.03391	0.00132	0.00836	0.00968	—	88.9067	88.9067	0.00101	0.01195	0.07716	92.5688
2029	0.02664	0.02313	0.12781	0.26117	0.00045	0.00091	0.05367	0.05458	0.00091	0.01316	0.01407	—	102.968	102.968	0.00243	0.01047	0.10592	106.256
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.00222	0.00199	0.02749	0.02129	0.00016	0.00024	0.00595	0.00619	0.00024	0.00153	0.00177	—	14.7195	14.7195	0.00017	0.00198	0.01277	15.3258
2029	0.00486	0.00422	0.02333	0.04766	0.00008	0.00017	0.00979	0.00996	0.00017	0.00240	0.00257	—	17.0475	17.0475	0.00040	0.00173	0.01754	17.5918

2.2.4. Total Construction Emissions by Year, Mitigated

Includes both onsite and offsite emissions.

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	1.07326	1.00682	5.37048	14.1318	0.02401	0.11885	0.13544	0.22912	0.11172	0.03175	0.13673	—	2,399.27	2,399.27	0.09398	0.03795	0.45629	2,413.38
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.85050	0.73125	5.47473	15.6485	0.03799	0.13072	2.85250	2.89869	0.12265	1.35681	1.40300	—	3,728.68	3,728.68	0.11444	0.19970	0.05833	3,790.97
2029	12.1202	12.0976	5.39060	14.0972	0.02401	0.11893	0.13544	0.22912	0.11172	0.03175	0.13673	—	2,394.20	2,394.20	0.09374	0.03820	0.01185	2,407.93
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.11688	0.10283	0.81834	2.58485	0.00496	0.01852	0.15752	0.17604	0.01763	0.04214	0.05977	—	499.296	499.296	0.01766	0.01527	0.07716	504.366
2029	0.77864	0.71709	2.83242	7.45838	0.01259	0.06339	0.05367	0.11706	0.05956	0.01316	0.07273	—	1,260.60	1,260.60	0.04939	0.01987	0.10592	1,267.86
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.02133	0.01877	0.14935	0.47173	0.00091	0.00338	0.02875	0.03213	0.00322	0.00769	0.01091	—	82.6641	82.6641	0.00292	0.00253	0.01277	83.5035
2029	0.14210	0.13087	0.51692	1.36116	0.00230	0.01157	0.00979	0.02136	0.01087	0.00240	0.01327	—	208.706	208.706	0.00818	0.00329	0.01754	209.908

2.2.5. Onsite Construction Emissions by Year, Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	0.98533	0.92899	5.13610	13.6204	0.02312	0.11706	0.00000	0.11706	0.10993	0.00000	0.10993	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.80070	0.68598	5.20210	15.0451	0.02505	0.12885	2.76221	2.80839	0.12078	1.33565	1.38183	—	2,711.99	2,711.99	0.11001	0.02200	0.00000	2,721.30
2029	12.1118	12.0903	5.13610	13.6204	0.02312	0.11706	0.00000	0.11706	0.10993	0.00000	0.10993	—	2,201.04	2,201.04	0.08928	0.01786	0.00000	2,208.60
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.10472	0.09191	0.66770	2.46819	0.00411	0.01720	0.12493	0.14213	0.01632	0.03378	0.05009	—	410.389	410.389	0.01665	0.00333	0.00000	411.797
2029	0.75200	0.69396	2.70460	7.19722	0.01213	0.06248	0.00000	0.06248	0.05866	0.00000	0.05866	—	1,157.63	1,157.63	0.04696	0.00939	0.00000	1,161.60
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.01911	0.01677	0.12185	0.45044	0.00075	0.00314	0.02280	0.02594	0.00298	0.00616	0.00914	—	67.9446	67.9446	0.00276	0.00055	0.00000	68.1777
2029	0.13724	0.12665	0.49359	1.31349	0.00221	0.01140	0.00000	0.01140	0.01070	0.00000	0.01070	—	191.659	191.659	0.00777	0.00155	0.00000	192.316

2.2.6. Offsite Construction Emissions by Year, Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2029	0.08793	0.07783	0.23438	0.94486	0.00089	0.00178	0.13544	0.13544	0.00178	0.03175	0.03175	—	198.224	198.224	0.00720	0.02009	0.45629	204.784
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.11168	0.09807	2.28798	1.01743	0.01406	0.02091	0.40117	0.42208	0.02091	0.10539	0.12630	—	1,234.15	1,234.15	0.00772	0.17946	0.05833	1,287.89

2029	0.08562	0.07485	0.25449	0.86902	0.00089	0.00187	0.13544	0.13544	0.00178	0.03175	0.03175	—	193.153	193.153	0.00853	0.02034	0.01185	199.337
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.01216	0.01092	0.15065	0.11666	0.00086	0.00132	0.03260	0.03391	0.00132	0.00836	0.00968	—	88.9067	88.9067	0.00101	0.01195	0.07716	92.5688
2029	0.02664	0.02313	0.12781	0.26117	0.00045	0.00091	0.05367	0.05458	0.00091	0.01316	0.01407	—	102.968	102.968	0.00243	0.01047	0.10592	106.256
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2028	0.00222	0.00199	0.02749	0.02129	0.00016	0.00024	0.00595	0.00619	0.00024	0.00153	0.00177	—	14.7195	14.7195	0.00017	0.00198	0.01277	15.3258
2029	0.00486	0.00422	0.02333	0.04766	0.00008	0.00017	0.00979	0.00996	0.00017	0.00240	0.00257	—	17.0475	17.0475	0.00040	0.00173	0.01754	17.5918

2.3. Operations Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	4.71954	4.21086	4.96395	42.4915	0.08893	0.09556	7.62802	7.72358	0.08969	1.94540	2.03510	19.4454	10,149.1	10,168.5	2.39121	0.37406	24.6180	10,364.4
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	4.48567	3.98224	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	19.4454	9,681.07	9,700.51	2.41999	0.41787	0.69308	9,886.23
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	3.58313	3.19952	4.20445	29.3411	0.06443	0.07187	5.54898	5.62085	0.06754	1.41631	1.48386	19.4454	7,660.25	7,679.70	2.31902	0.31145	8.08428	7,838.57
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.65392	0.58391	0.76731	5.35474	0.01176	0.01312	1.01269	1.02580	0.01233	0.25848	0.27080	3.21941	1,268.24	1,271.46	0.38394	0.05156	1.33844	1,297.76

2.4. Operations Emissions by Sector, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Sector	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Area	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.71954	4.21086	4.96395	42.4915	0.08893	0.09556	7.62802	7.72358	0.08969	1.94540	2.03510	19.4454	10,149.1	10,168.5	2.39121	0.37406	24.6180	10,364.4
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Area	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.48567	3.98224	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	19.4454	9,681.07	9,700.51	2.41999	0.41787	0.69308	9,886.23
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.96050	2.58369	4.20028	28.8456	0.06440	0.07099	5.54898	5.61997	0.06688	1.41631	1.48319	—	6,549.40	6,549.40	0.27430	0.28248	8.02810	6,648.47
Area	0.62262	0.61582	0.00417	0.49546	0.00003	0.00088	—	0.00088	0.00067	—	0.00067	—	2.03738	2.03738	0.00009	0.00002	—	2.04473
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	3.58313	3.19952	4.20445	29.3411	0.06443	0.07187	5.54898	5.62085	0.06754	1.41631	1.48386	19.4454	7,660.25	7,679.70	2.31902	0.31145	8.08428	7,838.57
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Mobile	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Area	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	180.917	180.917	0.01317	0.00160	—	181.722
Water	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808
Waste	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	0.65392	0.58391	0.76731	5.35474	0.01176	0.01312	1.01269	1.02580	0.01233	0.25848	0.27080	3.21941	1,268.24	1,271.46	0.38394	0.05156	1.33844	1,297.76

2.5. Operations Emissions by Sector, Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Sector	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Area	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.71954	4.21086	4.96395	42.4915	0.08893	0.09556	7.62802	7.72358	0.08969	1.94540	2.03510	19.4454	10,149.1	10,168.5	2.39121	0.37406	24.6180	10,364.4
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Area	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076

Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	4.48567	3.98224	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	19.4454	9,681.07	9,700.51	2.41999	0.41787	0.69308	9,886.23
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.96050	2.58369	4.20028	28.8456	0.06440	0.07099	5.54898	5.61997	0.06688	1.41631	1.48319	—	6,549.40	6,549.40	0.27430	0.28248	8.02810	6,648.47
Area	0.62262	0.61582	0.00417	0.49546	0.00003	0.00088	—	0.00088	0.00067	—	0.00067	—	2.03738	2.03738	0.00009	0.00002	—	2.04473
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Water	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Waste	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	3.58313	3.19952	4.20445	29.3411	0.06443	0.07187	5.54898	5.62085	0.06754	1.41631	1.48386	19.4454	7,660.25	7,679.70	2.31902	0.31145	8.08428	7,838.57
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Area	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Energy	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	180.917	180.917	0.01317	0.00160	—	181.722
Water	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808
Waste	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	0.65392	0.58391	0.76731	5.35474	0.01176	0.01312	1.01269	1.02580	0.01233	0.25848	0.27080	3.21941	1,268.24	1,271.46	0.38394	0.05156	1.33844	1,297.76

3. Construction Emissions Details

3.1. Demolition (2028)

3.1.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.58294	1.32747	12.1706	14.4591	0.02393	0.44950	—	0.44950	0.41354	—	0.41354	—	2,494.52	2,494.52	0.10119	0.02024	—	2,503.08
Demolition	—	—	—	—	—	—	1.35820	1.35820	—	0.20567	0.20567	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.08674	0.07274	0.66688	0.79228	0.00131	0.02463	—	0.02463	0.02266	—	0.02266	—	136.686	136.686	0.00554	0.00111	—	137.155
Demolition	—	—	—	—	—	—	0.07442	0.07442	—	0.01127	0.01127	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01583	0.01327	0.12171	0.14459	0.00024	0.00450	—	0.00450	0.00414	—	0.00414	—	22.6299	22.6299	0.00092	0.00018	—	22.7076
Demolition	—	—	—	—	—	—	0.01358	0.01358	—	0.00206	0.00206	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.1.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.07465	0.06893	0.07338	0.78706	0.00000	0.00000	0.11287	0.11287	0.00000	0.02646	0.02646	—	118.201	118.201	0.00738	0.00462	0.01068	119.774
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.03702	0.02914	2.21461	0.23037	0.01406	0.02091	0.28830	0.30921	0.02091	0.07893	0.09984	—	1,115.95	1,115.95	0.00034	0.17484	0.04765	1,168.11
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00403	0.00375	0.00356	0.04206	0.00000	0.00000	0.00594	0.00594	0.00000	0.00139	0.00139	—	6.55810	6.55810	0.00037	0.00025	0.00977	6.65273
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00207	0.00162	0.12047	0.01240	0.00077	0.00115	0.01532	0.01647	0.00115	0.00421	0.00535	—	61.1522	61.1522	0.00002	0.00958	0.04341	64.0509
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00074	0.00068	0.00065	0.00768	0.00000	0.00000	0.00108	0.00108	0.00000	0.00025	0.00025	—	1.08577	1.08577	0.00006	0.00004	0.00162	1.10144
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00038	0.00029	0.02198	0.00226	0.00014	0.00021	0.00280	0.00301	0.00021	0.00077	0.00098	—	10.1244	10.1244	< 0.000005	0.00159	0.00719	10.6044

3.1.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road Equipment	0.40209	0.36904	2.52141	14.6311	0.02393	0.06685	—	0.06685	0.06489	—	0.06489	—	2,494.52	2,494.52	0.10119	0.02024	—	2,503.08
Demolition	—	—	—	—	—	—	1.35820	1.35820	—	0.20567	0.20567	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02203	0.02022	0.13816	0.80170	0.00131	0.00366	—	0.00366	0.00356	—	0.00356	—	136.686	136.686	0.00554	0.00111	—	137.155
Demolition	—	—	—	—	—	—	0.07442	0.07442	—	0.01127	0.01127	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00402	0.00369	0.02521	0.14631	0.00024	0.00067	—	0.00067	0.00065	—	0.00065	—	22.6299	22.6299	0.00092	0.00018	—	22.7076
Demolition	—	—	—	—	—	—	0.01358	0.01358	—	0.00206	0.00206	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.1.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.07465	0.06893	0.07338	0.78706	0.00000	0.00000	0.11287	0.11287	0.00000	0.02646	0.02646	—	118.201	118.201	0.00738	0.00462	0.01068	119.774
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.03702	0.02914	2.21461	0.23037	0.01406	0.02091	0.28830	0.30921	0.02091	0.07893	0.09984	—	1,115.95	1,115.95	0.00034	0.17484	0.04765	1,168.11
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00403	0.00375	0.00356	0.04206	0.00000	0.00000	0.00594	0.00594	0.00000	0.00139	0.00139	—	6.55810	6.55810	0.00037	0.00025	0.00977	6.65273
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00207	0.00162	0.12047	0.01240	0.00077	0.00115	0.01532	0.01647	0.00115	0.00421	0.00535	—	61.1522	61.1522	0.00002	0.00958	0.04341	64.0509
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00074	0.00068	0.00065	0.00768	0.00000	0.00000	0.00108	0.00108	0.00000	0.00025	0.00025	—	1.08577	1.08577	0.00006	0.00004	0.00162	1.10144
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00038	0.00029	0.02198	0.00226	0.00014	0.00021	0.00280	0.00301	0.00021	0.00077	0.00098	—	10.1244	10.1244	< 0.000005	0.00159	0.00719	10.6044

3.2. Site Preparation (2028)

3.2.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24548	1.04655	8.41892	10.7072	0.02508	0.35834	—	0.35834	0.32967	—	0.32967	—	2,715.59	2,715.59	0.11016	0.02203	—	2,724.91

Dust From Material Movement	—	—	—	—	—	—	0.62039	0.62039	—	0.06699	0.06699	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01024	0.00860	0.06920	0.08800	0.00021	0.00295	—	0.00295	0.00271	—	0.00271	—	22.3199	22.3199	0.00091	0.00018	—	22.3965
Dust From Material Movement	—	—	—	—	—	—	0.00510	0.00510	—	0.00055	0.00055	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00187	0.00157	0.01263	0.01606	0.00004	0.00054	—	0.00054	0.00049	—	0.00049	—	3.69532	3.69532	0.00015	0.00003	—	3.70800
Dust From Material Movement	—	—	—	—	—	—	0.00093	0.00093	—	0.00010	0.00010	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.2.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04479	0.04136	0.04403	0.47223	0.00000	0.00000	0.06772	0.06772	0.00000	0.01587	0.01587	—	70.9208	70.9208	0.00443	0.00277	0.00641	71.8647
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00036	0.00034	0.00032	0.00379	0.00000	0.00000	0.00053	0.00053	0.00000	0.00012	0.00012	—	0.59023	0.59023	0.00003	0.00002	0.00088	0.59875
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00007	0.00006	0.00006	0.00069	0.00000	0.00000	0.00010	0.00010	0.00000	0.00002	0.00002	—	0.09772	0.09772	0.00001	< 0.000005	0.00015	0.09913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.2.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.25654	0.25654	1.33402	15.0451	0.02505	0.05131	—	0.05131	0.05131	—	0.05131	—	2,711.99	2,711.99	0.11001	0.02200	—	2,721.30

Dust From Material Movement	—	—	—	—	—	—	0.62039	0.62039	—	0.06699	0.06699	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00211	0.00211	0.01096	0.12366	0.00021	0.00042	—	0.00042	0.00042	—	0.00042	—	22.2904	22.2904	0.00090	0.00018	—	22.3668
Dust From Material Movement	—	—	—	—	—	—	0.00510	0.00510	—	0.00055	0.00055	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00038	0.00038	0.00200	0.02257	0.00004	0.00008	—	0.00008	0.00008	—	0.00008	—	3.69042	3.69042	0.00015	0.00003	—	3.70309
Dust From Material Movement	—	—	—	—	—	—	0.00093	0.00093	—	0.00010	0.00010	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.2.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04479	0.04136	0.04403	0.47223	0.00000	0.00000	0.06772	0.06772	0.00000	0.01587	0.01587	—	70.9208	70.9208	0.00443	0.00277	0.00641	71.8647
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00036	0.00034	0.00032	0.00379	0.00000	0.00000	0.00053	0.00053	0.00000	0.00012	0.00012	—	0.59023	0.59023	0.00003	0.00002	0.00088	0.59875
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00007	0.00006	0.00006	0.00069	0.00000	0.00000	0.00010	0.00010	0.00000	0.00002	0.00002	—	0.09772	0.09772	0.00001	< 0.000005	0.00015	0.09913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3. Grading (2028)

3.3.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.60969	1.35258	11.7838	13.9071	0.02268	0.51580	—	0.51580	0.47453	—	0.47453	—	2,456.26	2,456.26	0.09964	0.01993	—	2,464.69

Dust From Material Movement	—	—	—	—	—	—	2.76221	2.76221	—	1.33565	1.33565	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02646	0.02223	0.19371	0.22861	0.00037	0.00848	—	0.00848	0.00780	—	0.00780	—	40.3769	40.3769	0.00164	0.00033	—	40.5155
Dust From Material Movement	—	—	—	—	—	—	0.04541	0.04541	—	0.02196	0.02196	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00483	0.00406	0.03535	0.04172	0.00007	0.00155	—	0.00155	0.00142	—	0.00142	—	6.68486	6.68486	0.00027	0.00005	—	6.70781
Dust From Material Movement	—	—	—	—	—	—	0.00829	0.00829	—	0.00401	0.00401	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.05972	0.05514	0.05870	0.62964	0.00000	0.00000	0.09030	0.09030	0.00000	0.02117	0.02117	—	94.5610	94.5610	0.00590	0.00370	0.00854	95.8196
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00097	0.00090	0.00085	0.01010	0.00000	0.00000	0.00143	0.00143	0.00000	0.00033	0.00033	—	1.57394	1.57394	0.00009	0.00006	0.00234	1.59666
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00018	0.00016	0.00016	0.00184	0.00000	0.00000	0.00026	0.00026	0.00000	0.00006	0.00006	—	0.26058	0.26058	0.00001	0.00001	0.00039	0.26434
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.23093	0.23093	1.20083	14.2408	0.02264	0.04619	—	0.04619	0.04619	—	0.04619	—	2,452.67	2,452.67	0.09949	0.01990	—	2,461.08
Dust From Material Movement	—	—	—	—	—	—	2.76221	2.76221	—	1.33565	1.33565	—	—	—	—	—	—	—

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00380	0.00380	0.01974	0.23410	0.00037	0.00076	—	0.00076	0.00076	—	0.00076	—	40.3178	40.3178	0.00164	0.00033	—	40.4562
Dust From Material Movement	—	—	—	—	—	—	0.04541	0.04541	—	0.02196	0.02196	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00069	0.00069	0.00360	0.04272	0.00007	0.00014	—	0.00014	0.00014	—	0.00014	—	6.67507	6.67507	0.00027	0.00005	—	6.69798
Dust From Material Movement	—	—	—	—	—	—	0.00829	0.00829	—	0.00401	0.00401	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.3.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.05972	0.05514	0.05870	0.62964	0.00000	0.00000	0.09030	0.09030	0.00000	0.02117	0.02117	—	94.5610	94.5610	0.00590	0.00370	0.00854	95.8196

Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00097	0.00090	0.00085	0.01010	0.00000	0.00000	0.00143	0.00143	0.00000	0.00033	0.00033	—	1.57394	1.57394	0.00009	0.00006	0.00234	1.59666
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00018	0.00016	0.00016	0.00184	0.00000	0.00000	0.00026	0.00026	0.00000	0.00006	0.00006	—	0.26058	0.26058	0.00001	0.00001	0.00039	0.26434
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4. Building Construction (2028)

3.4.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.29438	1.07850	9.22917	11.6712	0.02312	0.28471	—	0.28471	0.26194	—	0.26194	—	2,201.41	2,201.41	0.08930	0.01786	—	2,208.97
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road	0.12412	0.10342	0.88499	1.11915	0.00222	0.02730	—	0.02730	0.02512	—	0.02512	—	211.095	211.095	0.00856	0.00171	—	211.819
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02265	0.01887	0.16151	0.20425	0.00040	0.00498	—	0.00498	0.00458	—	0.00458	—	34.9491	34.9491	0.00142	0.00028	—	35.0691
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04415	0.04076	0.04339	0.46543	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	69.8995	69.8995	0.00436	0.00273	0.00631	70.8298
Vendor	0.00565	0.00451	0.22924	0.05092	0.00089	0.00187	0.03481	0.03668	0.00187	0.00937	0.01124	—	127.691	127.691	0.00106	0.01850	0.00667	133.236
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00417	0.00388	0.00368	0.04353	0.00000	0.00000	0.00615	0.00615	0.00000	0.00144	0.00144	—	6.78685	6.78685	0.00039	0.00026	0.01011	6.88478
Vendor	0.00057	0.00045	0.02176	0.00478	0.00009	0.00017	0.00323	0.00340	0.00017	0.00087	0.00104	—	12.2455	12.2455	0.00011	0.00177	0.01065	12.7850
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00076	0.00071	0.00067	0.00794	0.00000	0.00000	0.00112	0.00112	0.00000	0.00026	0.00026	—	1.12364	1.12364	0.00006	0.00004	0.00167	1.13985
Vendor	0.00010	0.00008	0.00397	0.00087	0.00002	0.00003	0.00059	0.00062	0.00003	0.00016	0.00019	—	2.02737	2.02737	0.00002	0.00029	0.00176	2.11670

Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.80070	0.68598	5.20210	13.6482	0.02312	0.12885	—	0.12885	0.12078	—	0.12078	—	2,201.41	2,201.41	0.08930	0.01786	—	2,208.97
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.07678	0.06578	0.49883	1.30873	0.00222	0.01236	—	0.01236	0.01158	—	0.01158	—	211.095	211.095	0.00856	0.00171	—	211.819
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01401	0.01200	0.09104	0.23884	0.00040	0.00225	—	0.00225	0.00211	—	0.00211	—	34.9491	34.9491	0.00142	0.00028	—	35.0691
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.4.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04415	0.04076	0.04339	0.46543	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	69.8995	69.8995	0.00436	0.00273	0.00631	70.8298
Vendor	0.00565	0.00451	0.22924	0.05092	0.00089	0.00187	0.03481	0.03668	0.00187	0.00937	0.01124	—	127.691	127.691	0.00106	0.01850	0.00667	133.236
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00417	0.00388	0.00368	0.04353	0.00000	0.00000	0.00615	0.00615	0.00000	0.00144	0.00144	—	6.78685	6.78685	0.00039	0.00026	0.01011	6.88478
Vendor	0.00057	0.00045	0.02176	0.00478	0.00009	0.00017	0.00323	0.00340	0.00017	0.00087	0.00104	—	12.2455	12.2455	0.00011	0.00177	0.01065	12.7850
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00076	0.00071	0.00067	0.00794	0.00000	0.00000	0.00112	0.00112	0.00000	0.00026	0.00026	—	1.12364	1.12364	0.00006	0.00004	0.00167	1.13985
Vendor	0.00010	0.00008	0.00397	0.00087	0.00002	0.00003	0.00059	0.00062	0.00003	0.00016	0.00019	—	2.02737	2.02737	0.00002	0.00029	0.00176	2.11670
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5. Building Construction (2029)

3.5.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road Equipment	1.24858	1.04039	8.88672	11.6062	0.02312	0.25913	—	0.25913	0.23840	—	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24858	1.04039	8.88672	11.6062	0.02312	0.25913	—	0.25913	0.23840	—	0.23840	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.63528	0.52936	4.52162	5.90532	0.01176	0.13185	—	0.13185	0.12130	—	0.12130	—	1,119.90	1,119.90	0.04543	0.00909	—	1,123.75
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.11594	0.09661	0.82520	1.07772	0.00215	0.02406	—	0.02406	0.02214	—	0.02214	—	185.413	185.413	0.00752	0.00150	—	186.049
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04333	0.03835	0.02845	0.46563	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	73.7827	73.7827	0.00355	0.00257	0.22486	74.8626
Vendor	0.00582	0.00468	0.20592	0.04577	0.00089	0.00178	0.03481	0.03659	0.00178	0.00937	0.01115	—	124.441	124.441	0.00114	0.01752	0.23073	129.922
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04219	0.03689	0.03874	0.42825	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	68.7193	68.7193	0.00420	0.00273	0.00584	69.6450
Vendor	0.00565	0.00443	0.21576	0.04855	0.00089	0.00187	0.03481	0.03668	0.00178	0.00937	0.01115	—	124.433	124.433	0.00025	0.01761	0.00598	129.692
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02122	0.01860	0.01718	0.21192	0.00000	0.00000	0.03262	0.03262	0.00000	0.00762	0.00762	—	35.4036	35.4036	0.00205	0.00139	0.04940	35.9190
Vendor	0.00288	0.00230	0.10857	0.02381	0.00045	0.00091	0.01714	0.01804	0.00091	0.00462	0.00553	—	63.3146	63.3146	0.00013	0.00892	0.05059	66.0251
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00387	0.00339	0.00313	0.03868	0.00000	0.00000	0.00595	0.00595	0.00000	0.00139	0.00139	—	5.86148	5.86148	0.00034	0.00023	0.00818	5.94681
Vendor	0.00052	0.00042	0.01981	0.00435	0.00008	0.00017	0.00313	0.00329	0.00017	0.00084	0.00101	—	10.4825	10.4825	0.00002	0.00148	0.00838	10.9312
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.77273	0.66287	5.13610	13.6204	0.02312	0.11706	—	0.11706	0.10993	—	0.10993	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.77273	0.66287	5.13610	13.6204	0.02312	0.11706	—	0.11706	0.10993	—	0.10993	—	2,201.04	2,201.04	0.08928	0.01786	—	2,208.60
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.39317	0.33727	2.61328	6.93014	0.01176	0.05956	—	0.05956	0.05593	—	0.05593	—	1,119.90	1,119.90	0.04543	0.00909	—	1,123.75
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.07175	0.06155	0.47692	1.26475	0.00215	0.01087	—	0.01087	0.01021	—	0.01021	—	185.413	185.413	0.00752	0.00150	—	186.049
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.5.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04333	0.03835	0.02845	0.46563	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	73.7827	73.7827	0.00355	0.00257	0.22486	74.8626
Vendor	0.00582	0.00468	0.20592	0.04577	0.00089	0.00178	0.03481	0.03659	0.00178	0.00937	0.01115	—	124.441	124.441	0.00114	0.01752	0.23073	129.922

Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04219	0.03689	0.03874	0.42825	0.00000	0.00000	0.06675	0.06675	0.00000	0.01565	0.01565	—	68.7193	68.7193	0.00420	0.00273	0.00584	69.6450
Vendor	0.00565	0.00443	0.21576	0.04855	0.00089	0.00187	0.03481	0.03668	0.00178	0.00937	0.01115	—	124.433	124.433	0.00025	0.01761	0.00598	129.692
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02122	0.01860	0.01718	0.21192	0.00000	0.00000	0.03262	0.03262	0.00000	0.00762	0.00762	—	35.4036	35.4036	0.00205	0.00139	0.04940	35.9190
Vendor	0.00288	0.00230	0.10857	0.02381	0.00045	0.00091	0.01714	0.01804	0.00091	0.00462	0.00553	—	63.3146	63.3146	0.00013	0.00892	0.05059	66.0251
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00387	0.00339	0.00313	0.03868	0.00000	0.00000	0.00595	0.00595	0.00000	0.00139	0.00139	—	5.86148	5.86148	0.00034	0.00023	0.00818	5.94681
Vendor	0.00052	0.00042	0.01981	0.00435	0.00008	0.00017	0.00313	0.00329	0.00017	0.00084	0.00101	—	10.4825	10.4825	0.00002	0.00148	0.00838	10.9312
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6. Paving (2029)

3.6.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.71805	0.60245	5.41905	8.18783	0.01181	0.18968	—	0.18968	0.17450	—	0.17450	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.71805	0.60245	5.41905	8.18783	0.01181	0.18968	—	0.18968	0.17450	—	0.17450	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01967	0.01651	0.14847	0.22432	0.00032	0.00520	—	0.00520	0.00478	—	0.00478	—	34.0659	34.0659	0.00138	0.00028	—	34.1828
Paving	0.01514	0.01514	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00359	0.00301	0.02710	0.04094	0.00006	0.00095	—	0.00095	0.00087	—	0.00087	—	5.64000	5.64000	0.00023	0.00005	—	5.65936
Paving	0.00276	0.00276	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Worker	0.08793	0.07783	0.05773	0.94486	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	149.721	149.721	0.00720	0.00522	0.45629	151.913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.08562	0.07485	0.07861	0.86902	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	139.447	139.447	0.00853	0.00555	0.01185	141.325
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00232	0.00203	0.00188	0.02316	0.00000	0.00000	0.00356	0.00356	0.00000	0.00083	0.00083	—	3.86840	3.86840	0.00022	0.00015	0.00540	3.92472
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00042	0.00037	0.00034	0.00423	0.00000	0.00000	0.00065	0.00065	0.00000	0.00015	0.00015	—	0.64046	0.64046	0.00004	0.00003	0.00089	0.64978
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.43269	0.37635	2.53909	8.63613	0.01181	0.09368	—	0.09368	0.08756	—	0.08756	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.43269	0.37635	2.53909	8.63613	0.01181	0.09368	—	0.09368	0.08756	—	0.08756	—	1,243.41	1,243.41	0.05044	0.01009	—	1,247.67
Paving	0.55264	0.55264	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01185	0.01031	0.06956	0.23661	0.00032	0.00257	—	0.00257	0.00240	—	0.00240	—	34.0659	34.0659	0.00138	0.00028	—	34.1828
Paving	0.01514	0.01514	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00216	0.00188	0.01270	0.04318	0.00006	0.00047	—	0.00047	0.00044	—	0.00044	—	5.64000	5.64000	0.00023	0.00005	—	5.65936
Paving	0.00276	0.00276	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.6.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.08793	0.07783	0.05773	0.94486	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	149.721	149.721	0.00720	0.00522	0.45629	151.913
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.08562	0.07485	0.07861	0.86902	0.00000	0.00000	0.13544	0.13544	0.00000	0.03175	0.03175	—	139.447	139.447	0.00853	0.00555	0.01185	141.325
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00232	0.00203	0.00188	0.02316	0.00000	0.00000	0.00356	0.00356	0.00000	0.00083	0.00083	—	3.86840	3.86840	0.00022	0.00015	0.00540	3.92472
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00042	0.00037	0.00034	0.00423	0.00000	0.00000	0.00065	0.00065	0.00000	0.00015	0.00015	—	0.64046	0.64046	0.00004	0.00003	0.00089	0.64978
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7. Architectural Coating (2029)

3.7.1. Onsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.12385	0.10236	0.79416	1.11216	0.00173	0.01284	—	0.01284	0.01181	—	0.01181	—	133.510	133.510	0.00542	0.00108	—	133.968
Architectural Coatings	11.9879	11.9879	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00339	0.00280	0.02176	0.03047	0.00005	0.00035	—	0.00035	0.00032	—	0.00032	—	3.65780	3.65780	0.00015	0.00003	—	3.67035
Architectural Coatings	0.32844	0.32844	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00062	0.00051	0.00397	0.00556	0.00001	0.00006	—	0.00006	0.00006	—	0.00006	—	0.60559	0.60559	0.00002	< 0.000005	—	0.60767
Architectural Coatings	0.05994	0.05994	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7.2. Offsite - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00844	0.00738	0.00775	0.08565	0.00000	0.00000	0.01335	0.01335	0.00000	0.00313	0.00313	—	13.7439	13.7439	0.00084	0.00055	0.00117	13.9290
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00023	0.00020	0.00018	0.00228	0.00000	0.00000	0.00035	0.00035	0.00000	0.00008	0.00008	—	0.38127	0.38127	0.00002	0.00001	0.00053	0.38682
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00004	0.00004	0.00003	0.00042	0.00000	0.00000	0.00006	0.00006	0.00000	0.00001	0.00001	—	0.06312	0.06312	< 0.000005	< 0.000005	0.00009	0.06404
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7.3. Onsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.12385	0.10236	0.79416	1.11216	0.00173	0.01284	—	0.01284	0.01181	—	0.01181	—	133.510	133.510	0.00542	0.00108	—	133.968
Architectural Coatings	11.9879	11.9879	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00339	0.00280	0.02176	0.03047	0.00005	0.00035	—	0.00035	0.00032	—	0.00032	—	3.65780	3.65780	0.00015	0.00003	—	3.67035
Architectural Coatings	0.32844	0.32844	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.00062	0.00051	0.00397	0.00556	0.00001	0.00006	—	0.00006	0.00006	—	0.00006	—	0.60559	0.60559	0.00002	< 0.000005	—	0.60767
Architectural Coatings	0.05994	0.05994	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

3.7.4. Offsite - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00844	0.00738	0.00775	0.08565	0.00000	0.00000	0.01335	0.01335	0.00000	0.00313	0.00313	—	13.7439	13.7439	0.00084	0.00055	0.00117	13.9290
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00023	0.00020	0.00018	0.00228	0.00000	0.00000	0.00035	0.00035	0.00000	0.00008	0.00008	—	0.38127	0.38127	0.00002	0.00001	0.00053	0.38682
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.00004	0.00004	0.00003	0.00042	0.00000	0.00000	0.00006	0.00006	0.00000	0.00001	0.00001	—	0.06312	0.06312	< 0.000005	< 0.000005	0.00009	0.06404
Vendor	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Hauling	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

4. Operations Emissions Details

4.1. Mobile Emissions by Land Use

4.1.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73

4.1.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	4.00625	3.51136	4.95550	41.4868	0.08887	0.09377	7.62802	7.72179	0.08834	1.94540	2.03375	—	9,036.16	9,036.16	0.34641	0.34508	24.5618	9,172.21
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	3.95126	3.44783	5.85860	38.8217	0.08428	0.09379	7.62802	7.72181	0.08836	1.94540	2.03377	—	8,572.26	8,572.26	0.37536	0.38892	0.63690	8,698.17
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total	0.54029	0.47152	0.76655	5.26432	0.01175	0.01296	1.01269	1.02564	0.01221	0.25848	0.27068	—	1,084.33	1,084.33	0.04541	0.04677	1.32914	1,100.73

4.2. Energy

4.2.1. Electricity Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	164.371	164.371	0.01197	0.00145	—	165.103
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	16.5462	16.5462	0.00120	0.00015	—	16.6198
Total	—	—	—	—	—	—	—	—	—	—	—	—	180.917	180.917	0.01317	0.00160	—	181.722

4.2.2. Electricity Emissions By Land Use - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	992.810	992.810	0.07229	0.00876	—	997.229
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	99.9398	99.9398	0.00728	0.00088	—	100.385
Total	—	—	—	—	—	—	—	—	—	—	—	—	1,092.75	1,092.75	0.07957	0.00964	—	1,097.61
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	164.371	164.371	0.01197	0.00145	—	165.103
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	16.5462	16.5462	0.00120	0.00015	—	16.6198
Total	—	—	—	—	—	—	—	—	—	—	—	—	180.917	180.917	0.01317	0.00160	—	181.722

4.2.3. Natural Gas Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

4.2.4. Natural Gas Emissions By Land Use - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000	0.00000	—	0.00000	—	0.00000	0.00000	0.00000	0.00000	—	0.00000

4.3. Area Emissions by Source

4.3.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Source	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Landscape Equipm	0.17888	0.16509	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Total	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.09154	0.09154	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.00599	0.00599	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscape Equipment	0.01610	0.01486	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Total	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853

4.3.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Source	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscape Equipment	0.17888	0.16509	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Total	0.71329	0.69950	0.00845	1.00468	0.00006	0.00178	—	0.00178	0.00135	—	0.00135	—	4.13136	4.13136	0.00017	0.00004	—	4.14625
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.50157	0.50157	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.03284	0.03284	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	0.53441	0.53441	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Consumer Products	0.09154	0.09154	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architectural Coatings	0.00599	0.00599	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Landscape	0.01610	0.01486	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853
Total	0.11363	0.11239	0.00076	0.09042	0.00001	0.00016	—	0.00016	0.00012	—	0.00012	—	0.33731	0.33731	0.00001	< 0.000005	—	0.33853

4.4. Water Emissions by Land Use

4.4.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808

Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808

4.4.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	7.86739	16.0608	23.9282	0.80788	0.01931	—	49.8793
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.30254	2.65905	3.96158	0.13375	0.00320	—	8.25808

4.5. Waste Emissions by Land Use

4.5.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649

4.5.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	11.5780	0.00000	11.5780	1.15718	0.00000	—	40.5076
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00000	0.00000	0.00000	0.00000	0.00000	—	0.00000
Total	—	—	—	—	—	—	—	—	—	—	—	1.91687	0.00000	1.91687	0.19158	0.00000	—	6.70649

4.6. Refrigerant Emissions by Land Use

4.6.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930

4.6.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.05618	0.05618
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
General Office Building	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00930	0.00930

4.7. Offroad Emissions By Equipment Type

4.7.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.7.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipm Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.8. Stationary Emissions By Equipment Type

4.8.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.8.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.9. User Defined Emissions By Equipment Type

4.9.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.9.2. Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10. Soil Carbon Accumulation By Vegetation Type

4.10.1. Soil Carbon Accumulation By Vegetation Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Vegetation	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.2. Above and Belowground Carbon Accumulation by Land Use Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.3. Avoided and Sequestered Emissions by Species - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Species	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.4. Soil Carbon Accumulation By Vegetation Type - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Vegetation	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.5. Above and Belowground Carbon Accumulation by Land Use Type - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

4.10.6. Avoided and Sequestered Emissions by Species - Mitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Species	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

5. Activity Data

5.1. Construction Schedule

Phase Name	Phase Type	Start Date	End Date	Days Per Week	Work Days per Phase	Phase Description
Demolition	Demolition	10/1/2028	10/29/2028	5.00000	20.0000	—
Site Preparation	Site Preparation	10/30/2028	11/3/2028	5.00000	3.00000	—
Grading	Grading	11/4/2028	11/12/2028	5.00000	6.00000	—
Building Construction	Building Construction	11/13/2028	9/17/2029	5.00000	220.000	—
Paving	Paving	9/18/2029	10/2/2029	5.00000	10.00000	—
Architectural Coating	Architectural Coating	10/3/2029	10/17/2029	5.00000	10.00000	—

5.2. Off-Road Equipment

5.2.1. Unmitigated

Phase Name	Equipment Type	Fuel Type	Engine Tier	Number per Day	Hours Per Day	Horsepower	Load Factor
Demolition	Concrete/Industrial Saws	Diesel	Average	1.000000	8.00000	33.0000	0.73000
Demolition	Rubber Tired Dozers	Diesel	Average	1.000000	8.00000	367.000	0.40000
Demolition	Tractors/Loaders/Backhoes	Diesel	Average	3.00000	8.00000	84.0000	0.37000
Site Preparation	Graders	Diesel	Average	1.000000	8.00000	148.000	0.41000
Site Preparation	Scrapers	Diesel	Average	1.000000	8.00000	423.000	0.48000
Site Preparation	Tractors/Loaders/Backhoes	Diesel	Average	1.000000	7.00000	84.0000	0.37000
Grading	Graders	Diesel	Average	1.000000	8.00000	148.000	0.41000
Grading	Rubber Tired Dozers	Diesel	Average	1.000000	8.00000	367.000	0.40000
Grading	Tractors/Loaders/Backhoes	Diesel	Average	2.00000	7.00000	84.0000	0.37000
Building Construction	Cranes	Diesel	Average	1.000000	8.00000	367.000	0.29000
Building Construction	Forklifts	Diesel	Average	2.00000	7.00000	82.0000	0.20000
Building Construction	Generator Sets	Diesel	Average	1.000000	8.00000	14.0000	0.74000

Building Construction	Tractors/Loaders/Back	Diesel	Average	1.000000	6.00000	84.0000	0.37000
Building Construction	Welders	Diesel	Average	3.00000	8.00000	46.0000	0.45000
Paving	Cement and Mortar Mixers	Diesel	Average	1.000000	8.00000	10.00000	0.56000
Paving	Pavers	Diesel	Average	1.000000	8.00000	81.0000	0.42000
Paving	Paving Equipment	Diesel	Average	1.000000	8.00000	89.0000	0.36000
Paving	Rollers	Diesel	Average	2.00000	8.00000	36.0000	0.38000
Paving	Tractors/Loaders/Backhoes	Diesel	Average	1.000000	8.00000	84.0000	0.37000
Architectural Coating	Air Compressors	Diesel	Average	1.000000	6.00000	37.0000	0.48000

5.2.2. Mitigated

Phase Name	Equipment Type	Fuel Type	Engine Tier	Number per Day	Hours Per Day	Horsepower	Load Factor
Demolition	Concrete/Industrial Saws	Diesel	Average	1.000000	8.00000	33.0000	0.73000
Demolition	Rubber Tired Dozers	Diesel	Tier 4 Final	1.000000	8.00000	367.000	0.40000
Demolition	Tractors/Loaders/Backhoes	Diesel	Tier 4 Final	3.00000	8.00000	84.0000	0.37000
Site Preparation	Graders	Diesel	Tier 4 Final	1.000000	8.00000	148.000	0.41000
Site Preparation	Scrapers	Diesel	Tier 4 Final	1.000000	8.00000	423.000	0.48000
Site Preparation	Tractors/Loaders/Backhoes	Diesel	Tier 4 Final	1.000000	7.00000	84.0000	0.37000
Grading	Graders	Diesel	Tier 4 Final	1.000000	8.00000	148.000	0.41000
Grading	Rubber Tired Dozers	Diesel	Tier 4 Final	1.000000	8.00000	367.000	0.40000
Grading	Tractors/Loaders/Backhoes	Diesel	Tier 4 Final	2.00000	7.00000	84.0000	0.37000
Building Construction	Cranes	Diesel	Tier 4 Final	1.000000	8.00000	367.000	0.29000
Building Construction	Forklifts	Diesel	Tier 4 Final	2.00000	7.00000	82.0000	0.20000
Building Construction	Generator Sets	Diesel	Average	1.000000	8.00000	14.0000	0.74000
Building Construction	Tractors/Loaders/Backhoes	Diesel	Tier 4 Final	1.000000	6.00000	84.0000	0.37000

Building Construction	Welders	Diesel	Average	3.00000	8.00000	46.0000	0.45000
Paving	Cement and Mortar Mixers	Diesel	Average	1.000000	8.00000	10.00000	0.56000
Paving	Pavers	Diesel	Tier 4 Final	1.000000	8.00000	81.0000	0.42000
Paving	Paving Equipment	Diesel	Tier 4 Final	1.000000	8.00000	89.0000	0.36000
Paving	Rollers	Diesel	Average	2.00000	8.00000	36.0000	0.38000
Paving	Tractors/Loaders/Backhoes	Diesel	Tier 4 Final	1.000000	8.00000	84.0000	0.37000
Architectural Coating	Air Compressors	Diesel	Average	1.000000	6.00000	37.0000	0.48000

5.3. Construction Vehicles

5.3.1. Unmitigated

Phase Name	Trip Type	One-Way Trips per Day	Miles per Trip	Vehicle Mix
Demolition	Worker	12.5000	12.7800	LDA,LDT1,LDT2
Demolition	Vendor	—	10.6800	HHDT,MHDT
Demolition	Hauling	15.5500	20.0000	HHDT
Demolition	Onsite truck	—	—	HHDT
Site Preparation	Worker	7.50000	12.7800	LDA,LDT1,LDT2
Site Preparation	Vendor	—	10.6800	HHDT,MHDT
Site Preparation	Hauling	0.00000	20.0000	HHDT
Site Preparation	Onsite truck	—	—	HHDT
Grading	Worker	10.00000	12.7800	LDA,LDT1,LDT2
Grading	Vendor	—	10.6800	HHDT,MHDT
Grading	Hauling	0.00000	20.0000	HHDT
Grading	Onsite truck	—	—	HHDT
Building Construction	Worker	7.39200	12.7800	LDA,LDT1,LDT2
Building Construction	Vendor	3.78609	10.6800	HHDT,MHDT
Building Construction	Hauling	0.00000	20.0000	HHDT

Building Construction	Onsite truck	—	—	HHDT
Paving	Worker	15.0000	12.7800	LDA,LDT1,LDT2
Paving	Vendor	—	10.6800	HHDT,MHDT
Paving	Hauling	0.00000	20.0000	HHDT
Paving	Onsite truck	—	—	HHDT
Architectural Coating	Worker	1.47840	12.7800	LDA,LDT1,LDT2
Architectural Coating	Vendor	—	10.6800	HHDT,MHDT
Architectural Coating	Hauling	0.00000	20.0000	HHDT
Architectural Coating	Onsite truck	—	—	HHDT

5.3.2. Mitigated

Phase Name	Trip Type	One-Way Trips per Day	Miles per Trip	Vehicle Mix
Demolition	Worker	12.5000	12.7800	LDA,LDT1,LDT2
Demolition	Vendor	—	10.6800	HHDT,MHDT
Demolition	Hauling	15.5500	20.0000	HHDT
Demolition	Onsite truck	—	—	HHDT
Site Preparation	Worker	7.50000	12.7800	LDA,LDT1,LDT2
Site Preparation	Vendor	—	10.6800	HHDT,MHDT
Site Preparation	Hauling	0.00000	20.0000	HHDT
Site Preparation	Onsite truck	—	—	HHDT
Grading	Worker	10.00000	12.7800	LDA,LDT1,LDT2
Grading	Vendor	—	10.6800	HHDT,MHDT
Grading	Hauling	0.00000	20.0000	HHDT
Grading	Onsite truck	—	—	HHDT
Building Construction	Worker	7.39200	12.7800	LDA,LDT1,LDT2
Building Construction	Vendor	3.78609	10.6800	HHDT,MHDT
Building Construction	Hauling	0.00000	20.0000	HHDT
Building Construction	Onsite truck	—	—	HHDT

Paving	Worker	15.0000	12.7800	LDA,LDT1,LDT2
Paving	Vendor	—	10.6800	HHDT,MHDT
Paving	Hauling	0.00000	20.0000	HHDT
Paving	Onsite truck	—	—	HHDT
Architectural Coating	Worker	1.47840	12.7800	LDA,LDT1,LDT2
Architectural Coating	Vendor	—	10.6800	HHDT,MHDT
Architectural Coating	Hauling	0.00000	20.0000	HHDT
Architectural Coating	Onsite truck	—	—	HHDT

5.4. Vehicles

5.4.1. Construction Vehicle Control Strategies

Non-applicable. No control strategies activated by user.

5.5. Architectural Coatings

Phase Name	Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)
Architectural Coating	0.00000	0.00000	34,650.0	11,550.0	5,512.90

5.6. Dust Mitigation

5.6.1. Construction Earthmoving Activities

Phase Name	Material Imported (Ton of Debris)	Material Exported (Ton of Debris)	Acres Graded (acres)	Material Demolished (Building Square Footage)	Acres Paved (acres)
Demolition	0.00000	0.00000	0.00000	27,000.0	0.00000
Site Preparation	0.00000	0.00000	4.50000	0.00000	0.00000
Grading	0.00000	0.00000	6.00000	0.00000	0.00000
Paving	0.00000	0.00000	0.00000	0.00000	2.10931

5.6.2. Construction Earthmoving Control Strategies

Control Strategies Applied	Frequency (per day)	PM10 Reduction	PM2.5 Reduction
Water Exposed Area	2	61%	61%

5.7. Construction Paving

Phase Name	Land Use	Area Paved (acres)	% Asphalt
Paving	General Office Building	0.00000	0%
Paving	Parking Lot	2.10931	100%

5.8. Construction Electricity Consumption and Emissions Factors

kWh per Year and Emission Factor (lb/MWh)

Year	kWh per Year	CO2	CH4	N2O
2028	0.00000	453.209	0.03300	0.00400
2029	0.00000	453.209	0.03300	0.00400

5.9. Operational Mobile Sources

5.9.1. Unmitigated

Land Use Type	Trips/Weekday	Trips/Saturday	Trips/Sunday	Trips/Year	VMT/Weekday	VMT/Saturday	VMT/Sunday	VMT/Year
General Office Building	435.950	98.9169	31.3311	120,450	10,643.2	2,414.94	764.914	2,940,651
Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

5.9.2. Mitigated

Land Use Type	Trips/Weekday	Trips/Saturday	Trips/Sunday	Trips/Year	VMT/Weekday	VMT/Saturday	VMT/Sunday	VMT/Year
General Office Building	435.950	98.9169	31.3311	120,450	10,643.2	2,414.94	764.914	2,940,651

Parking Lot	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

5.10. Operational Area Sources

5.10.1. Hearths

Land Use	Hearth Type	Unmitigated (number)	Mitigated (number)
General Office Building	Wood Fireplaces	0	0
General Office Building	Gas Fireplaces	0	0
General Office Building	Propane Fireplaces	0	0
General Office Building	Electric Fireplaces	0	0
General Office Building	No Fireplaces	0	0
General Office Building	Conventional Wood Stoves	0	0
General Office Building	Catalytic Wood Stoves	0	0
General Office Building	Non-Catalytic Wood Stoves	0	0
General Office Building	Pellet Wood Stoves	0	0
Parking Lot	Wood Fireplaces	0	0
Parking Lot	Gas Fireplaces	0	0
Parking Lot	Propane Fireplaces	0	0
Parking Lot	Electric Fireplaces	0	0
Parking Lot	No Fireplaces	0	0
Parking Lot	Conventional Wood Stoves	0	0
Parking Lot	Catalytic Wood Stoves	0	0
Parking Lot	Non-Catalytic Wood Stoves	0	0
Parking Lot	Pellet Wood Stoves	0	0

5.10.2. Architectural Coatings

Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)

0.00000	0.00000	34,650.0	11,550.0	5,512.90

5.10.3. Landscape Equipment

Season	Unit	Value
Snow Days	day/yr	0.00000
Summer Days	day/yr	180.000

5.10.4. Landscape Equipment - Mitigated

Season	Unit	Value
Snow Days	day/yr	0.00000
Summer Days	day/yr	180.000

5.11. Operational Energy Consumption

5.11.1. Unmitigated

Electricity (kWh/yr) and CO2 and CH4 and N2O and Natural Gas (kBTU/yr)

Land Use	Electricity (kWh/yr)	CO2	CH4	N2O	Natural Gas (kBTU/yr)
General Office Building	799,577	453.209	0.0330	0.0040	0.00000
Parking Lot	80,488.3	453.209	0.0330	0.0040	0.00000

5.11.2. Mitigated

Electricity (kWh/yr) and CO2 and CH4 and N2O and Natural Gas (kBTU/yr)

Land Use	Electricity (kWh/yr)	CO2	CH4	N2O	Natural Gas (kBTU/yr)
General Office Building	799,577	453.209	0.0330	0.0040	0.00000
Parking Lot	80,488.3	453.209	0.0330	0.0040	0.00000

5.12. Operational Water and Wastewater Consumption

5.12.1. Unmitigated

Land Use	Indoor Water (gal/year)	Outdoor Water (gal/year)
General Office Building	4,105,650	47,553.0
Parking Lot	0.00000	0.00000

5.12.2. Mitigated

Land Use	Indoor Water (gal/year)	Outdoor Water (gal/year)
General Office Building	4,105,650	47,553.0
Parking Lot	0.00000	0.00000

5.13. Operational Waste Generation

5.13.1. Unmitigated

Land Use	Waste (ton/year)	Cogeneration (kWh/year)
General Office Building	21.4830	0.00000
Parking Lot	0.00000	0.00000

5.13.2. Mitigated

Land Use	Waste (ton/year)	Cogeneration (kWh/year)
General Office Building	21.4830	0.00000
Parking Lot	0.00000	0.00000

5.14. Operational Refrigeration and Air Conditioning Equipment

5.14.1. Unmitigated

Land Use	Equipment Type	Refrigerant	GWP	Quantity (kg)	Operations Leak Rate	Service Leak Rate	Times Serviced

General Office Building	Household refrigerators and/or freezers	R-134a	1,430.00	0.01679	0.60000	0.00000	1.000000
General Office Building	Other commercial A/C and heat pumps	R-410A	2,088.00	0.00180	4.00000	4.00000	18.0000

5.14.2. Mitigated

Land Use	Equipment Type	Refrigerant	GWP	Quantity (kg)	Operations Leak Rate	Service Leak Rate	Times Serviced
General Office Building	Household refrigerators and/or freezers	R-134a	1,430.00	0.01679	0.60000	0.00000	1.000000
General Office Building	Other commercial A/C and heat pumps	R-410A	2,088.00	0.00180	4.00000	4.00000	18.0000

5.15. Operational Off-Road Equipment

5.15.1. Unmitigated

5.15.2. Mitigated

5.16. Stationary Sources

5.16.1. Emergency Generators and Fire Pumps

5.16.2. Process Boilers

5.17. User Defined

5.18. Vegetation

5.18.1. Land Use Change

5.18.1.1. Unmitigated

Vegetation Land Use Type	Vegetation Soil Type	Initial Acres	Final Acres

5.18.1.2. Mitigated

Vegetation Land Use Type	Vegetation Soil Type	Initial Acres	Final Acres

5.18.1. Biomass Cover Type

5.18.1.1. Unmitigated

Biomass Cover Type	Initial Acres	Final Acres

5.18.1.2. Mitigated

Biomass Cover Type	Initial Acres	Final Acres

5.18.2. Sequestration

5.18.2.1. Unmitigated

Tree Type	Number	Electricity Saved (kWh/year)	Natural Gas Saved (btu/year)

5.18.2.2. Mitigated

Tree Type	Number	Electricity Saved (kWh/year)	Natural Gas Saved (btu/year)

6. Climate Risk Detailed Report

6.1. Climate Risk Summary

Cal-Adapt midcentury 2040–2059 average projections for four hazards are reported below for your project location. These are under Representation Concentration Pathway (RCP) 8.5 which assumes GHG emissions will continue to rise strongly through 2050 and then plateau around 2100.

Climate Hazard	Result for Project Location	Unit

Temperature and Extreme Heat	25.8300	annual days of extreme heat
Extreme Precipitation	14.2000	annual days with precipitation above 20 mm
Sea Level Rise	—	meters of inundation depth
Wildfire	58.0900	annual hectares burned

Temperature and Extreme Heat data are for grid cell in which your project are located. The projection is based on the 98th historical percentile of daily maximum/minimum temperatures from observed historical data (32 climate model ensemble from Cal-Adapt, 2040–2059 average under RCP 8.5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.
Extreme Precipitation data are for the grid cell in which your project are located. The threshold of 20 mm is equivalent to about ¾ an inch of rain, which would be light to moderate rainfall if received over a full day or heavy rain if received over a period of 2 to 4 hours. Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.
Sea Level Rise data are for the grid cell in which your project are located. The projections are from Radke et al. (2017), as reported in Cal-Adapt (Radke et al., 2017, CEC-500-2017-008), and consider inundation location and depth for the San Francisco Bay, the Sacramento-San Joaquin River Delta and California coast resulting different increments of sea level rise coupled with extreme storm events. Users may select from four scenarios to view the range in potential inundation depth for the grid cell. The four scenarios are: No rise, 0.5 meter, 1.0 meter, 1.41 meters
Wildfire data are for the grid cell in which your project are located. The projections are from UC Davis, as reported in Cal-Adapt (2040–2059 average under RCP 8.5), and consider historical data of climate, vegetation, population density, and large (> 400 ha) fire history. Users may select from four model simulations to view the range in potential wildfire probabilities for the grid cell. The four simulations make different assumptions about expected rainfall and temperature are: Warmer/drier (HadGEM2-ES), Cooler/wetter (CNRM-CM5), Average conditions (CanESM2), Range of different rainfall and temperature possibilities (MIROC5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.

6.2. Initial Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score
Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	2	0	0	N/A
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	1	0	0	N/A
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	0	0	0	N/A
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.
The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.
The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores do not include implementation of climate risk reduction measures.

6.3. Adjusted Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score
Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	2	1	1	3
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	1	1	1	2
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	1	1	1	2
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.
The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.
The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores include implementation of climate risk reduction measures.

6.4. Climate Risk Reduction Measures

7. Health and Equity Details

7.1. CalEnviroScreen 4.0 Scores

The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.

Indicator	Result for Project Census Tract
Exposure Indicators	—
AQ-Ozone	72.5451
AQ-PM	40.0124
AQ-DPM	3.97013
Drinking Water	8.77982
Lead Risk Housing	47.6497
Pesticides	28.7586
Toxic Releases	3.37584

Traffic	6.03750
Effect Indicators	—
CleanUp Sites	0.00000
Groundwater	63.3737
Haz Waste Facilities/Generators	50.1390
Impaired Water Bodies	12.4528
Solid Waste	88.9347
Sensitive Population	—
Asthma	58.4247
Cardio-vascular	65.3166
Low Birth Weights	16.7693
Socioeconomic Factor Indicators	—
Education	28.0815
Housing	31.7364
Linguistic	12.2750
Poverty	51.0930
Unemployment	17.1135

7.2. Healthy Places Index Scores

The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

Indicator	Result for Project Census Tract
Economic	—
Above Poverty	40.54921083
Employed	20.45425382
Median HI	34.74913384
Education	—
Bachelor's or higher	37.46952393
High school enrollment	100

Preschool enrollment	9.713845759
Transportation	—
Auto Access	27.83267035
Active commuting	68.45887335
Social	—
2-parent households	32.0544078
Voting	70.19119723
Neighborhood	—
Alcohol availability	62.49197998
Park access	29.33401771
Retail density	10.97138458
Supermarket access	62.94110099
Tree canopy	96.09906326
Housing	—
Homeownership	65.75131528
Housing habitability	72.97574747
Low-inc homeowner severe housing cost burden	24.72731939
Low-inc renter severe housing cost burden	70.92262287
Uncrowded housing	84.29359682
Health Outcomes	—
Insured adults	79.19928141
Arthritis	0.0
Asthma ER Admissions	40.0
High Blood Pressure	0.0
Cancer (excluding skin)	0.0
Asthma	0.0
Coronary Heart Disease	0.0
Chronic Obstructive Pulmonary Disease	0.0

Diagnosed Diabetes	0.0
Life Expectancy at Birth	39.1
Cognitively Disabled	0.5
Physically Disabled	1.3
Heart Attack ER Admissions	29.4
Mental Health Not Good	0.0
Chronic Kidney Disease	0.0
Obesity	0.0
Pedestrian Injuries	48.7
Physical Health Not Good	0.0
Stroke	0.0
Health Risk Behaviors	—
Binge Drinking	0.0
Current Smoker	0.0
No Leisure Time for Physical Activity	0.0
Climate Change Exposures	—
Wildfire Risk	49.2
SLR Inundation Area	0.0
Children	72.4
Elderly	8.9
English Speaking	92.4
Foreign-born	1.1
Outdoor Workers	24.1
Climate Change Adaptive Capacity	—
Impervious Surface Cover	90.5
Traffic Density	10.7
Traffic Access	0.0
Other Indices	—

Hardship	52.4
Other Decision Support	—
2016 Voting	76.8

7.3. Overall Health & Equity Scores

Metric	Result for Project Census Tract
CalEnviroScreen 4.0 Score for Project Location (a)	26.0000
Healthy Places Index Score for Project Location (b)	43.0000
Project Located in a Designated Disadvantaged Community (Senate Bill 535)	No
Project Located in a Low-Income Community (Assembly Bill 1550)	No
Project Located in a Community Air Protection Program Community (Assembly Bill 617)	No

a: The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.
b: The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

7.4. Health & Equity Measures

No Health & Equity Measures selected.

7.5. Evaluation Scorecard

Health & Equity Evaluation Scorecard not completed.

7.6. Health & Equity Custom Measures

No Health & Equity Custom Measures created.

8. User Changes to Default Data

8.1. Justifications

Screen	Justification
Land Use	Updated land use lot acreage and landscape square footage based on project specific details
Construction: Architectural Coatings	Updated VOC content to 50 g/L per NSAQMD Rule 230.

Operations: Vehicle Data	Updated Government Office Building vehicle trip rates and trip lengths consistent with the Quincy Courthouse Transportation Analysis Draft Memo prepared by Fehr and Peers 11/14/25.
Operations: Architectural Coatings	Updated VOC content to 50 g/L per NSAQMD Rule 230.
Operations: Energy Use	Updated total annual consumption for Government Office Building land use based on all-electric building design.

8.3. Land Use

Model Parameter	Units	Default Value	New Value
Lot Area	acre	0.53030	0.75069
Landscape Area	sq. ft	—	5,000.00
Lot Area	acre	1.08000	2.10931
Landscape Area	sq. ft	—	0.00000

8.4. Construction

8.4.8. Architectural Coatings

Phase Name	Model Parameter	Units	Default Value	New Value
Architectural Coating	Residential Interior VOC	g/L	250.000	50.0000
Architectural Coating	Non-Residential Interior VOC	g/L	250.000	50.0000
Architectural Coating	Residential Exterior VOC	g/L	250.000	50.0000
Architectural Coating	Non-Residential Exterior VOC	g/L	250.000	50.0000
Architectural Coating	VOC for Parking Paint	g/L	250.000	50.0000

8.5. Operations

8.5.1. Mobile Sources

8.5.1.1. Vehicle Data

Land Use	Model Parameter	Units	Default Value	New Value

General Office Building	Weekday Trip Rate	size/day	9.74000	18.8723
General Office Building	Saturday Trip Rate	size/day	2.21000	4.28212
General Office Building	Sunday Trip Rate	size/day	0.70000	1.35633
General Office Building	Non-Res H-W Trip Length	miles	13.4405	28.2403
General Office Building	Non-Res W-O Trip Length	miles	11.3555	23.8594
General Office Building	Non-Res O-O Trip Length	miles	11.0835	23.2879

8.5.2. Area Sources

8.5.2.3. Architectural Coatings

Model Parameter	Units	Default Value	New Value
Residential Interior VOC	g/L	250.000	50.0000
Non-Residential Interior VOC	g/L	250.000	50.0000
Residential Exterior VOC	g/L	250.000	50.0000
Non-Residential Exterior VOC	g/L	250.000	50.0000
VOC for Parking Paint	g/L	250.000	50.0000

8.5.3. Energy Usage

Land Use	Model Parameter	Units	Default Value	New Value
General Office Building	Electricity	kWh/yr	535,217	799,577
General Office Building	Electricity (Subject to Title 24)	kWh/yr	369,153	600,257
General Office Building	Electricity (Not Subject to Title 24)	kWh/yr	166,064	199,320
General Office Building	Natural Gas	kBTU/yr	901,997	0.00000
General Office Building	Natural Gas (Subject to Title 24)	kBTU/yr	788,529	0.00000
General Office Building	Natural Gas (Not Subject to Title 24)	kBTU/yr	113,469	0.00000

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** AERMOD Input Produced by:
** AERMOD View Ver. 12.0.0
** Lakes Environmental Software Inc.
** Date: 12/16/2025
** File: C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208
\Quincy_Courthouse_Construction_Unmit_20251208.ADI
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**
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** AERMOD Control Pathway
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   AVERTIME PERIOD
   URBANOPT 22000 Plumas_County
   POLLUTID PM_2.5
   RUNORNOT RUN
   ERRORFIL Quincy_Courthouse_Construction_Unmit_20251208.err
CO FINISHED
**
**************************************
** AERMOD Source Pathway
**************************************
**
**
SO STARTING
** Source Location **
** Source ID - Type - X Coord. - Y Coord. **
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1042.440
** DESCRSRC Y1_Onsite
** ------------------------------------------------------------------
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** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN1
** DESCRSRC Y1_Lawrence_Central
** PREFIX
** Length of Side = 10.00
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 5.8183E-11
** Nodes = 4
```

```
** 676049.325, 4422856.804, 1040.14, 4.12
** 676017.666, 4422849.839, 1040.55, 4.12
** 675980.169, 4422849.410, 1040.79, 4.12
** 675182.135, 4422849.719, 1042.62, 4.12
** ----------------------------------------------------------------
-------
   LOCATION A0000001     AREA     676048.251 4422861.687 1040.05
   LOCATION A0000002     AREA     676017.609 4422854.838 1040.35
   LOCATION A0000003     AREA     675980.171 4422854.410 1040.62
   LOCATION A0000004     AREA     675880.417 4422854.449 1041.60
   LOCATION A0000005     AREA     675780.663 4422854.487 1042.30
   LOCATION A0000006     AREA     675680.909 4422854.526 1042.43
   LOCATION A0000007     AREA     675581.154 4422854.565 1043.23
   LOCATION A0000008     AREA     675481.400 4422854.603 1043.98
   LOCATION A0000023     AREA     675381.646 4422854.642 1044.38
   LOCATION A0000024     AREA     675281.892 4422854.681 1043.45
** End of LINE AREA Source ID = ARLN1
** ----------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN2
** DESCRSRC Y1_Main_Central
** PREFIX
** Length of Side = 10.50
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 2.7749E-11
** Nodes = 13
** 675180.533, 4422843.703, 1042.61, 4.12
** 675203.836, 4422815.981, 1043.03, 4.12
** 675244.447, 4422757.080, 1045.06, 4.12
** 675257.312, 4422748.986, 1045.42, 4.12
** 675278.417, 4422748.263, 1045.56, 4.12
** 675481.643, 4422753.197, 1046.58, 4.12
** 675639.972, 4422753.040, 1045.64, 4.12
** 675832.221, 4422750.683, 1043.81, 4.12
** 675853.502, 4422751.890, 1043.55, 4.12
** 675879.475, 4422757.980, 1043.45, 4.12
** 675990.143, 4422815.958, 1040.82, 4.12
** 676030.094, 4422834.512, 1040.42, 4.12
** 676056.065, 4422847.179, 1040.17, 4.12
** ----------------------------------------------------------------
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   LOCATION A0000009     AREA     675176.514 4422840.324 1042.54
   LOCATION A0000010     AREA     675199.514 4422813.000 1043.14
   LOCATION A0000011     AREA     675241.651 4422752.637 1045.18
   LOCATION A0000012     AREA     675257.133 4422743.739 1045.57
   LOCATION A0000013     AREA     675278.544 4422743.014 1045.68
   LOCATION A0000014     AREA     675380.157 4422745.482 1046.74
   LOCATION A0000015     AREA     675481.638 4422747.947 1046.79
   LOCATION A0000016     AREA     675560.802 4422747.869 1046.45
   LOCATION A0000017     AREA     675639.907 4422747.791 1045.99
```

```
   LOCATION A0000018     AREA     675736.032 4422746.612 1045.10
   LOCATION A0000019     AREA     675832.518 4422745.441 1044.07
   LOCATION A0000020     AREA     675854.701 4422746.779 1043.72
   LOCATION A0000021     AREA     675881.911 4422753.329 1043.34
   LOCATION A0000022     AREA     675937.245 4422782.319 1042.04
   LOCATION A0000025     AREA     675992.354 4422811.197 1040.85
   LOCATION A0000026     AREA     676032.396 4422829.794 1040.35
** End of LINE AREA Source ID = ARLN2
   LOCATION PAREA2       AREAPOLY   675645.170  4422859.920
1042.440
** DESCRSRC Y2_Onsite
** ----------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN3
** DESCRSRC Y2_Lawrence_Central
** PREFIX
** Length of Side = 10.00
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 4.0671E-11
** Nodes = 4
** 676049.320, 4422856.800, 1040.14, 4.12
** 676017.670, 4422849.840, 1040.55, 4.12
** 675980.170, 4422849.410, 1040.79, 4.12
** 675182.140, 4422849.720, 1042.62, 4.12
** ----------------------------------------------------------------
-------
   LOCATION A0000027     AREA     676048.246 4422861.683 1040.05
   LOCATION A0000028     AREA     676017.613 4422854.840 1040.35
   LOCATION A0000029     AREA     675980.172 4422854.410 1040.62
   LOCATION A0000030     AREA     675880.418 4422854.449 1041.60
   LOCATION A0000031     AREA     675780.664 4422854.487 1042.30
   LOCATION A0000032     AREA     675680.911 4422854.526 1042.43
   LOCATION A0000033     AREA     675581.157 4422854.565 1043.23
   LOCATION A0000034     AREA     675481.403 4422854.604 1043.98
   LOCATION A0000035     AREA     675381.649 4422854.642 1044.38
   LOCATION A0000036     AREA     675281.896 4422854.681 1043.45
** End of LINE AREA Source ID = ARLN3
** ----------------------------------------------------------------
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** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN4
** DESCRSRC Y2_Main_Central
** PREFIX
** Length of Side = 10.50
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 1.9374E-11
** Nodes = 13
** 675180.530, 4422843.700, 1042.61, 4.12
** 675203.840, 4422815.980, 1043.03, 4.12
```

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** 675244.450, 4422757.080, 1045.06, 4.12
** 675257.310, 4422748.990, 1045.42, 4.12
** 675278.420, 4422748.260, 1045.56, 4.12
** 675481.640, 4422753.200, 1046.58, 4.12
** 675639.970, 4422753.040, 1045.64, 4.12
** 675832.220, 4422750.680, 1043.81, 4.12
** 675853.500, 4422751.890, 1043.55, 4.12
** 675879.480, 4422757.980, 1043.45, 4.12
** 675990.140, 4422815.960, 1040.82, 4.12
** 676030.090, 4422834.510, 1040.42, 4.12
** 676056.060, 4422847.180, 1040.17, 4.12
** ------------------------------------------------------------
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   LOCATION A0000037     AREA     675176.512 4422840.321 1042.54
   LOCATION A0000038     AREA     675199.518 4422813.000 1043.14
   LOCATION A0000039     AREA     675241.654 4422752.636 1045.18
   LOCATION A0000040     AREA     675257.129 4422743.743 1045.57
   LOCATION A0000041     AREA     675278.548 4422743.012 1045.68
   LOCATION A0000042     AREA     675380.158 4422745.482 1046.74
   LOCATION A0000043     AREA     675481.635 4422747.950 1046.79
   LOCATION A0000044     AREA     675560.800 4422747.870 1046.45
   LOCATION A0000045     AREA     675639.906 4422747.790 1045.99
   LOCATION A0000046     AREA     675736.031 4422746.610 1045.10
   LOCATION A0000047     AREA     675832.518 4422745.438 1044.08
   LOCATION A0000048     AREA     675854.698 4422746.779 1043.72
   LOCATION A0000049     AREA     675881.917 4422753.330 1043.34
   LOCATION A0000050     AREA     675937.247 4422782.320 1042.04
   LOCATION A0000051     AREA     675992.351 4422811.198 1040.85
   LOCATION A0000052     AREA     676032.392 4422829.792 1040.35
** End of LINE AREA Source ID = ARLN4
** Source Parameters **
   SRCPARAM PAREA1         7.9E-08     5.000         7
   AREAVERT PAREA1       675645.171 4422859.916 675645.741
4422952.467
   AREAVERT PAREA1       675604.204 4422951.815 675683.614
4423024.566
   AREAVERT PAREA1       675705.612 4423024.794 675711.995
4422973.145
   AREAVERT PAREA1       675711.099 4422858.744
** LINE AREA Source ID = ARLN1
   SRCPARAM A0000001     5.8183E-11     4.120    32.416    10.000
167.593
   SRCPARAM A0000002     5.8183E-11     4.120    37.499    10.000
179.345
   SRCPARAM A0000003     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000004     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000005     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000006     5.8183E-11     4.120    99.754
10.000  -179.978
```

```
   SRCPARAM A0000007     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000008     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000023     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000024     5.8183E-11     4.120    99.754
10.000  -179.978
** ------------------------------------------------------------
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** LINE AREA Source ID = ARLN2
   SRCPARAM A0000009     2.7749E-11     4.120    36.215    10.500
49.950
   SRCPARAM A0000010     2.7749E-11     4.120    71.544    10.500
55.414
   SRCPARAM A0000011     2.7749E-11     4.120    15.200    10.500
32.179
   SRCPARAM A0000012     2.7749E-11     4.120    21.117    10.500
1.961
   SRCPARAM A0000013     2.7749E-11     4.120   101.643
10.500    -1.391
   SRCPARAM A0000014     2.7749E-11     4.120   101.643
10.500    -1.391
   SRCPARAM A0000015     2.7749E-11     4.120    79.164    10.500
0.057
   SRCPARAM A0000016     2.7749E-11     4.120    79.164    10.500
0.057
   SRCPARAM A0000017     2.7749E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000018     2.7749E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000019     2.7749E-11     4.120    21.316
10.500    -3.247
   SRCPARAM A0000020     2.7749E-11     4.120    26.677
10.500   -13.196
   SRCPARAM A0000021     2.7749E-11     4.120    62.468
10.500   -27.650
   SRCPARAM A0000022     2.7749E-11     4.120    62.468
10.500   -27.650
   SRCPARAM A0000025     2.7749E-11     4.120    44.050
10.500   -24.911
   SRCPARAM A0000026     2.7749E-11     4.120    28.894
10.500   -25.999
** ------------------------------------------------------------
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   SRCPARAM PAREA2        1.71E-07     5.000         7
   AREAVERT PAREA2       675645.170 4422859.920 675645.740
4422952.470
   AREAVERT PAREA2       675604.200 4422951.820 675683.610
4423024.570
   AREAVERT PAREA2       675705.610 4423024.790 675711.990
4422973.150
```

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   AREAVERT PAREA2       675711.100 4422858.740
** LINE AREA Source ID = ARLN3
   SRCPARAM A0000027     4.0671E-11     4.120    32.406    10.000
167.598
   SRCPARAM A0000028     4.0671E-11     4.120    37.502    10.000
179.343
   SRCPARAM A0000029     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000030     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000031     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000032     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000033     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000034     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000035     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000036     4.0671E-11     4.120    99.754
10.000  -179.978
** ------------------------------------------------------------
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** LINE AREA Source ID = ARLN4
   SRCPARAM A0000037     1.9374E-11     4.120    36.218    10.500
49.939
   SRCPARAM A0000038     1.9374E-11     4.120    71.543    10.500
55.415
   SRCPARAM A0000039     1.9374E-11     4.120    15.193    10.500
32.173
   SRCPARAM A0000040     1.9374E-11     4.120    21.123    10.500
1.981
   SRCPARAM A0000041     1.9374E-11     4.120   101.640
10.500    -1.393
   SRCPARAM A0000042     1.9374E-11     4.120   101.640
10.500    -1.393
   SRCPARAM A0000043     1.9374E-11     4.120    79.165    10.500
0.058
   SRCPARAM A0000044     1.9374E-11     4.120    79.165    10.500
0.058
   SRCPARAM A0000045     1.9374E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000046     1.9374E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000047     1.9374E-11     4.120    21.314
10.500    -3.254
   SRCPARAM A0000048     1.9374E-11     4.120    26.684
10.500   -13.193
   SRCPARAM A0000049     1.9374E-11     4.120    62.465
10.500   -27.652
   SRCPARAM A0000050     1.9374E-11     4.120    62.465
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10.500   -27.652
   SRCPARAM A0000051     1.9374E-11     4.120    44.047
10.500   -24.907
   SRCPARAM A0000052     1.9374E-11     4.120    28.896
10.500   -26.006
** ------------------------------------------------------------
-------
   URBANSRC ALL

** Variable Emissions Type: "By Hour / Seven Days (HRDOW7)"
** Variable Emission Scenario: "ALL"
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
```

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EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000012     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000014     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000014     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000016     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000012     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000012     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000014     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000014     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000015     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000015     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000016     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000030     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000035     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000028     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000029     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000029     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000031     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000031     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000033     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000034     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000034     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000035     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000031     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000031     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000035     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000035     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000035     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000036     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000036     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000036     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000031     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000035     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000042     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000040     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000041     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000046     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000047     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000050     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000052     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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A0000005
   SRCGROUP Y1_ALL   A0000006 A0000007 A0000008 A0000023 A0000024
A0000009
   SRCGROUP Y1_ALL   A0000010 A0000011 A0000012 A0000013 A0000014
A0000015
   SRCGROUP Y1_ALL   A0000016 A0000017 A0000018 A0000019 A0000020
A0000021
   SRCGROUP Y1_ALL   A0000022 A0000025 A0000026
   SRCGROUP Y1_ON    PAREA1
   SRCGROUP Y1_OFF   A0000001 A0000002 A0000003 A0000004 A0000005
A0000006
   SRCGROUP Y1_OFF   A0000007 A0000008 A0000023 A0000024 A0000009
A0000010
   SRCGROUP Y1_OFF   A0000011 A0000012 A0000013 A0000014 A0000015
A0000016
   SRCGROUP Y1_OFF   A0000017 A0000018 A0000019 A0000020 A0000021
A0000022
   SRCGROUP Y1_OFF   A0000025 A0000026
   SRCGROUP Y2_ALL   PAREA2 A0000027 A0000028 A0000029 A0000030
A0000031
   SRCGROUP Y2_ALL   A0000032 A0000033 A0000034 A0000035 A0000036
A0000037
   SRCGROUP Y2_ALL   A0000038 A0000039 A0000040 A0000041 A0000042
A0000043
   SRCGROUP Y2_ALL   A0000044 A0000045 A0000046 A0000047 A0000048
A0000049
   SRCGROUP Y2_ALL   A0000050 A0000051 A0000052
   SRCGROUP Y2_ON    PAREA2
   SRCGROUP Y2_OFF   A0000027 A0000028 A0000029 A0000030 A0000031
A0000032
   SRCGROUP Y2_OFF   A0000033 A0000034 A0000035 A0000036 A0000037
A0000038
   SRCGROUP Y2_OFF   A0000039 A0000040 A0000041 A0000042 A0000043
A0000044
   SRCGROUP Y2_OFF   A0000045 A0000046 A0000047 A0000048 A0000049
A0000050
   SRCGROUP Y2_OFF   A0000051 A0000052
SO FINISHED
**
**************************************
** AERMOD Receptor Pathway
**************************************
**
**
RE STARTING
   INCLUDED Quincy_Courthouse_Construction_Unmit_20251208.rou
RE FINISHED
**
**************************************
** AERMOD Meteorology Pathway
```

```
**************************************
**
**
ME STARTING
   SURFFILE "Z:\Shared\San Jose\Env\16230_13 New Quincy
Courthouse EIR\Project Data\ACES\MET\KBLU_725845_23225\KBLU_
725845_23225\KBLU_2014-2016_2018_2019_ADJU.SFC"
   PROFFILE "Z:\Shared\San Jose\Env\16230_13 New Quincy
Courthouse EIR\Project Data\ACES\MET\KBLU_725845_23225\KBLU_
725845_23225\KBLU_2014-2016_2018_2019_ADJU.PFL"
   SURFDATA 23225 2014 Blue_Canyon_NYACK_Airport
   UAIRDATA 23230 2014 OAKLAND/WSO_AP
   PROFBASE 1608.1 METERS
ME FINISHED
**
**************************************
** AERMOD Output Pathway
**************************************
**
**
OU STARTING
** Auto-Generated Plotfiles
   PLOTFILE PERIOD Y1_ALL Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G001.PLT 31
   PLOTFILE PERIOD Y1_ON Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G002.PLT 32
   PLOTFILE PERIOD Y1_OFF Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G003.PLT 33
   PLOTFILE PERIOD Y2_ALL Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G004.PLT 34
   PLOTFILE PERIOD Y2_ON Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G005.PLT 35
   PLOTFILE PERIOD Y2_OFF Quincy_Courthouse_Construction_Unmit_
20251208.AD\PE00G006.PLT 36
   SUMMFILE Quincy_Courthouse_Construction_Unmit_20251208.sum
OU FINISHED


  *** Message Summary For AERMOD Model Setup ***

  --------- Summary of Total Messages --------

 A Total of            0 Fatal Error Message(s)
 A Total of            2 Warning Message(s)
 A Total of            0 Informational Message(s)


    ******** FATAL ERROR MESSAGES ********
               ***  NONE  ***


    ********   WARNING MESSAGES   ********
```

```
 ME W186    1427       MEOPEN: THRESH_1MIN 1-min ASOS wind speed
threshold used           0.50
 ME W187    1427       MEOPEN: ADJ_U* Option for Stable Low Winds
used in AERMET

 ***********************************
 *** SETUP Finishes Successfully ***
 ***********************************
```

```
 *** AERMOD - VERSION 23132  ***   *** C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208\Q ***
12/16/25
 *** AERMET - VERSION  19191 ***   ***
***        07:50:23

PAGE   1
 *** MODELOPTs:    RegDFAULT  CONC  ELEV  URBAN  ADJ_U*

                                              ***     MODEL SETUP
OPTIONS SUMMARY       ***
 - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -
- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

 ** Model Options Selected:
      * Model Uses Regulatory DEFAULT Options
      * Model Is Setup For Calculation of Average CONCentration
Values.
      * NO GAS DEPOSITION Data Provided.
      * NO PARTICLE DEPOSITION Data Provided.
      * Model Uses NO DRY DEPLETION. DDPLETE  =  F
      * Model Uses NO WET DEPLETION. WETDPLT  =  F
      * Stack-tip Downwash.
      * Model Accounts for ELEVated Terrain Effects.
      * Use Calms Processing Routine.
      * Use Missing Data Processing Routine.
      * No Exponential Decay.
      * Model Uses URBAN Dispersion Algorithm for the SBL for
54 Source(s),
        for Total of    1 Urban Area(s):
   Urban Population =     22000.0 ;  Urban Roughness Length =
1.000 m
      * Urban Roughness Length of 1.0 Meter Used.
      * ADJ_U*   - Use ADJ_U* option for SBL in AERMET
      * CCVR_Sub - Meteorological data includes CCVR
substitutions
      * TEMP_Sub - Meteorological data includes TEMP
substitutions
      * Model Assumes No FLAGPOLE Receptor Heights.
      * The User Specified a Pollutant Type of: PM_2.5

 **Model Calculates PERIOD Averages Only

 **This Run Includes:     54 Source(s);       6 Source Group(s);
and     265 Receptor(s)

                with:      0 POINT(s), including
                           0 POINTCAP(s) and      0 POINTHOR(s)
                 and:      0 VOLUME source(s)
                 and:     54 AREA type source(s)
                 and:      0 LINE source(s)
                 and:      0 RLINE/RLINEXT source(s)
```

```
                and:      0 OPENPIT source(s)
                and:      0 BUOYANT LINE source(s) with a total
of     0 line(s)
                and:      0 SWPOINT source(s)


 **Model Set To Continue RUNning After the Setup Testing.

 **The AERMET Input Meteorological Data Version Date:  19191

 **Output Options Selected:
         Model Outputs Tables of PERIOD Averages by Receptor
         Model Outputs External File(s) of High Values for
Plotting (PLOTFILE Keyword)
         Model Outputs Separate Summary File of High Ranked
Values (SUMMFILE Keyword)

 **NOTE:  The Following Flags May Appear Following CONC Values:
c for Calm Hours

m for Missing Hours

b for Both Calm and Missing Hours

 **Misc. Inputs:  Base Elev. for Pot. Temp. Profile (m MSL) =
1608.10 ;  Decay Coef. =    0.000     ;  Rot. Angle =     0.0
                 Emission Units =
GRAMS/SEC                                ;  Emission Rate Unit
Factor =   0.10000E+07
                 Output Units   = MICROGRAMS/M**3

 **Approximate Storage Requirements of Model =      3.7 MB of
RAM.

 **Input Runstream File:          aermod.inp
 **Output Print File:             aermod.out

 **Detailed Error/Message File:
Quincy_Courthouse_Construction_Unmit_20251208.err
 **File for Summary of Results:
Quincy_Courthouse_Construction_Unmit_20251208.sum
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** AREA SOURCE DATA ***

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (GRAMS/SEC /METER**2)	COORD (SW CORNER) X (METERS)	Y (METERS)	BASE ELEV. (METERS)	RELEASE HEIGHT (METERS)	X-DIM OF AREA (METERS)	Y-DIM OF AREA (METERS)	ORIENT. OF AREA (DEG.)	INIT. SZ (METERS)	URBAN SOURCE	EMISSION RATE SCALAR BY	AIRCRAFT VARY
A0000001	0	0.58183E-10	676048.3	4422861.7	1040.0	4.12	32.42	10.00	167.59	0.00	YES	HRDOW7	NO
A0000002	0	0.58183E-10	676017.6	4422854.8	1040.3	4.12	37.50	10.00	179.34	0.00	YES	HRDOW7	NO
A0000003	0	0.58183E-10	675980.2	4422854.4	1040.6	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000004	0	0.58183E-10	675880.4	4422854.4	1041.6	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000005	0	0.58183E-10	675780.7	4422854.5	1042.3	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000006	0	0.58183E-10	675680.9	4422854.5	1042.4	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000007	0	0.58183E-10	675581.2	4422854.6	1043.2	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000008	0	0.58183E-10	675481.4	4422854.6	1044.0	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000023	0	0.58183E-10	675381.6	4422854.6	1044.4	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO

```
 A0000024         0   0.58183E-10  675281.9 4422854.7  1043.5
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000009         0   0.27749E-10  675176.5 4422840.3  1042.5
4.12     36.22     10.50     49.95     0.00     YES   HRDOW7
NO
 A0000010         0   0.27749E-10  675199.5 4422813.0  1043.1
4.12     71.54     10.50     55.41     0.00     YES   HRDOW7
NO
 A0000011         0   0.27749E-10  675241.7 4422752.6  1045.2
4.12     15.20     10.50     32.18     0.00     YES   HRDOW7
NO
 A0000012         0   0.27749E-10  675257.1 4422743.7  1045.6
4.12     21.12     10.50      1.96     0.00     YES   HRDOW7
NO
 A0000013         0   0.27749E-10  675278.5 4422743.0  1045.7
4.12    101.64     10.50     -1.39     0.00     YES   HRDOW7
NO
 A0000014         0   0.27749E-10  675380.2 4422745.5  1046.7
4.12    101.64     10.50     -1.39     0.00     YES   HRDOW7
NO
 A0000015         0   0.27749E-10  675481.6 4422747.9  1046.8
4.12     79.16     10.50      0.06     0.00     YES   HRDOW7
NO
 A0000016         0   0.27749E-10  675560.8 4422747.9  1046.5
4.12     79.16     10.50      0.06     0.00     YES   HRDOW7
NO
 A0000017         0   0.27749E-10  675639.9 4422747.8  1046.0
4.12     96.13     10.50      0.70     0.00     YES   HRDOW7
NO
 A0000018         0   0.27749E-10  675736.0 4422746.6  1045.1
4.12     96.13     10.50      0.70     0.00     YES   HRDOW7
NO
 A0000019         0   0.27749E-10  675832.5 4422745.4  1044.1
4.12     21.32     10.50     -3.25     0.00     YES   HRDOW7
NO
 A0000020         0   0.27749E-10  675854.7 4422746.8  1043.7
4.12     26.68     10.50    -13.20     0.00     YES   HRDOW7
NO
 A0000021         0   0.27749E-10  675881.9 4422753.3  1043.3
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000022         0   0.27749E-10  675937.2 4422782.3  1042.0
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000025         0   0.27749E-10  675992.4 4422811.2  1040.8
4.12     44.05     10.50    -24.91     0.00     YES   HRDOW7
NO
 A0000026         0   0.27749E-10  676032.4 4422829.8  1040.3
4.12     28.89     10.50    -26.00     0.00     YES   HRDOW7
NO
 A0000027         0   0.40671E-10  676048.2 4422861.7  1040.0
```

```
4.12     32.41     10.00    167.60     0.00     YES   HRDOW7
NO
 A0000028         0   0.40671E-10  676017.6 4422854.8  1040.3
4.12     37.50     10.00    179.34     0.00     YES   HRDOW7
NO
 A0000029         0   0.40671E-10  675980.2 4422854.4  1040.6
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000030         0   0.40671E-10  675880.4 4422854.4  1041.6
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000031         0   0.40671E-10  675780.7 4422854.5  1042.3
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000032         0   0.40671E-10  675680.9 4422854.5  1042.4
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000033         0   0.40671E-10  675581.2 4422854.6  1043.2
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000034         0   0.40671E-10  675481.4 4422854.6  1044.0
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000035         0   0.40671E-10  675381.6 4422854.6  1044.4
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000036         0   0.40671E-10  675281.9 4422854.7  1043.5
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000037         0   0.19374E-10  675176.5 4422840.3  1042.5
4.12     36.22     10.50     49.94     0.00     YES   HRDOW7
NO
 A0000038         0   0.19374E-10  675199.5 4422813.0  1043.1
4.12     71.54     10.50     55.41     0.00     YES   HRDOW7
NO
 A0000039         0   0.19374E-10  675241.7 4422752.6  1045.2
4.12     15.19     10.50     32.17     0.00     YES   HRDOW7
NO
 A0000040         0   0.19374E-10  675257.1 4422743.7  1045.6
4.12     21.12     10.50      1.98     0.00     YES   HRDOW7
NO
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** AREA SOURCE DATA ***

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (GRAMS/SEC /METER**2)	COORD (SW CORNER) X (METERS)	Y (METERS)	BASE ELEV. (METERS)	RELEASE HEIGHT (METERS)	X-DIM OF AREA (METERS)	Y-DIM OF AREA (METERS)	ORIENT. OF AREA (DEG.)	INIT. SZ (METERS)	URBAN SOURCE	EMISSION RATE SCALAR VARY BY	AIRCRAFT
A0000041	0	0.19374E-10	675278.5	4422743.0	1045.7	4.12	101.64	10.50	-1.39	0.00	YES	HRDOW7	NO
A0000042	0	0.19374E-10	675380.2	4422745.5	1046.7	4.12	101.64	10.50	-1.39	0.00	YES	HRDOW7	NO
A0000043	0	0.19374E-10	675481.6	4422748.0	1046.8	4.12	79.16	10.50	0.06	0.00	YES	HRDOW7	NO
A0000044	0	0.19374E-10	675560.8	4422747.9	1046.5	4.12	79.16	10.50	0.06	0.00	YES	HRDOW7	NO
A0000045	0	0.19374E-10	675639.9	4422747.8	1046.0	4.12	96.13	10.50	0.70	0.00	YES	HRDOW7	NO
A0000046	0	0.19374E-10	675736.0	4422746.6	1045.1	4.12	96.13	10.50	0.70	0.00	YES	HRDOW7	NO
A0000047	0	0.19374E-10	675832.5	4422745.4	1044.1	4.12	21.31	10.50	-3.25	0.00	YES	HRDOW7	NO
A0000048	0	0.19374E-10	675854.7	4422746.8	1043.7	4.12	26.68	10.50	-13.19	0.00	YES	HRDOW7	NO
A0000049	0	0.19374E-10	675881.9	4422753.3	1043.3	4.12	62.47	10.50	-27.65	0.00	YES	HRDOW7	NO

```
 A0000050          0   0.19374E-10  675937.2 4422782.3  1042.0
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000051          0   0.19374E-10  675992.4 4422811.2  1040.8
4.12     44.05     10.50    -24.91     0.00     YES   HRDOW7
NO
 A0000052          0   0.19374E-10  676032.4 4422829.8  1040.3
4.12     28.90     10.50    -26.01     0.00     YES   HRDOW7
NO
```

*** AREAPOLY SOURCE DATA ***

RELEASE HEIGHT (METERS)	NUMBER OF VERTS.	EMISSION RATE INIT. SZ (METERS)	URBAN SOURCE	LOCATION OF AREA EMISSION RATE X (METERS)	Y (METERS)	BASE ELEV. (METERS)	AIRCRAFT SCALAR VARY BY
PAREA1 5.00	7	0 0.00	YES	0.79000E-07 675645.2	4422859.9	1042.4	NO HRDOW7
PAREA2 5.00	7	0 0.00	YES	0.17100E-06 675645.2	4422859.9	1042.4	NO HRDOW7

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** SOURCE IDs DEFINING SOURCE GROUPS ***

SRCGROUP ID	SOURCE IDs
Y1_ALL	PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 ,
	A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 ,
	A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 ,
	A0000022 , A0000025 , A0000026 ,
Y1_ON	PAREA1 ,
Y1_OFF	A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 , A0000008 ,
	A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 , A0000014 ,
	A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 , A0000022 ,
	A0000025 , A0000026 ,
Y2_ALL	PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 , A0000031 , A0000032 , A0000033 ,

```
             A0000034    , A0000035    , A0000036    ,
A0000037    , A0000038    , A0000039    , A0000040    ,
A0000041    ,

             A0000042    , A0000043    , A0000044    ,
A0000045    , A0000046    , A0000047    , A0000048    ,
A0000049    ,

             A0000050    , A0000051    , A0000052    ,

  Y2_ON      PAREA2      ,

  Y2_OFF     A0000027    , A0000028    , A0000029    ,
A0000030    , A0000031    , A0000032    , A0000033    ,
A0000034    ,

             A0000035    , A0000036    , A0000037    ,
A0000038    , A0000039    , A0000040    , A0000041    ,
A0000042    ,

             A0000043    , A0000044    , A0000045    ,
A0000046    , A0000047    , A0000048    , A0000049    ,
A0000050    ,

             A0000051    , A0000052    ,
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** SOURCE IDs DEFINED AS URBAN SOURCES ***

URBAN ID	URBAN POP	SOURCE IDs
	22000.	PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 ,
		A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 ,
		A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 ,
		A0000022 , A0000025 , A0000026 , PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
		A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
		A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
		A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = PAREA1 ; SOURCE TYPE = AREAPOLY :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000001 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000002 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000003 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000004 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000005 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000006 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000007 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000008 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000023 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000024 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000009 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000010 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000011 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000012 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000013 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000014 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000015 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000016 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000017 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000018 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000019 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000020 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000021 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000022 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000025 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000026 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = PAREA2 ; SOURCE TYPE = AREAPOLY :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000027 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000028 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000029 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000030 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000031 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000032 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000033 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000034 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000035 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000036 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000037 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000038 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000039 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000040 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000041 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000042 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000043 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000044 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000045 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000046 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                 DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                 DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000047 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000048 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000049 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000050 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000051 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000052 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675133.1, 4422610.1, 1051.9, 2131.6, 0.0);
(675208.1, 4422610.1, 1051.3, 2131.6, 0.0);
(675283.1, 4422610.1, 1050.7, 2131.6, 0.0);
(675358.1, 4422610.1, 1050.6, 2131.6, 0.0);
(675433.1, 4422610.1, 1050.8, 2131.6, 0.0);
(675508.1, 4422610.1, 1051.0, 2131.6, 0.0);
(675583.1, 4422610.1, 1051.4, 2131.6, 0.0);
(675658.1, 4422610.1, 1050.3, 2131.6, 0.0);
(675733.1, 4422610.1, 1048.8, 2131.6, 0.0);
(675808.1, 4422610.1, 1047.3, 2131.6, 0.0);
(675883.1, 4422610.1, 1045.5, 2131.6, 0.0);
(675958.1, 4422610.1, 1043.3, 2131.6, 0.0);
(676033.1, 4422610.1, 1042.3, 2131.6, 0.0);
(676108.1, 4422610.1, 1042.4, 2131.6, 0.0);
(675133.1, 4422660.1, 1048.4, 2131.6, 0.0);
(675208.1, 4422660.1, 1048.5, 2131.6, 0.0);
(675283.1, 4422660.1, 1048.7, 2131.6, 0.0);
(675358.1, 4422660.1, 1048.9, 2131.6, 0.0);
(675433.1, 4422660.1, 1049.2, 2131.6, 0.0);
(675508.1, 4422660.1, 1049.4, 2131.6, 0.0);
(675583.1, 4422660.1, 1049.4, 2131.6, 0.0);
(675658.1, 4422660.1, 1048.2, 2131.6, 0.0);
(675733.1, 4422660.1, 1047.3, 2131.6, 0.0);
(675808.1, 4422660.1, 1046.4, 2131.6, 0.0);
(675883.1, 4422660.1, 1044.4, 2131.6, 0.0);
(675958.1, 4422660.1, 1042.7, 2131.6, 0.0);
(676033.1, 4422660.1, 1041.4, 2131.6, 0.0);
(676108.1, 4422660.1, 1040.7, 2131.6, 0.0);
(675133.1, 4422710.1, 1045.6, 2131.6, 0.0);
(675208.1, 4422710.1, 1046.4, 2131.6, 0.0);
(675283.1, 4422710.1, 1046.8, 2131.6, 0.0);
(675358.1, 4422710.1, 1047.5, 2131.6, 0.0);
(675433.1, 4422710.1, 1047.7, 2131.6, 0.0);
(675508.1, 4422710.1, 1047.9, 2131.6, 0.0);
(675583.1, 4422710.1, 1047.6, 2131.6, 0.0);
(675658.1, 4422710.1, 1046.7, 2131.6, 0.0);

```
     ( 675733.1, 4422710.1,    1046.2,    2131.6,       0.0);
( 675808.1, 4422710.1,    1045.2,    2131.6,       0.0);
     ( 675883.1, 4422710.1,    1044.2,    2131.6,       0.0);
( 675958.1, 4422710.1,    1042.3,    2131.6,       0.0);
     ( 676033.1, 4422710.1,    1041.1,    2131.6,       0.0);
( 676108.1, 4422710.1,    1040.5,    2131.6,       0.0);
     ( 675133.1, 4422760.1,    1044.4,    2131.6,       0.0);
( 675208.1, 4422760.1,    1045.0,    2131.6,       0.0);
     ( 675283.1, 4422760.1,    1045.3,    2131.6,       0.0);
( 675358.1, 4422760.1,    1046.4,    2131.6,       0.0);
     ( 675433.1, 4422760.1,    1046.5,    2131.6,       0.0);
( 675508.1, 4422760.1,    1046.4,    2131.6,       0.0);
     ( 675583.1, 4422760.1,    1045.9,    2131.6,       0.0);
( 675658.1, 4422760.1,    1045.2,    2131.6,       0.0);
     ( 675733.1, 4422760.1,    1044.8,    2131.6,       0.0);
( 675808.1, 4422760.1,    1043.9,    2131.6,       0.0);
     ( 675883.1, 4422760.1,    1043.1,    2131.6,       0.0);
( 675958.1, 4422760.1,    1042.1,    2131.6,       0.0);
     ( 676033.1, 4422760.1,    1040.8,    2131.6,       0.0);
( 676108.1, 4422760.1,    1040.2,    2131.6,       0.0);
     ( 675133.1, 4422810.1,    1043.0,    2131.6,       0.0);
( 675208.1, 4422810.1,    1043.2,    2131.6,       0.0);
     ( 675283.1, 4422810.1,    1044.2,    2131.6,       0.0);
( 675358.1, 4422810.1,    1045.1,    2131.6,       0.0);
     ( 675433.1, 4422810.1,    1045.2,    2131.6,       0.0);
( 675508.1, 4422810.1,    1044.9,    2131.6,       0.0);
     ( 675583.1, 4422810.1,    1044.2,    2131.6,       0.0);
( 675658.1, 4422810.1,    1043.5,    2131.6,       0.0);
     ( 675733.1, 4422810.1,    1043.9,    2131.6,       0.0);
( 675808.1, 4422810.1,    1043.2,    2131.6,       0.0);
     ( 675883.1, 4422810.1,    1042.2,    2131.6,       0.0);
( 675958.1, 4422810.1,    1041.3,    2131.6,       0.0);
     ( 676033.1, 4422810.1,    1040.2,    2131.6,       0.0);
( 676108.1, 4422810.1,    1039.8,    2131.6,       0.0);
     ( 675133.1, 4422860.1,    1042.0,    2131.6,       0.0);
( 675208.1, 4422860.1,    1042.6,    2131.6,       0.0);
     ( 675283.1, 4422860.1,    1043.4,    2131.6,       0.0);
( 675358.1, 4422860.1,    1044.0,    2131.6,       0.0);
     ( 675433.1, 4422860.1,    1044.2,    2131.6,       0.0);
( 675508.1, 4422860.1,    1043.7,    2131.6,       0.0);
     ( 675583.1, 4422860.1,    1043.1,    2131.6,       0.0);
( 675733.1, 4422860.1,    1042.6,    2131.6,       0.0);
     ( 675808.1, 4422860.1,    1042.1,    2131.6,       0.0);
( 675883.1, 4422860.1,    1041.5,    2131.6,       0.0);
     ( 675958.1, 4422860.1,    1040.9,    2131.6,       0.0);
( 676033.1, 4422860.1,    1040.1,    2131.6,       0.0);
     ( 676108.1, 4422860.1,    1039.7,    2131.6,       0.0);
( 675133.1, 4422910.1,    1041.7,    2131.6,       0.0);
     ( 675208.1, 4422910.1,    1042.7,    2131.6,       0.0);
( 675283.1, 4422910.1,    1042.5,    2131.6,       0.0);
     ( 675358.1, 4422910.1,    1042.8,    2131.6,       0.0);
( 675433.1, 4422910.1,    1043.0,    2131.6,       0.0);
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     ( 675508.1, 4422910.1,    1042.5,    2131.6,       0.0);
( 675583.1, 4422910.1,    1041.9,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675733.1, 4422910.1, 1041.4, 2131.6, 0.0);
(675808.1, 4422910.1, 1040.9, 2131.6, 0.0);
(675883.1, 4422910.1, 1040.7, 2131.6, 0.0);
(675958.1, 4422910.1, 1040.3, 2131.6, 0.0);
(676033.1, 4422910.1, 1039.5, 2131.6, 0.0);
(676108.1, 4422910.1, 1039.5, 2131.6, 0.0);
(675133.1, 4422960.1, 1041.2, 2131.6, 0.0);
(675208.1, 4422960.1, 1041.2, 2131.6, 0.0);
(675283.1, 4422960.1, 1041.7, 2131.6, 0.0);
(675358.1, 4422960.1, 1041.9, 2131.6, 0.0);
(675433.1, 4422960.1, 1042.1, 2131.6, 0.0);
(675508.1, 4422960.1, 1041.5, 2131.6, 0.0);
(675583.1, 4422960.1, 1040.9, 2131.6, 0.0);
(675733.1, 4422960.1, 1040.5, 2131.6, 0.0);
(675808.1, 4422960.1, 1039.8, 2131.6, 0.0);
(675883.1, 4422960.1, 1039.8, 2131.6, 0.0);
(675958.1, 4422960.1, 1039.5, 2131.6, 0.0);
(676033.1, 4422960.1, 1039.0, 2131.6, 0.0);
(676108.1, 4422960.1, 1039.0, 2131.6, 0.0);
(675133.1, 4423010.1, 1040.8, 2131.6, 0.0);
(675208.1, 4423010.1, 1040.8, 2131.6, 0.0);
(675283.1, 4423010.1, 1041.0, 2131.6, 0.0);
(675358.1, 4423010.1, 1041.2, 2131.6, 0.0);
(675433.1, 4423010.1, 1041.1, 2131.6, 0.0);
(675508.1, 4423010.1, 1040.9, 2131.6, 0.0);
(675583.1, 4423010.1, 1040.4, 2131.6, 0.0);
(675658.1, 4423010.1, 1040.0, 2131.6, 0.0);
(675733.1, 4423010.1, 1039.8, 2131.6, 0.0);
(675808.1, 4423010.1, 1039.2, 2131.6, 0.0);
(675883.1, 4423010.1, 1039.6, 2131.6, 0.0);
(675958.1, 4423010.1, 1039.1, 2131.6, 0.0);
(676033.1, 4423010.1, 1038.8, 2131.6, 0.0);
(676108.1, 4423010.1, 1038.8, 2131.6, 0.0);
(675133.1, 4423060.1, 1041.5, 2131.6, 0.0);
(675208.1, 4423060.1, 1042.0, 2131.6, 0.0);
(675283.1, 4423060.1, 1042.3, 2131.6, 0.0);

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     ( 675358.1, 4423060.1,    1041.0,    2131.6,       0.0);
( 675433.1, 4423060.1,    1040.1,    2131.6,       0.0);
     ( 675508.1, 4423060.1,    1039.8,    2131.6,       0.0);
( 675583.1, 4423060.1,    1039.5,    2131.6,       0.0);
     ( 675658.1, 4423060.1,    1040.3,    2131.6,       0.0);
( 675733.1, 4423060.1,    1039.5,    2131.6,       0.0);
     ( 675808.1, 4423060.1,    1038.8,    2131.6,       0.0);
( 675883.1, 4423060.1,    1038.5,    2131.6,       0.0);
     ( 675958.1, 4423060.1,    1038.5,    2131.6,       0.0);
( 676033.1, 4423060.1,    1038.3,    2131.6,       0.0);
     ( 676108.1, 4423060.1,    1038.4,    2131.6,       0.0);
( 675133.1, 4423110.1,    1041.4,    2131.6,       0.0);
     ( 675208.1, 4423110.1,    1041.3,    2131.6,       0.0);
( 675283.1, 4423110.1,    1041.9,    2131.6,       0.0);
     ( 675358.1, 4423110.1,    1041.7,    2131.6,       0.0);
( 675433.1, 4423110.1,    1039.6,    2131.6,       0.0);
     ( 675508.1, 4423110.1,    1039.7,    2131.6,       0.0);
( 675583.1, 4423110.1,    1039.4,    2131.6,       0.0);
     ( 675658.1, 4423110.1,    1039.1,    2131.6,       0.0);
( 675733.1, 4423110.1,    1039.0,    2131.6,       0.0);
     ( 675808.1, 4423110.1,    1038.9,    2131.6,       0.0);
( 675883.1, 4423110.1,    1038.5,    2131.6,       0.0);
     ( 675958.1, 4423110.1,    1038.3,    2131.6,       0.0);
( 676033.1, 4423110.1,    1038.0,    2131.6,       0.0);
     ( 676108.1, 4423110.1,    1038.2,    2131.6,       0.0);
( 675544.6, 4422816.8,    1044.4,    2131.6,       0.0);
     ( 675569.6, 4422816.8,    1044.0,    2131.6,       0.0);
( 675594.6, 4422816.8,    1044.0,    2131.6,       0.0);
     ( 675619.6, 4422816.8,    1043.8,    2131.6,       0.0);
( 675644.6, 4422816.8,    1043.5,    2131.6,       0.0);
     ( 675669.6, 4422816.8,    1043.1,    2131.6,       0.0);
( 675694.6, 4422816.8,    1042.9,    2131.6,       0.0);
     ( 675719.6, 4422816.8,    1043.6,    2131.6,       0.0);
( 675744.6, 4422816.8,    1043.6,    2131.6,       0.0);
     ( 675769.6, 4422816.8,    1043.2,    2131.6,       0.0);
( 675794.6, 4422816.8,    1043.0,    2131.6,       0.0);
     ( 675544.6, 4422841.8,    1043.8,    2131.6,       0.0);
( 675569.6, 4422841.8,    1043.6,    2131.6,       0.0);
     ( 675594.6, 4422841.8,    1043.2,    2131.6,       0.0);
( 675619.6, 4422841.8,    1043.0,    2131.6,       0.0);
     ( 675644.6, 4422841.8,    1042.8,    2131.6,       0.0);
( 675669.6, 4422841.8,    1042.6,    2131.6,       0.0);
     ( 675694.6, 4422841.8,    1042.8,    2131.6,       0.0);
( 675719.6, 4422841.8,    1042.8,    2131.6,       0.0);
     ( 675744.6, 4422841.8,    1042.7,    2131.6,       0.0);
( 675769.6, 4422841.8,    1042.5,    2131.6,       0.0);
     ( 675794.6, 4422841.8,    1042.4,    2131.6,       0.0);
( 675544.6, 4422866.8,    1043.4,    2131.6,       0.0);
     ( 675569.6, 4422866.8,    1043.1,    2131.6,       0.0);
( 675594.6, 4422866.8,    1042.8,    2131.6,       0.0);
     ( 675619.6, 4422866.8,    1042.4,    2131.6,       0.0);
( 675644.6, 4422866.8,    1042.3,    2131.6,       0.0);
```

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     ( 675719.6, 4422866.8,    1042.3,    2131.6,       0.0);
( 675744.6, 4422866.8,    1042.3,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675769.6, 4422866.8, 1042.0, 2131.6, 0.0);
(675794.6, 4422866.8, 1042.1, 2131.6, 0.0);
(675544.6, 4422891.8, 1042.7, 2131.6, 0.0);
(675569.6, 4422891.8, 1042.5, 2131.6, 0.0);
(675594.6, 4422891.8, 1042.2, 2131.6, 0.0);
(675619.6, 4422891.8, 1041.9, 2131.6, 0.0);
(675644.6, 4422891.8, 1041.8, 2131.6, 0.0);
(675719.6, 4422891.8, 1041.6, 2131.6, 0.0);
(675744.6, 4422891.8, 1041.6, 2131.6, 0.0);
(675769.6, 4422891.8, 1041.3, 2131.6, 0.0);
(675794.6, 4422891.8, 1041.5, 2131.6, 0.0);
(675544.6, 4422916.8, 1042.1, 2131.6, 0.0);
(675569.6, 4422916.8, 1042.1, 2131.6, 0.0);
(675594.6, 4422916.8, 1041.7, 2131.6, 0.0);
(675619.6, 4422916.8, 1041.4, 2131.6, 0.0);
(675644.6, 4422916.8, 1041.3, 2131.6, 0.0);
(675719.6, 4422916.8, 1041.2, 2131.6, 0.0);
(675744.6, 4422916.8, 1041.0, 2131.6, 0.0);
(675769.6, 4422916.8, 1040.9, 2131.6, 0.0);
(675794.6, 4422916.8, 1040.9, 2131.6, 0.0);
(675544.6, 4422941.8, 1041.8, 2131.6, 0.0);
(675569.6, 4422941.8, 1041.5, 2131.6, 0.0);
(675594.6, 4422941.8, 1041.3, 2131.6, 0.0);
(675619.6, 4422941.8, 1041.1, 2131.6, 0.0);
(675644.6, 4422941.8, 1041.1, 2131.6, 0.0);
(675719.6, 4422941.8, 1040.9, 2131.6, 0.0);
(675744.6, 4422941.8, 1040.5, 2131.6, 0.0);
(675769.6, 4422941.8, 1040.4, 2131.6, 0.0);
(675794.6, 4422941.8, 1040.3, 2131.6, 0.0);
(675544.6, 4422966.8, 1041.1, 2131.6, 0.0);
(675569.6, 4422966.8, 1041.0, 2131.6, 0.0);
(675594.6, 4422966.8, 1040.8, 2131.6, 0.0);
(675619.6, 4422966.8, 1040.4, 2131.6, 0.0);
(675719.6, 4422966.8, 1040.6, 2131.6, 0.0);
(675744.6, 4422966.8, 1040.0, 2131.6, 0.0);
(675769.6, 4422966.8, 1039.9, 2131.6, 0.0);

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     ( 675794.6, 4422966.8,    1039.7,    2131.6,       0.0);
( 675544.6, 4422991.8,    1040.7,    2131.6,       0.0);
     ( 675569.6, 4422991.8,    1040.5,    2131.6,       0.0);
( 675594.6, 4422991.8,    1040.4,    2131.6,       0.0);
     ( 675619.6, 4422991.8,    1040.2,    2131.6,       0.0);
( 675644.6, 4422991.8,    1040.0,    2131.6,       0.0);
     ( 675719.6, 4422991.8,    1040.1,    2131.6,       0.0);
( 675744.6, 4422991.8,    1039.8,    2131.6,       0.0);
     ( 675769.6, 4422991.8,    1039.8,    2131.6,       0.0);
( 675794.6, 4422991.8,    1039.4,    2131.6,       0.0);
     ( 675544.6, 4423016.8,    1040.4,    2131.6,       0.0);
( 675569.6, 4423016.8,    1040.3,    2131.6,       0.0);
     ( 675594.6, 4423016.8,    1040.2,    2131.6,       0.0);
( 675619.6, 4423016.8,    1040.3,    2131.6,       0.0);
     ( 675644.6, 4423016.8,    1040.2,    2131.6,       0.0);
( 675669.6, 4423016.8,    1039.9,    2131.6,       0.0);
     ( 675719.6, 4423016.8,    1039.7,    2131.6,       0.0);
( 675744.6, 4423016.8,    1040.0,    2131.6,       0.0);
     ( 675769.6, 4423016.8,    1039.6,    2131.6,       0.0);
( 675794.6, 4423016.8,    1039.2,    2131.6,       0.0);
     ( 675544.6, 4423041.8,    1040.0,    2131.6,       0.0);
( 675569.6, 4423041.8,    1039.8,    2131.6,       0.0);
     ( 675594.6, 4423041.8,    1040.0,    2131.6,       0.0);
( 675619.6, 4423041.8,    1040.8,    2131.6,       0.0);
     ( 675644.6, 4423041.8,    1040.3,    2131.6,       0.0);
( 675669.6, 4423041.8,    1040.1,    2131.6,       0.0);
     ( 675694.6, 4423041.8,    1039.9,    2131.6,       0.0);
( 675719.6, 4423041.8,    1039.5,    2131.6,       0.0);
     ( 675744.6, 4423041.8,    1039.2,    2131.6,       0.0);
( 675769.6, 4423041.8,    1039.1,    2131.6,       0.0);
     ( 675794.6, 4423041.8,    1039.0,    2131.6,       0.0);
( 675544.6, 4423066.8,    1039.6,    2131.6,       0.0);
     ( 675569.6, 4423066.8,    1039.5,    2131.6,       0.0);
( 675594.6, 4423066.8,    1039.6,    2131.6,       0.0);
     ( 675619.6, 4423066.8,    1041.4,    2131.6,       0.0);
( 675644.6, 4423066.8,    1040.5,    2131.6,       0.0);
     ( 675669.6, 4423066.8,    1040.2,    2131.6,       0.0);
( 675694.6, 4423066.8,    1040.3,    2131.6,       0.0);
     ( 675719.6, 4423066.8,    1039.8,    2131.6,       0.0);
( 675744.6, 4423066.8,    1039.5,    2131.6,       0.0);
     ( 675769.6, 4423066.8,    1040.1,    2131.6,       0.0);
( 675794.6, 4423066.8,    1038.6,    2131.6,       0.0);
     ( 675644.8, 4422859.7,    1042.4,    2131.6,       0.0);
( 675645.6, 4422952.4,    1040.8,    2131.6,       0.0);
     ( 675604.0, 4422951.7,    1041.0,    2131.6,       0.0);
( 675683.6, 4423024.7,    1039.9,    2131.6,       0.0);
     ( 675705.7, 4423024.9,    1039.9,    2131.6,       0.0);
( 675712.5, 4422972.8,    1040.8,    2131.6,       0.0);
     ( 675711.6, 4422858.5,    1042.6,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** METEOROLOGICAL DAYS SELECTED FOR PROCESSING ***

(1=YES; 0=NO)

```
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
```

NOTE: METEOROLOGICAL DATA ACTUALLY PROCESSED WILL ALSO DEPEND ON WHAT IS INCLUDED IN THE DATA FILE.

*** UPPER BOUND OF FIRST THROUGH FIFTH WIND SPEED CATEGORIES ***

(METERS/SEC)

1.54, 3.09, 5.14, 8.23, 10.80,

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** UP TO THE FIRST 24 HOURS OF METEOROLOGICAL DATA ***

Surface file: Z:\Shared\San Jose\Env\16230_13 New Quincy Courthouse EIR\Project Data\ACES\MET\ Met Version: 19191
Profile file: Z:\Shared\San Jose\Env\16230_13 New Quincy Courthouse EIR\Project Data\ACES\MET\
Surface format: FREE
Profile format: FREE
Surface station no.: 23225 Upper air station no.: 23230
Name: BLUE_CANYON_NYACK_AIRPORT Name: OAKLAND/WSO_AP
Year: 2014 Year: 2014

First 24 hours of scalar data

YR	MO	DY	JDY	HR	H0	U*	W*	DT/DZ	ZICNV	ZIMCH	M-O LEN	Z0	BOWEN	ALBEDO	REF WS	WD	HT	REF TA	HT
14	01	01	1	01	-33.3	0.399	-9.000	-9.000	-999.	604.	174.9	0.49	0.50	1.00	2.86	999.	10.0	283.1	2.0
14	01	01	1	02	-39.3	0.472	-9.000	-9.000	-999.	777.	244.8	0.49	0.50	1.00	3.36	999.	10.0	283.1	2.0
14	01	01	1	03	-41.1	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	1.00	3.86	54.	10.0	283.1	2.0
14	01	01	1	04	-30.0	0.360	-9.000	-9.000	-999.	532.	142.7	0.39	0.50	1.00	2.86	53.	10.0	283.1	2.0
14	01	01	1	05	-39.3	0.472	-9.000	-9.000	-999.	777.	244.8	0.49	0.50	1.00	3.36	999.	10.0	283.1	2.0
14	01	01	1	06	-33.3	0.399	-9.000	-9.000	-999.	609.	174.9	0.49	0.50	1.00	2.86	999.	10.0	283.1	2.0
14	01	01	1	07	-41.2	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	1.00	3.86	55.	10.0	282.5	2.0
14	01	01	1	08	-41.1	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	0.88	3.86	53.	10.0	282.5	2.0
14	01	01	1	09	-15.8	0.434	-9.000	-9.000	-999.	689.	387.8	0.39	0.50	0.58	3.36	47.	10.0	283.8	2.0
14	01	01	1	10	14.3	0.264	0.282	0.012	47.	349.	-97.3	0.54	0.50	0.47	1.76	81.	10.0	285.9	2.0
14	01	01	1	11	31.8	-9.000	-9.000	-9.000	121.	-999.	-99999.0	0.49	0.50	0.43	0.00	0.	10.0	286.4	2.0

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 14 01 01   1 12   41.5  0.278  0.612  0.012  166.  352.    -39.1
0.49   0.50   0.42    1.76  999.   10.0  287.5    2.0
 14 01 01   1 13   42.3  0.264  0.656  0.013  201.  325.    -32.6
0.40   0.50   0.41    1.76  253.   10.0  287.0    2.0
 14 01 01   1 14   34.7  0.326  0.632  0.012  219.  446.    -75.0
0.40   0.50   0.43    2.36  269.   10.0  287.5    2.0
 14 01 01   1 15   18.8  0.372  0.523  0.011  228.  545.   -206.0
0.40   0.50   0.46    2.86  242.   10.0  287.5    2.0
 14 01 01   1 16   -4.8  0.307 -9.000 -9.000 -999.  411.    457.0
0.40   0.50   0.54    2.36  264.   10.0  285.9    2.0
 14 01 01   1 17  -25.6  0.320 -9.000 -9.000 -999.  435.    112.9
0.77   0.50   0.79    1.76   21.   10.0  285.4    2.0
 14 01 01   1 18  -17.9  0.217 -9.000 -9.000 -999.  247.     51.6
0.39   0.50   1.00    1.76   47.   10.0  284.9    2.0
 14 01 01   1 19 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  284.9    2.0
 14 01 01   1 20 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  283.8    2.0
 14 01 01   1 21  -21.0  0.252 -9.000 -9.000 -999.  303.     69.8
0.54   0.50   1.00    1.76   80.   10.0  283.8    2.0
 14 01 01   1 22  -29.4  0.353 -9.000 -9.000 -999.  503.    136.9
0.86   0.50   1.00    1.76  132.   10.0  283.8    2.0
 14 01 01   1 23 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  282.5    2.0
 14 01 01   1 24  -40.0  0.479 -9.000 -9.000 -999.  796.    252.4
0.86   0.50   1.00    2.36  140.   10.0  283.1    2.0


 First hour of profile data
 YR MO DY HR HEIGHT F  WDIR    WSPD AMB_TMP sigmaA  sigmaW
sigmaV
 14 01 01 01   10.0 1 -999.    2.86   283.2
99.0  -99.00  -99.00

 F indicates top of profile (=1) or below (=0)
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00027	675208.07	4422610.07	0.00033
675283.07	4422610.07	0.00041	675358.07	4422610.07	0.00048
675433.07	4422610.07	0.00050	675508.07	4422610.07	0.00045
675583.07	4422610.07	0.00035	675658.07	4422610.07	0.00034
675733.07	4422610.07	0.00037	675808.07	4422610.07	0.00039
675883.07	4422610.07	0.00037	675958.07	4422610.07	0.00033
676033.07	4422610.07	0.00029	676108.07	4422610.07	0.00024
675133.07	4422660.07	0.00027	675208.07	4422660.07	0.00035
675283.07	4422660.07	0.00045	675358.07	4422660.07	0.00057
675433.07	4422660.07	0.00067			

675508.07 4422660.07 0.00067
675583.07 4422660.07 0.00054
675658.07 4422660.07 0.00048
675733.07 4422660.07 0.00053
675808.07 4422660.07 0.00053
675883.07 4422660.07 0.00049
675958.07 4422660.07 0.00041
676033.07 4422660.07 0.00034
676108.07 4422660.07 0.00029
675133.07 4422710.07 0.00028
675208.07 4422710.07 0.00036
675283.07 4422710.07 0.00048
675358.07 4422710.07 0.00066
675433.07 4422710.07 0.00086
675508.07 4422710.07 0.00101
675583.07 4422710.07 0.00092
675658.07 4422710.07 0.00085
675733.07 4422710.07 0.00081
675808.07 4422710.07 0.00078
675883.07 4422710.07 0.00066
675958.07 4422710.07 0.00053
676033.07 4422710.07 0.00042
676108.07 4422710.07 0.00034
675133.07 4422760.07 0.00028
675208.07 4422760.07 0.00037
675283.07 4422760.07 0.00051
675358.07 4422760.07 0.00071
675433.07 4422760.07 0.00101
675508.07 4422760.07 0.00141
675583.07 4422760.07 0.00174
675658.07 4422760.07 0.00156
675733.07 4422760.07 0.00143
675808.07 4422760.07 0.00123
675883.07 4422760.07 0.00093
675958.07 4422760.07 0.00069
676033.07 4422760.07 0.00052
676108.07 4422760.07 0.00040
675133.07 4422810.07 0.00027
675208.07 4422810.07 0.00037
675283.07 4422810.07 0.00051
675358.07 4422810.07 0.00075
675433.07 4422810.07 0.00117
675508.07 4422810.07 0.00193
675583.07 4422810.07 0.00321
675658.07 4422810.07 0.00394
675733.07 4422810.07 0.00317
675808.07 4422810.07 0.00212
675883.07 4422810.07 0.00135
675958.07 4422810.07 0.00092
676033.07 4422810.07 0.00065
676108.07 4422810.07 0.00049
675133.07 4422860.07 0.00026

```
675208.07    4422860.07        0.00036
         675283.07    4422860.07        0.00050
675358.07    4422860.07        0.00075
         675433.07    4422860.07        0.00125
675508.07    4422860.07        0.00236
         675583.07    4422860.07        0.00545
675733.07    4422860.07        0.01180
         675808.07    4422860.07        0.00386
675883.07    4422860.07        0.00198
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00121	676033.07	4422860.07	0.00082
676108.07	4422860.07	0.00058	675133.07	4422910.07	0.00024
675208.07	4422910.07	0.00032	675283.07	4422910.07	0.00046
675358.07	4422910.07	0.00070	675433.07	4422910.07	0.00120
675508.07	4422910.07	0.00249	675583.07	4422910.07	0.00720
675733.07	4422910.07	0.02342	675808.07	4422910.07	0.00581
675883.07	4422910.07	0.00264	675958.07	4422910.07	0.00150
676033.07	4422910.07	0.00097	676108.07	4422910.07	0.00068
675133.07	4422960.07	0.00022	675208.07	4422960.07	0.00030
675283.07	4422960.07	0.00041			

675358.07 4422960.07 0.00062
675433.07 4422960.07 0.00106
675508.07 4422960.07 0.00225
675583.07 4422960.07 0.00816
675733.07 4422960.07 0.02712
675808.07 4422960.07 0.00669
675883.07 4422960.07 0.00301
675958.07 4422960.07 0.00169
676033.07 4422960.07 0.00108
676108.07 4422960.07 0.00074
675133.07 4423010.07 0.00020
675208.07 4423010.07 0.00027
675283.07 4423010.07 0.00037
675358.07 4423010.07 0.00055
675433.07 4423010.07 0.00092
675508.07 4423010.07 0.00189
675583.07 4423010.07 0.00634
675658.07 4423010.07 0.03885
675733.07 4423010.07 0.02252
675808.07 4423010.07 0.00604
675883.07 4423010.07 0.00290
675958.07 4423010.07 0.00169
676033.07 4423010.07 0.00110
676108.07 4423010.07 0.00077
675133.07 4423060.07 0.00019
675208.07 4423060.07 0.00025
675283.07 4423060.07 0.00034
675358.07 4423060.07 0.00050
675433.07 4423060.07 0.00082
675508.07 4423060.07 0.00168
675583.07 4423060.07 0.00484
675658.07 4423060.07 0.01583
675733.07 4423060.07 0.01189
675808.07 4423060.07 0.00443
675883.07 4423060.07 0.00240
675958.07 4423060.07 0.00152
676033.07 4423060.07 0.00104
676108.07 4423060.07 0.00075
675133.07 4423110.07 0.00018
675208.07 4423110.07 0.00023
675283.07 4423110.07 0.00031
675358.07 4423110.07 0.00046
675433.07 4423110.07 0.00077
675508.07 4423110.07 0.00155
675583.07 4423110.07 0.00369
675658.07 4423110.07 0.00778
675733.07 4423110.07 0.00670
675808.07 4423110.07 0.00314
675883.07 4423110.07 0.00184
675958.07 4423110.07 0.00126
676033.07 4423110.07 0.00092
676108.07 4423110.07 0.00069

```
675544.56    4422816.83        0.00261
         675569.56    4422816.83        0.00316
675594.56    4422816.83        0.00379
         675619.56    4422816.83        0.00441
675644.56    4422816.83        0.00472
         675669.56    4422816.83        0.00455
675694.56    4422816.83        0.00421
         675719.56    4422816.83        0.00384
675744.56    4422816.83        0.00347
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00301	675794.56	4422816.83	0.00254
675544.56	4422841.83	0.00310	675569.56	4422841.83	0.00399
675594.56	4422841.83	0.00528	675619.56	4422841.83	0.00723
675644.56	4422841.83	0.00939	675669.56	4422841.83	0.01012
675694.56	4422841.83	0.00938	675719.56	4422841.83	0.00785
675744.56	4422841.83	0.00613	675769.56	4422841.83	0.00461
675794.56	4422841.83	0.00356	675544.56	4422866.83	0.00352
675569.56	4422866.83	0.00477	675594.56	4422866.83	0.00681
675619.56	4422866.83	0.01090	675644.56	4422866.83	0.01787
675719.56	4422866.83	0.01794			

```
675744.56    4422866.83        0.01075
         675769.56    4422866.83        0.00686
675794.56    4422866.83        0.00487
         675544.56    4422891.83        0.00382
675569.56    4422891.83        0.00538
         675594.56    4422891.83        0.00801
675619.56    4422891.83        0.01364
         675644.56    4422891.83        0.02685
675719.56    4422891.83        0.02774
         675744.56    4422891.83        0.01512
675769.56    4422891.83        0.00911
         675794.56    4422891.83        0.00619
675544.56    4422916.83        0.00398
         675569.56    4422916.83        0.00587
675594.56    4422916.83        0.00924
         675619.56    4422916.83        0.01614
675644.56    4422916.83        0.03228
         675719.56    4422916.83        0.03347
675744.56    4422916.83        0.01803
         675769.56    4422916.83        0.01080
675794.56    4422916.83        0.00724
         675544.56    4422941.83        0.00395
675569.56    4422941.83        0.00619
         675594.56    4422941.83        0.01093
675619.56    4422941.83        0.01939
         675644.56    4422941.83        0.03653
675719.56    4422941.83        0.03644
         675744.56    4422941.83        0.01974
675769.56    4422941.83        0.01179
         675794.56    4422941.83        0.00789
675544.56    4422966.83        0.00367
         675569.56    4422966.83        0.00581
675594.56    4422966.83        0.01082
         675619.56    4422966.83        0.02182
675719.56    4422966.83        0.03741
         675744.56    4422966.83        0.02023
675769.56    4422966.83        0.01206
         675794.56    4422966.83        0.00805
675544.56    4422991.83        0.00331
         675569.56    4422991.83        0.00517
675594.56    4422991.83        0.00938
         675619.56    4422991.83        0.02024
675644.56    4422991.83        0.03791
         675719.56    4422991.83        0.03551
675744.56    4422991.83        0.01913
         675769.56    4422991.83        0.01150
675794.56    4422991.83        0.00772
         675544.56    4423016.83        0.00303
675569.56    4423016.83        0.00466
         675594.56    4423016.83        0.00789
675619.56    4423016.83        0.01458
         675644.56    4423016.83        0.02661
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675669.56    4423016.83        0.04007
         675719.56    4423016.83        0.02940
675744.56    4423016.83        0.01623
         675769.56    4423016.83        0.01005
675794.56    4423016.83        0.00693
         675544.56    4423041.83        0.00282
675569.56    4423041.83        0.00420
         675594.56    4423041.83        0.00663
675619.56    4423041.83        0.01090
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.01736	675669.56	4423041.83	0.02548
675694.56	4423041.83	0.02895	675719.56	4423041.83	0.01980
675744.56	4423041.83	0.01219	675769.56	4423041.83	0.00815
675794.56	4423041.83	0.00587	675544.56	4423066.83	0.00264
675569.56	4423066.83	0.00379	675594.56	4423066.83	0.00561
675619.56	4423066.83	0.00844	675644.56	4423066.83	0.01207
675669.56	4423066.83	0.01579	675694.56	4423066.83	0.01695
675719.56	4423066.83	0.01335	675744.56	4423066.83	0.00920
675769.56	4423066.83	0.00654	675794.56	4423066.83	0.00484
675644.84	4422859.71	0.01552			

675645.56 4422952.37 0.03850
675603.96 4422951.71 0.01446
675683.55 4423024.69 0.03843
675705.67 4423024.92 0.03363
675712.54 4422972.82 0.04214
675711.55 4422858.53 0.01437

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00027	675208.07	4422610.07	0.00033
675283.07	4422610.07	0.00041	675358.07	4422610.07	0.00048
675433.07	4422610.07	0.00050	675508.07	4422610.07	0.00045
675583.07	4422610.07	0.00035	675658.07	4422610.07	0.00034
675733.07	4422610.07	0.00037	675808.07	4422610.07	0.00038
675883.07	4422610.07	0.00037	675958.07	4422610.07	0.00033
676033.07	4422610.07	0.00029	676108.07	4422610.07	0.00024
675133.07	4422660.07	0.00027	675208.07	4422660.07	0.00035
675283.07	4422660.07	0.00045	675358.07	4422660.07	0.00057
675433.07	4422660.07	0.00067	675508.07	4422660.07	0.00067
675583.07	4422660.07	0.00054	675658.07	4422660.07	0.00048
675733.07	4422660.07	0.00053	675808.07	4422660.07	0.00053
675883.07	4422660.07	0.00049	675958.07	4422660.07	0.00041
676033.07	4422660.07	0.00034	676108.07	4422660.07	0.00029

675133.07 4422710.07 0.00028
675208.07 4422710.07 0.00036
675283.07 4422710.07 0.00047
675358.07 4422710.07 0.00066
675433.07 4422710.07 0.00086
675508.07 4422710.07 0.00101
675583.07 4422710.07 0.00091
675658.07 4422710.07 0.00085
675733.07 4422710.07 0.00081
675808.07 4422710.07 0.00078
675883.07 4422710.07 0.00065
675958.07 4422710.07 0.00053
676033.07 4422710.07 0.00042
676108.07 4422710.07 0.00034
675133.07 4422760.07 0.00028
675208.07 4422760.07 0.00037
675283.07 4422760.07 0.00050
675358.07 4422760.07 0.00070
675433.07 4422760.07 0.00101
675508.07 4422760.07 0.00141
675583.07 4422760.07 0.00173
675658.07 4422760.07 0.00155
675733.07 4422760.07 0.00142
675808.07 4422760.07 0.00123
675883.07 4422760.07 0.00092
675958.07 4422760.07 0.00068
676033.07 4422760.07 0.00052
676108.07 4422760.07 0.00040
675133.07 4422810.07 0.00027
675208.07 4422810.07 0.00036
675283.07 4422810.07 0.00050
675358.07 4422810.07 0.00074
675433.07 4422810.07 0.00117
675508.07 4422810.07 0.00192
675583.07 4422810.07 0.00321
675658.07 4422810.07 0.00393
675733.07 4422810.07 0.00316
675808.07 4422810.07 0.00212
675883.07 4422810.07 0.00135
675958.07 4422810.07 0.00091
676033.07 4422810.07 0.00065
676108.07 4422810.07 0.00049
675133.07 4422860.07 0.00026
675208.07 4422860.07 0.00035
675283.07 4422860.07 0.00049
675358.07 4422860.07 0.00074
675433.07 4422860.07 0.00124
675508.07 4422860.07 0.00235
675583.07 4422860.07 0.00544
675733.07 4422860.07 0.01179
675808.07 4422860.07 0.00385
675883.07 4422860.07 0.00197

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00120	676033.07	4422860.07	0.00081
676108.07	4422860.07	0.00058	675133.07	4422910.07	0.00024
675208.07	4422910.07	0.00032	675283.07	4422910.07	0.00045
675358.07	4422910.07	0.00070	675433.07	4422910.07	0.00120
675508.07	4422910.07	0.00248	675583.07	4422910.07	0.00719
675733.07	4422910.07	0.02341	675808.07	4422910.07	0.00581
675883.07	4422910.07	0.00263	675958.07	4422910.07	0.00150
676033.07	4422910.07	0.00096	676108.07	4422910.07	0.00067
675133.07	4422960.07	0.00022	675208.07	4422960.07	0.00029
675283.07	4422960.07	0.00041	675358.07	4422960.07	0.00062
675433.07	4422960.07	0.00106	675508.07	4422960.07	0.00225
675583.07	4422960.07	0.00816	675733.07	4422960.07	0.02712
675808.07	4422960.07	0.00669	675883.07	4422960.07	0.00301
675958.07	4422960.07	0.00169	676033.07	4422960.07	0.00107

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          676108.07    4422960.07         0.00074
675133.07    4423010.07         0.00020
          675208.07    4423010.07         0.00027
675283.07    4423010.07         0.00037
          675358.07    4423010.07         0.00055
675433.07    4423010.07         0.00092
          675508.07    4423010.07         0.00189
675583.07    4423010.07         0.00634
          675658.07    4423010.07         0.03885
675733.07    4423010.07         0.02251
          675808.07    4423010.07         0.00603
675883.07    4423010.07         0.00289
          675958.07    4423010.07         0.00169
676033.07    4423010.07         0.00110
          676108.07    4423010.07         0.00077
675133.07    4423060.07         0.00019
          675208.07    4423060.07         0.00024
675283.07    4423060.07         0.00034
          675358.07    4423060.07         0.00050
675433.07    4423060.07         0.00082
          675508.07    4423060.07         0.00168
675583.07    4423060.07         0.00484
          675658.07    4423060.07         0.01582
675733.07    4423060.07         0.01189
          675808.07    4423060.07         0.00443
675883.07    4423060.07         0.00240
          675958.07    4423060.07         0.00152
676033.07    4423060.07         0.00104
          676108.07    4423060.07         0.00075
675133.07    4423110.07         0.00018
          675208.07    4423110.07         0.00023
675283.07    4423110.07         0.00031
          675358.07    4423110.07         0.00046
675433.07    4423110.07         0.00077
          675508.07    4423110.07         0.00155
675583.07    4423110.07         0.00369
          675658.07    4423110.07         0.00778
675733.07    4423110.07         0.00669
          675808.07    4423110.07         0.00314
675883.07    4423110.07         0.00184
          675958.07    4423110.07         0.00126
676033.07    4423110.07         0.00091
          676108.07    4423110.07         0.00069
675544.56    4422816.83         0.00261
          675569.56    4422816.83         0.00315
675594.56    4422816.83         0.00378
          675619.56    4422816.83         0.00441
675644.56    4422816.83         0.00471
          675669.56    4422816.83         0.00455
675694.56    4422816.83         0.00420
          675719.56    4422816.83         0.00384
675744.56    4422816.83         0.00346
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00300	675794.56	4422816.83	0.00254
675544.56	4422841.83	0.00309	675569.56	4422841.83	0.00398
675594.56	4422841.83	0.00526	675619.56	4422841.83	0.00722
675644.56	4422841.83	0.00938	675669.56	4422841.83	0.01011
675694.56	4422841.83	0.00937	675719.56	4422841.83	0.00784
675744.56	4422841.83	0.00612	675769.56	4422841.83	0.00460
675794.56	4422841.83	0.00355	675544.56	4422866.83	0.00351
675569.56	4422866.83	0.00476	675594.56	4422866.83	0.00680
675619.56	4422866.83	0.01088	675644.56	4422866.83	0.01786
675719.56	4422866.83	0.01793	675744.56	4422866.83	0.01074
675769.56	4422866.83	0.00685	675794.56	4422866.83	0.00485
675544.56	4422891.83	0.00382	675569.56	4422891.83	0.00537
675594.56	4422891.83	0.00801	675619.56	4422891.83	0.01363
675644.56	4422891.83	0.02684	675719.56	4422891.83	0.02773

```
         675744.56    4422891.83        0.01511
675769.56    4422891.83        0.00910
         675794.56    4422891.83        0.00618
675544.56    4422916.83        0.00397
         675569.56    4422916.83        0.00587
675594.56    4422916.83        0.00923
         675619.56    4422916.83        0.01614
675644.56    4422916.83        0.03227
         675719.56    4422916.83        0.03347
675744.56    4422916.83        0.01802
         675769.56    4422916.83        0.01079
675794.56    4422916.83        0.00724
         675544.56    4422941.83        0.00395
675569.56    4422941.83        0.00618
         675594.56    4422941.83        0.01093
675619.56    4422941.83        0.01938
         675644.56    4422941.83        0.03653
675719.56    4422941.83        0.03644
         675744.56    4422941.83        0.01974
675769.56    4422941.83        0.01179
         675794.56    4422941.83        0.00788
675544.56    4422966.83        0.00367
         675569.56    4422966.83        0.00581
675594.56    4422966.83        0.01082
         675619.56    4422966.83        0.02182
675719.56    4422966.83        0.03740
         675744.56    4422966.83        0.02022
675769.56    4422966.83        0.01206
         675794.56    4422966.83        0.00805
675544.56    4422991.83        0.00331
         675569.56    4422991.83        0.00517
675594.56    4422991.83        0.00938
         675619.56    4422991.83        0.02024
675644.56    4422991.83        0.03791
         675719.56    4422991.83        0.03551
675744.56    4422991.83        0.01913
         675769.56    4422991.83        0.01150
675794.56    4422991.83        0.00772
         675544.56    4423016.83        0.00303
675569.56    4423016.83        0.00465
         675594.56    4423016.83        0.00789
675619.56    4423016.83        0.01457
         675644.56    4423016.83        0.02661
675669.56    4423016.83        0.04007
         675719.56    4423016.83        0.02940
675744.56    4423016.83        0.01623
         675769.56    4423016.83        0.01005
675794.56    4423016.83        0.00693
         675544.56    4423041.83        0.00282
675569.56    4423041.83        0.00420
         675594.56    4423041.83        0.00663
675619.56    4423041.83        0.01090
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.01736	675669.56	4423041.83	0.02548
675694.56	4423041.83	0.02895	675719.56	4423041.83	0.01980
675744.56	4423041.83	0.01219	675769.56	4423041.83	0.00815
675794.56	4423041.83	0.00587	675544.56	4423066.83	0.00264
675569.56	4423066.83	0.00379	675594.56	4423066.83	0.00561
675619.56	4423066.83	0.00844	675644.56	4423066.83	0.01207
675669.56	4423066.83	0.01579	675694.56	4423066.83	0.01695
675719.56	4423066.83	0.01335	675744.56	4423066.83	0.00920
675769.56	4423066.83	0.00654	675794.56	4423066.83	0.00484
675644.84	4422859.71	0.01550	675645.56	4422952.37	0.03850
675603.96	4422951.71	0.01446	675683.55	4423024.69	0.03843
675705.67	4423024.92	0.03363	675712.54	4422972.82	0.04214
675711.55	4422858.53	0.01436			

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00000	675208.07	4422610.07	0.00000
675283.07	4422610.07	0.00000	675358.07	4422610.07	0.00000
675433.07	4422610.07	0.00000	675508.07	4422610.07	0.00000
675583.07	4422610.07	0.00000	675658.07	4422610.07	0.00000
675733.07	4422610.07	0.00000	675808.07	4422610.07	0.00000
675883.07	4422610.07	0.00000	675958.07	4422610.07	0.00000
676033.07	4422610.07	0.00000	676108.07	4422610.07	0.00000
675133.07	4422660.07	0.00000	675208.07	4422660.07	0.00000
675283.07	4422660.07	0.00000	675358.07	4422660.07	0.00000
675433.07	4422660.07	0.00000			

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675508.07    4422660.07        0.00000
         675583.07    4422660.07        0.00000
675658.07    4422660.07        0.00000
         675733.07    4422660.07        0.00000
675808.07    4422660.07        0.00000
         675883.07    4422660.07        0.00000
675958.07    4422660.07        0.00000
         676033.07    4422660.07        0.00000
676108.07    4422660.07        0.00000
         675133.07    4422710.07        0.00000
675208.07    4422710.07        0.00000
         675283.07    4422710.07        0.00000
675358.07    4422710.07        0.00000
         675433.07    4422710.07        0.00000
675508.07    4422710.07        0.00000
         675583.07    4422710.07        0.00000
675658.07    4422710.07        0.00000
         675733.07    4422710.07        0.00000
675808.07    4422710.07        0.00000
         675883.07    4422710.07        0.00000
675958.07    4422710.07        0.00000
         676033.07    4422710.07        0.00000
676108.07    4422710.07        0.00000
         675133.07    4422760.07        0.00000
675208.07    4422760.07        0.00000
         675283.07    4422760.07        0.00001
675358.07    4422760.07        0.00001
         675433.07    4422760.07        0.00001
675508.07    4422760.07        0.00001
         675583.07    4422760.07        0.00001
675658.07    4422760.07        0.00001
         675733.07    4422760.07        0.00001
675808.07    4422760.07        0.00001
         675883.07    4422760.07        0.00001
675958.07    4422760.07        0.00000
         676033.07    4422760.07        0.00000
676108.07    4422760.07        0.00000
         675133.07    4422810.07        0.00000
675208.07    4422810.07        0.00001
         675283.07    4422810.07        0.00001
675358.07    4422810.07        0.00001
         675433.07    4422810.07        0.00001
675508.07    4422810.07        0.00001
         675583.07    4422810.07        0.00001
675658.07    4422810.07        0.00001
         675733.07    4422810.07        0.00001
675808.07    4422810.07        0.00001
         675883.07    4422810.07        0.00001
675958.07    4422810.07        0.00001
         676033.07    4422810.07        0.00000
676108.07    4422810.07        0.00000
         675133.07    4422860.07        0.00000
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675208.07    4422860.07        0.00001
         675283.07    4422860.07        0.00001
675358.07    4422860.07        0.00001
         675433.07    4422860.07        0.00001
675508.07    4422860.07        0.00001
         675583.07    4422860.07        0.00001
675733.07    4422860.07        0.00001
         675808.07    4422860.07        0.00001
675883.07    4422860.07        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00001	676033.07	4422860.07	0.00001
676108.07	4422860.07	0.00000	675133.07	4422910.07	0.00000
675208.07	4422910.07	0.00000	675283.07	4422910.07	0.00000
675358.07	4422910.07	0.00000	675433.07	4422910.07	0.00000
675508.07	4422910.07	0.00001	675583.07	4422910.07	0.00001
675733.07	4422910.07	0.00001	675808.07	4422910.07	0.00001
675883.07	4422910.07	0.00001	675958.07	4422910.07	0.00001
676033.07	4422910.07	0.00000	676108.07	4422910.07	0.00000
675133.07	4422960.07	0.00000	675208.07	4422960.07	0.00000
675283.07	4422960.07	0.00000			

```
675358.07    4422960.07        0.00000
         675433.07    4422960.07        0.00000
675508.07    4422960.07        0.00000
         675583.07    4422960.07        0.00000
675733.07    4422960.07        0.00000
         675808.07    4422960.07        0.00000
675883.07    4422960.07        0.00000
         675958.07    4422960.07        0.00000
676033.07    4422960.07        0.00000
         676108.07    4422960.07        0.00000
675133.07    4423010.07        0.00000
         675208.07    4423010.07        0.00000
675283.07    4423010.07        0.00000
         675358.07    4423010.07        0.00000
675433.07    4423010.07        0.00000
         675508.07    4423010.07        0.00000
675583.07    4423010.07        0.00000
         675658.07    4423010.07        0.00000
675733.07    4423010.07        0.00000
         675808.07    4423010.07        0.00000
675883.07    4423010.07        0.00000
         675958.07    4423010.07        0.00000
676033.07    4423010.07        0.00000
         676108.07    4423010.07        0.00000
675133.07    4423060.07        0.00000
         675208.07    4423060.07        0.00000
675283.07    4423060.07        0.00000
         675358.07    4423060.07        0.00000
675433.07    4423060.07        0.00000
         675508.07    4423060.07        0.00000
675583.07    4423060.07        0.00000
         675658.07    4423060.07        0.00000
675733.07    4423060.07        0.00000
         675808.07    4423060.07        0.00000
675883.07    4423060.07        0.00000
         675958.07    4423060.07        0.00000
676033.07    4423060.07        0.00000
         676108.07    4423060.07        0.00000
675133.07    4423110.07        0.00000
         675208.07    4423110.07        0.00000
675283.07    4423110.07        0.00000
         675358.07    4423110.07        0.00000
675433.07    4423110.07        0.00000
         675508.07    4423110.07        0.00000
675583.07    4423110.07        0.00000
         675658.07    4423110.07        0.00000
675733.07    4423110.07        0.00000
         675808.07    4423110.07        0.00000
675883.07    4423110.07        0.00000
         675958.07    4423110.07        0.00000
676033.07    4423110.07        0.00000
         676108.07    4423110.07        0.00000
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675544.56    4422816.83        0.00001
         675569.56    4422816.83        0.00001
675594.56    4422816.83        0.00001
         675619.56    4422816.83        0.00001
675644.56    4422816.83        0.00001
         675669.56    4422816.83        0.00001
675694.56    4422816.83        0.00001
         675719.56    4422816.83        0.00001
675744.56    4422816.83        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00001	675794.56	4422816.83	0.00001
675544.56	4422841.83	0.00001	675569.56	4422841.83	0.00001
675594.56	4422841.83	0.00001	675619.56	4422841.83	0.00001
675644.56	4422841.83	0.00001	675669.56	4422841.83	0.00001
675694.56	4422841.83	0.00001	675719.56	4422841.83	0.00001
675744.56	4422841.83	0.00001	675769.56	4422841.83	0.00001
675794.56	4422841.83	0.00001	675544.56	4422866.83	0.00001
675569.56	4422866.83	0.00001	675594.56	4422866.83	0.00001
675619.56	4422866.83	0.00001	675644.56	4422866.83	0.00001
675719.56	4422866.83	0.00001			

```
675744.56    4422866.83        0.00001
         675769.56    4422866.83        0.00001
675794.56    4422866.83        0.00001
         675544.56    4422891.83        0.00001
675569.56    4422891.83        0.00001
         675594.56    4422891.83        0.00001
675619.56    4422891.83        0.00001
         675644.56    4422891.83        0.00001
675719.56    4422891.83        0.00001
         675744.56    4422891.83        0.00001
675769.56    4422891.83        0.00001
         675794.56    4422891.83        0.00001
675544.56    4422916.83        0.00000
         675569.56    4422916.83        0.00000
675594.56    4422916.83        0.00000
         675619.56    4422916.83        0.00000
675644.56    4422916.83        0.00000
         675719.56    4422916.83        0.00000
675744.56    4422916.83        0.00000
         675769.56    4422916.83        0.00000
675794.56    4422916.83        0.00000
         675544.56    4422941.83        0.00000
675569.56    4422941.83        0.00000
         675594.56    4422941.83        0.00000
675619.56    4422941.83        0.00000
         675644.56    4422941.83        0.00000
675719.56    4422941.83        0.00000
         675744.56    4422941.83        0.00000
675769.56    4422941.83        0.00000
         675794.56    4422941.83        0.00000
675544.56    4422966.83        0.00000
         675569.56    4422966.83        0.00000
675594.56    4422966.83        0.00000
         675619.56    4422966.83        0.00000
675719.56    4422966.83        0.00000
         675744.56    4422966.83        0.00000
675769.56    4422966.83        0.00000
         675794.56    4422966.83        0.00000
675544.56    4422991.83        0.00000
         675569.56    4422991.83        0.00000
675594.56    4422991.83        0.00000
         675619.56    4422991.83        0.00000
675644.56    4422991.83        0.00000
         675719.56    4422991.83        0.00000
675744.56    4422991.83        0.00000
         675769.56    4422991.83        0.00000
675794.56    4422991.83        0.00000
         675544.56    4423016.83        0.00000
675569.56    4423016.83        0.00000
         675594.56    4423016.83        0.00000
675619.56    4423016.83        0.00000
         675644.56    4423016.83        0.00000
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```
675669.56    4423016.83        0.00000
         675719.56    4423016.83        0.00000
675744.56    4423016.83        0.00000
         675769.56    4423016.83        0.00000
675794.56    4423016.83        0.00000
         675544.56    4423041.83        0.00000
675569.56    4423041.83        0.00000
         675594.56    4423041.83        0.00000
675619.56    4423041.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00000	675669.56	4423041.83	0.00000
675694.56	4423041.83	0.00000	675719.56	4423041.83	0.00000
675744.56	4423041.83	0.00000	675769.56	4423041.83	0.00000
675794.56	4423041.83	0.00000	675544.56	4423066.83	0.00000
675569.56	4423066.83	0.00000	675594.56	4423066.83	0.00000
675619.56	4423066.83	0.00000	675644.56	4423066.83	0.00000
675669.56	4423066.83	0.00000	675694.56	4423066.83	0.00000
675719.56	4423066.83	0.00000	675744.56	4423066.83	0.00000
675769.56	4423066.83	0.00000	675794.56	4423066.83	0.00000
675644.84	4422859.71	0.00001			

```
675645.56    4422952.37        0.00000
         675603.96    4422951.71        0.00000
675683.55    4423024.69        0.00000
         675705.67    4423024.92        0.00000
675712.54    4422972.82        0.00000
         675711.55    4422858.53        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00057	675208.07	4422610.07	0.00072
675283.07	4422610.07	0.00088	675358.07	4422610.07	0.00103
675433.07	4422610.07	0.00109	675508.07	4422610.07	0.00096
675583.07	4422610.07	0.00075	675658.07	4422610.07	0.00073
675733.07	4422610.07	0.00081	675808.07	4422610.07	0.00083
675883.07	4422610.07	0.00080	675958.07	4422610.07	0.00072
676033.07	4422610.07	0.00062	676108.07	4422610.07	0.00053
675133.07	4422660.07	0.00059	675208.07	4422660.07	0.00076
675283.07	4422660.07	0.00098	675358.07	4422660.07	0.00124
675433.07	4422660.07	0.00145			

675508.07 4422660.07 0.00145
675583.07 4422660.07 0.00116
675658.07 4422660.07 0.00104
675733.07 4422660.07 0.00115
675808.07 4422660.07 0.00115
675883.07 4422660.07 0.00105
675958.07 4422660.07 0.00090
676033.07 4422660.07 0.00074
676108.07 4422660.07 0.00062
675133.07 4422710.07 0.00060
675208.07 4422710.07 0.00078
675283.07 4422710.07 0.00103
675358.07 4422710.07 0.00142
675433.07 4422710.07 0.00187
675508.07 4422710.07 0.00218
675583.07 4422710.07 0.00198
675658.07 4422710.07 0.00183
675733.07 4422710.07 0.00176
675808.07 4422710.07 0.00169
675883.07 4422710.07 0.00142
675958.07 4422710.07 0.00114
676033.07 4422710.07 0.00091
676108.07 4422710.07 0.00073
675133.07 4422760.07 0.00060
675208.07 4422760.07 0.00079
675283.07 4422760.07 0.00109
675358.07 4422760.07 0.00153
675433.07 4422760.07 0.00218
675508.07 4422760.07 0.00305
675583.07 4422760.07 0.00375
675658.07 4422760.07 0.00337
675733.07 4422760.07 0.00308
675808.07 4422760.07 0.00266
675883.07 4422760.07 0.00200
675958.07 4422760.07 0.00148
676033.07 4422760.07 0.00112
676108.07 4422760.07 0.00088
675133.07 4422810.07 0.00058
675208.07 4422810.07 0.00079
675283.07 4422810.07 0.00110
675358.07 4422810.07 0.00162
675433.07 4422810.07 0.00253
675508.07 4422810.07 0.00416
675583.07 4422810.07 0.00695
675658.07 4422810.07 0.00852
675733.07 4422810.07 0.00685
675808.07 4422810.07 0.00459
675883.07 4422810.07 0.00292
675958.07 4422810.07 0.00197
676033.07 4422810.07 0.00141
676108.07 4422810.07 0.00106
675133.07 4422860.07 0.00056

```
675208.07    4422860.07        0.00076
         675283.07    4422860.07        0.00107
675358.07    4422860.07        0.00161
         675433.07    4422860.07        0.00269
675508.07    4422860.07        0.00509
         675583.07    4422860.07        0.01178
675733.07    4422860.07        0.02553
         675808.07    4422860.07        0.00834
675883.07    4422860.07        0.00427
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00261	676033.07	4422860.07	0.00176
676108.07	4422860.07	0.00126	675133.07	4422910.07	0.00052
675208.07	4422910.07	0.00070	675283.07	4422910.07	0.00099
675358.07	4422910.07	0.00151	675433.07	4422910.07	0.00259
675508.07	4422910.07	0.00538	675583.07	4422910.07	0.01557
675733.07	4422910.07	0.05068	675808.07	4422910.07	0.01258
675883.07	4422910.07	0.00570	675958.07	4422910.07	0.00324
676033.07	4422910.07	0.00209	676108.07	4422910.07	0.00146
675133.07	4422960.07	0.00048	675208.07	4422960.07	0.00064
675283.07	4422960.07	0.00089			

675358.07 4422960.07 0.00135
675433.07 4422960.07 0.00230
675508.07 4422960.07 0.00487
675583.07 4422960.07 0.01766
675733.07 4422960.07 0.05870
675808.07 4422960.07 0.01448
675883.07 4422960.07 0.00651
675958.07 4422960.07 0.00365
676033.07 4422960.07 0.00232
676108.07 4422960.07 0.00161
675133.07 4423010.07 0.00044
675208.07 4423010.07 0.00058
675283.07 4423010.07 0.00080
675358.07 4423010.07 0.00119
675433.07 4423010.07 0.00199
675508.07 4423010.07 0.00409
675583.07 4423010.07 0.01372
675658.07 4423010.07 0.08410
675733.07 4423010.07 0.04873
675808.07 4423010.07 0.01306
675883.07 4423010.07 0.00626
675958.07 4423010.07 0.00366
676033.07 4423010.07 0.00238
676108.07 4423010.07 0.00166
675133.07 4423060.07 0.00041
675208.07 4423060.07 0.00053
675283.07 4423060.07 0.00073
675358.07 4423060.07 0.00107
675433.07 4423060.07 0.00178
675508.07 4423060.07 0.00364
675583.07 4423060.07 0.01048
675658.07 4423060.07 0.03426
675733.07 4423060.07 0.02574
675808.07 4423060.07 0.00959
675883.07 4423060.07 0.00519
675958.07 4423060.07 0.00329
676033.07 4423060.07 0.00225
676108.07 4423060.07 0.00162
675133.07 4423110.07 0.00038
675208.07 4423110.07 0.00050
675283.07 4423110.07 0.00068
675358.07 4423110.07 0.00100
675433.07 4423110.07 0.00167
675508.07 4423110.07 0.00335
675583.07 4423110.07 0.00798
675658.07 4423110.07 0.01684
675733.07 4423110.07 0.01449
675808.07 4423110.07 0.00679
675883.07 4423110.07 0.00399
675958.07 4423110.07 0.00273
676033.07 4423110.07 0.00198
676108.07 4423110.07 0.00149

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675544.56    4422816.83        0.00565
         675569.56    4422816.83        0.00682
675594.56    4422816.83        0.00819
         675619.56    4422816.83        0.00954
675644.56    4422816.83        0.01020
         675669.56    4422816.83        0.00985
675694.56    4422816.83        0.00911
         675719.56    4422816.83        0.00831
675744.56    4422816.83        0.00749
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00650	675794.56	4422816.83	0.00549
675544.56	4422841.83	0.00670	675569.56	4422841.83	0.00862
675594.56	4422841.83	0.01140	675619.56	4422841.83	0.01563
675644.56	4422841.83	0.02030	675669.56	4422841.83	0.02190
675694.56	4422841.83	0.02029	675719.56	4422841.83	0.01698
675744.56	4422841.83	0.01326	675769.56	4422841.83	0.00997
675794.56	4422841.83	0.00770	675544.56	4422866.83	0.00761
675569.56	4422866.83	0.01030	675594.56	4422866.83	0.01473
675619.56	4422866.83	0.02357	675644.56	4422866.83	0.03866
675719.56	4422866.83	0.03882			

675744.56 4422866.83 0.02326
675769.56 4422866.83 0.01484
675794.56 4422866.83 0.01051
675544.56 4422891.83 0.00826
675569.56 4422891.83 0.01163
675594.56 4422891.83 0.01734
675619.56 4422891.83 0.02950
675644.56 4422891.83 0.05810
675719.56 4422891.83 0.06003
675744.56 4422891.83 0.03272
675769.56 4422891.83 0.01971
675794.56 4422891.83 0.01338
675544.56 4422916.83 0.00860
675569.56 4422916.83 0.01270
675594.56 4422916.83 0.01999
675619.56 4422916.83 0.03494
675644.56 4422916.83 0.06986
675719.56 4422916.83 0.07245
675744.56 4422916.83 0.03901
675769.56 4422916.83 0.02336
675794.56 4422916.83 0.01567
675544.56 4422941.83 0.00855
675569.56 4422941.83 0.01339
675594.56 4422941.83 0.02366
675619.56 4422941.83 0.04196
675644.56 4422941.83 0.07908
675719.56 4422941.83 0.07887
675744.56 4422941.83 0.04272
675769.56 4422941.83 0.02552
675794.56 4422941.83 0.01707
675544.56 4422966.83 0.00794
675569.56 4422966.83 0.01257
675594.56 4422966.83 0.02343
675619.56 4422966.83 0.04724
675719.56 4422966.83 0.08096
675744.56 4422966.83 0.04377
675769.56 4422966.83 0.02610
675794.56 4422966.83 0.01743
675544.56 4422991.83 0.00716
675569.56 4422991.83 0.01119
675594.56 4422991.83 0.02031
675619.56 4422991.83 0.04381
675644.56 4422991.83 0.08206
675719.56 4422991.83 0.07686
675744.56 4422991.83 0.04141
675769.56 4422991.83 0.02489
675794.56 4422991.83 0.01671
675544.56 4423016.83 0.00656
675569.56 4423016.83 0.01007
675594.56 4423016.83 0.01707
675619.56 4423016.83 0.03155
675644.56 4423016.83 0.05761

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675669.56    4423016.83        0.08673
         675719.56    4423016.83        0.06363
675744.56    4423016.83        0.03513
         675769.56    4423016.83        0.02176
675794.56    4423016.83        0.01499
         675544.56    4423041.83        0.00611
675569.56    4423041.83        0.00909
         675594.56    4423041.83        0.01436
675619.56    4423041.83        0.02360
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.03759	675669.56	4423041.83	0.05516
675694.56	4423041.83	0.06266	675719.56	4423041.83	0.04286
675744.56	4423041.83	0.02639	675769.56	4423041.83	0.01765
675794.56	4423041.83	0.01271	675544.56	4423066.83	0.00571
675569.56	4423066.83	0.00820	675594.56	4423066.83	0.01214
675619.56	4423066.83	0.01826	675644.56	4423066.83	0.02612
675669.56	4423066.83	0.03418	675694.56	4423066.83	0.03668
675719.56	4423066.83	0.02889	675744.56	4423066.83	0.01991
675769.56	4423066.83	0.01416	675794.56	4423066.83	0.01048
675644.84	4422859.71	0.03357			

675645.56   4422952.37   0.08334
         675603.96   4422951.71   0.03130
675683.55   4423024.69   0.08318
         675705.67   4423024.92   0.07280
675712.54   4422972.82   0.09121
         675711.55   4422858.53   0.03109

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00057	675208.07	4422610.07	0.00072
675283.07	4422610.07	0.00088	675358.07	4422610.07	0.00103
675433.07	4422610.07	0.00109	675508.07	4422610.07	0.00096
675583.07	4422610.07	0.00075	675658.07	4422610.07	0.00073
675733.07	4422610.07	0.00081	675808.07	4422610.07	0.00083
675883.07	4422610.07	0.00080	675958.07	4422610.07	0.00072
676033.07	4422610.07	0.00062	676108.07	4422610.07	0.00053
675133.07	4422660.07	0.00059	675208.07	4422660.07	0.00076
675283.07	4422660.07	0.00098	675358.07	4422660.07	0.00124
675433.07	4422660.07	0.00145	675508.07	4422660.07	0.00145
675583.07	4422660.07	0.00116	675658.07	4422660.07	0.00104
675733.07	4422660.07	0.00115	675808.07	4422660.07	0.00115
675883.07	4422660.07	0.00105	675958.07	4422660.07	0.00090
676033.07	4422660.07	0.00074	676108.07	4422660.07	0.00062

675133.07 4422710.07 0.00060
675208.07 4422710.07 0.00078
675283.07 4422710.07 0.00102
675358.07 4422710.07 0.00142
675433.07 4422710.07 0.00187
675508.07 4422710.07 0.00218
675583.07 4422710.07 0.00198
675658.07 4422710.07 0.00183
675733.07 4422710.07 0.00176
675808.07 4422710.07 0.00169
675883.07 4422710.07 0.00142
675958.07 4422710.07 0.00114
676033.07 4422710.07 0.00091
676108.07 4422710.07 0.00073
675133.07 4422760.07 0.00060
675208.07 4422760.07 0.00079
675283.07 4422760.07 0.00108
675358.07 4422760.07 0.00152
675433.07 4422760.07 0.00218
675508.07 4422760.07 0.00304
675583.07 4422760.07 0.00374
675658.07 4422760.07 0.00336
675733.07 4422760.07 0.00308
675808.07 4422760.07 0.00265
675883.07 4422760.07 0.00200
675958.07 4422760.07 0.00148
676033.07 4422760.07 0.00112
676108.07 4422760.07 0.00087
675133.07 4422810.07 0.00058
675208.07 4422810.07 0.00078
675283.07 4422810.07 0.00109
675358.07 4422810.07 0.00161
675433.07 4422810.07 0.00252
675508.07 4422810.07 0.00416
675583.07 4422810.07 0.00694
675658.07 4422810.07 0.00852
675733.07 4422810.07 0.00685
675808.07 4422810.07 0.00459
675883.07 4422810.07 0.00292
675958.07 4422810.07 0.00197
676033.07 4422810.07 0.00141
676108.07 4422810.07 0.00105
675133.07 4422860.07 0.00056
675208.07 4422860.07 0.00075
675283.07 4422860.07 0.00106
675358.07 4422860.07 0.00160
675433.07 4422860.07 0.00268
675508.07 4422860.07 0.00508
675583.07 4422860.07 0.01177
675733.07 4422860.07 0.02552
675808.07 4422860.07 0.00833
675883.07 4422860.07 0.00426

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00260	676033.07	4422860.07	0.00175
676108.07	4422860.07	0.00126	675133.07	4422910.07	0.00052
675208.07	4422910.07	0.00070	675283.07	4422910.07	0.00098
675358.07	4422910.07	0.00151	675433.07	4422910.07	0.00259
675508.07	4422910.07	0.00538	675583.07	4422910.07	0.01557
675733.07	4422910.07	0.05068	675808.07	4422910.07	0.01257
675883.07	4422910.07	0.00569	675958.07	4422910.07	0.00324
676033.07	4422910.07	0.00209	676108.07	4422910.07	0.00146
675133.07	4422960.07	0.00048	675208.07	4422960.07	0.00064
675283.07	4422960.07	0.00089	675358.07	4422960.07	0.00135
675433.07	4422960.07	0.00230	675508.07	4422960.07	0.00487
675583.07	4422960.07	0.01766	675733.07	4422960.07	0.05869
675808.07	4422960.07	0.01448	675883.07	4422960.07	0.00650
675958.07	4422960.07	0.00365	676033.07	4422960.07	0.00232

```
          676108.07    4422960.07         0.00161
675133.07    4423010.07         0.00044
          675208.07    4423010.07         0.00058
675283.07    4423010.07         0.00080
          675358.07    4423010.07         0.00119
675433.07    4423010.07         0.00198
          675508.07    4423010.07         0.00409
675583.07    4423010.07         0.01372
          675658.07    4423010.07         0.08410
675733.07    4423010.07         0.04873
          675808.07    4423010.07         0.01306
675883.07    4423010.07         0.00626
          675958.07    4423010.07         0.00366
676033.07    4423010.07         0.00238
          676108.07    4423010.07         0.00166
675133.07    4423060.07         0.00041
          675208.07    4423060.07         0.00053
675283.07    4423060.07         0.00073
          675358.07    4423060.07         0.00107
675433.07    4423060.07         0.00178
          675508.07    4423060.07         0.00364
675583.07    4423060.07         0.01048
          675658.07    4423060.07         0.03425
675733.07    4423060.07         0.02573
          675808.07    4423060.07         0.00959
675883.07    4423060.07         0.00519
          675958.07    4423060.07         0.00329
676033.07    4423060.07         0.00224
          676108.07    4423060.07         0.00161
675133.07    4423110.07         0.00038
          675208.07    4423110.07         0.00049
675283.07    4423110.07         0.00068
          675358.07    4423110.07         0.00100
675433.07    4423110.07         0.00167
          675508.07    4423110.07         0.00335
675583.07    4423110.07         0.00798
          675658.07    4423110.07         0.01684
675733.07    4423110.07         0.01449
          675808.07    4423110.07         0.00679
675883.07    4423110.07         0.00399
          675958.07    4423110.07         0.00273
676033.07    4423110.07         0.00198
          676108.07    4423110.07         0.00149
675544.56    4422816.83         0.00565
          675569.56    4422816.83         0.00682
675594.56    4422816.83         0.00818
          675619.56    4422816.83         0.00953
675644.56    4422816.83         0.01019
          675669.56    4422816.83         0.00985
675694.56    4422816.83         0.00910
          675719.56    4422816.83         0.00830
675744.56    4422816.83         0.00749
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00649	675794.56	4422816.83	0.00549
675544.56	4422841.83	0.00670	675569.56	4422841.83	0.00861
675594.56	4422841.83	0.01139	675619.56	4422841.83	0.01562
675644.56	4422841.83	0.02030	675669.56	4422841.83	0.02189
675694.56	4422841.83	0.02028	675719.56	4422841.83	0.01697
675744.56	4422841.83	0.01325	675769.56	4422841.83	0.00996
675794.56	4422841.83	0.00769	675544.56	4422866.83	0.00760
675569.56	4422866.83	0.01029	675594.56	4422866.83	0.01472
675619.56	4422866.83	0.02356	675644.56	4422866.83	0.03865
675719.56	4422866.83	0.03881	675744.56	4422866.83	0.02325
675769.56	4422866.83	0.01483	675794.56	4422866.83	0.01051
675544.56	4422891.83	0.00826	675569.56	4422891.83	0.01162
675594.56	4422891.83	0.01733	675619.56	4422891.83	0.02950
675644.56	4422891.83	0.05809	675719.56	4422891.83	0.06003

675744.56 4422891.83 0.03272
675769.56 4422891.83 0.01970
675794.56 4422891.83 0.01338
675544.56 4422916.83 0.00860
675569.56 4422916.83 0.01270
675594.56 4422916.83 0.01998
675619.56 4422916.83 0.03493
675644.56 4422916.83 0.06986
675719.56 4422916.83 0.07244
675744.56 4422916.83 0.03901
675769.56 4422916.83 0.02336
675794.56 4422916.83 0.01567
675544.56 4422941.83 0.00855
675569.56 4422941.83 0.01339
675594.56 4422941.83 0.02366
675619.56 4422941.83 0.04196
675644.56 4422941.83 0.07907
675719.56 4422941.83 0.07886
675744.56 4422941.83 0.04272
675769.56 4422941.83 0.02552
675794.56 4422941.83 0.01706
675544.56 4422966.83 0.00794
675569.56 4422966.83 0.01257
675594.56 4422966.83 0.02342
675619.56 4422966.83 0.04723
675719.56 4422966.83 0.08096
675744.56 4422966.83 0.04377
675769.56 4422966.83 0.02610
675794.56 4422966.83 0.01743
675544.56 4422991.83 0.00716
675569.56 4422991.83 0.01119
675594.56 4422991.83 0.02030
675619.56 4422991.83 0.04381
675644.56 4422991.83 0.08206
675719.56 4422991.83 0.07685
675744.56 4422991.83 0.04141
675769.56 4422991.83 0.02489
675794.56 4422991.83 0.01671
675544.56 4423016.83 0.00656
675569.56 4423016.83 0.01007
675594.56 4423016.83 0.01707
675619.56 4423016.83 0.03155
675644.56 4423016.83 0.05760
675669.56 4423016.83 0.08673
675719.56 4423016.83 0.06363
675744.56 4423016.83 0.03513
675769.56 4423016.83 0.02175
675794.56 4423016.83 0.01499
675544.56 4423041.83 0.00610
675569.56 4423041.83 0.00909
675594.56 4423041.83 0.01435
675619.56 4423041.83 0.02360

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.03759	675669.56	4423041.83	0.05516
675694.56	4423041.83	0.06266	675719.56	4423041.83	0.04286
675744.56	4423041.83	0.02639	675769.56	4423041.83	0.01764
675794.56	4423041.83	0.01271	675544.56	4423066.83	0.00571
675569.56	4423066.83	0.00820	675594.56	4423066.83	0.01214
675619.56	4423066.83	0.01826	675644.56	4423066.83	0.02612
675669.56	4423066.83	0.03418	675694.56	4423066.83	0.03668
675719.56	4423066.83	0.02889	675744.56	4423066.83	0.01991
675769.56	4423066.83	0.01416	675794.56	4423066.83	0.01048
675644.84	4422859.71	0.03356	675645.56	4422952.37	0.08334
675603.96	4422951.71	0.03129	675683.55	4423024.69	0.08318
675705.67	4423024.92	0.07280	675712.54	4422972.82	0.09121
675711.55	4422858.53	0.03108			

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00000	675208.07	4422610.07	0.00000
675283.07	4422610.07	0.00000	675358.07	4422610.07	0.00000
675433.07	4422610.07	0.00000	675508.07	4422610.07	0.00000
675583.07	4422610.07	0.00000	675658.07	4422610.07	0.00000
675733.07	4422610.07	0.00000	675808.07	4422610.07	0.00000
675883.07	4422610.07	0.00000	675958.07	4422610.07	0.00000
676033.07	4422610.07	0.00000	676108.07	4422610.07	0.00000
675133.07	4422660.07	0.00000	675208.07	4422660.07	0.00000
675283.07	4422660.07	0.00000	675358.07	4422660.07	0.00000
675433.07	4422660.07	0.00000			

```
675508.07    4422660.07        0.00000
         675583.07    4422660.07        0.00000
675658.07    4422660.07        0.00000
         675733.07    4422660.07        0.00000
675808.07    4422660.07        0.00000
         675883.07    4422660.07        0.00000
675958.07    4422660.07        0.00000
         676033.07    4422660.07        0.00000
676108.07    4422660.07        0.00000
         675133.07    4422710.07        0.00000
675208.07    4422710.07        0.00000
         675283.07    4422710.07        0.00000
675358.07    4422710.07        0.00000
         675433.07    4422710.07        0.00000
675508.07    4422710.07        0.00000
         675583.07    4422710.07        0.00000
675658.07    4422710.07        0.00000
         675733.07    4422710.07        0.00000
675808.07    4422710.07        0.00000
         675883.07    4422710.07        0.00000
675958.07    4422710.07        0.00000
         676033.07    4422710.07        0.00000
676108.07    4422710.07        0.00000
         675133.07    4422760.07        0.00000
675208.07    4422760.07        0.00000
         675283.07    4422760.07        0.00001
675358.07    4422760.07        0.00001
         675433.07    4422760.07        0.00001
675508.07    4422760.07        0.00000
         675583.07    4422760.07        0.00000
675658.07    4422760.07        0.00000
         675733.07    4422760.07        0.00000
675808.07    4422760.07        0.00000
         675883.07    4422760.07        0.00000
675958.07    4422760.07        0.00000
         676033.07    4422760.07        0.00000
676108.07    4422760.07        0.00000
         675133.07    4422810.07        0.00000
675208.07    4422810.07        0.00000
         675283.07    4422810.07        0.00000
675358.07    4422810.07        0.00000
         675433.07    4422810.07        0.00000
675508.07    4422810.07        0.00000
         675583.07    4422810.07        0.00000
675658.07    4422810.07        0.00000
         675733.07    4422810.07        0.00000
675808.07    4422810.07        0.00000
         675883.07    4422810.07        0.00000
675958.07    4422810.07        0.00001
         676033.07    4422810.07        0.00000
676108.07    4422810.07        0.00000
         675133.07    4422860.07        0.00000
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```
675208.07    4422860.07        0.00001
         675283.07    4422860.07        0.00001
675358.07    4422860.07        0.00001
         675433.07    4422860.07        0.00001
675508.07    4422860.07        0.00001
         675583.07    4422860.07        0.00001
675733.07    4422860.07        0.00001
         675808.07    4422860.07        0.00001
675883.07    4422860.07        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00001	676033.07	4422860.07	0.00001
676108.07	4422860.07	0.00000	675133.07	4422910.07	0.00000
675208.07	4422910.07	0.00000	675283.07	4422910.07	0.00000
675358.07	4422910.07	0.00000	675433.07	4422910.07	0.00000
675508.07	4422910.07	0.00000	675583.07	4422910.07	0.00000
675733.07	4422910.07	0.00000	675808.07	4422910.07	0.00000
675883.07	4422910.07	0.00000	675958.07	4422910.07	0.00000
676033.07	4422910.07	0.00000	676108.07	4422910.07	0.00000
675133.07	4422960.07	0.00000	675208.07	4422960.07	0.00000
675283.07	4422960.07	0.00000			

675358.07 4422960.07 0.00000
675433.07 4422960.07 0.00000
675508.07 4422960.07 0.00000
675583.07 4422960.07 0.00000
675733.07 4422960.07 0.00000
675808.07 4422960.07 0.00000
675883.07 4422960.07 0.00000
675958.07 4422960.07 0.00000
676033.07 4422960.07 0.00000
676108.07 4422960.07 0.00000
675133.07 4423010.07 0.00000
675208.07 4423010.07 0.00000
675283.07 4423010.07 0.00000
675358.07 4423010.07 0.00000
675433.07 4423010.07 0.00000
675508.07 4423010.07 0.00000
675583.07 4423010.07 0.00000
675658.07 4423010.07 0.00000
675733.07 4423010.07 0.00000
675808.07 4423010.07 0.00000
675883.07 4423010.07 0.00000
675958.07 4423010.07 0.00000
676033.07 4423010.07 0.00000
676108.07 4423010.07 0.00000
675133.07 4423060.07 0.00000
675208.07 4423060.07 0.00000
675283.07 4423060.07 0.00000
675358.07 4423060.07 0.00000
675433.07 4423060.07 0.00000
675508.07 4423060.07 0.00000
675583.07 4423060.07 0.00000
675658.07 4423060.07 0.00000
675733.07 4423060.07 0.00000
675808.07 4423060.07 0.00000
675883.07 4423060.07 0.00000
675958.07 4423060.07 0.00000
676033.07 4423060.07 0.00000
676108.07 4423060.07 0.00000
675133.07 4423110.07 0.00000
675208.07 4423110.07 0.00000
675283.07 4423110.07 0.00000
675358.07 4423110.07 0.00000
675433.07 4423110.07 0.00000
675508.07 4423110.07 0.00000
675583.07 4423110.07 0.00000
675658.07 4423110.07 0.00000
675733.07 4423110.07 0.00000
675808.07 4423110.07 0.00000
675883.07 4423110.07 0.00000
675958.07 4423110.07 0.00000
676033.07 4423110.07 0.00000
676108.07 4423110.07 0.00000

```
675544.56    4422816.83        0.00000
         675569.56    4422816.83        0.00000
675594.56    4422816.83        0.00000
         675619.56    4422816.83        0.00000
675644.56    4422816.83        0.00000
         675669.56    4422816.83        0.00000
675694.56    4422816.83        0.00000
         675719.56    4422816.83        0.00000
675744.56    4422816.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00000	675794.56	4422816.83	0.00000
675544.56	4422841.83	0.00001	675569.56	4422841.83	0.00001
675594.56	4422841.83	0.00001	675619.56	4422841.83	0.00001
675644.56	4422841.83	0.00001	675669.56	4422841.83	0.00001
675694.56	4422841.83	0.00001	675719.56	4422841.83	0.00001
675744.56	4422841.83	0.00001	675769.56	4422841.83	0.00001
675794.56	4422841.83	0.00001	675544.56	4422866.83	0.00001
675569.56	4422866.83	0.00001	675594.56	4422866.83	0.00001
675619.56	4422866.83	0.00001	675644.56	4422866.83	0.00001
675719.56	4422866.83	0.00001			

675744.56 4422866.83 0.00001
675769.56 4422866.83 0.00001
675794.56 4422866.83 0.00001
675544.56 4422891.83 0.00000
675569.56 4422891.83 0.00000
675594.56 4422891.83 0.00000
675619.56 4422891.83 0.00000
675644.56 4422891.83 0.00000
675719.56 4422891.83 0.00000
675744.56 4422891.83 0.00000
675769.56 4422891.83 0.00000
675794.56 4422891.83 0.00000
675544.56 4422916.83 0.00000
675569.56 4422916.83 0.00000
675594.56 4422916.83 0.00000
675619.56 4422916.83 0.00000
675644.56 4422916.83 0.00000
675719.56 4422916.83 0.00000
675744.56 4422916.83 0.00000
675769.56 4422916.83 0.00000
675794.56 4422916.83 0.00000
675544.56 4422941.83 0.00000
675569.56 4422941.83 0.00000
675594.56 4422941.83 0.00000
675619.56 4422941.83 0.00000
675644.56 4422941.83 0.00000
675719.56 4422941.83 0.00000
675744.56 4422941.83 0.00000
675769.56 4422941.83 0.00000
675794.56 4422941.83 0.00000
675544.56 4422966.83 0.00000
675569.56 4422966.83 0.00000
675594.56 4422966.83 0.00000
675619.56 4422966.83 0.00000
675719.56 4422966.83 0.00000
675744.56 4422966.83 0.00000
675769.56 4422966.83 0.00000
675794.56 4422966.83 0.00000
675544.56 4422991.83 0.00000
675569.56 4422991.83 0.00000
675594.56 4422991.83 0.00000
675619.56 4422991.83 0.00000
675644.56 4422991.83 0.00000
675719.56 4422991.83 0.00000
675744.56 4422991.83 0.00000
675769.56 4422991.83 0.00000
675794.56 4422991.83 0.00000
675544.56 4423016.83 0.00000
675569.56 4423016.83 0.00000
675594.56 4423016.83 0.00000
675619.56 4423016.83 0.00000
675644.56 4423016.83 0.00000

```
675669.56    4423016.83        0.00000
         675719.56    4423016.83        0.00000
675744.56    4423016.83        0.00000
         675769.56    4423016.83        0.00000
675794.56    4423016.83        0.00000
         675544.56    4423041.83        0.00000
675569.56    4423041.83        0.00000
         675594.56    4423041.83        0.00000
675619.56    4423041.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00000	675669.56	4423041.83	0.00000
675694.56	4423041.83	0.00000	675719.56	4423041.83	0.00000
675744.56	4423041.83	0.00000	675769.56	4423041.83	0.00000
675794.56	4423041.83	0.00000	675544.56	4423066.83	0.00000
675569.56	4423066.83	0.00000	675594.56	4423066.83	0.00000
675619.56	4423066.83	0.00000	675644.56	4423066.83	0.00000
675669.56	4423066.83	0.00000	675694.56	4423066.83	0.00000
675719.56	4423066.83	0.00000	675744.56	4423066.83	0.00000
675769.56	4423066.83	0.00000	675794.56	4423066.83	0.00000
675644.84	4422859.71	0.00001			

```
675645.56    4422952.37        0.00000
         675603.96    4422951.71        0.00000
675683.55    4423024.69        0.00000
         675705.67    4423024.92        0.00000
675712.54    4422972.82        0.00000
         675711.55    4422858.53        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE SUMMARY OF MAXIMUM PERIOD (43824 HRS) RESULTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

NETWORK GROUP ID	AVERAGE CONC	RECEPTOR (XR, YR, ZELEV, ZHILL, ZFLAG)	OF TYPE	GRID-ID
Y1_ALL	1ST HIGHEST VALUE IS	0.04214 AT (675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.04007 AT (675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.03885 AT (675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.03850 AT (675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	
	5TH HIGHEST VALUE IS	0.03843 AT (675683.55, 4423024.69, 1039.91, 2131.63, 0.00)	DC	
	6TH HIGHEST VALUE IS	0.03791 AT (675644.56, 4422991.83, 1040.04, 2131.63, 0.00)	DC	
	7TH HIGHEST VALUE IS	0.03741 AT (675719.56, 4422966.83, 1040.60, 2131.63, 0.00)	DC	
	8TH HIGHEST VALUE IS	0.03653 AT (675644.56, 4422941.83, 1041.07, 2131.63, 0.00)	DC	
	9TH HIGHEST VALUE IS	0.03644 AT (675719.56, 4422941.83, 1040.89, 2131.63, 0.00)	DC	
	10TH HIGHEST VALUE IS	0.03551 AT (675719.56, 4422991.83, 1040.09, 2131.63, 0.00)	DC	
Y1_ON	1ST HIGHEST VALUE IS	0.04214 AT (675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.04007 AT (675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.03885 AT (675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.03850 AT (675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	

```
          5TH HIGHEST VALUE IS       0.03843 AT (  675683.55,
4423024.69,  1039.91,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.03791 AT (  675644.56,
4422991.83,  1040.04,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.03740 AT (  675719.56,
4422966.83,  1040.60,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.03653 AT (  675644.56,
4422941.83,  1041.07,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.03644 AT (  675719.56,
4422941.83,  1040.89,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.03551 AT (  675719.56,
4422991.83,  1040.09,  2131.63,    0.00)  DC

Y1_OFF    1ST HIGHEST VALUE IS       0.00001 AT (  675958.07,
4422860.07,  1040.91,  2131.63,    0.00)  DC
          2ND HIGHEST VALUE IS       0.00001 AT (  676033.07,
4422860.07,  1040.14,  2131.63,    0.00)  DC
          3RD HIGHEST VALUE IS       0.00001 AT (  675883.07,
4422860.07,  1041.49,  2131.63,    0.00)  DC
          4TH HIGHEST VALUE IS       0.00001 AT (  675808.07,
4422860.07,  1042.15,  2131.63,    0.00)  DC
          5TH HIGHEST VALUE IS       0.00001 AT (  675733.07,
4422860.07,  1042.62,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.00001 AT (  675644.84,
4422859.71,  1042.44,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.00001 AT (  675508.07,
4422860.07,  1043.69,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.00001 AT (  675583.07,
4422860.07,  1043.12,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.00001 AT (  675711.55,
4422858.53,  1042.60,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.00001 AT (  675433.07,
4422860.07,  1044.16,  2131.63,    0.00)  DC

Y2_ALL    1ST HIGHEST VALUE IS       0.09121 AT (  675712.54,
4422972.82,  1040.77,  2131.63,    0.00)  DC
          2ND HIGHEST VALUE IS       0.08673 AT (  675669.56,
4423016.83,  1039.88,  2131.63,    0.00)  DC
          3RD HIGHEST VALUE IS       0.08410 AT (  675658.07,
4423010.07,  1040.01,  2131.63,    0.00)  DC
          4TH HIGHEST VALUE IS       0.08334 AT (  675645.56,
4422952.37,  1040.81,  2131.63,    0.00)  DC
          5TH HIGHEST VALUE IS       0.08318 AT (  675683.55,
4423024.69,  1039.91,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.08206 AT (  675644.56,
4422991.83,  1040.04,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.08096 AT (  675719.56,
4422966.83,  1040.60,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.07908 AT (  675644.56,
4422941.83,  1041.07,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.07887 AT (  675719.56,
4422941.83,  1040.89,  2131.63,    0.00)  DC
```

```
         10TH HIGHEST VALUE IS       0.07686 AT (  675719.56,
4422991.83,  1040.09,  2131.63,    0.00)  DC
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE SUMMARY OF MAXIMUM PERIOD (43824 HRS) RESULTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

NETWORK GROUP ID		AVERAGE CONC	RECEPTOR (XR, YR, ZELEV, ZHILL, ZFLAG)	OF TYPE	GRID-ID
Y2_ON	1ST HIGHEST VALUE IS	0.09121	AT (675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.08673	AT (675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.08410	AT (675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.08334	AT (675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	
	5TH HIGHEST VALUE IS	0.08318	AT (675683.55, 4423024.69, 1039.91, 2131.63, 0.00)	DC	
	6TH HIGHEST VALUE IS	0.08206	AT (675644.56, 4422991.83, 1040.04, 2131.63, 0.00)	DC	
	7TH HIGHEST VALUE IS	0.08096	AT (675719.56, 4422966.83, 1040.60, 2131.63, 0.00)	DC	
	8TH HIGHEST VALUE IS	0.07907	AT (675644.56, 4422941.83, 1041.07, 2131.63, 0.00)	DC	
	9TH HIGHEST VALUE IS	0.07886	AT (675719.56, 4422941.83, 1040.89, 2131.63, 0.00)	DC	
	10TH HIGHEST VALUE IS	0.07685	AT (675719.56, 4422991.83, 1040.09, 2131.63, 0.00)	DC	
Y2_OFF	1ST HIGHEST VALUE IS	0.00001	AT (675958.07, 4422860.07, 1040.91, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.00001	AT (676033.07, 4422860.07, 1040.14, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.00001	AT (675883.07, 4422860.07, 1041.49, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.00001	AT (675808.07, 4422860.07, 1042.15, 2131.63, 0.00)	DC	

```
          5TH HIGHEST VALUE IS       0.00001 AT (  675733.07,
4422860.07,  1042.62,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.00001 AT (  675644.84,
4422859.71,  1042.44,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.00001 AT (  675508.07,
4422860.07,  1043.69,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.00001 AT (  675583.07,
4422860.07,  1043.12,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.00001 AT (  675711.55,
4422858.53,  1042.60,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.00001 AT (  675433.07,
4422860.07,  1044.16,  2131.63,    0.00)  DC


 *** RECEPTOR TYPES:  GC = GRIDCART
                      GP = GRIDPOLR
                      DC = DISCCART
                      DP = DISCPOLR
```

```
 *** AERMOD - VERSION 23132  ***   *** C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208\Q ***
12/16/25
 *** AERMET - VERSION  19191 ***   ***
***        07:50:23

PAGE  92
 *** MODELOPTs:    RegDFAULT  CONC  ELEV  URBAN  ADJ_U*

 *** Message Summary : AERMOD Model Execution ***

  --------- Summary of Total Messages --------

 A Total of            0 Fatal Error Message(s)
 A Total of            4 Warning Message(s)
 A Total of         1651 Informational Message(s)

 A Total of        43824 Hours Were Processed

 A Total of          479 Calm Hours Identified

 A Total of         1172 Missing Hours Identified (  2.67
Percent)


    ******** FATAL ERROR MESSAGES ********
                ***  NONE  ***


    ********   WARNING MESSAGES   ********
 ME W186    1427       MEOPEN: THRESH_1MIN 1-min ASOS wind speed
threshold used           0.50
 ME W187    1427       MEOPEN: ADJ_U* Option for Stable Low Winds
used in AERMET
 MX W450   26305       CHKDAT: Record Out of Sequence in
Meteorological File at:      18010101
 MX W450   26305       CHKDAT: Record Out of Sequence in
Meteorological File at:    1 year gap

    ***********************************
    *** AERMOD Finishes Successfully ***
    ***********************************
```

```
**
**************************************
**
** AERMOD Input Produced by:
** AERMOD View Ver. 12.0.0
** Lakes Environmental Software Inc.
** Date: 12/16/2025
** File: C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Mitigated_20251210
\Quincy_Courthouse_Construction_Mitigated_20251210.ADI
**
**************************************
**
**
**************************************
** AERMOD Control Pathway
**************************************
**
**
CO STARTING
   TITLEONE C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208\Q
   MODELOPT DFAULT CONC
   AVERTIME PERIOD
   URBANOPT 22000 Plumas_County
   POLLUTID PM_2.5
   RUNORNOT RUN
   ERRORFIL Quincy_Courthouse_Construction_Mitigated_20251210.err
CO FINISHED
**
**************************************
** AERMOD Source Pathway
**************************************
**
**
SO STARTING
** Source Location **
** Source ID - Type - X Coord. - Y Coord. **
   LOCATION PAREA1       AREAPOLY   675645.171  4422859.916
1042.440
** DESCRSRC Y1_Onsite
** ------------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN1
** DESCRSRC Y1_Lawrence_Central
** PREFIX
** Length of Side = 10.00
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 5.8183E-11
** Nodes = 4
```

```
** 676049.325, 4422856.804, 1040.14, 4.12
** 676017.666, 4422849.839, 1040.55, 4.12
** 675980.169, 4422849.410, 1040.79, 4.12
** 675182.135, 4422849.719, 1042.62, 4.12
** ----------------------------------------------------------------
-------
   LOCATION A0000001     AREA     676048.251 4422861.687 1040.05
   LOCATION A0000002     AREA     676017.609 4422854.838 1040.35
   LOCATION A0000003     AREA     675980.171 4422854.410 1040.62
   LOCATION A0000004     AREA     675880.417 4422854.449 1041.60
   LOCATION A0000005     AREA     675780.663 4422854.487 1042.30
   LOCATION A0000006     AREA     675680.909 4422854.526 1042.43
   LOCATION A0000007     AREA     675581.154 4422854.565 1043.23
   LOCATION A0000008     AREA     675481.400 4422854.603 1043.98
   LOCATION A0000023     AREA     675381.646 4422854.642 1044.38
   LOCATION A0000024     AREA     675281.892 4422854.681 1043.45
** End of LINE AREA Source ID = ARLN1
** ----------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN2
** DESCRSRC Y1_Main_Central
** PREFIX
** Length of Side = 10.50
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 2.7749E-11
** Nodes = 13
** 675180.533, 4422843.703, 1042.61, 4.12
** 675203.836, 4422815.981, 1043.03, 4.12
** 675244.447, 4422757.080, 1045.06, 4.12
** 675257.312, 4422748.986, 1045.42, 4.12
** 675278.417, 4422748.263, 1045.56, 4.12
** 675481.643, 4422753.197, 1046.58, 4.12
** 675639.972, 4422753.040, 1045.64, 4.12
** 675832.221, 4422750.683, 1043.81, 4.12
** 675853.502, 4422751.890, 1043.55, 4.12
** 675879.475, 4422757.980, 1043.45, 4.12
** 675990.143, 4422815.958, 1040.82, 4.12
** 676030.094, 4422834.512, 1040.42, 4.12
** 676056.065, 4422847.179, 1040.17, 4.12
** ----------------------------------------------------------------
-------
   LOCATION A0000009     AREA     675176.514 4422840.324 1042.54
   LOCATION A0000010     AREA     675199.514 4422813.000 1043.14
   LOCATION A0000011     AREA     675241.651 4422752.637 1045.18
   LOCATION A0000012     AREA     675257.133 4422743.739 1045.57
   LOCATION A0000013     AREA     675278.544 4422743.014 1045.68
   LOCATION A0000014     AREA     675380.157 4422745.482 1046.74
   LOCATION A0000015     AREA     675481.638 4422747.947 1046.79
   LOCATION A0000016     AREA     675560.802 4422747.869 1046.45
   LOCATION A0000017     AREA     675639.907 4422747.791 1045.99
```

```
   LOCATION A0000018     AREA     675736.032 4422746.612 1045.10
   LOCATION A0000019     AREA     675832.518 4422745.441 1044.07
   LOCATION A0000020     AREA     675854.701 4422746.779 1043.72
   LOCATION A0000021     AREA     675881.911 4422753.329 1043.34
   LOCATION A0000022     AREA     675937.245 4422782.319 1042.04
   LOCATION A0000025     AREA     675992.354 4422811.197 1040.85
   LOCATION A0000026     AREA     676032.396 4422829.794 1040.35
** End of LINE AREA Source ID = ARLN2
   LOCATION PAREA2       AREAPOLY   675645.170  4422859.920
1042.440
** DESCRSRC Y2_Onsite
** ----------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN3
** DESCRSRC Y2_Lawrence_Central
** PREFIX
** Length of Side = 10.00
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 4.0671E-11
** Nodes = 4
** 676049.320, 4422856.800, 1040.14, 4.12
** 676017.670, 4422849.840, 1040.55, 4.12
** 675980.170, 4422849.410, 1040.79, 4.12
** 675182.140, 4422849.720, 1042.62, 4.12
** ----------------------------------------------------------------
-------
   LOCATION A0000027     AREA     676048.246 4422861.683 1040.05
   LOCATION A0000028     AREA     676017.613 4422854.840 1040.35
   LOCATION A0000029     AREA     675980.172 4422854.410 1040.62
   LOCATION A0000030     AREA     675880.418 4422854.449 1041.60
   LOCATION A0000031     AREA     675780.664 4422854.487 1042.30
   LOCATION A0000032     AREA     675680.911 4422854.526 1042.43
   LOCATION A0000033     AREA     675581.157 4422854.565 1043.23
   LOCATION A0000034     AREA     675481.403 4422854.604 1043.98
   LOCATION A0000035     AREA     675381.649 4422854.642 1044.38
   LOCATION A0000036     AREA     675281.896 4422854.681 1043.45
** End of LINE AREA Source ID = ARLN3
** ----------------------------------------------------------------
-------
** Line Source Represented by Area Sources
** LINE AREA Source ID = ARLN4
** DESCRSRC Y2_Main_Central
** PREFIX
** Length of Side = 10.50
** Ratio = 10
** Vertical Dimension = 0.00
** Emission Rate = 1.9374E-11
** Nodes = 13
** 675180.530, 4422843.700, 1042.61, 4.12
** 675203.840, 4422815.980, 1043.03, 4.12
```

```
** 675244.450, 4422757.080, 1045.06, 4.12
** 675257.310, 4422748.990, 1045.42, 4.12
** 675278.420, 4422748.260, 1045.56, 4.12
** 675481.640, 4422753.200, 1046.58, 4.12
** 675639.970, 4422753.040, 1045.64, 4.12
** 675832.220, 4422750.680, 1043.81, 4.12
** 675853.500, 4422751.890, 1043.55, 4.12
** 675879.480, 4422757.980, 1043.45, 4.12
** 675990.140, 4422815.960, 1040.82, 4.12
** 676030.090, 4422834.510, 1040.42, 4.12
** 676056.060, 4422847.180, 1040.17, 4.12
** ------------------------------------------------------------
-------
   LOCATION A0000037     AREA     675176.512 4422840.321 1042.54
   LOCATION A0000038     AREA     675199.518 4422813.000 1043.14
   LOCATION A0000039     AREA     675241.654 4422752.636 1045.18
   LOCATION A0000040     AREA     675257.129 4422743.743 1045.57
   LOCATION A0000041     AREA     675278.548 4422743.012 1045.68
   LOCATION A0000042     AREA     675380.158 4422745.482 1046.74
   LOCATION A0000043     AREA     675481.635 4422747.950 1046.79
   LOCATION A0000044     AREA     675560.800 4422747.870 1046.45
   LOCATION A0000045     AREA     675639.906 4422747.790 1045.99
   LOCATION A0000046     AREA     675736.031 4422746.610 1045.10
   LOCATION A0000047     AREA     675832.518 4422745.438 1044.08
   LOCATION A0000048     AREA     675854.698 4422746.779 1043.72
   LOCATION A0000049     AREA     675881.917 4422753.330 1043.34
   LOCATION A0000050     AREA     675937.247 4422782.320 1042.04
   LOCATION A0000051     AREA     675992.351 4422811.198 1040.85
   LOCATION A0000052     AREA     676032.392 4422829.792 1040.35
** End of LINE AREA Source ID = ARLN4
** Source Parameters **
   SRCPARAM PAREA1        2.21E-08     5.000         7
   AREAVERT PAREA1       675645.171 4422859.916 675645.741
4422952.467
   AREAVERT PAREA1       675604.204 4422951.815 675683.614
4423024.566
   AREAVERT PAREA1       675705.612 4423024.794 675711.995
4422973.145
   AREAVERT PAREA1       675711.099 4422858.744
** LINE AREA Source ID = ARLN1
   SRCPARAM A0000001     5.8183E-11     4.120    32.416    10.000
167.593
   SRCPARAM A0000002     5.8183E-11     4.120    37.499    10.000
179.345
   SRCPARAM A0000003     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000004     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000005     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000006     5.8183E-11     4.120    99.754
10.000  -179.978
```

```
   SRCPARAM A0000007     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000008     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000023     5.8183E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000024     5.8183E-11     4.120    99.754
10.000  -179.978
** ------------------------------------------------------------
-------
** LINE AREA Source ID = ARLN2
   SRCPARAM A0000009     2.7749E-11     4.120    36.215    10.500
49.950
   SRCPARAM A0000010     2.7749E-11     4.120    71.544    10.500
55.414
   SRCPARAM A0000011     2.7749E-11     4.120    15.200    10.500
32.179
   SRCPARAM A0000012     2.7749E-11     4.120    21.117    10.500
1.961
   SRCPARAM A0000013     2.7749E-11     4.120   101.643
10.500    -1.391
   SRCPARAM A0000014     2.7749E-11     4.120   101.643
10.500    -1.391
   SRCPARAM A0000015     2.7749E-11     4.120    79.164    10.500
0.057
   SRCPARAM A0000016     2.7749E-11     4.120    79.164    10.500
0.057
   SRCPARAM A0000017     2.7749E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000018     2.7749E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000019     2.7749E-11     4.120    21.316
10.500    -3.247
   SRCPARAM A0000020     2.7749E-11     4.120    26.677
10.500   -13.196
   SRCPARAM A0000021     2.7749E-11     4.120    62.468
10.500   -27.650
   SRCPARAM A0000022     2.7749E-11     4.120    62.468
10.500   -27.650
   SRCPARAM A0000025     2.7749E-11     4.120    44.050
10.500   -24.911
   SRCPARAM A0000026     2.7749E-11     4.120    28.894
10.500   -25.999
** ------------------------------------------------------------
-------
   SRCPARAM PAREA2        7.95E-08     5.000         7
   AREAVERT PAREA2       675645.170 4422859.920 675645.740
4422952.470
   AREAVERT PAREA2       675604.200 4422951.820 675683.610
4423024.570
   AREAVERT PAREA2       675705.610 4423024.790 675711.990
4422973.150
```

```
   AREAVERT PAREA2       675711.100 4422858.740
** LINE AREA Source ID = ARLN3
   SRCPARAM A0000027     4.0671E-11     4.120    32.406    10.000
167.598
   SRCPARAM A0000028     4.0671E-11     4.120    37.502    10.000
179.343
   SRCPARAM A0000029     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000030     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000031     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000032     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000033     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000034     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000035     4.0671E-11     4.120    99.754
10.000  -179.978
   SRCPARAM A0000036     4.0671E-11     4.120    99.754
10.000  -179.978
** ------------------------------------------------------------
-------
** LINE AREA Source ID = ARLN4
   SRCPARAM A0000037     1.9374E-11     4.120    36.218    10.500
49.939
   SRCPARAM A0000038     1.9374E-11     4.120    71.543    10.500
55.415
   SRCPARAM A0000039     1.9374E-11     4.120    15.193    10.500
32.173
   SRCPARAM A0000040     1.9374E-11     4.120    21.123    10.500
1.981
   SRCPARAM A0000041     1.9374E-11     4.120   101.640
10.500    -1.393
   SRCPARAM A0000042     1.9374E-11     4.120   101.640
10.500    -1.393
   SRCPARAM A0000043     1.9374E-11     4.120    79.165    10.500
0.058
   SRCPARAM A0000044     1.9374E-11     4.120    79.165    10.500
0.058
   SRCPARAM A0000045     1.9374E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000046     1.9374E-11     4.120    96.132    10.500
0.703
   SRCPARAM A0000047     1.9374E-11     4.120    21.314
10.500    -3.254
   SRCPARAM A0000048     1.9374E-11     4.120    26.684
10.500   -13.193
   SRCPARAM A0000049     1.9374E-11     4.120    62.465
10.500   -27.652
   SRCPARAM A0000050     1.9374E-11     4.120    62.465
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10.500   -27.652
   SRCPARAM A0000051     1.9374E-11     4.120    44.047
10.500   -24.907
   SRCPARAM A0000052     1.9374E-11     4.120    28.896
10.500   -26.006
** ------------------------------------------------------------
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   URBANSRC ALL

** Variable Emissions Type: "By Hour / Seven Days (HRDOW7)"
** Variable Emission Scenario: "ALL"
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT PAREA1       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT PAREA1       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
   EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
   EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
   EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000001     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000002     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000003     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000004     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000005     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000006     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000007     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000008     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000023     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000024     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000001     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000002     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000003     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000004     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000005     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000006     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000007     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000008     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000023     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000024     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000014     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000012     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000012     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000015     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000016     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000009     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000010     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000011     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000013     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000016     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000018     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000019     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000020     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000021     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000022     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000025     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000026     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000009     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000010     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000011     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000012     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000013     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000014     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000015     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000016     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000017     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000018     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000019     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000020     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000021     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000022     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000025     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000026     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT PAREA2       HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT PAREA2       HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000028     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000028     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000029     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000029     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000030     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000030     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000031     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000031     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000031     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000032     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000033     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000033     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000034     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000034     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000035     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000035     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000035     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000036     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000036     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000036     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000027     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000028     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000032     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000029     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000027     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000028     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000029     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000030     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000033     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000034     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000038     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000039     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000043     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000044     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000045     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000037     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
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EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.0
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EMISFACT A0000048     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
EMISFACT A0000049     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000051     HRDOW7 1.0 1.0 1.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
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EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
```

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EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000037     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000038     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000039     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000040     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000041     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000042     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000043     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000044     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000045     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000046     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000047     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000048     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000049     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000050     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000051     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
```

```
   EMISFACT A0000052     HRDOW7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
   SRCGROUP Y1_ALL   PAREA1 A0000001 A0000002 A0000003 A0000004
A0000005
   SRCGROUP Y1_ALL   A0000006 A0000007 A0000008 A0000023 A0000024
A0000009
   SRCGROUP Y1_ALL   A0000010 A0000011 A0000012 A0000013 A0000014
A0000015
   SRCGROUP Y1_ALL   A0000016 A0000017 A0000018 A0000019 A0000020
A0000021
   SRCGROUP Y1_ALL   A0000022 A0000025 A0000026
   SRCGROUP Y1_ON    PAREA1
   SRCGROUP Y1_OFF   A0000001 A0000002 A0000003 A0000004 A0000005
A0000006
   SRCGROUP Y1_OFF   A0000007 A0000008 A0000023 A0000024 A0000009
A0000010
   SRCGROUP Y1_OFF   A0000011 A0000012 A0000013 A0000014 A0000015
A0000016
   SRCGROUP Y1_OFF   A0000017 A0000018 A0000019 A0000020 A0000021
A0000022
   SRCGROUP Y1_OFF   A0000025 A0000026
   SRCGROUP Y2_ALL   PAREA2 A0000027 A0000028 A0000029 A0000030
A0000031
   SRCGROUP Y2_ALL   A0000032 A0000033 A0000034 A0000035 A0000036
A0000037
   SRCGROUP Y2_ALL   A0000038 A0000039 A0000040 A0000041 A0000042
A0000043
   SRCGROUP Y2_ALL   A0000044 A0000045 A0000046 A0000047 A0000048
A0000049
   SRCGROUP Y2_ALL   A0000050 A0000051 A0000052
   SRCGROUP Y2_ON    PAREA2
   SRCGROUP Y2_OFF   A0000027 A0000028 A0000029 A0000030 A0000031
A0000032
   SRCGROUP Y2_OFF   A0000033 A0000034 A0000035 A0000036 A0000037
A0000038
   SRCGROUP Y2_OFF   A0000039 A0000040 A0000041 A0000042 A0000043
A0000044
   SRCGROUP Y2_OFF   A0000045 A0000046 A0000047 A0000048 A0000049
A0000050
   SRCGROUP Y2_OFF   A0000051 A0000052
SO FINISHED
**
****************************************
** AERMOD Receptor Pathway
****************************************
**
**
RE STARTING
   INCLUDED Quincy_Courthouse_Construction_Mitigated_20251210.rou
RE FINISHED
**
****************************************
** AERMOD Meteorology Pathway
```

```
**************************************
**
**
ME STARTING
   SURFFILE "Z:\Shared\San Jose\Env\16230_13 New Quincy
Courthouse EIR\Project Data\ACES\MET\KBLU_725845_23225\KBLU_
725845_23225\KBLU_2014-2016_2018_2019_ADJU.SFC"
   PROFFILE "Z:\Shared\San Jose\Env\16230_13 New Quincy
Courthouse EIR\Project Data\ACES\MET\KBLU_725845_23225\KBLU_
725845_23225\KBLU_2014-2016_2018_2019_ADJU.PFL"
   SURFDATA 23225 2014 Blue_Canyon_NYACK_Airport
   UAIRDATA 23230 2014 OAKLAND/WSO_AP
   PROFBASE 1608.1 METERS
ME FINISHED
**
**************************************
** AERMOD Output Pathway
**************************************
**
**
OU STARTING
** Auto-Generated Plotfiles
   PLOTFILE PERIOD Y1_ALL
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G001.PLT
31
   PLOTFILE PERIOD Y1_ON
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G002.PLT
32
   PLOTFILE PERIOD Y1_OFF
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G003.PLT
33
   PLOTFILE PERIOD Y2_ALL
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G004.PLT
34
   PLOTFILE PERIOD Y2_ON
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G005.PLT
35
   PLOTFILE PERIOD Y2_OFF
QUINCY_COURTHOUSE_CONSTRUCTION_MITIGATED_20251210.AD\PE00G006.PLT
36
   SUMMFILE Quincy_Courthouse_Construction_Mitigated_20251210.sum
OU FINISHED


  *** Message Summary For AERMOD Model Setup ***

  --------- Summary of Total Messages --------

 A Total of            0 Fatal Error Message(s)
 A Total of            2 Warning Message(s)
 A Total of            0 Informational Message(s)
```

```
    ******** FATAL ERROR MESSAGES ********
                ***  NONE  ***


    ********   WARNING MESSAGES   ********
 ME W186    1427       MEOPEN: THRESH_1MIN 1-min ASOS wind speed
threshold used           0.50
 ME W187    1427       MEOPEN: ADJ_U* Option for Stable Low Winds
used in AERMET

 ***********************************
 *** SETUP Finishes Successfully ***
 ***********************************
```

```
 *** AERMOD - VERSION 23132  ***   *** C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208\Q ***
12/16/25
 *** AERMET - VERSION  19191 ***   ***
***        11:10:26

PAGE   1
 *** MODELOPTs:    RegDFAULT  CONC  ELEV  URBAN  ADJ_U*

                                              ***     MODEL SETUP
OPTIONS SUMMARY       ***
 - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -
- - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -

 ** Model Options Selected:
      * Model Uses Regulatory DEFAULT Options
      * Model Is Setup For Calculation of Average CONCentration
Values.
      * NO GAS DEPOSITION Data Provided.
      * NO PARTICLE DEPOSITION Data Provided.
      * Model Uses NO DRY DEPLETION. DDPLETE  =  F
      * Model Uses NO WET DEPLETION. WETDPLT  =  F
      * Stack-tip Downwash.
      * Model Accounts for ELEVated Terrain Effects.
      * Use Calms Processing Routine.
      * Use Missing Data Processing Routine.
      * No Exponential Decay.
      * Model Uses URBAN Dispersion Algorithm for the SBL for
54 Source(s),
        for Total of    1 Urban Area(s):
   Urban Population =     22000.0 ;  Urban Roughness Length =
1.000 m
      * Urban Roughness Length of 1.0 Meter Used.
      * ADJ_U*   - Use ADJ_U* option for SBL in AERMET
      * CCVR_Sub - Meteorological data includes CCVR
substitutions
      * TEMP_Sub - Meteorological data includes TEMP
substitutions
      * Model Assumes No FLAGPOLE Receptor Heights.
      * The User Specified a Pollutant Type of: PM_2.5

 **Model Calculates PERIOD Averages Only

 **This Run Includes:     54 Source(s);       6 Source Group(s);
and     265 Receptor(s)

                with:      0 POINT(s), including
                           0 POINTCAP(s) and      0 POINTHOR(s)
                 and:      0 VOLUME source(s)
                 and:     54 AREA type source(s)
                 and:      0 LINE source(s)
                 and:      0 RLINE/RLINEXT source(s)
```

```
                and:      0 OPENPIT source(s)
                and:      0 BUOYANT LINE source(s) with a total
of     0 line(s)
                and:      0 SWPOINT source(s)


 **Model Set To Continue RUNning After the Setup Testing.

 **The AERMET Input Meteorological Data Version Date:  19191

 **Output Options Selected:
         Model Outputs Tables of PERIOD Averages by Receptor
         Model Outputs External File(s) of High Values for
Plotting (PLOTFILE Keyword)
         Model Outputs Separate Summary File of High Ranked
Values (SUMMFILE Keyword)

 **NOTE:  The Following Flags May Appear Following CONC Values:
c for Calm Hours

m for Missing Hours

b for Both Calm and Missing Hours

 **Misc. Inputs:  Base Elev. for Pot. Temp. Profile (m MSL) =
1608.10 ;  Decay Coef. =    0.000     ;  Rot. Angle =     0.0
                 Emission Units =
GRAMS/SEC                                ;  Emission Rate Unit
Factor =   0.10000E+07
                 Output Units   = MICROGRAMS/M**3

 **Approximate Storage Requirements of Model =      3.7 MB of
RAM.

 **Input Runstream File:          aermod.inp
 **Output Print File:             aermod.out

 **Detailed Error/Message File:
Quincy_Courthouse_Construction_Mitigated_20251210.err
 **File for Summary of Results:
Quincy_Courthouse_Construction_Mitigated_20251210.sum
```

*** AREA SOURCE DATA ***

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (GRAMS/SEC /METER**2)	X COORD (SW CORNER) (METERS)	Y COORD (SW CORNER) (METERS)	BASE ELEV. (METERS)	RELEASE HEIGHT (METERS)	X-DIM OF AREA (METERS)	Y-DIM OF AREA (METERS)	ORIENT. OF AREA (DEG.)	INIT. SZ (METERS)	URBAN SOURCE	EMISSION RATE SCALAR VARY BY	AIRCRAFT
A0000001	0	0.58183E-10	676048.3	4422861.7	1040.0	4.12	32.42	10.00	167.59	0.00	YES	HRDOW7	NO
A0000002	0	0.58183E-10	676017.6	4422854.8	1040.3	4.12	37.50	10.00	179.34	0.00	YES	HRDOW7	NO
A0000003	0	0.58183E-10	675980.2	4422854.4	1040.6	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000004	0	0.58183E-10	675880.4	4422854.4	1041.6	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000005	0	0.58183E-10	675780.7	4422854.5	1042.3	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000006	0	0.58183E-10	675680.9	4422854.5	1042.4	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000007	0	0.58183E-10	675581.2	4422854.6	1043.2	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000008	0	0.58183E-10	675481.4	4422854.6	1044.0	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO
A0000023	0	0.58183E-10	675381.6	4422854.6	1044.4	4.12	99.75	10.00	-179.98	0.00	YES	HRDOW7	NO

```
 A0000024         0   0.58183E-10  675281.9 4422854.7  1043.5
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000009         0   0.27749E-10  675176.5 4422840.3  1042.5
4.12     36.22     10.50     49.95     0.00     YES   HRDOW7
NO
 A0000010         0   0.27749E-10  675199.5 4422813.0  1043.1
4.12     71.54     10.50     55.41     0.00     YES   HRDOW7
NO
 A0000011         0   0.27749E-10  675241.7 4422752.6  1045.2
4.12     15.20     10.50     32.18     0.00     YES   HRDOW7
NO
 A0000012         0   0.27749E-10  675257.1 4422743.7  1045.6
4.12     21.12     10.50      1.96     0.00     YES   HRDOW7
NO
 A0000013         0   0.27749E-10  675278.5 4422743.0  1045.7
4.12    101.64     10.50     -1.39     0.00     YES   HRDOW7
NO
 A0000014         0   0.27749E-10  675380.2 4422745.5  1046.7
4.12    101.64     10.50     -1.39     0.00     YES   HRDOW7
NO
 A0000015         0   0.27749E-10  675481.6 4422747.9  1046.8
4.12     79.16     10.50      0.06     0.00     YES   HRDOW7
NO
 A0000016         0   0.27749E-10  675560.8 4422747.9  1046.5
4.12     79.16     10.50      0.06     0.00     YES   HRDOW7
NO
 A0000017         0   0.27749E-10  675639.9 4422747.8  1046.0
4.12     96.13     10.50      0.70     0.00     YES   HRDOW7
NO
 A0000018         0   0.27749E-10  675736.0 4422746.6  1045.1
4.12     96.13     10.50      0.70     0.00     YES   HRDOW7
NO
 A0000019         0   0.27749E-10  675832.5 4422745.4  1044.1
4.12     21.32     10.50     -3.25     0.00     YES   HRDOW7
NO
 A0000020         0   0.27749E-10  675854.7 4422746.8  1043.7
4.12     26.68     10.50    -13.20     0.00     YES   HRDOW7
NO
 A0000021         0   0.27749E-10  675881.9 4422753.3  1043.3
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000022         0   0.27749E-10  675937.2 4422782.3  1042.0
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000025         0   0.27749E-10  675992.4 4422811.2  1040.8
4.12     44.05     10.50    -24.91     0.00     YES   HRDOW7
NO
 A0000026         0   0.27749E-10  676032.4 4422829.8  1040.3
4.12     28.89     10.50    -26.00     0.00     YES   HRDOW7
NO
 A0000027         0   0.40671E-10  676048.2 4422861.7  1040.0
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4.12     32.41     10.00    167.60     0.00     YES   HRDOW7
NO
 A0000028         0   0.40671E-10  676017.6 4422854.8  1040.3
4.12     37.50     10.00    179.34     0.00     YES   HRDOW7
NO
 A0000029         0   0.40671E-10  675980.2 4422854.4  1040.6
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000030         0   0.40671E-10  675880.4 4422854.4  1041.6
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000031         0   0.40671E-10  675780.7 4422854.5  1042.3
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000032         0   0.40671E-10  675680.9 4422854.5  1042.4
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000033         0   0.40671E-10  675581.2 4422854.6  1043.2
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000034         0   0.40671E-10  675481.4 4422854.6  1044.0
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000035         0   0.40671E-10  675381.6 4422854.6  1044.4
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000036         0   0.40671E-10  675281.9 4422854.7  1043.5
4.12     99.75     10.00   -179.98     0.00     YES   HRDOW7
NO
 A0000037         0   0.19374E-10  675176.5 4422840.3  1042.5
4.12     36.22     10.50     49.94     0.00     YES   HRDOW7
NO
 A0000038         0   0.19374E-10  675199.5 4422813.0  1043.1
4.12     71.54     10.50     55.41     0.00     YES   HRDOW7
NO
 A0000039         0   0.19374E-10  675241.7 4422752.6  1045.2
4.12     15.19     10.50     32.17     0.00     YES   HRDOW7
NO
 A0000040         0   0.19374E-10  675257.1 4422743.7  1045.6
4.12     21.12     10.50      1.98     0.00     YES   HRDOW7
NO
```

*** AREA SOURCE DATA ***

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (GRAMS/SEC /METER**2)	COORD (SW CORNER) X (METERS)	Y (METERS)	BASE ELEV. (METERS)	RELEASE HEIGHT (METERS)	X-DIM OF AREA (METERS)	Y-DIM OF AREA (METERS)	ORIENT. OF AREA (DEG.)	INIT. SZ (METERS)	URBAN SOURCE	EMISSION RATE SCALAR VARY BY	AIRCRAFT
A0000041	0	0.19374E-10	675278.5	4422743.0	1045.7	4.12	101.64	10.50	-1.39	0.00	YES	HRDOW7	NO
A0000042	0	0.19374E-10	675380.2	4422745.5	1046.7	4.12	101.64	10.50	-1.39	0.00	YES	HRDOW7	NO
A0000043	0	0.19374E-10	675481.6	4422748.0	1046.8	4.12	79.16	10.50	0.06	0.00	YES	HRDOW7	NO
A0000044	0	0.19374E-10	675560.8	4422747.9	1046.5	4.12	79.16	10.50	0.06	0.00	YES	HRDOW7	NO
A0000045	0	0.19374E-10	675639.9	4422747.8	1046.0	4.12	96.13	10.50	0.70	0.00	YES	HRDOW7	NO
A0000046	0	0.19374E-10	675736.0	4422746.6	1045.1	4.12	96.13	10.50	0.70	0.00	YES	HRDOW7	NO
A0000047	0	0.19374E-10	675832.5	4422745.4	1044.1	4.12	21.31	10.50	-3.25	0.00	YES	HRDOW7	NO
A0000048	0	0.19374E-10	675854.7	4422746.8	1043.7	4.12	26.68	10.50	-13.19	0.00	YES	HRDOW7	NO
A0000049	0	0.19374E-10	675881.9	4422753.3	1043.3	4.12	62.47	10.50	-27.65	0.00	YES	HRDOW7	NO

```
 A0000050          0   0.19374E-10  675937.2 4422782.3  1042.0
4.12     62.47     10.50    -27.65     0.00     YES   HRDOW7
NO
 A0000051          0   0.19374E-10  675992.4 4422811.2  1040.8
4.12     44.05     10.50    -24.91     0.00     YES   HRDOW7
NO
 A0000052          0   0.19374E-10  676032.4 4422829.8  1040.3
4.12     28.90     10.50    -26.01     0.00     YES   HRDOW7
NO
```

*** AREAPOLY SOURCE DATA ***

RELEASE HEIGHT (METERS)	NUMBER OF VERTS.	EMISSION RATE INIT. SZ (METERS)	URBAN SOURCE	LOCATION OF AREA EMISSION RATE X (METERS)	Y (METERS)	BASE ELEV. (METERS)	AIRCRAFT
PAREA1 5.00	7	0 0.22100E-07 0.00	YES	675645.2	4422859.9	1042.4	NO
PAREA2 5.00	7	0 0.79500E-07 0.00	YES	675645.2	4422859.9	1042.4	NO

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** SOURCE IDs DEFINING SOURCE GROUPS ***

SRCGROUP ID	SOURCE IDs
Y1_ALL	PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 ,
	A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 ,
	A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 ,
	A0000022 , A0000025 , A0000026 ,
Y1_ON	PAREA1 ,
Y1_OFF	A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 , A0000008 ,
	A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 , A0000014 ,
	A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 , A0000022 ,
	A0000025 , A0000026 ,
Y2_ALL	PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 , A0000031 , A0000032 , A0000033 ,

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             A0000034    , A0000035    , A0000036    ,
A0000037    , A0000038    , A0000039    , A0000040    ,
A0000041    ,

             A0000042    , A0000043    , A0000044    ,
A0000045    , A0000046    , A0000047    , A0000048    ,
A0000049    ,

             A0000050    , A0000051    , A0000052    ,

  Y2_ON      PAREA2      ,

  Y2_OFF     A0000027    , A0000028    , A0000029    ,
A0000030    , A0000031    , A0000032    , A0000033    ,
A0000034    ,

             A0000035    , A0000036    , A0000037    ,
A0000038    , A0000039    , A0000040    , A0000041    ,
A0000042    ,

             A0000043    , A0000044    , A0000045    ,
A0000046    , A0000047    , A0000048    , A0000049    ,
A0000050    ,

             A0000051    , A0000052    ,
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** SOURCE IDs DEFINED AS URBAN SOURCES ***

URBAN ID	URBAN POP	SOURCE IDs
	22000.	PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 , A0000005 , A0000006 , A0000007 ,
		A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 , A0000012 , A0000013 ,
		A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 , A0000020 , A0000021 ,
		A0000022 , A0000025 , A0000026 , PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
		A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
		A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
		A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = PAREA1 ; SOURCE TYPE = AREAPOLY :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000001 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000002 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000003 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000004 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000005 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000006 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000007 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000008 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000023 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000024 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000009 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000010 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000011 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000012 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000013 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000014 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000015 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000016 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000017 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000018 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000019 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000020 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000021 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000022 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000025 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000026 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = PAREA2 ; SOURCE TYPE = AREAPOLY :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000027 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000028 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000029 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000030 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000031 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000032 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000033 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000034 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000035 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000036 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000037 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000038 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000039 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000040 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000041 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000042 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000043 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000044 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = MONDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = TUESDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = WEDNESDY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = THURSDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00

DAY OF WEEK = FRIDAY

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000045 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000046 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                 DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                 DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000047 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

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5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000048 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000049 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
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*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000050 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000051 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

* SOURCE EMISSION RATE SCALARS WHICH VARY DIURNALLY AND BY DAY OF WEEK (HRDOW7) *

SOURCE ID = A0000052 ; SOURCE TYPE = AREA :

HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR	HOUR	SCALAR
DAY OF WEEK = MONDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = TUESDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = WEDNESDY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = THURSDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00	5	.0000E+00	6	.0000E+00	7	.0000E+00	8	.1000E+01
9	.1000E+01	10	.1000E+01	11	.1000E+01	12	.1000E+01	13	.1000E+01	14	.1000E+01	15	.1000E+01	16	.1000E+01
17	.1000E+01	18	.1000E+01	19	.1000E+01	20	.0000E+00	21	.0000E+00	22	.0000E+00	23	.0000E+00	24	.0000E+00
DAY OF WEEK = FRIDAY															
1	.0000E+00	2	.0000E+00	3	.0000E+00	4	.0000E+00								

```
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .1000E+01
    9  .1000E+01   10  .1000E+01   11  .1000E+01   12  .1000E+01
13  .1000E+01   14  .1000E+01   15  .1000E+01   16  .1000E+01
   17  .1000E+01   18  .1000E+01   19  .1000E+01   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SATURDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
                                                DAY OF WEEK =
SUNDAY
    1  .0000E+00    2  .0000E+00    3  .0000E+00    4  .0000E+00
5  .0000E+00    6  .0000E+00    7  .0000E+00    8  .0000E+00
    9  .0000E+00   10  .0000E+00   11  .0000E+00   12  .0000E+00
13  .0000E+00   14  .0000E+00   15  .0000E+00   16  .0000E+00
   17  .0000E+00   18  .0000E+00   19  .0000E+00   20  .0000E+00
21  .0000E+00   22  .0000E+00   23  .0000E+00   24  .0000E+00
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675133.1, 4422610.1, 1051.9, 2131.6, 0.0);
(675208.1, 4422610.1, 1051.3, 2131.6, 0.0);
(675283.1, 4422610.1, 1050.7, 2131.6, 0.0);
(675358.1, 4422610.1, 1050.6, 2131.6, 0.0);
(675433.1, 4422610.1, 1050.8, 2131.6, 0.0);
(675508.1, 4422610.1, 1051.0, 2131.6, 0.0);
(675583.1, 4422610.1, 1051.4, 2131.6, 0.0);
(675658.1, 4422610.1, 1050.3, 2131.6, 0.0);
(675733.1, 4422610.1, 1048.8, 2131.6, 0.0);
(675808.1, 4422610.1, 1047.3, 2131.6, 0.0);
(675883.1, 4422610.1, 1045.5, 2131.6, 0.0);
(675958.1, 4422610.1, 1043.3, 2131.6, 0.0);
(676033.1, 4422610.1, 1042.3, 2131.6, 0.0);
(676108.1, 4422610.1, 1042.4, 2131.6, 0.0);
(675133.1, 4422660.1, 1048.4, 2131.6, 0.0);
(675208.1, 4422660.1, 1048.5, 2131.6, 0.0);
(675283.1, 4422660.1, 1048.7, 2131.6, 0.0);
(675358.1, 4422660.1, 1048.9, 2131.6, 0.0);
(675433.1, 4422660.1, 1049.2, 2131.6, 0.0);
(675508.1, 4422660.1, 1049.4, 2131.6, 0.0);
(675583.1, 4422660.1, 1049.4, 2131.6, 0.0);
(675658.1, 4422660.1, 1048.2, 2131.6, 0.0);
(675733.1, 4422660.1, 1047.3, 2131.6, 0.0);
(675808.1, 4422660.1, 1046.4, 2131.6, 0.0);
(675883.1, 4422660.1, 1044.4, 2131.6, 0.0);
(675958.1, 4422660.1, 1042.7, 2131.6, 0.0);
(676033.1, 4422660.1, 1041.4, 2131.6, 0.0);
(676108.1, 4422660.1, 1040.7, 2131.6, 0.0);
(675133.1, 4422710.1, 1045.6, 2131.6, 0.0);
(675208.1, 4422710.1, 1046.4, 2131.6, 0.0);
(675283.1, 4422710.1, 1046.8, 2131.6, 0.0);
(675358.1, 4422710.1, 1047.5, 2131.6, 0.0);
(675433.1, 4422710.1, 1047.7, 2131.6, 0.0);
(675508.1, 4422710.1, 1047.9, 2131.6, 0.0);
(675583.1, 4422710.1, 1047.6, 2131.6, 0.0);
(675658.1, 4422710.1, 1046.7, 2131.6, 0.0);

```
     ( 675733.1, 4422710.1,    1046.2,    2131.6,       0.0);
( 675808.1, 4422710.1,    1045.2,    2131.6,       0.0);
     ( 675883.1, 4422710.1,    1044.2,    2131.6,       0.0);
( 675958.1, 4422710.1,    1042.3,    2131.6,       0.0);
     ( 676033.1, 4422710.1,    1041.1,    2131.6,       0.0);
( 676108.1, 4422710.1,    1040.5,    2131.6,       0.0);
     ( 675133.1, 4422760.1,    1044.4,    2131.6,       0.0);
( 675208.1, 4422760.1,    1045.0,    2131.6,       0.0);
     ( 675283.1, 4422760.1,    1045.3,    2131.6,       0.0);
( 675358.1, 4422760.1,    1046.4,    2131.6,       0.0);
     ( 675433.1, 4422760.1,    1046.5,    2131.6,       0.0);
( 675508.1, 4422760.1,    1046.4,    2131.6,       0.0);
     ( 675583.1, 4422760.1,    1045.9,    2131.6,       0.0);
( 675658.1, 4422760.1,    1045.2,    2131.6,       0.0);
     ( 675733.1, 4422760.1,    1044.8,    2131.6,       0.0);
( 675808.1, 4422760.1,    1043.9,    2131.6,       0.0);
     ( 675883.1, 4422760.1,    1043.1,    2131.6,       0.0);
( 675958.1, 4422760.1,    1042.1,    2131.6,       0.0);
     ( 676033.1, 4422760.1,    1040.8,    2131.6,       0.0);
( 676108.1, 4422760.1,    1040.2,    2131.6,       0.0);
     ( 675133.1, 4422810.1,    1043.0,    2131.6,       0.0);
( 675208.1, 4422810.1,    1043.2,    2131.6,       0.0);
     ( 675283.1, 4422810.1,    1044.2,    2131.6,       0.0);
( 675358.1, 4422810.1,    1045.1,    2131.6,       0.0);
     ( 675433.1, 4422810.1,    1045.2,    2131.6,       0.0);
( 675508.1, 4422810.1,    1044.9,    2131.6,       0.0);
     ( 675583.1, 4422810.1,    1044.2,    2131.6,       0.0);
( 675658.1, 4422810.1,    1043.5,    2131.6,       0.0);
     ( 675733.1, 4422810.1,    1043.9,    2131.6,       0.0);
( 675808.1, 4422810.1,    1043.2,    2131.6,       0.0);
     ( 675883.1, 4422810.1,    1042.2,    2131.6,       0.0);
( 675958.1, 4422810.1,    1041.3,    2131.6,       0.0);
     ( 676033.1, 4422810.1,    1040.2,    2131.6,       0.0);
( 676108.1, 4422810.1,    1039.8,    2131.6,       0.0);
     ( 675133.1, 4422860.1,    1042.0,    2131.6,       0.0);
( 675208.1, 4422860.1,    1042.6,    2131.6,       0.0);
     ( 675283.1, 4422860.1,    1043.4,    2131.6,       0.0);
( 675358.1, 4422860.1,    1044.0,    2131.6,       0.0);
     ( 675433.1, 4422860.1,    1044.2,    2131.6,       0.0);
( 675508.1, 4422860.1,    1043.7,    2131.6,       0.0);
     ( 675583.1, 4422860.1,    1043.1,    2131.6,       0.0);
( 675733.1, 4422860.1,    1042.6,    2131.6,       0.0);
     ( 675808.1, 4422860.1,    1042.1,    2131.6,       0.0);
( 675883.1, 4422860.1,    1041.5,    2131.6,       0.0);
     ( 675958.1, 4422860.1,    1040.9,    2131.6,       0.0);
( 676033.1, 4422860.1,    1040.1,    2131.6,       0.0);
     ( 676108.1, 4422860.1,    1039.7,    2131.6,       0.0);
( 675133.1, 4422910.1,    1041.7,    2131.6,       0.0);
     ( 675208.1, 4422910.1,    1042.7,    2131.6,       0.0);
( 675283.1, 4422910.1,    1042.5,    2131.6,       0.0);
     ( 675358.1, 4422910.1,    1042.8,    2131.6,       0.0);
( 675433.1, 4422910.1,    1043.0,    2131.6,       0.0);
```

```
     ( 675508.1, 4422910.1,    1042.5,    2131.6,       0.0);
( 675583.1, 4422910.1,    1041.9,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675733.1, 4422910.1, 1041.4, 2131.6, 0.0);
(675808.1, 4422910.1, 1040.9, 2131.6, 0.0);
(675883.1, 4422910.1, 1040.7, 2131.6, 0.0);
(675958.1, 4422910.1, 1040.3, 2131.6, 0.0);
(676033.1, 4422910.1, 1039.5, 2131.6, 0.0);
(676108.1, 4422910.1, 1039.5, 2131.6, 0.0);
(675133.1, 4422960.1, 1041.2, 2131.6, 0.0);
(675208.1, 4422960.1, 1041.2, 2131.6, 0.0);
(675283.1, 4422960.1, 1041.7, 2131.6, 0.0);
(675358.1, 4422960.1, 1041.9, 2131.6, 0.0);
(675433.1, 4422960.1, 1042.1, 2131.6, 0.0);
(675508.1, 4422960.1, 1041.5, 2131.6, 0.0);
(675583.1, 4422960.1, 1040.9, 2131.6, 0.0);
(675733.1, 4422960.1, 1040.5, 2131.6, 0.0);
(675808.1, 4422960.1, 1039.8, 2131.6, 0.0);
(675883.1, 4422960.1, 1039.8, 2131.6, 0.0);
(675958.1, 4422960.1, 1039.5, 2131.6, 0.0);
(676033.1, 4422960.1, 1039.0, 2131.6, 0.0);
(676108.1, 4422960.1, 1039.0, 2131.6, 0.0);
(675133.1, 4423010.1, 1040.8, 2131.6, 0.0);
(675208.1, 4423010.1, 1040.8, 2131.6, 0.0);
(675283.1, 4423010.1, 1041.0, 2131.6, 0.0);
(675358.1, 4423010.1, 1041.2, 2131.6, 0.0);
(675433.1, 4423010.1, 1041.1, 2131.6, 0.0);
(675508.1, 4423010.1, 1040.9, 2131.6, 0.0);
(675583.1, 4423010.1, 1040.4, 2131.6, 0.0);
(675658.1, 4423010.1, 1040.0, 2131.6, 0.0);
(675733.1, 4423010.1, 1039.8, 2131.6, 0.0);
(675808.1, 4423010.1, 1039.2, 2131.6, 0.0);
(675883.1, 4423010.1, 1039.6, 2131.6, 0.0);
(675958.1, 4423010.1, 1039.1, 2131.6, 0.0);
(676033.1, 4423010.1, 1038.8, 2131.6, 0.0);
(676108.1, 4423010.1, 1038.8, 2131.6, 0.0);
(675133.1, 4423060.1, 1041.5, 2131.6, 0.0);
(675208.1, 4423060.1, 1042.0, 2131.6, 0.0);
(675283.1, 4423060.1, 1042.3, 2131.6, 0.0);

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     ( 675358.1, 4423060.1,    1041.0,    2131.6,       0.0);
( 675433.1, 4423060.1,    1040.1,    2131.6,       0.0);
     ( 675508.1, 4423060.1,    1039.8,    2131.6,       0.0);
( 675583.1, 4423060.1,    1039.5,    2131.6,       0.0);
     ( 675658.1, 4423060.1,    1040.3,    2131.6,       0.0);
( 675733.1, 4423060.1,    1039.5,    2131.6,       0.0);
     ( 675808.1, 4423060.1,    1038.8,    2131.6,       0.0);
( 675883.1, 4423060.1,    1038.5,    2131.6,       0.0);
     ( 675958.1, 4423060.1,    1038.5,    2131.6,       0.0);
( 676033.1, 4423060.1,    1038.3,    2131.6,       0.0);
     ( 676108.1, 4423060.1,    1038.4,    2131.6,       0.0);
( 675133.1, 4423110.1,    1041.4,    2131.6,       0.0);
     ( 675208.1, 4423110.1,    1041.3,    2131.6,       0.0);
( 675283.1, 4423110.1,    1041.9,    2131.6,       0.0);
     ( 675358.1, 4423110.1,    1041.7,    2131.6,       0.0);
( 675433.1, 4423110.1,    1039.6,    2131.6,       0.0);
     ( 675508.1, 4423110.1,    1039.7,    2131.6,       0.0);
( 675583.1, 4423110.1,    1039.4,    2131.6,       0.0);
     ( 675658.1, 4423110.1,    1039.1,    2131.6,       0.0);
( 675733.1, 4423110.1,    1039.0,    2131.6,       0.0);
     ( 675808.1, 4423110.1,    1038.9,    2131.6,       0.0);
( 675883.1, 4423110.1,    1038.5,    2131.6,       0.0);
     ( 675958.1, 4423110.1,    1038.3,    2131.6,       0.0);
( 676033.1, 4423110.1,    1038.0,    2131.6,       0.0);
     ( 676108.1, 4423110.1,    1038.2,    2131.6,       0.0);
( 675544.6, 4422816.8,    1044.4,    2131.6,       0.0);
     ( 675569.6, 4422816.8,    1044.0,    2131.6,       0.0);
( 675594.6, 4422816.8,    1044.0,    2131.6,       0.0);
     ( 675619.6, 4422816.8,    1043.8,    2131.6,       0.0);
( 675644.6, 4422816.8,    1043.5,    2131.6,       0.0);
     ( 675669.6, 4422816.8,    1043.1,    2131.6,       0.0);
( 675694.6, 4422816.8,    1042.9,    2131.6,       0.0);
     ( 675719.6, 4422816.8,    1043.6,    2131.6,       0.0);
( 675744.6, 4422816.8,    1043.6,    2131.6,       0.0);
     ( 675769.6, 4422816.8,    1043.2,    2131.6,       0.0);
( 675794.6, 4422816.8,    1043.0,    2131.6,       0.0);
     ( 675544.6, 4422841.8,    1043.8,    2131.6,       0.0);
( 675569.6, 4422841.8,    1043.6,    2131.6,       0.0);
     ( 675594.6, 4422841.8,    1043.2,    2131.6,       0.0);
( 675619.6, 4422841.8,    1043.0,    2131.6,       0.0);
     ( 675644.6, 4422841.8,    1042.8,    2131.6,       0.0);
( 675669.6, 4422841.8,    1042.6,    2131.6,       0.0);
     ( 675694.6, 4422841.8,    1042.8,    2131.6,       0.0);
( 675719.6, 4422841.8,    1042.8,    2131.6,       0.0);
     ( 675744.6, 4422841.8,    1042.7,    2131.6,       0.0);
( 675769.6, 4422841.8,    1042.5,    2131.6,       0.0);
     ( 675794.6, 4422841.8,    1042.4,    2131.6,       0.0);
( 675544.6, 4422866.8,    1043.4,    2131.6,       0.0);
     ( 675569.6, 4422866.8,    1043.1,    2131.6,       0.0);
( 675594.6, 4422866.8,    1042.8,    2131.6,       0.0);
     ( 675619.6, 4422866.8,    1042.4,    2131.6,       0.0);
( 675644.6, 4422866.8,    1042.3,    2131.6,       0.0);
```

```
     ( 675719.6, 4422866.8,    1042.3,    2131.6,       0.0);
( 675744.6, 4422866.8,    1042.3,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** DISCRETE CARTESIAN RECEPTORS ***
(X-COORD, Y-COORD, ZELEV, ZHILL, ZFLAG)

(METERS)

(675769.6, 4422866.8, 1042.0, 2131.6, 0.0);
(675794.6, 4422866.8, 1042.1, 2131.6, 0.0);
(675544.6, 4422891.8, 1042.7, 2131.6, 0.0);
(675569.6, 4422891.8, 1042.5, 2131.6, 0.0);
(675594.6, 4422891.8, 1042.2, 2131.6, 0.0);
(675619.6, 4422891.8, 1041.9, 2131.6, 0.0);
(675644.6, 4422891.8, 1041.8, 2131.6, 0.0);
(675719.6, 4422891.8, 1041.6, 2131.6, 0.0);
(675744.6, 4422891.8, 1041.6, 2131.6, 0.0);
(675769.6, 4422891.8, 1041.3, 2131.6, 0.0);
(675794.6, 4422891.8, 1041.5, 2131.6, 0.0);
(675544.6, 4422916.8, 1042.1, 2131.6, 0.0);
(675569.6, 4422916.8, 1042.1, 2131.6, 0.0);
(675594.6, 4422916.8, 1041.7, 2131.6, 0.0);
(675619.6, 4422916.8, 1041.4, 2131.6, 0.0);
(675644.6, 4422916.8, 1041.3, 2131.6, 0.0);
(675719.6, 4422916.8, 1041.2, 2131.6, 0.0);
(675744.6, 4422916.8, 1041.0, 2131.6, 0.0);
(675769.6, 4422916.8, 1040.9, 2131.6, 0.0);
(675794.6, 4422916.8, 1040.9, 2131.6, 0.0);
(675544.6, 4422941.8, 1041.8, 2131.6, 0.0);
(675569.6, 4422941.8, 1041.5, 2131.6, 0.0);
(675594.6, 4422941.8, 1041.3, 2131.6, 0.0);
(675619.6, 4422941.8, 1041.1, 2131.6, 0.0);
(675644.6, 4422941.8, 1041.1, 2131.6, 0.0);
(675719.6, 4422941.8, 1040.9, 2131.6, 0.0);
(675744.6, 4422941.8, 1040.5, 2131.6, 0.0);
(675769.6, 4422941.8, 1040.4, 2131.6, 0.0);
(675794.6, 4422941.8, 1040.3, 2131.6, 0.0);
(675544.6, 4422966.8, 1041.1, 2131.6, 0.0);
(675569.6, 4422966.8, 1041.0, 2131.6, 0.0);
(675594.6, 4422966.8, 1040.8, 2131.6, 0.0);
(675619.6, 4422966.8, 1040.4, 2131.6, 0.0);
(675719.6, 4422966.8, 1040.6, 2131.6, 0.0);
(675744.6, 4422966.8, 1040.0, 2131.6, 0.0);
(675769.6, 4422966.8, 1039.9, 2131.6, 0.0);

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     ( 675794.6, 4422966.8,    1039.7,    2131.6,       0.0);
( 675544.6, 4422991.8,    1040.7,    2131.6,       0.0);
     ( 675569.6, 4422991.8,    1040.5,    2131.6,       0.0);
( 675594.6, 4422991.8,    1040.4,    2131.6,       0.0);
     ( 675619.6, 4422991.8,    1040.2,    2131.6,       0.0);
( 675644.6, 4422991.8,    1040.0,    2131.6,       0.0);
     ( 675719.6, 4422991.8,    1040.1,    2131.6,       0.0);
( 675744.6, 4422991.8,    1039.8,    2131.6,       0.0);
     ( 675769.6, 4422991.8,    1039.8,    2131.6,       0.0);
( 675794.6, 4422991.8,    1039.4,    2131.6,       0.0);
     ( 675544.6, 4423016.8,    1040.4,    2131.6,       0.0);
( 675569.6, 4423016.8,    1040.3,    2131.6,       0.0);
     ( 675594.6, 4423016.8,    1040.2,    2131.6,       0.0);
( 675619.6, 4423016.8,    1040.3,    2131.6,       0.0);
     ( 675644.6, 4423016.8,    1040.2,    2131.6,       0.0);
( 675669.6, 4423016.8,    1039.9,    2131.6,       0.0);
     ( 675719.6, 4423016.8,    1039.7,    2131.6,       0.0);
( 675744.6, 4423016.8,    1040.0,    2131.6,       0.0);
     ( 675769.6, 4423016.8,    1039.6,    2131.6,       0.0);
( 675794.6, 4423016.8,    1039.2,    2131.6,       0.0);
     ( 675544.6, 4423041.8,    1040.0,    2131.6,       0.0);
( 675569.6, 4423041.8,    1039.8,    2131.6,       0.0);
     ( 675594.6, 4423041.8,    1040.0,    2131.6,       0.0);
( 675619.6, 4423041.8,    1040.8,    2131.6,       0.0);
     ( 675644.6, 4423041.8,    1040.3,    2131.6,       0.0);
( 675669.6, 4423041.8,    1040.1,    2131.6,       0.0);
     ( 675694.6, 4423041.8,    1039.9,    2131.6,       0.0);
( 675719.6, 4423041.8,    1039.5,    2131.6,       0.0);
     ( 675744.6, 4423041.8,    1039.2,    2131.6,       0.0);
( 675769.6, 4423041.8,    1039.1,    2131.6,       0.0);
     ( 675794.6, 4423041.8,    1039.0,    2131.6,       0.0);
( 675544.6, 4423066.8,    1039.6,    2131.6,       0.0);
     ( 675569.6, 4423066.8,    1039.5,    2131.6,       0.0);
( 675594.6, 4423066.8,    1039.6,    2131.6,       0.0);
     ( 675619.6, 4423066.8,    1041.4,    2131.6,       0.0);
( 675644.6, 4423066.8,    1040.5,    2131.6,       0.0);
     ( 675669.6, 4423066.8,    1040.2,    2131.6,       0.0);
( 675694.6, 4423066.8,    1040.3,    2131.6,       0.0);
     ( 675719.6, 4423066.8,    1039.8,    2131.6,       0.0);
( 675744.6, 4423066.8,    1039.5,    2131.6,       0.0);
     ( 675769.6, 4423066.8,    1040.1,    2131.6,       0.0);
( 675794.6, 4423066.8,    1038.6,    2131.6,       0.0);
     ( 675644.8, 4422859.7,    1042.4,    2131.6,       0.0);
( 675645.6, 4422952.4,    1040.8,    2131.6,       0.0);
     ( 675604.0, 4422951.7,    1041.0,    2131.6,       0.0);
( 675683.6, 4423024.7,    1039.9,    2131.6,       0.0);
     ( 675705.7, 4423024.9,    1039.9,    2131.6,       0.0);
( 675712.5, 4422972.8,    1040.8,    2131.6,       0.0);
     ( 675711.6, 4422858.5,    1042.6,    2131.6,       0.0);
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** METEOROLOGICAL DAYS SELECTED FOR PROCESSING ***

(1=YES; 0=NO)

```
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
1 1 1 1 1   1 1 1 1 1 1 1 1 1 1   1 1 1 1 1 1 1 1 1 1
            1 1 1 1 1 1 1 1 1 1   1 1 1 1 1
```

NOTE: METEOROLOGICAL DATA ACTUALLY PROCESSED WILL ALSO DEPEND ON WHAT IS INCLUDED IN THE DATA FILE.

*** UPPER BOUND OF FIRST THROUGH FIFTH WIND SPEED CATEGORIES ***

(METERS/SEC)

1.54, 3.09, 5.14, 8.23, 10.80,

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** UP TO THE FIRST 24 HOURS OF METEOROLOGICAL DATA ***

Surface file: Z:\Shared\San Jose\Env\16230_13 New Quincy Courthouse EIR\Project Data\ACES\MET\ Met Version: 19191
Profile file: Z:\Shared\San Jose\Env\16230_13 New Quincy Courthouse EIR\Project Data\ACES\MET\
Surface format: FREE
Profile format: FREE
Surface station no.: 23225 Upper air station no.: 23230
Name: BLUE_CANYON_NYACK_AIRPORT Name: OAKLAND/WSO_AP
Year: 2014 Year: 2014

First 24 hours of scalar data

YR	MO	DY	JDY	HR	H0	U*	W*	DT/DZ	ZICNV	ZIMCH	M-O LEN	Z0	BOWEN	ALBEDO	REF WS	WD	HT	REF TA	HT
14	01	01	1	01	-33.3	0.399	-9.000	-9.000	-999.	604.	174.9	0.49	0.50	1.00	2.86	999.	10.0	283.1	2.0
14	01	01	1	02	-39.3	0.472	-9.000	-9.000	-999.	777.	244.8	0.49	0.50	1.00	3.36	999.	10.0	283.1	2.0
14	01	01	1	03	-41.1	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	1.00	3.86	54.	10.0	283.1	2.0
14	01	01	1	04	-30.0	0.360	-9.000	-9.000	-999.	532.	142.7	0.39	0.50	1.00	2.86	53.	10.0	283.1	2.0
14	01	01	1	05	-39.3	0.472	-9.000	-9.000	-999.	777.	244.8	0.49	0.50	1.00	3.36	999.	10.0	283.1	2.0
14	01	01	1	06	-33.3	0.399	-9.000	-9.000	-999.	609.	174.9	0.49	0.50	1.00	2.86	999.	10.0	283.1	2.0
14	01	01	1	07	-41.2	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	1.00	3.86	55.	10.0	282.5	2.0
14	01	01	1	08	-41.1	0.492	-9.000	-9.000	-999.	829.	266.7	0.39	0.50	0.88	3.86	53.	10.0	282.5	2.0
14	01	01	1	09	-15.8	0.434	-9.000	-9.000	-999.	689.	387.8	0.39	0.50	0.58	3.36	47.	10.0	283.8	2.0
14	01	01	1	10	14.3	0.264	0.282	0.012	47.	349.	-97.3	0.54	0.50	0.47	1.76	81.	10.0	285.9	2.0
14	01	01	1	11	31.8	-9.000	-9.000	-9.000	121.	-999.	-99999.0	0.49	0.50	0.43	0.00	0.	10.0	286.4	2.0

```
 14 01 01   1 12   41.5  0.278  0.612  0.012  166.  352.    -39.1
0.49   0.50   0.42    1.76  999.   10.0  287.5    2.0
 14 01 01   1 13   42.3  0.264  0.656  0.013  201.  325.    -32.6
0.40   0.50   0.41    1.76  253.   10.0  287.0    2.0
 14 01 01   1 14   34.7  0.326  0.632  0.012  219.  446.    -75.0
0.40   0.50   0.43    2.36  269.   10.0  287.5    2.0
 14 01 01   1 15   18.8  0.372  0.523  0.011  228.  545.   -206.0
0.40   0.50   0.46    2.86  242.   10.0  287.5    2.0
 14 01 01   1 16   -4.8  0.307 -9.000 -9.000 -999.  411.    457.0
0.40   0.50   0.54    2.36  264.   10.0  285.9    2.0
 14 01 01   1 17  -25.6  0.320 -9.000 -9.000 -999.  435.    112.9
0.77   0.50   0.79    1.76   21.   10.0  285.4    2.0
 14 01 01   1 18  -17.9  0.217 -9.000 -9.000 -999.  247.     51.6
0.39   0.50   1.00    1.76   47.   10.0  284.9    2.0
 14 01 01   1 19 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  284.9    2.0
 14 01 01   1 20 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  283.8    2.0
 14 01 01   1 21  -21.0  0.252 -9.000 -9.000 -999.  303.     69.8
0.54   0.50   1.00    1.76   80.   10.0  283.8    2.0
 14 01 01   1 22  -29.4  0.353 -9.000 -9.000 -999.  503.    136.9
0.86   0.50   1.00    1.76  132.   10.0  283.8    2.0
 14 01 01   1 23 -999.0 -9.000 -9.000 -9.000 -999. -999. -99999.0
0.49   0.50   1.00    0.00    0.   10.0  282.5    2.0
 14 01 01   1 24  -40.0  0.479 -9.000 -9.000 -999.  796.    252.4
0.86   0.50   1.00    2.36  140.   10.0  283.1    2.0


 First hour of profile data
 YR MO DY HR HEIGHT F  WDIR    WSPD AMB_TMP sigmaA  sigmaW
sigmaV
 14 01 01 01   10.0 1 -999.    2.86   283.2
99.0  -99.00  -99.00

 F indicates top of profile (=1) or below (=0)
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00007	675208.07	4422610.07	0.00009
675283.07	4422610.07	0.00011	675358.07	4422610.07	0.00013
675433.07	4422610.07	0.00014	675508.07	4422610.07	0.00013
675583.07	4422610.07	0.00010	675658.07	4422610.07	0.00009
675733.07	4422610.07	0.00010	675808.07	4422610.07	0.00011
675883.07	4422610.07	0.00010	675958.07	4422610.07	0.00009
676033.07	4422610.07	0.00008	676108.07	4422610.07	0.00007
675133.07	4422660.07	0.00008	675208.07	4422660.07	0.00010
675283.07	4422660.07	0.00013	675358.07	4422660.07	0.00016
675433.07	4422660.07	0.00019			

675508.07 4422660.07 0.00019
675583.07 4422660.07 0.00015
675658.07 4422660.07 0.00014
675733.07 4422660.07 0.00015
675808.07 4422660.07 0.00015
675883.07 4422660.07 0.00014
675958.07 4422660.07 0.00012
676033.07 4422660.07 0.00010
676108.07 4422660.07 0.00008
675133.07 4422710.07 0.00008
675208.07 4422710.07 0.00010
675283.07 4422710.07 0.00013
675358.07 4422710.07 0.00019
675433.07 4422710.07 0.00024
675508.07 4422710.07 0.00028
675583.07 4422710.07 0.00026
675658.07 4422710.07 0.00024
675733.07 4422710.07 0.00023
675808.07 4422710.07 0.00022
675883.07 4422710.07 0.00018
675958.07 4422710.07 0.00015
676033.07 4422710.07 0.00012
676108.07 4422710.07 0.00010
675133.07 4422760.07 0.00008
675208.07 4422760.07 0.00010
675283.07 4422760.07 0.00015
675358.07 4422760.07 0.00020
675433.07 4422760.07 0.00029
675508.07 4422760.07 0.00040
675583.07 4422760.07 0.00049
675658.07 4422760.07 0.00044
675733.07 4422760.07 0.00040
675808.07 4422760.07 0.00035
675883.07 4422760.07 0.00026
675958.07 4422760.07 0.00019
676033.07 4422760.07 0.00015
676108.07 4422760.07 0.00011
675133.07 4422810.07 0.00008
675208.07 4422810.07 0.00011
675283.07 4422810.07 0.00015
675358.07 4422810.07 0.00021
675433.07 4422810.07 0.00033
675508.07 4422810.07 0.00054
675583.07 4422810.07 0.00090
675658.07 4422810.07 0.00111
675733.07 4422810.07 0.00089
675808.07 4422810.07 0.00060
675883.07 4422810.07 0.00038
675958.07 4422810.07 0.00026
676033.07 4422810.07 0.00019
676108.07 4422810.07 0.00014
675133.07 4422860.07 0.00007

```
675208.07    4422860.07        0.00011
         675283.07    4422860.07        0.00015
675358.07    4422860.07        0.00022
         675433.07    4422860.07        0.00036
675508.07    4422860.07        0.00067
         675583.07    4422860.07        0.00153
675733.07    4422860.07        0.00331
         675808.07    4422860.07        0.00109
675883.07    4422860.07        0.00056
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00035	676033.07	4422860.07	0.00024
676108.07	4422860.07	0.00017	675133.07	4422910.07	0.00007
675208.07	4422910.07	0.00009	675283.07	4422910.07	0.00013
675358.07	4422910.07	0.00020	675433.07	4422910.07	0.00034
675508.07	4422910.07	0.00070	675583.07	4422910.07	0.00202
675733.07	4422910.07	0.00655	675808.07	4422910.07	0.00163
675883.07	4422910.07	0.00074	675958.07	4422910.07	0.00042
676033.07	4422910.07	0.00027	676108.07	4422910.07	0.00019
675133.07	4422960.07	0.00006	675208.07	4422960.07	0.00008
675283.07	4422960.07	0.00012			

675358.07 4422960.07 0.00018
675433.07 4422960.07 0.00030
675508.07 4422960.07 0.00063
675583.07 4422960.07 0.00228
675733.07 4422960.07 0.00759
675808.07 4422960.07 0.00187
675883.07 4422960.07 0.00084
675958.07 4422960.07 0.00047
676033.07 4422960.07 0.00030
676108.07 4422960.07 0.00021
675133.07 4423010.07 0.00006
675208.07 4423010.07 0.00008
675283.07 4423010.07 0.00010
675358.07 4423010.07 0.00016
675433.07 4423010.07 0.00026
675508.07 4423010.07 0.00053
675583.07 4423010.07 0.00177
675658.07 4423010.07 0.01087
675733.07 4423010.07 0.00630
675808.07 4423010.07 0.00169
675883.07 4423010.07 0.00081
675958.07 4423010.07 0.00047
676033.07 4423010.07 0.00031
676108.07 4423010.07 0.00022
675133.07 4423060.07 0.00005
675208.07 4423060.07 0.00007
675283.07 4423060.07 0.00010
675358.07 4423060.07 0.00014
675433.07 4423060.07 0.00023
675508.07 4423060.07 0.00047
675583.07 4423060.07 0.00136
675658.07 4423060.07 0.00443
675733.07 4423060.07 0.00333
675808.07 4423060.07 0.00124
675883.07 4423060.07 0.00067
675958.07 4423060.07 0.00043
676033.07 4423060.07 0.00029
676108.07 4423060.07 0.00021
675133.07 4423110.07 0.00005
675208.07 4423110.07 0.00006
675283.07 4423110.07 0.00009
675358.07 4423110.07 0.00013
675433.07 4423110.07 0.00022
675508.07 4423110.07 0.00043
675583.07 4423110.07 0.00103
675658.07 4423110.07 0.00218
675733.07 4423110.07 0.00187
675808.07 4423110.07 0.00088
675883.07 4423110.07 0.00052
675958.07 4423110.07 0.00035
676033.07 4423110.07 0.00026
676108.07 4423110.07 0.00019

```
675544.56    4422816.83        0.00074
         675569.56    4422816.83        0.00089
675594.56    4422816.83        0.00106
         675619.56    4422816.83        0.00124
675644.56    4422816.83        0.00132
         675669.56    4422816.83        0.00128
675694.56    4422816.83        0.00118
         675719.56    4422816.83        0.00108
675744.56    4422816.83        0.00097
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00084	675794.56	4422816.83	0.00072
675544.56	4422841.83	0.00088	675569.56	4422841.83	0.00112
675594.56	4422841.83	0.00148	675619.56	4422841.83	0.00203
675644.56	4422841.83	0.00263	675669.56	4422841.83	0.00284
675694.56	4422841.83	0.00263	675719.56	4422841.83	0.00220
675744.56	4422841.83	0.00172	675769.56	4422841.83	0.00130
675794.56	4422841.83	0.00100	675544.56	4422866.83	0.00100
675569.56	4422866.83	0.00134	675594.56	4422866.83	0.00192
675619.56	4422866.83	0.00306	675644.56	4422866.83	0.00501
675719.56	4422866.83	0.00503			

675744.56 4422866.83 0.00302
675769.56 4422866.83 0.00193
675794.56 4422866.83 0.00137
675544.56 4422891.83 0.00107
675569.56 4422891.83 0.00151
675594.56 4422891.83 0.00225
675619.56 4422891.83 0.00382
675644.56 4422891.83 0.00752
675719.56 4422891.83 0.00776
675744.56 4422891.83 0.00424
675769.56 4422891.83 0.00255
675794.56 4422891.83 0.00174
675544.56 4422916.83 0.00112
675569.56 4422916.83 0.00165
675594.56 4422916.83 0.00259
675619.56 4422916.83 0.00452
675644.56 4422916.83 0.00903
675719.56 4422916.83 0.00937
675744.56 4422916.83 0.00505
675769.56 4422916.83 0.00302
675794.56 4422916.83 0.00203
675544.56 4422941.83 0.00111
675569.56 4422941.83 0.00173
675594.56 4422941.83 0.00306
675619.56 4422941.83 0.00543
675644.56 4422941.83 0.01022
675719.56 4422941.83 0.01020
675744.56 4422941.83 0.00552
675769.56 4422941.83 0.00330
675794.56 4422941.83 0.00221
675544.56 4422966.83 0.00103
675569.56 4422966.83 0.00163
675594.56 4422966.83 0.00303
675619.56 4422966.83 0.00611
675719.56 4422966.83 0.01047
675744.56 4422966.83 0.00566
675769.56 4422966.83 0.00338
675794.56 4422966.83 0.00225
675544.56 4422991.83 0.00093
675569.56 4422991.83 0.00145
675594.56 4422991.83 0.00263
675619.56 4422991.83 0.00566
675644.56 4422991.83 0.01061
675719.56 4422991.83 0.00994
675744.56 4422991.83 0.00535
675769.56 4422991.83 0.00322
675794.56 4422991.83 0.00216
675544.56 4423016.83 0.00085
675569.56 4423016.83 0.00130
675594.56 4423016.83 0.00221
675619.56 4423016.83 0.00408
675644.56 4423016.83 0.00745

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675669.56    4423016.83        0.01121
         675719.56    4423016.83        0.00823
675744.56    4423016.83        0.00454
         675769.56    4423016.83        0.00281
675794.56    4423016.83        0.00194
         675544.56    4423041.83        0.00079
675569.56    4423041.83        0.00118
         675594.56    4423041.83        0.00186
675619.56    4423041.83        0.00305
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ALL ***
INCLUDING SOURCE(S):
PAREA1 , A0000001 , A0000002 , A0000003 , A0000004 ,
A0000005 , A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 ,
A0000011 , A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 ,
A0000019 , A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00486	675669.56	4423041.83	0.00713
675694.56	4423041.83	0.00810	675719.56	4423041.83	0.00554
675744.56	4423041.83	0.00341	675769.56	4423041.83	0.00228
675794.56	4423041.83	0.00164	675544.56	4423066.83	0.00074
675569.56	4423066.83	0.00106	675594.56	4423066.83	0.00157
675619.56	4423066.83	0.00236	675644.56	4423066.83	0.00338
675669.56	4423066.83	0.00442	675694.56	4423066.83	0.00474
675719.56	4423066.83	0.00373	675744.56	4423066.83	0.00257
675769.56	4423066.83	0.00183	675794.56	4423066.83	0.00136
675644.84	4422859.71	0.00435			

675645.56 4422952.37 0.01077
675603.96 4422951.71 0.00405
675683.55 4423024.69 0.01075
675705.67 4423024.92 0.00941
675712.54 4422972.82 0.01179
675711.55 4422858.53 0.00403

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00007	675208.07	4422610.07	0.00009
675283.07	4422610.07	0.00011	675358.07	4422610.07	0.00013
675433.07	4422610.07	0.00014	675508.07	4422610.07	0.00012
675583.07	4422610.07	0.00010	675658.07	4422610.07	0.00009
675733.07	4422610.07	0.00010	675808.07	4422610.07	0.00011
675883.07	4422610.07	0.00010	675958.07	4422610.07	0.00009
676033.07	4422610.07	0.00008	676108.07	4422610.07	0.00007
675133.07	4422660.07	0.00008	675208.07	4422660.07	0.00010
675283.07	4422660.07	0.00013	675358.07	4422660.07	0.00016
675433.07	4422660.07	0.00019	675508.07	4422660.07	0.00019
675583.07	4422660.07	0.00015	675658.07	4422660.07	0.00013
675733.07	4422660.07	0.00015	675808.07	4422660.07	0.00015
675883.07	4422660.07	0.00014	675958.07	4422660.07	0.00012
676033.07	4422660.07	0.00010	676108.07	4422660.07	0.00008

```
         675133.07    4422710.07        0.00008
675208.07    4422710.07        0.00010
         675283.07    4422710.07        0.00013
675358.07    4422710.07        0.00018
         675433.07    4422710.07        0.00024
675508.07    4422710.07        0.00028
         675583.07    4422710.07        0.00026
675658.07    4422710.07        0.00024
         675733.07    4422710.07        0.00023
675808.07    4422710.07        0.00022
         675883.07    4422710.07        0.00018
675958.07    4422710.07        0.00015
         676033.07    4422710.07        0.00012
676108.07    4422710.07        0.00009
         675133.07    4422760.07        0.00008
675208.07    4422760.07        0.00010
         675283.07    4422760.07        0.00014
675358.07    4422760.07        0.00020
         675433.07    4422760.07        0.00028
675508.07    4422760.07        0.00039
         675583.07    4422760.07        0.00048
675658.07    4422760.07        0.00043
         675733.07    4422760.07        0.00040
675808.07    4422760.07        0.00034
         675883.07    4422760.07        0.00026
675958.07    4422760.07        0.00019
         676033.07    4422760.07        0.00015
676108.07    4422760.07        0.00011
         675133.07    4422810.07        0.00008
675208.07    4422810.07        0.00010
         675283.07    4422810.07        0.00014
675358.07    4422810.07        0.00021
         675433.07    4422810.07        0.00033
675508.07    4422810.07        0.00054
         675583.07    4422810.07        0.00090
675658.07    4422810.07        0.00110
         675733.07    4422810.07        0.00088
675808.07    4422810.07        0.00059
         675883.07    4422810.07        0.00038
675958.07    4422810.07        0.00025
         676033.07    4422810.07        0.00018
676108.07    4422810.07        0.00014
         675133.07    4422860.07        0.00007
675208.07    4422860.07        0.00010
         675283.07    4422860.07        0.00014
675358.07    4422860.07        0.00021
         675433.07    4422860.07        0.00035
675508.07    4422860.07        0.00066
         675583.07    4422860.07        0.00152
675733.07    4422860.07        0.00330
         675808.07    4422860.07        0.00108
675883.07    4422860.07        0.00055
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00034	676033.07	4422860.07	0.00023
676108.07	4422860.07	0.00016	675133.07	4422910.07	0.00007
675208.07	4422910.07	0.00009	675283.07	4422910.07	0.00013
675358.07	4422910.07	0.00019	675433.07	4422910.07	0.00033
675508.07	4422910.07	0.00070	675583.07	4422910.07	0.00201
675733.07	4422910.07	0.00655	675808.07	4422910.07	0.00163
675883.07	4422910.07	0.00074	675958.07	4422910.07	0.00042
676033.07	4422910.07	0.00027	676108.07	4422910.07	0.00019
675133.07	4422960.07	0.00006	675208.07	4422960.07	0.00008
675283.07	4422960.07	0.00011	675358.07	4422960.07	0.00017
675433.07	4422960.07	0.00030	675508.07	4422960.07	0.00063
675583.07	4422960.07	0.00228	675733.07	4422960.07	0.00759
675808.07	4422960.07	0.00187	675883.07	4422960.07	0.00084
675958.07	4422960.07	0.00047	676033.07	4422960.07	0.00030

```
          676108.07    4422960.07        0.00021
675133.07    4423010.07        0.00006
          675208.07    4423010.07        0.00007
675283.07    4423010.07        0.00010
          675358.07    4423010.07        0.00015
675433.07    4423010.07        0.00026
          675508.07    4423010.07        0.00053
675583.07    4423010.07        0.00177
          675658.07    4423010.07        0.01087
675733.07    4423010.07        0.00630
          675808.07    4423010.07        0.00169
675883.07    4423010.07        0.00081
          675958.07    4423010.07        0.00047
676033.07    4423010.07        0.00031
          676108.07    4423010.07        0.00021
675133.07    4423060.07        0.00005
          675208.07    4423060.07        0.00007
675283.07    4423060.07        0.00009
          675358.07    4423060.07        0.00014
675433.07    4423060.07        0.00023
          675508.07    4423060.07        0.00047
675583.07    4423060.07        0.00135
          675658.07    4423060.07        0.00443
675733.07    4423060.07        0.00333
          675808.07    4423060.07        0.00124
675883.07    4423060.07        0.00067
          675958.07    4423060.07        0.00042
676033.07    4423060.07        0.00029
          676108.07    4423060.07        0.00021
675133.07    4423110.07        0.00005
          675208.07    4423110.07        0.00006
675283.07    4423110.07        0.00009
          675358.07    4423110.07        0.00013
675433.07    4423110.07        0.00022
          675508.07    4423110.07        0.00043
675583.07    4423110.07        0.00103
          675658.07    4423110.07        0.00218
675733.07    4423110.07        0.00187
          675808.07    4423110.07        0.00088
675883.07    4423110.07        0.00052
          675958.07    4423110.07        0.00035
676033.07    4423110.07        0.00026
          676108.07    4423110.07        0.00019
675544.56    4422816.83        0.00073
          675569.56    4422816.83        0.00088
675594.56    4422816.83        0.00106
          675619.56    4422816.83        0.00123
675644.56    4422816.83        0.00132
          675669.56    4422816.83        0.00127
675694.56    4422816.83        0.00118
          675719.56    4422816.83        0.00107
675744.56    4422816.83        0.00097
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00084	675794.56	4422816.83	0.00071
675544.56	4422841.83	0.00087	675569.56	4422841.83	0.00111
675594.56	4422841.83	0.00147	675619.56	4422841.83	0.00202
675644.56	4422841.83	0.00262	675669.56	4422841.83	0.00283
675694.56	4422841.83	0.00262	675719.56	4422841.83	0.00219
675744.56	4422841.83	0.00171	675769.56	4422841.83	0.00129
675794.56	4422841.83	0.00099	675544.56	4422866.83	0.00098
675569.56	4422866.83	0.00133	675594.56	4422866.83	0.00190
675619.56	4422866.83	0.00304	675644.56	4422866.83	0.00500
675719.56	4422866.83	0.00502	675744.56	4422866.83	0.00300
675769.56	4422866.83	0.00192	675794.56	4422866.83	0.00136
675544.56	4422891.83	0.00107	675569.56	4422891.83	0.00150
675594.56	4422891.83	0.00224	675619.56	4422891.83	0.00381
675644.56	4422891.83	0.00751	675719.56	4422891.83	0.00776

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         675744.56    4422891.83        0.00423
675769.56    4422891.83        0.00255
         675794.56    4422891.83        0.00173
675544.56    4422916.83        0.00111
         675569.56    4422916.83        0.00164
675594.56    4422916.83        0.00258
         675619.56    4422916.83        0.00451
675644.56    4422916.83        0.00903
         675719.56    4422916.83        0.00936
675744.56    4422916.83        0.00504
         675769.56    4422916.83        0.00302
675794.56    4422916.83        0.00203
         675544.56    4422941.83        0.00110
675569.56    4422941.83        0.00173
         675594.56    4422941.83        0.00306
675619.56    4422941.83        0.00542
         675644.56    4422941.83        0.01022
675719.56    4422941.83        0.01019
         675744.56    4422941.83        0.00552
675769.56    4422941.83        0.00330
         675794.56    4422941.83        0.00221
675544.56    4422966.83        0.00103
         675569.56    4422966.83        0.00162
675594.56    4422966.83        0.00303
         675619.56    4422966.83        0.00610
675719.56    4422966.83        0.01046
         675744.56    4422966.83        0.00566
675769.56    4422966.83        0.00337
         675794.56    4422966.83        0.00225
675544.56    4422991.83        0.00093
         675569.56    4422991.83        0.00145
675594.56    4422991.83        0.00262
         675619.56    4422991.83        0.00566
675644.56    4422991.83        0.01060
         675719.56    4422991.83        0.00993
675744.56    4422991.83        0.00535
         675769.56    4422991.83        0.00322
675794.56    4422991.83        0.00216
         675544.56    4423016.83        0.00085
675569.56    4423016.83        0.00130
         675594.56    4423016.83        0.00221
675619.56    4423016.83        0.00408
         675644.56    4423016.83        0.00744
675669.56    4423016.83        0.01121
         675719.56    4423016.83        0.00822
675744.56    4423016.83        0.00454
         675769.56    4423016.83        0.00281
675794.56    4423016.83        0.00194
         675544.56    4423041.83        0.00079
675569.56    4423041.83        0.00117
         675594.56    4423041.83        0.00186
675619.56    4423041.83        0.00305
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_ON ***
INCLUDING SOURCE(S):
PAREA1 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00486	675669.56	4423041.83	0.00713
675694.56	4423041.83	0.00810	675719.56	4423041.83	0.00554
675744.56	4423041.83	0.00341	675769.56	4423041.83	0.00228
675794.56	4423041.83	0.00164	675544.56	4423066.83	0.00074
675569.56	4423066.83	0.00106	675594.56	4423066.83	0.00157
675619.56	4423066.83	0.00236	675644.56	4423066.83	0.00338
675669.56	4423066.83	0.00442	675694.56	4423066.83	0.00474
675719.56	4423066.83	0.00373	675744.56	4423066.83	0.00257
675769.56	4423066.83	0.00183	675794.56	4423066.83	0.00135
675644.84	4422859.71	0.00434	675645.56	4422952.37	0.01077
675603.96	4422951.71	0.00404	675683.55	4423024.69	0.01075
675705.67	4423024.92	0.00941	675712.54	4422972.82	0.01179
675711.55	4422858.53	0.00402			

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00000	675208.07	4422610.07	0.00000
675283.07	4422610.07	0.00000	675358.07	4422610.07	0.00000
675433.07	4422610.07	0.00000	675508.07	4422610.07	0.00000
675583.07	4422610.07	0.00000	675658.07	4422610.07	0.00000
675733.07	4422610.07	0.00000	675808.07	4422610.07	0.00000
675883.07	4422610.07	0.00000	675958.07	4422610.07	0.00000
676033.07	4422610.07	0.00000	676108.07	4422610.07	0.00000
675133.07	4422660.07	0.00000	675208.07	4422660.07	0.00000
675283.07	4422660.07	0.00000	675358.07	4422660.07	0.00000
675433.07	4422660.07	0.00000			

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675508.07    4422660.07        0.00000
         675583.07    4422660.07        0.00000
675658.07    4422660.07        0.00000
         675733.07    4422660.07        0.00000
675808.07    4422660.07        0.00000
         675883.07    4422660.07        0.00000
675958.07    4422660.07        0.00000
         676033.07    4422660.07        0.00000
676108.07    4422660.07        0.00000
         675133.07    4422710.07        0.00000
675208.07    4422710.07        0.00000
         675283.07    4422710.07        0.00000
675358.07    4422710.07        0.00000
         675433.07    4422710.07        0.00000
675508.07    4422710.07        0.00000
         675583.07    4422710.07        0.00000
675658.07    4422710.07        0.00000
         675733.07    4422710.07        0.00000
675808.07    4422710.07        0.00000
         675883.07    4422710.07        0.00000
675958.07    4422710.07        0.00000
         676033.07    4422710.07        0.00000
676108.07    4422710.07        0.00000
         675133.07    4422760.07        0.00000
675208.07    4422760.07        0.00000
         675283.07    4422760.07        0.00001
675358.07    4422760.07        0.00001
         675433.07    4422760.07        0.00001
675508.07    4422760.07        0.00001
         675583.07    4422760.07        0.00001
675658.07    4422760.07        0.00001
         675733.07    4422760.07        0.00001
675808.07    4422760.07        0.00001
         675883.07    4422760.07        0.00001
675958.07    4422760.07        0.00000
         676033.07    4422760.07        0.00000
676108.07    4422760.07        0.00000
         675133.07    4422810.07        0.00000
675208.07    4422810.07        0.00001
         675283.07    4422810.07        0.00001
675358.07    4422810.07        0.00001
         675433.07    4422810.07        0.00001
675508.07    4422810.07        0.00001
         675583.07    4422810.07        0.00001
675658.07    4422810.07        0.00001
         675733.07    4422810.07        0.00001
675808.07    4422810.07        0.00001
         675883.07    4422810.07        0.00001
675958.07    4422810.07        0.00001
         676033.07    4422810.07        0.00000
676108.07    4422810.07        0.00000
         675133.07    4422860.07        0.00000
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675208.07    4422860.07        0.00001
         675283.07    4422860.07        0.00001
675358.07    4422860.07        0.00001
         675433.07    4422860.07        0.00001
675508.07    4422860.07        0.00001
         675583.07    4422860.07        0.00001
675733.07    4422860.07        0.00001
         675808.07    4422860.07        0.00001
675883.07    4422860.07        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00001	676033.07	4422860.07	0.00001
676108.07	4422860.07	0.00000	675133.07	4422910.07	0.00000
675208.07	4422910.07	0.00000	675283.07	4422910.07	0.00000
675358.07	4422910.07	0.00000	675433.07	4422910.07	0.00000
675508.07	4422910.07	0.00001	675583.07	4422910.07	0.00001
675733.07	4422910.07	0.00001	675808.07	4422910.07	0.00001
675883.07	4422910.07	0.00001	675958.07	4422910.07	0.00001
676033.07	4422910.07	0.00000	676108.07	4422910.07	0.00000
675133.07	4422960.07	0.00000	675208.07	4422960.07	0.00000
675283.07	4422960.07	0.00000			

```
675358.07    4422960.07        0.00000
         675433.07    4422960.07        0.00000
675508.07    4422960.07        0.00000
         675583.07    4422960.07        0.00000
675733.07    4422960.07        0.00000
         675808.07    4422960.07        0.00000
675883.07    4422960.07        0.00000
         675958.07    4422960.07        0.00000
676033.07    4422960.07        0.00000
         676108.07    4422960.07        0.00000
675133.07    4423010.07        0.00000
         675208.07    4423010.07        0.00000
675283.07    4423010.07        0.00000
         675358.07    4423010.07        0.00000
675433.07    4423010.07        0.00000
         675508.07    4423010.07        0.00000
675583.07    4423010.07        0.00000
         675658.07    4423010.07        0.00000
675733.07    4423010.07        0.00000
         675808.07    4423010.07        0.00000
675883.07    4423010.07        0.00000
         675958.07    4423010.07        0.00000
676033.07    4423010.07        0.00000
         676108.07    4423010.07        0.00000
675133.07    4423060.07        0.00000
         675208.07    4423060.07        0.00000
675283.07    4423060.07        0.00000
         675358.07    4423060.07        0.00000
675433.07    4423060.07        0.00000
         675508.07    4423060.07        0.00000
675583.07    4423060.07        0.00000
         675658.07    4423060.07        0.00000
675733.07    4423060.07        0.00000
         675808.07    4423060.07        0.00000
675883.07    4423060.07        0.00000
         675958.07    4423060.07        0.00000
676033.07    4423060.07        0.00000
         676108.07    4423060.07        0.00000
675133.07    4423110.07        0.00000
         675208.07    4423110.07        0.00000
675283.07    4423110.07        0.00000
         675358.07    4423110.07        0.00000
675433.07    4423110.07        0.00000
         675508.07    4423110.07        0.00000
675583.07    4423110.07        0.00000
         675658.07    4423110.07        0.00000
675733.07    4423110.07        0.00000
         675808.07    4423110.07        0.00000
675883.07    4423110.07        0.00000
         675958.07    4423110.07        0.00000
676033.07    4423110.07        0.00000
         676108.07    4423110.07        0.00000
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675544.56    4422816.83        0.00001
         675569.56    4422816.83        0.00001
675594.56    4422816.83        0.00001
         675619.56    4422816.83        0.00001
675644.56    4422816.83        0.00001
         675669.56    4422816.83        0.00001
675694.56    4422816.83        0.00001
         675719.56    4422816.83        0.00001
675744.56    4422816.83        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00001	675794.56	4422816.83	0.00001
675544.56	4422841.83	0.00001	675569.56	4422841.83	0.00001
675594.56	4422841.83	0.00001	675619.56	4422841.83	0.00001
675644.56	4422841.83	0.00001	675669.56	4422841.83	0.00001
675694.56	4422841.83	0.00001	675719.56	4422841.83	0.00001
675744.56	4422841.83	0.00001	675769.56	4422841.83	0.00001
675794.56	4422841.83	0.00001	675544.56	4422866.83	0.00001
675569.56	4422866.83	0.00001	675594.56	4422866.83	0.00001
675619.56	4422866.83	0.00001	675644.56	4422866.83	0.00001
675719.56	4422866.83	0.00001			

```
675744.56    4422866.83        0.00001
         675769.56    4422866.83        0.00001
675794.56    4422866.83        0.00001
         675544.56    4422891.83        0.00001
675569.56    4422891.83        0.00001
         675594.56    4422891.83        0.00001
675619.56    4422891.83        0.00001
         675644.56    4422891.83        0.00001
675719.56    4422891.83        0.00001
         675744.56    4422891.83        0.00001
675769.56    4422891.83        0.00001
         675794.56    4422891.83        0.00001
675544.56    4422916.83        0.00000
         675569.56    4422916.83        0.00000
675594.56    4422916.83        0.00000
         675619.56    4422916.83        0.00000
675644.56    4422916.83        0.00000
         675719.56    4422916.83        0.00000
675744.56    4422916.83        0.00000
         675769.56    4422916.83        0.00000
675794.56    4422916.83        0.00000
         675544.56    4422941.83        0.00000
675569.56    4422941.83        0.00000
         675594.56    4422941.83        0.00000
675619.56    4422941.83        0.00000
         675644.56    4422941.83        0.00000
675719.56    4422941.83        0.00000
         675744.56    4422941.83        0.00000
675769.56    4422941.83        0.00000
         675794.56    4422941.83        0.00000
675544.56    4422966.83        0.00000
         675569.56    4422966.83        0.00000
675594.56    4422966.83        0.00000
         675619.56    4422966.83        0.00000
675719.56    4422966.83        0.00000
         675744.56    4422966.83        0.00000
675769.56    4422966.83        0.00000
         675794.56    4422966.83        0.00000
675544.56    4422991.83        0.00000
         675569.56    4422991.83        0.00000
675594.56    4422991.83        0.00000
         675619.56    4422991.83        0.00000
675644.56    4422991.83        0.00000
         675719.56    4422991.83        0.00000
675744.56    4422991.83        0.00000
         675769.56    4422991.83        0.00000
675794.56    4422991.83        0.00000
         675544.56    4423016.83        0.00000
675569.56    4423016.83        0.00000
         675594.56    4423016.83        0.00000
675619.56    4423016.83        0.00000
         675644.56    4423016.83        0.00000
```

```
675669.56    4423016.83        0.00000
         675719.56    4423016.83        0.00000
675744.56    4423016.83        0.00000
         675769.56    4423016.83        0.00000
675794.56    4423016.83        0.00000
         675544.56    4423041.83        0.00000
675569.56    4423041.83        0.00000
         675594.56    4423041.83        0.00000
675619.56    4423041.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y1_OFF ***
INCLUDING SOURCE(S):
A0000001 , A0000002 , A0000003 , A0000004 , A0000005 ,
A0000006 , A0000007 , A0000008 , A0000023 , A0000024 , A0000009 , A0000010 , A0000011 ,
A0000012 , A0000013 , A0000014 , A0000015 , A0000016 , A0000017 , A0000018 , A0000019 ,
A0000020 , A0000021 , A0000022 , A0000025 , A0000026 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00000	675669.56	4423041.83	0.00000
675694.56	4423041.83	0.00000	675719.56	4423041.83	0.00000
675744.56	4423041.83	0.00000	675769.56	4423041.83	0.00000
675794.56	4423041.83	0.00000	675544.56	4423066.83	0.00000
675569.56	4423066.83	0.00000	675594.56	4423066.83	0.00000
675619.56	4423066.83	0.00000	675644.56	4423066.83	0.00000
675669.56	4423066.83	0.00000	675694.56	4423066.83	0.00000
675719.56	4423066.83	0.00000	675744.56	4423066.83	0.00000
675769.56	4423066.83	0.00000	675794.56	4423066.83	0.00000
675644.84	4422859.71	0.00001			

```
675645.56    4422952.37        0.00000
         675603.96    4422951.71        0.00000
675683.55    4423024.69        0.00000
         675705.67    4423024.92        0.00000
675712.54    4422972.82        0.00000
         675711.55    4422858.53        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00027	675208.07	4422610.07	0.00033
675283.07	4422610.07	0.00041	675358.07	4422610.07	0.00048
675433.07	4422610.07	0.00051	675508.07	4422610.07	0.00045
675583.07	4422610.07	0.00035	675658.07	4422610.07	0.00034
675733.07	4422610.07	0.00038	675808.07	4422610.07	0.00039
675883.07	4422610.07	0.00037	675958.07	4422610.07	0.00033
676033.07	4422610.07	0.00029	676108.07	4422610.07	0.00025
675133.07	4422660.07	0.00027	675208.07	4422660.07	0.00035
675283.07	4422660.07	0.00046	675358.07	4422660.07	0.00058
675433.07	4422660.07	0.00068			

675508.07 4422660.07 0.00067
675583.07 4422660.07 0.00054
675658.07 4422660.07 0.00048
675733.07 4422660.07 0.00053
675808.07 4422660.07 0.00054
675883.07 4422660.07 0.00049
675958.07 4422660.07 0.00042
676033.07 4422660.07 0.00035
676108.07 4422660.07 0.00029
675133.07 4422710.07 0.00028
675208.07 4422710.07 0.00036
675283.07 4422710.07 0.00048
675358.07 4422710.07 0.00066
675433.07 4422710.07 0.00087
675508.07 4422710.07 0.00102
675583.07 4422710.07 0.00092
675658.07 4422710.07 0.00085
675733.07 4422710.07 0.00082
675808.07 4422710.07 0.00079
675883.07 4422710.07 0.00066
675958.07 4422710.07 0.00053
676033.07 4422710.07 0.00042
676108.07 4422710.07 0.00034
675133.07 4422760.07 0.00028
675208.07 4422760.07 0.00037
675283.07 4422760.07 0.00051
675358.07 4422760.07 0.00071
675433.07 4422760.07 0.00102
675508.07 4422760.07 0.00142
675583.07 4422760.07 0.00174
675658.07 4422760.07 0.00157
675733.07 4422760.07 0.00144
675808.07 4422760.07 0.00124
675883.07 4422760.07 0.00093
675958.07 4422760.07 0.00069
676033.07 4422760.07 0.00052
676108.07 4422760.07 0.00041
675133.07 4422810.07 0.00027
675208.07 4422810.07 0.00037
675283.07 4422810.07 0.00051
675358.07 4422810.07 0.00075
675433.07 4422810.07 0.00118
675508.07 4422810.07 0.00194
675583.07 4422810.07 0.00323
675658.07 4422810.07 0.00396
675733.07 4422810.07 0.00319
675808.07 4422810.07 0.00214
675883.07 4422810.07 0.00136
675958.07 4422810.07 0.00092
676033.07 4422810.07 0.00066
676108.07 4422810.07 0.00049
675133.07 4422860.07 0.00026

```
675208.07    4422860.07        0.00036
         675283.07    4422860.07        0.00050
675358.07    4422860.07        0.00076
         675433.07    4422860.07        0.00125
675508.07    4422860.07        0.00237
         675583.07    4422860.07        0.00548
675733.07    4422860.07        0.01187
         675808.07    4422860.07        0.00388
675883.07    4422860.07        0.00199
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00122	676033.07	4422860.07	0.00082
676108.07	4422860.07	0.00059	675133.07	4422910.07	0.00024
675208.07	4422910.07	0.00033	675283.07	4422910.07	0.00046
675358.07	4422910.07	0.00070	675433.07	4422910.07	0.00121
675508.07	4422910.07	0.00250	675583.07	4422910.07	0.00724
675733.07	4422910.07	0.02356	675808.07	4422910.07	0.00585
675883.07	4422910.07	0.00265	675958.07	4422910.07	0.00151
676033.07	4422910.07	0.00097	676108.07	4422910.07	0.00068
675133.07	4422960.07	0.00022	675208.07	4422960.07	0.00030
675283.07	4422960.07	0.00042			

675358.07 4422960.07 0.00063
675433.07 4422960.07 0.00107
675508.07 4422960.07 0.00226
675583.07 4422960.07 0.00821
675733.07 4422960.07 0.02729
675808.07 4422960.07 0.00673
675883.07 4422960.07 0.00303
675958.07 4422960.07 0.00170
676033.07 4422960.07 0.00108
676108.07 4422960.07 0.00075
675133.07 4423010.07 0.00020
675208.07 4423010.07 0.00027
675283.07 4423010.07 0.00037
675358.07 4423010.07 0.00055
675433.07 4423010.07 0.00092
675508.07 4423010.07 0.00190
675583.07 4423010.07 0.00638
675658.07 4423010.07 0.03910
675733.07 4423010.07 0.02266
675808.07 4423010.07 0.00607
675883.07 4423010.07 0.00291
675958.07 4423010.07 0.00170
676033.07 4423010.07 0.00111
676108.07 4423010.07 0.00077
675133.07 4423060.07 0.00019
675208.07 4423060.07 0.00025
675283.07 4423060.07 0.00034
675358.07 4423060.07 0.00050
675433.07 4423060.07 0.00083
675508.07 4423060.07 0.00169
675583.07 4423060.07 0.00487
675658.07 4423060.07 0.01593
675733.07 4423060.07 0.01197
675808.07 4423060.07 0.00446
675883.07 4423060.07 0.00242
675958.07 4423060.07 0.00153
676033.07 4423060.07 0.00104
676108.07 4423060.07 0.00075
675133.07 4423110.07 0.00018
675208.07 4423110.07 0.00023
675283.07 4423110.07 0.00032
675358.07 4423110.07 0.00047
675433.07 4423110.07 0.00078
675508.07 4423110.07 0.00156
675583.07 4423110.07 0.00371
675658.07 4423110.07 0.00783
675733.07 4423110.07 0.00674
675808.07 4423110.07 0.00316
675883.07 4423110.07 0.00185
675958.07 4423110.07 0.00127
676033.07 4423110.07 0.00092
676108.07 4423110.07 0.00069

```
675544.56    4422816.83        0.00263
         675569.56    4422816.83        0.00317
675594.56    4422816.83        0.00381
         675619.56    4422816.83        0.00444
675644.56    4422816.83        0.00474
         675669.56    4422816.83        0.00458
675694.56    4422816.83        0.00424
         675719.56    4422816.83        0.00386
675744.56    4422816.83        0.00349
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00302	675794.56	4422816.83	0.00256
675544.56	4422841.83	0.00312	675569.56	4422841.83	0.00401
675594.56	4422841.83	0.00531	675619.56	4422841.83	0.00727
675644.56	4422841.83	0.00944	675669.56	4422841.83	0.01018
675694.56	4422841.83	0.00944	675719.56	4422841.83	0.00790
675744.56	4422841.83	0.00617	675769.56	4422841.83	0.00464
675794.56	4422841.83	0.00358	675544.56	4422866.83	0.00354
675569.56	4422866.83	0.00479	675594.56	4422866.83	0.00685
675619.56	4422866.83	0.01096	675644.56	4422866.83	0.01798
675719.56	4422866.83	0.01805			

675744.56 4422866.83 0.01082
675769.56 4422866.83 0.00690
675794.56 4422866.83 0.00489
675544.56 4422891.83 0.00384
675569.56 4422891.83 0.00541
675594.56 4422891.83 0.00806
675619.56 4422891.83 0.01372
675644.56 4422891.83 0.02701
675719.56 4422891.83 0.02791
675744.56 4422891.83 0.01522
675769.56 4422891.83 0.00916
675794.56 4422891.83 0.00622
675544.56 4422916.83 0.00400
675569.56 4422916.83 0.00591
675594.56 4422916.83 0.00929
675619.56 4422916.83 0.01624
675644.56 4422916.83 0.03248
675719.56 4422916.83 0.03368
675744.56 4422916.83 0.01814
675769.56 4422916.83 0.01086
675794.56 4422916.83 0.00729
675544.56 4422941.83 0.00398
675569.56 4422941.83 0.00623
675594.56 4422941.83 0.01100
675619.56 4422941.83 0.01951
675644.56 4422941.83 0.03676
675719.56 4422941.83 0.03667
675744.56 4422941.83 0.01986
675769.56 4422941.83 0.01186
675794.56 4422941.83 0.00794
675544.56 4422966.83 0.00369
675569.56 4422966.83 0.00584
675594.56 4422966.83 0.01089
675619.56 4422966.83 0.02196
675719.56 4422966.83 0.03764
675744.56 4422966.83 0.02035
675769.56 4422966.83 0.01213
675794.56 4422966.83 0.00810
675544.56 4422991.83 0.00333
675569.56 4422991.83 0.00520
675594.56 4422991.83 0.00944
675619.56 4422991.83 0.02037
675644.56 4422991.83 0.03815
675719.56 4422991.83 0.03573
675744.56 4422991.83 0.01925
675769.56 4422991.83 0.01157
675794.56 4422991.83 0.00777
675544.56 4423016.83 0.00305
675569.56 4423016.83 0.00468
675594.56 4423016.83 0.00794
675619.56 4423016.83 0.01467
675644.56 4423016.83 0.02678

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675669.56    4423016.83        0.04032
         675719.56    4423016.83        0.02958
675744.56    4423016.83        0.01633
         675769.56    4423016.83        0.01012
675794.56    4423016.83        0.00697
         675544.56    4423041.83        0.00284
675569.56    4423041.83        0.00423
         675594.56    4423041.83        0.00667
675619.56    4423041.83        0.01097
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ALL ***
INCLUDING SOURCE(S):
PAREA2 , A0000027 , A0000028 , A0000029 , A0000030 ,
A0000031 , A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 ,
A0000039 , A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 ,
A0000047 , A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.01748	675669.56	4423041.83	0.02565
675694.56	4423041.83	0.02913	675719.56	4423041.83	0.01992
675744.56	4423041.83	0.01227	675769.56	4423041.83	0.00820
675794.56	4423041.83	0.00591	675544.56	4423066.83	0.00265
675569.56	4423066.83	0.00381	675594.56	4423066.83	0.00564
675619.56	4423066.83	0.00849	675644.56	4423066.83	0.01215
675669.56	4423066.83	0.01589	675694.56	4423066.83	0.01705
675719.56	4423066.83	0.01343	675744.56	4423066.83	0.00926
675769.56	4423066.83	0.00659	675794.56	4423066.83	0.00487
675644.84	4422859.71	0.01561			

675645.56   4422952.37   0.03875
         675603.96   4422951.71   0.01455
675683.55   4423024.69   0.03867
         675705.67   4423024.92   0.03385
675712.54   4422972.82   0.04240
         675711.55   4422858.53   0.01446

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00027	675208.07	4422610.07	0.00033
675283.07	4422610.07	0.00041	675358.07	4422610.07	0.00048
675433.07	4422610.07	0.00051	675508.07	4422610.07	0.00045
675583.07	4422610.07	0.00035	675658.07	4422610.07	0.00034
675733.07	4422610.07	0.00038	675808.07	4422610.07	0.00039
675883.07	4422610.07	0.00037	675958.07	4422610.07	0.00033
676033.07	4422610.07	0.00029	676108.07	4422610.07	0.00025
675133.07	4422660.07	0.00027	675208.07	4422660.07	0.00035
675283.07	4422660.07	0.00046	675358.07	4422660.07	0.00057
675433.07	4422660.07	0.00067	675508.07	4422660.07	0.00067
675583.07	4422660.07	0.00054	675658.07	4422660.07	0.00048
675733.07	4422660.07	0.00053	675808.07	4422660.07	0.00054
675883.07	4422660.07	0.00049	675958.07	4422660.07	0.00042
676033.07	4422660.07	0.00035	676108.07	4422660.07	0.00029

675133.07 4422710.07 0.00028
675208.07 4422710.07 0.00036
675283.07 4422710.07 0.00048
675358.07 4422710.07 0.00066
675433.07 4422710.07 0.00087
675508.07 4422710.07 0.00101
675583.07 4422710.07 0.00092
675658.07 4422710.07 0.00085
675733.07 4422710.07 0.00082
675808.07 4422710.07 0.00079
675883.07 4422710.07 0.00066
675958.07 4422710.07 0.00053
676033.07 4422710.07 0.00042
676108.07 4422710.07 0.00034
675133.07 4422760.07 0.00028
675208.07 4422760.07 0.00037
675283.07 4422760.07 0.00050
675358.07 4422760.07 0.00071
675433.07 4422760.07 0.00101
675508.07 4422760.07 0.00142
675583.07 4422760.07 0.00174
675658.07 4422760.07 0.00156
675733.07 4422760.07 0.00143
675808.07 4422760.07 0.00123
675883.07 4422760.07 0.00093
675958.07 4422760.07 0.00069
676033.07 4422760.07 0.00052
676108.07 4422760.07 0.00041
675133.07 4422810.07 0.00027
675208.07 4422810.07 0.00036
675283.07 4422810.07 0.00051
675358.07 4422810.07 0.00075
675433.07 4422810.07 0.00117
675508.07 4422810.07 0.00193
675583.07 4422810.07 0.00323
675658.07 4422810.07 0.00396
675733.07 4422810.07 0.00318
675808.07 4422810.07 0.00213
675883.07 4422810.07 0.00136
675958.07 4422810.07 0.00092
676033.07 4422810.07 0.00065
676108.07 4422810.07 0.00049
675133.07 4422860.07 0.00026
675208.07 4422860.07 0.00035
675283.07 4422860.07 0.00049
675358.07 4422860.07 0.00075
675433.07 4422860.07 0.00124
675508.07 4422860.07 0.00236
675583.07 4422860.07 0.00547
675733.07 4422860.07 0.01186
675808.07 4422860.07 0.00388
675883.07 4422860.07 0.00198

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00121	676033.07	4422860.07	0.00081
676108.07	4422860.07	0.00059	675133.07	4422910.07	0.00024
675208.07	4422910.07	0.00032	675283.07	4422910.07	0.00046
675358.07	4422910.07	0.00070	675433.07	4422910.07	0.00120
675508.07	4422910.07	0.00250	675583.07	4422910.07	0.00724
675733.07	4422910.07	0.02356	675808.07	4422910.07	0.00585
675883.07	4422910.07	0.00265	675958.07	4422910.07	0.00151
676033.07	4422910.07	0.00097	676108.07	4422910.07	0.00068
675133.07	4422960.07	0.00022	675208.07	4422960.07	0.00030
675283.07	4422960.07	0.00041	675358.07	4422960.07	0.00063
675433.07	4422960.07	0.00107	675508.07	4422960.07	0.00226
675583.07	4422960.07	0.00821	675733.07	4422960.07	0.02729
675808.07	4422960.07	0.00673	675883.07	4422960.07	0.00302
675958.07	4422960.07	0.00170	676033.07	4422960.07	0.00108

```
          676108.07    4422960.07         0.00075
675133.07    4423010.07         0.00020
          675208.07    4423010.07         0.00027
675283.07    4423010.07         0.00037
          675358.07    4423010.07         0.00055
675433.07    4423010.07         0.00092
          675508.07    4423010.07         0.00190
675583.07    4423010.07         0.00638
          675658.07    4423010.07         0.03910
675733.07    4423010.07         0.02265
          675808.07    4423010.07         0.00607
675883.07    4423010.07         0.00291
          675958.07    4423010.07         0.00170
676033.07    4423010.07         0.00111
          676108.07    4423010.07         0.00077
675133.07    4423060.07         0.00019
          675208.07    4423060.07         0.00025
675283.07    4423060.07         0.00034
          675358.07    4423060.07         0.00050
675433.07    4423060.07         0.00083
          675508.07    4423060.07         0.00169
675583.07    4423060.07         0.00487
          675658.07    4423060.07         0.01593
675733.07    4423060.07         0.01196
          675808.07    4423060.07         0.00446
675883.07    4423060.07         0.00241
          675958.07    4423060.07         0.00153
676033.07    4423060.07         0.00104
          676108.07    4423060.07         0.00075
675133.07    4423110.07         0.00018
          675208.07    4423110.07         0.00023
675283.07    4423110.07         0.00032
          675358.07    4423110.07         0.00047
675433.07    4423110.07         0.00078
          675508.07    4423110.07         0.00156
675583.07    4423110.07         0.00371
          675658.07    4423110.07         0.00783
675733.07    4423110.07         0.00674
          675808.07    4423110.07         0.00315
675883.07    4423110.07         0.00185
          675958.07    4423110.07         0.00127
676033.07    4423110.07         0.00092
          676108.07    4423110.07         0.00069
675544.56    4422816.83         0.00263
          675569.56    4422816.83         0.00317
675594.56    4422816.83         0.00380
          675619.56    4422816.83         0.00443
675644.56    4422816.83         0.00474
          675669.56    4422816.83         0.00458
675694.56    4422816.83         0.00423
          675719.56    4422816.83         0.00386
675744.56    4422816.83         0.00348
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00302	675794.56	4422816.83	0.00255
675544.56	4422841.83	0.00311	675569.56	4422841.83	0.00400
675594.56	4422841.83	0.00530	675619.56	4422841.83	0.00726
675644.56	4422841.83	0.00944	675669.56	4422841.83	0.01018
675694.56	4422841.83	0.00943	675719.56	4422841.83	0.00789
675744.56	4422841.83	0.00616	675769.56	4422841.83	0.00463
675794.56	4422841.83	0.00357	675544.56	4422866.83	0.00353
675569.56	4422866.83	0.00479	675594.56	4422866.83	0.00684
675619.56	4422866.83	0.01095	675644.56	4422866.83	0.01797
675719.56	4422866.83	0.01804	675744.56	4422866.83	0.01081
675769.56	4422866.83	0.00689	675794.56	4422866.83	0.00488
675544.56	4422891.83	0.00384	675569.56	4422891.83	0.00540
675594.56	4422891.83	0.00806	675619.56	4422891.83	0.01371
675644.56	4422891.83	0.02701	675719.56	4422891.83	0.02791

675744.56 4422891.83 0.01521
675769.56 4422891.83 0.00916
675794.56 4422891.83 0.00622
675544.56 4422916.83 0.00400
675569.56 4422916.83 0.00590
675594.56 4422916.83 0.00929
675619.56 4422916.83 0.01624
675644.56 4422916.83 0.03248
675719.56 4422916.83 0.03368
675744.56 4422916.83 0.01814
675769.56 4422916.83 0.01086
675794.56 4422916.83 0.00729
675544.56 4422941.83 0.00397
675569.56 4422941.83 0.00622
675594.56 4422941.83 0.01100
675619.56 4422941.83 0.01951
675644.56 4422941.83 0.03676
675719.56 4422941.83 0.03667
675744.56 4422941.83 0.01986
675769.56 4422941.83 0.01186
675794.56 4422941.83 0.00793
675544.56 4422966.83 0.00369
675569.56 4422966.83 0.00584
675594.56 4422966.83 0.01089
675619.56 4422966.83 0.02196
675719.56 4422966.83 0.03764
675744.56 4422966.83 0.02035
675769.56 4422966.83 0.01213
675794.56 4422966.83 0.00810
675544.56 4422991.83 0.00333
675569.56 4422991.83 0.00520
675594.56 4422991.83 0.00944
675619.56 4422991.83 0.02037
675644.56 4422991.83 0.03815
675719.56 4422991.83 0.03573
675744.56 4422991.83 0.01925
675769.56 4422991.83 0.01157
675794.56 4422991.83 0.00777
675544.56 4423016.83 0.00305
675569.56 4423016.83 0.00468
675594.56 4423016.83 0.00794
675619.56 4423016.83 0.01467
675644.56 4423016.83 0.02678
675669.56 4423016.83 0.04032
675719.56 4423016.83 0.02958
675744.56 4423016.83 0.01633
675769.56 4423016.83 0.01011
675794.56 4423016.83 0.00697
675544.56 4423041.83 0.00284
675569.56 4423041.83 0.00423
675594.56 4423041.83 0.00667
675619.56 4423041.83 0.01097

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_ON ***
INCLUDING SOURCE(S):
PAREA2 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.01747	675669.56	4423041.83	0.02564
675694.56	4423041.83	0.02913	675719.56	4423041.83	0.01992
675744.56	4423041.83	0.01227	675769.56	4423041.83	0.00820
675794.56	4423041.83	0.00591	675544.56	4423066.83	0.00265
675569.56	4423066.83	0.00381	675594.56	4423066.83	0.00564
675619.56	4423066.83	0.00849	675644.56	4423066.83	0.01214
675669.56	4423066.83	0.01589	675694.56	4423066.83	0.01705
675719.56	4423066.83	0.01343	675744.56	4423066.83	0.00925
675769.56	4423066.83	0.00658	675794.56	4423066.83	0.00487
675644.84	4422859.71	0.01560	675645.56	4422952.37	0.03875
675603.96	4422951.71	0.01455	675683.55	4423024.69	0.03867
675705.67	4423024.92	0.03384	675712.54	4422972.82	0.04240
675711.55	4422858.53	0.01445			

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675133.07	4422610.07	0.00000	675208.07	4422610.07	0.00000
675283.07	4422610.07	0.00000	675358.07	4422610.07	0.00000
675433.07	4422610.07	0.00000	675508.07	4422610.07	0.00000
675583.07	4422610.07	0.00000	675658.07	4422610.07	0.00000
675733.07	4422610.07	0.00000	675808.07	4422610.07	0.00000
675883.07	4422610.07	0.00000	675958.07	4422610.07	0.00000
676033.07	4422610.07	0.00000	676108.07	4422610.07	0.00000
675133.07	4422660.07	0.00000	675208.07	4422660.07	0.00000
675283.07	4422660.07	0.00000	675358.07	4422660.07	0.00000
675433.07	4422660.07	0.00000			

```
675508.07    4422660.07        0.00000
         675583.07    4422660.07        0.00000
675658.07    4422660.07        0.00000
         675733.07    4422660.07        0.00000
675808.07    4422660.07        0.00000
         675883.07    4422660.07        0.00000
675958.07    4422660.07        0.00000
         676033.07    4422660.07        0.00000
676108.07    4422660.07        0.00000
         675133.07    4422710.07        0.00000
675208.07    4422710.07        0.00000
         675283.07    4422710.07        0.00000
675358.07    4422710.07        0.00000
         675433.07    4422710.07        0.00000
675508.07    4422710.07        0.00000
         675583.07    4422710.07        0.00000
675658.07    4422710.07        0.00000
         675733.07    4422710.07        0.00000
675808.07    4422710.07        0.00000
         675883.07    4422710.07        0.00000
675958.07    4422710.07        0.00000
         676033.07    4422710.07        0.00000
676108.07    4422710.07        0.00000
         675133.07    4422760.07        0.00000
675208.07    4422760.07        0.00000
         675283.07    4422760.07        0.00001
675358.07    4422760.07        0.00001
         675433.07    4422760.07        0.00001
675508.07    4422760.07        0.00000
         675583.07    4422760.07        0.00000
675658.07    4422760.07        0.00000
         675733.07    4422760.07        0.00000
675808.07    4422760.07        0.00000
         675883.07    4422760.07        0.00000
675958.07    4422760.07        0.00000
         676033.07    4422760.07        0.00000
676108.07    4422760.07        0.00000
         675133.07    4422810.07        0.00000
675208.07    4422810.07        0.00000
         675283.07    4422810.07        0.00000
675358.07    4422810.07        0.00000
         675433.07    4422810.07        0.00000
675508.07    4422810.07        0.00000
         675583.07    4422810.07        0.00000
675658.07    4422810.07        0.00000
         675733.07    4422810.07        0.00000
675808.07    4422810.07        0.00000
         675883.07    4422810.07        0.00000
675958.07    4422810.07        0.00001
         676033.07    4422810.07        0.00000
676108.07    4422810.07        0.00000
         675133.07    4422860.07        0.00000
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675208.07    4422860.07        0.00001
         675283.07    4422860.07        0.00001
675358.07    4422860.07        0.00001
         675433.07    4422860.07        0.00001
675508.07    4422860.07        0.00001
         675583.07    4422860.07        0.00001
675733.07    4422860.07        0.00001
         675808.07    4422860.07        0.00001
675883.07    4422860.07        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675958.07	4422860.07	0.00001	676033.07	4422860.07	0.00001
676108.07	4422860.07	0.00000	675133.07	4422910.07	0.00000
675208.07	4422910.07	0.00000	675283.07	4422910.07	0.00000
675358.07	4422910.07	0.00000	675433.07	4422910.07	0.00000
675508.07	4422910.07	0.00000	675583.07	4422910.07	0.00000
675733.07	4422910.07	0.00000	675808.07	4422910.07	0.00000
675883.07	4422910.07	0.00000	675958.07	4422910.07	0.00000
676033.07	4422910.07	0.00000	676108.07	4422910.07	0.00000
675133.07	4422960.07	0.00000	675208.07	4422960.07	0.00000
675283.07	4422960.07	0.00000			

675358.07 4422960.07 0.00000
675433.07 4422960.07 0.00000
675508.07 4422960.07 0.00000
675583.07 4422960.07 0.00000
675733.07 4422960.07 0.00000
675808.07 4422960.07 0.00000
675883.07 4422960.07 0.00000
675958.07 4422960.07 0.00000
676033.07 4422960.07 0.00000
676108.07 4422960.07 0.00000
675133.07 4423010.07 0.00000
675208.07 4423010.07 0.00000
675283.07 4423010.07 0.00000
675358.07 4423010.07 0.00000
675433.07 4423010.07 0.00000
675508.07 4423010.07 0.00000
675583.07 4423010.07 0.00000
675658.07 4423010.07 0.00000
675733.07 4423010.07 0.00000
675808.07 4423010.07 0.00000
675883.07 4423010.07 0.00000
675958.07 4423010.07 0.00000
676033.07 4423010.07 0.00000
676108.07 4423010.07 0.00000
675133.07 4423060.07 0.00000
675208.07 4423060.07 0.00000
675283.07 4423060.07 0.00000
675358.07 4423060.07 0.00000
675433.07 4423060.07 0.00000
675508.07 4423060.07 0.00000
675583.07 4423060.07 0.00000
675658.07 4423060.07 0.00000
675733.07 4423060.07 0.00000
675808.07 4423060.07 0.00000
675883.07 4423060.07 0.00000
675958.07 4423060.07 0.00000
676033.07 4423060.07 0.00000
676108.07 4423060.07 0.00000
675133.07 4423110.07 0.00000
675208.07 4423110.07 0.00000
675283.07 4423110.07 0.00000
675358.07 4423110.07 0.00000
675433.07 4423110.07 0.00000
675508.07 4423110.07 0.00000
675583.07 4423110.07 0.00000
675658.07 4423110.07 0.00000
675733.07 4423110.07 0.00000
675808.07 4423110.07 0.00000
675883.07 4423110.07 0.00000
675958.07 4423110.07 0.00000
676033.07 4423110.07 0.00000
676108.07 4423110.07 0.00000

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675544.56    4422816.83        0.00000
         675569.56    4422816.83        0.00000
675594.56    4422816.83        0.00000
         675619.56    4422816.83        0.00000
675644.56    4422816.83        0.00000
         675669.56    4422816.83        0.00000
675694.56    4422816.83        0.00000
         675719.56    4422816.83        0.00000
675744.56    4422816.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675769.56	4422816.83	0.00000	675794.56	4422816.83	0.00000
675544.56	4422841.83	0.00001	675569.56	4422841.83	0.00001
675594.56	4422841.83	0.00001	675619.56	4422841.83	0.00001
675644.56	4422841.83	0.00001	675669.56	4422841.83	0.00001
675694.56	4422841.83	0.00001	675719.56	4422841.83	0.00001
675744.56	4422841.83	0.00001	675769.56	4422841.83	0.00001
675794.56	4422841.83	0.00001	675544.56	4422866.83	0.00001
675569.56	4422866.83	0.00001	675594.56	4422866.83	0.00001
675619.56	4422866.83	0.00001	675644.56	4422866.83	0.00001
675719.56	4422866.83	0.00001			

675744.56 4422866.83 0.00001
675769.56 4422866.83 0.00001
675794.56 4422866.83 0.00001
675544.56 4422891.83 0.00000
675569.56 4422891.83 0.00000
675594.56 4422891.83 0.00000
675619.56 4422891.83 0.00000
675644.56 4422891.83 0.00000
675719.56 4422891.83 0.00000
675744.56 4422891.83 0.00000
675769.56 4422891.83 0.00000
675794.56 4422891.83 0.00000
675544.56 4422916.83 0.00000
675569.56 4422916.83 0.00000
675594.56 4422916.83 0.00000
675619.56 4422916.83 0.00000
675644.56 4422916.83 0.00000
675719.56 4422916.83 0.00000
675744.56 4422916.83 0.00000
675769.56 4422916.83 0.00000
675794.56 4422916.83 0.00000
675544.56 4422941.83 0.00000
675569.56 4422941.83 0.00000
675594.56 4422941.83 0.00000
675619.56 4422941.83 0.00000
675644.56 4422941.83 0.00000
675719.56 4422941.83 0.00000
675744.56 4422941.83 0.00000
675769.56 4422941.83 0.00000
675794.56 4422941.83 0.00000
675544.56 4422966.83 0.00000
675569.56 4422966.83 0.00000
675594.56 4422966.83 0.00000
675619.56 4422966.83 0.00000
675719.56 4422966.83 0.00000
675744.56 4422966.83 0.00000
675769.56 4422966.83 0.00000
675794.56 4422966.83 0.00000
675544.56 4422991.83 0.00000
675569.56 4422991.83 0.00000
675594.56 4422991.83 0.00000
675619.56 4422991.83 0.00000
675644.56 4422991.83 0.00000
675719.56 4422991.83 0.00000
675744.56 4422991.83 0.00000
675769.56 4422991.83 0.00000
675794.56 4422991.83 0.00000
675544.56 4423016.83 0.00000
675569.56 4423016.83 0.00000
675594.56 4423016.83 0.00000
675619.56 4423016.83 0.00000
675644.56 4423016.83 0.00000

```
675669.56    4423016.83        0.00000
         675719.56    4423016.83        0.00000
675744.56    4423016.83        0.00000
         675769.56    4423016.83        0.00000
675794.56    4423016.83        0.00000
         675544.56    4423041.83        0.00000
675569.56    4423041.83        0.00000
         675594.56    4423041.83        0.00000
675619.56    4423041.83        0.00000
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE PERIOD (43824 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: Y2_OFF ***
INCLUDING SOURCE(S):
A0000027 , A0000028 , A0000029 , A0000030 , A0000031 ,
A0000032 , A0000033 , A0000034 , A0000035 , A0000036 , A0000037 , A0000038 , A0000039 ,
A0000040 , A0000041 , A0000042 , A0000043 , A0000044 , A0000045 , A0000046 , A0000047 ,
A0000048 , A0000049 , A0000050 , A0000051 , A0000052 ,

*** DISCRETE CARTESIAN RECEPTOR POINTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
675644.56	4423041.83	0.00000	675669.56	4423041.83	0.00000
675694.56	4423041.83	0.00000	675719.56	4423041.83	0.00000
675744.56	4423041.83	0.00000	675769.56	4423041.83	0.00000
675794.56	4423041.83	0.00000	675544.56	4423066.83	0.00000
675569.56	4423066.83	0.00000	675594.56	4423066.83	0.00000
675619.56	4423066.83	0.00000	675644.56	4423066.83	0.00000
675669.56	4423066.83	0.00000	675694.56	4423066.83	0.00000
675719.56	4423066.83	0.00000	675744.56	4423066.83	0.00000
675769.56	4423066.83	0.00000	675794.56	4423066.83	0.00000
675644.84	4422859.71	0.00001			

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675645.56    4422952.37        0.00000
         675603.96    4422951.71        0.00000
675683.55    4423024.69        0.00000
         675705.67    4423024.92        0.00000
675712.54    4422972.82        0.00000
         675711.55    4422858.53        0.00001
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE SUMMARY OF MAXIMUM PERIOD (43824 HRS) RESULTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

NETWORK GROUP ID	AVERAGE CONC	RECEPTOR (XR, YR, ZELEV, ZHILL, ZFLAG)	OF TYPE	GRID-ID
Y1_ALL	1ST HIGHEST VALUE IS	0.01179	AT	(675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.01121	AT	(675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.01087	AT	(675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.01077	AT	(675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	
	5TH HIGHEST VALUE IS	0.01075	AT	(675683.55, 4423024.69, 1039.91, 2131.63, 0.00)	DC	
	6TH HIGHEST VALUE IS	0.01061	AT	(675644.56, 4422991.83, 1040.04, 2131.63, 0.00)	DC	
	7TH HIGHEST VALUE IS	0.01047	AT	(675719.56, 4422966.83, 1040.60, 2131.63, 0.00)	DC	
	8TH HIGHEST VALUE IS	0.01022	AT	(675644.56, 4422941.83, 1041.07, 2131.63, 0.00)	DC	
	9TH HIGHEST VALUE IS	0.01020	AT	(675719.56, 4422941.83, 1040.89, 2131.63, 0.00)	DC	
	10TH HIGHEST VALUE IS	0.00994	AT	(675719.56, 4422991.83, 1040.09, 2131.63, 0.00)	DC	
Y1_ON	1ST HIGHEST VALUE IS	0.01179	AT	(675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.01121	AT	(675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.01087	AT	(675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.01077	AT	(675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	

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          5TH HIGHEST VALUE IS       0.01075 AT (  675683.55,
4423024.69,  1039.91,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.01060 AT (  675644.56,
4422991.83,  1040.04,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.01046 AT (  675719.56,
4422966.83,  1040.60,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.01022 AT (  675644.56,
4422941.83,  1041.07,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.01019 AT (  675719.56,
4422941.83,  1040.89,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.00993 AT (  675719.56,
4422991.83,  1040.09,  2131.63,    0.00)  DC

Y1_OFF    1ST HIGHEST VALUE IS       0.00001 AT (  675958.07,
4422860.07,  1040.91,  2131.63,    0.00)  DC
          2ND HIGHEST VALUE IS       0.00001 AT (  676033.07,
4422860.07,  1040.14,  2131.63,    0.00)  DC
          3RD HIGHEST VALUE IS       0.00001 AT (  675883.07,
4422860.07,  1041.49,  2131.63,    0.00)  DC
          4TH HIGHEST VALUE IS       0.00001 AT (  675808.07,
4422860.07,  1042.15,  2131.63,    0.00)  DC
          5TH HIGHEST VALUE IS       0.00001 AT (  675733.07,
4422860.07,  1042.62,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.00001 AT (  675644.84,
4422859.71,  1042.44,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.00001 AT (  675508.07,
4422860.07,  1043.69,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.00001 AT (  675583.07,
4422860.07,  1043.12,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.00001 AT (  675711.55,
4422858.53,  1042.60,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.00001 AT (  675433.07,
4422860.07,  1044.16,  2131.63,    0.00)  DC

Y2_ALL    1ST HIGHEST VALUE IS       0.04240 AT (  675712.54,
4422972.82,  1040.77,  2131.63,    0.00)  DC
          2ND HIGHEST VALUE IS       0.04032 AT (  675669.56,
4423016.83,  1039.88,  2131.63,    0.00)  DC
          3RD HIGHEST VALUE IS       0.03910 AT (  675658.07,
4423010.07,  1040.01,  2131.63,    0.00)  DC
          4TH HIGHEST VALUE IS       0.03875 AT (  675645.56,
4422952.37,  1040.81,  2131.63,    0.00)  DC
          5TH HIGHEST VALUE IS       0.03867 AT (  675683.55,
4423024.69,  1039.91,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.03815 AT (  675644.56,
4422991.83,  1040.04,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.03764 AT (  675719.56,
4422966.83,  1040.60,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.03676 AT (  675644.56,
4422941.83,  1041.07,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.03667 AT (  675719.56,
4422941.83,  1040.89,  2131.63,    0.00)  DC
```

```
         10TH HIGHEST VALUE IS       0.03573 AT (  675719.56,
4422991.83,  1040.09,  2131.63,    0.00)  DC
```

*** MODELOPTs: RegDFAULT CONC ELEV URBAN ADJ_U*

*** THE SUMMARY OF MAXIMUM PERIOD (43824 HRS) RESULTS ***

** CONC OF PM_2.5 IN MICROGRAMS/M**3 **

NETWORK GROUP ID		AVERAGE CONC	RECEPTOR (XR, YR, ZELEV, ZHILL, ZFLAG)	OF TYPE	GRID-ID
Y2_ON	1ST HIGHEST VALUE IS	0.04240	AT (675712.54, 4422972.82, 1040.77, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.04032	AT (675669.56, 4423016.83, 1039.88, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.03910	AT (675658.07, 4423010.07, 1040.01, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.03875	AT (675645.56, 4422952.37, 1040.81, 2131.63, 0.00)	DC	
	5TH HIGHEST VALUE IS	0.03867	AT (675683.55, 4423024.69, 1039.91, 2131.63, 0.00)	DC	
	6TH HIGHEST VALUE IS	0.03815	AT (675644.56, 4422991.83, 1040.04, 2131.63, 0.00)	DC	
	7TH HIGHEST VALUE IS	0.03764	AT (675719.56, 4422966.83, 1040.60, 2131.63, 0.00)	DC	
	8TH HIGHEST VALUE IS	0.03676	AT (675644.56, 4422941.83, 1041.07, 2131.63, 0.00)	DC	
	9TH HIGHEST VALUE IS	0.03667	AT (675719.56, 4422941.83, 1040.89, 2131.63, 0.00)	DC	
	10TH HIGHEST VALUE IS	0.03573	AT (675719.56, 4422991.83, 1040.09, 2131.63, 0.00)	DC	
Y2_OFF	1ST HIGHEST VALUE IS	0.00001	AT (675958.07, 4422860.07, 1040.91, 2131.63, 0.00)	DC	
	2ND HIGHEST VALUE IS	0.00001	AT (676033.07, 4422860.07, 1040.14, 2131.63, 0.00)	DC	
	3RD HIGHEST VALUE IS	0.00001	AT (675883.07, 4422860.07, 1041.49, 2131.63, 0.00)	DC	
	4TH HIGHEST VALUE IS	0.00001	AT (675808.07, 4422860.07, 1042.15, 2131.63, 0.00)	DC	

```
          5TH HIGHEST VALUE IS       0.00001 AT (  675733.07,
4422860.07,  1042.62,  2131.63,    0.00)  DC
          6TH HIGHEST VALUE IS       0.00001 AT (  675644.84,
4422859.71,  1042.44,  2131.63,    0.00)  DC
          7TH HIGHEST VALUE IS       0.00001 AT (  675508.07,
4422860.07,  1043.69,  2131.63,    0.00)  DC
          8TH HIGHEST VALUE IS       0.00001 AT (  675583.07,
4422860.07,  1043.12,  2131.63,    0.00)  DC
          9TH HIGHEST VALUE IS       0.00001 AT (  675711.55,
4422858.53,  1042.60,  2131.63,    0.00)  DC
         10TH HIGHEST VALUE IS       0.00001 AT (  675433.07,
4422860.07,  1044.16,  2131.63,    0.00)  DC


 *** RECEPTOR TYPES:  GC = GRIDCART
                      GP = GRIDPOLR
                      DC = DISCCART
                      DP = DISCPOLR
```

```
 *** AERMOD - VERSION 23132  ***   *** C:\Lakes\AERMOD View
\Quincy_Courthouse_Construction_Unmit_20251208\Q ***
12/16/25
 *** AERMET - VERSION  19191 ***   ***
***        11:10:26

PAGE  92
 *** MODELOPTs:    RegDFAULT  CONC  ELEV  URBAN  ADJ_U*

 *** Message Summary : AERMOD Model Execution ***

  --------- Summary of Total Messages --------

 A Total of            0 Fatal Error Message(s)
 A Total of            4 Warning Message(s)
 A Total of         1651 Informational Message(s)

 A Total of        43824 Hours Were Processed

 A Total of          479 Calm Hours Identified

 A Total of         1172 Missing Hours Identified (  2.67
Percent)


    ******** FATAL ERROR MESSAGES ********
                ***  NONE  ***


    ********   WARNING MESSAGES   ********
 ME W186    1427       MEOPEN: THRESH_1MIN 1-min ASOS wind speed
threshold used           0.50
 ME W187    1427       MEOPEN: ADJ_U* Option for Stable Low Winds
used in AERMET
 MX W450   26305       CHKDAT: Record Out of Sequence in
Meteorological File at:      18010101
 MX W450   26305       CHKDAT: Record Out of Sequence in
Meteorological File at:    1 year gap

    ***********************************
    *** AERMOD Finishes Successfully ***
    ***********************************
```

Appendix C: Construction Health Risk Assessment Calculations (DPM)
Quincy Courthouse Project HRA
Unmitigated Health Risk Calculations - Residential

METHODOLOGY

Dose (Air) = Cair x DBR x A x EF x CF

Where:
- Cair: Chemical concentration in air (µg/m^3)
- DBR: Daily breathing rate (L/kg-day)
- A: Inhalation adsorption factor (unitless)
- EF: Exposure Frequency, days at home / days in year (unitless)
- CF: 10^-6 Conversion Factor (m^3/L and mg/µg)

Cancer Risk (per million) = Dose (Air) x CPF x ASF x (ED/AT) x FAH x 1,000,000

Where:
- Dose: Dose of chemical in the air (µg/m3)
- CPF: Cancer Potency Factor (mg/kg-day)$^{-1}$
- ASF: Age Sensitivity Factor
- ED: Exposure Duration (years)
- AT: Averaging Time for lifetime cancer risks
- FAH: Fraction of daily time spent at home / school

Risk Parameter Values by Age Bin

Variable	Residential Age Bin				
	3rd Trimester	0-2 Years	2-16 Years	16-30 Years	16-70 Years
DBR	361	1090	572	261	233
A	1	1	1	1	1
EF	0.96	0.96	0.96	0.96	0.96
CF	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
CPF	1.1	1.1	1.1	1.1	1.1
ASF	10	10	3	1	1
ED	0.25	2	14	14	54
AT	70	70	70	70	70
FAH	0.85	0.85	0.72	0.73	0.73

AERMOD Modeled DPM Concentrations (PMI/MEIR)

	PMI			MEIR		
	Conc.	X	Y	Conc.	X	Y
Year 1	0.04214	675712.54	4422972.82	0.03885	675658.07	4423010.07
Year 2	0.09121	675712.54	4422972.82	0.0841	675658.07	4423010.07

Risk Assessment Year 1 MEIR

Scenario	AERMOD DPM Conc.	Chronic Hazard Quotient
Year 1	0.03885	0.00777
Year 2	0.0841	0.01682

Year 1 Dose @ MEIR

Age Group	Cair x	BR	A	EF	CF		Dose
3rd Trimester	0.03885	361	1	0.96	1.00E-06	=	1.34E-05
0-2 Years	0.03885	1090	1	0.96	1.00E-06	=	4.06E-05
2-16 Years	0.03885	572	1	0.96	1.00E-06	=	2.13E-05
16-30 Years	0.03885	261	1	0.96	1.00E-06	=	9.72E-06
30-70 Years	0.03885	233	1	0.96	1.00E-06	=	8.68E-06

Year 1 Excess Risk at MEIR

Age Group	Dose	CPF	ASF	ED	AT	FAH	Conversion	Risk
3rd Trimester	1.34E-05	1.1	10	0.25	70	0.85	1,000,000	0.4
0-2 Years	4.06E-05	1.1	10	0.75	70	0.85	1,000,000	4.1
0-2 Years	4.06E-05	1.1	10	1.00	70	0.85	1,000,000	5.4

2-16 Years	2.13E-05	1.1	3	1.00	70	0.72	1,000,000	0.7
16-30 Years	9.72E-06	1.1	1	1.00	70	0.73	1,000,000	0.1
30-70 Years	8.68E-06	1.1	1	1.00	70	0.73	1,000,000	0.1

Year 2 Dose @ MEIR

Age Group	Cair x	BR	A	EF	CF		Dose
0-2 Years	0.0841	1090	1	0.96	1.00E-06	=	8.79E-05
2-16 Years	0.0841	572	1	0.96	1.00E-06	=	4.61E-05
16-30 Years	0.0841	261	1	0.96	1.00E-06	=	2.10E-05
30-70 Years	0.0841	233	1	0.96	1.00E-06	=	1.88E-05

Year 2 Excess Risk at MEIR

Age Group	Dose	CPF	ASF	ED	AT	FAH	Conversion	Risk
0-2 Years	8.79E-05	1.1	10	1.00	70	0.85	1,000,000	11.7
2-16 Years	4.61E-05	1.1	3	1.00	70	0.72	1,000,000	1.6
16-30 Years	2.10E-05	1.1	1	1.00	70	0.73	1,000,000	0.2
30-70 Years	1.88E-05	1.1	1	1.00	70	0.73	1,000,000	0.2

Total Excess Risk at MEIR (Cumulative, Based on Age at Start of Construction)

	Infant	Child < 2	Child 2<x<16	Adult 16<x<30	Adult 30<x<70
Year 1	4.5	5.4	0.7	0.1	0.1
Year 2	11.7	11.7	1.6	0.2	0.2
Total	16.3	17.2	2.3	0.4	0.3

Appendix C: Construction Health Risk Assessment Calculations (DPM)
Quincy Courthouse Project HRA
Mitigated Health Risk Calculations - Residential

METHODOLOGY

Dose (Air) = Cair x DBR x A x EF x CF

Where:
- Cair: Chemical concentration in air (µg/m^3)
- DBR: Daily breathing rate (L/kg-day)
- A: Inhalation adsorption factor (unitless)
- EF: Exposure Frequency, days at home / days in year (unitless)
- CF: 10^{-6} Conversion Factor (m^3/L and mg/µg)

Cancer Risk (per million) = Dose (Air) x CPF x ASF x (ED/AT) x FAH x 1,000,000

Where:
- Dose: Dose of chemical in the air (µg/m3)
- CPF: Cancer Potency Factor $(mg/kg\text{-}day)^{-1}$
- ASF: Age Sensitivity Factor
- ED: Exposure Duration (years)
- AT: Averaging Time for lifetime cancer risks
- FAH: Fraction of daily time spent at home / school

Risk Parameter Values by Age Bin

Variable	Residential Age Bin				
	3rd Trimester	0-2 Years	2-16 Years	16-30 Years	16-70 Years
DBR	361	1090	572	261	233
A	1	1	1	1	1
EF	0.96	0.96	0.96	0.96	0.96
CF	1.00E-06	1.00E-06	1.00E-06	1.00E-06	1.00E-06
CPF	1.1	1.1	1.1	1.1	1.1
ASF	10	10	3	1	1
ED	0.25	2	14	14	54
AT	70	70	70	70	70
FAH	0.85	0.85	0.72	0.73	0.73

AERMOD Modeled DPM Concentrations (PMI/MEIR)

	PMI			MEIR		
	Conc.	X	Y	Conc.	X	Y
Year 1	0.01179	675712.54	4422972.82	0.01087	675658.07	4423010.07
Year 2	0.0424	675712.54	4422972.82	0.0391	675658.07	4423010.07

Risk Assessment Year 1 MEIR

Scenario	AERMOD DPM Conc.	Chronic Hazard Quotient
Year 1	0.01087	0.002174
Year 2	0.0391	0.00782

Year 1 Dose @ MEIR

Age Group	Cair x	BR	A	EF	CF		Dose
3rd Trimester	0.01087	361	1	0.96	1.00E-06	=	3.76E-06
0-2 Years	0.01087	1090	1	0.96	1.00E-06	=	1.14E-05
2-16 Years	0.01087	572	1	0.96	1.00E-06	=	5.96E-06
16-30 Years	0.01087	261	1	0.96	1.00E-06	=	2.72E-06
30-70 Years	0.01087	233	1	0.96	1.00E-06	=	2.43E-06

Year 1 Excess Risk at MEIR

Age Group	Dose	CPF	ASF	ED	AT	FAH	Conversion	Risk
3rd Trimester	3.76E-06	1.1	10	0.25	70	0.85	1,000,000	0.1
0-2 Years	1.14E-05	1.1	10	0.75	70	0.85	1,000,000	1.1

0-2 Years	1.14E-05	1.1	10	1.00	70	0.85	1,000,000	1.5
2-16 Years	5.96E-06	1.1	3	1.00	70	0.72	1,000,000	0.2
16-30 Years	2.72E-06	1.1	1	1.00	70	0.73	1,000,000	0.0
30-70 Years	2.43E-06	1.1	1	1.00	70	0.73	1,000,000	0.0

Year 2 Dose @ MEIR

Age Group	Cair x	BR	A	EF	CF		Dose
0-2 Years	0.0391	1090	1	0.96	1.00E-06	=	4.09E-05
2-16 Years	0.0391	572	1	0.96	1.00E-06	=	2.14E-05
16-30 Years	0.0391	261	1	0.96	1.00E-06	=	9.79E-06
30-70 Years	0.0391	233	1	0.96	1.00E-06	=	8.74E-06

Year 2 Excess Risk at MEIR

Age Group	Dose	CPF	ASF	ED	AT	FAH	Conversion	Risk
0-2 Years	4.09E-05	1.1	10	1.00	70	0.85	1,000,000	5.5
2-16 Years	2.14E-05	1.1	3	1.00	70	0.72	1,000,000	0.7
16-30 Years	9.79E-06	1.1	1	1.00	70	0.73	1,000,000	0.1
30-70 Years	8.74E-06	1.1	1	1.00	70	0.73	1,000,000	0.1

Total Excess Risk at MEIR (Cumulative, Based on Age at Start of Construction)

	Infant	Child < 2	Child 2<x<16	Adult 16<x<30	Adult 30<x<70
Year 1	1.3	1.5	0.2	0.0	0.0
Year 2	5.5	5.5	0.7	0.1	0.1
Total	6.7	7.0	0.9	0.1	0.1

APPENDIX C

Biological Resources Report

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Biological Resources Report

New Quincy Courthouse Project, Plumas County, California



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October 2026

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1 Introduction

This report identifies sensitive biological resources with the potential to be impacted by the construction of the proposed New Quincy Courthouse Project (Project) in Quincy, Plumas County, California; and recommended measures to avoid significant impacts defined by the California Environmental Quality Act (CEQA).

The report will be used during project planning and to support the CEQA process. This report is also suitable for submission to regulatory agencies in support of permit applications. The report includes the following sections:

- Section 2 Project Location and Description: provides an overview of the activities proposed under the project.
- Section 3 Regulatory Setting: provides a brief explanation of the federal, state, and local regulations that pertain to the project.
- Section 4 Methods: explains the approach used for the evaluation, including field work and literature review.
- Section 5 Environmental Setting: provides a description of the environmental conditions in the project area, including vegetation communities and associated wildlife habitats present.
- Section 6 Special-status Species and Sensitive Habitats: describes special-status plant and animal species, and sensitive communities that are known to occur or that could potentially occur in the project site.
- Section 7 Biological Impact Assessment: provides an evaluation of the potential impacts to biological resources that may occur as a result of the project; and provides recommendations to avoid or minimize impacts to biological resources, as needed, to ensure that the project remains in compliance with all applicable federal, state, and local regulatory requirements.

2 Project Location and Description

The Project site consists of three contiguous, privately-owned parcels in the unincorporated town of Quincy in Plumas County. Site addresses include 253 Lawrence Street (APN 115-031-055), 287 Lawrence Street (APN 115-031-052), and 293 Lawrence Street (APN 115-031-054). The Project site is approximately 2.86 acres (Appendix A, Figure 1).

The Project site is currently occupied by three commercial buildings (two buildings and one open parking garage). The Judicial Council of California (Judicial Council) proposes purchasing the three parcels from the current private owners for the construction of the new courthouse to relocate Superior Court operations that are currently housed in the Plumas County Courthouse located in Quincy at 520 Main Street. The new courthouse will provide a new permanent state-

owned facility that is accessible to the public and can provide enhanced public services. The courthouse building will include construction of new courtrooms with support spaces, and administrative and operations areas. The Project also includes site improvements, including new on-site surface parking lots and drive aisles, and rerouted utility connections to serve the new building.

The proposed new Quincy Courthouse will be an approximately 23,100 square-foot, one-story building. An approximately 9,980 square-foot outdoor, ground-level access area for loading, in-custody sallyport, and secure parking will be located immediately adjacent to the courthouse building to the north/northwest. The proposed Project includes 117 parking spaces north/northwest and east of the building (Appendix A, Figure 2).

The Project would be designed and constructed according to the California Trial Court Facilities Standards that reflect best practices for basic components of trial court buildings and form the basis for design and construction of functional, durable, maintainable, efficient, and secure contemporary court facilities. The Project would incorporate sustainability measures throughout its design, construction, operation, and maintenance; comply with the Nonresidential Mandatory Measures of the current version of the California Green Building Standards (“CALGreen”) Code as well as the current version of the California Energy Code requirements; and achieve a minimum Silver certification level under the United States Green Building Council’s Leadership in Energy and Environmental Design (LEED) program.

Currently the stormwater runoff from the site sheet flows to an open drainage channel within the Project site that runs along the eastern boundary. Under the Project as proposed, storm water runoff would be collected and directed to treatment features constructed as part of the Project. Once the stormwater runoff passes through these treatment features, it would be piped to the drainage channel along the eastern property boundary for discharge. The design of the stormwater discharge point would be dependent upon the selection of a strategy for long-term management of the drainage channel.

Design Options for Drainage Channel

The Project may implement one of two potential approaches to the long-term management of the open drainage channel that would be determined at the design/build stage and in consultation with the resource agencies responsible for permitting work on water features. Construction of either option may occur below the top of the drainage channel bank and may require permits with mitigation conditions issued by the U.S. Army Corps of Engineers (USACE), Regional Water Quality Control Board (RWQCB), and/or California Department of Fish and Wildlife (CDFW) as described in this report. Both design options are analyzed in this report to determine whether the Project may have a significant effect on the environment.

Design Option 1: Leave the drainage channel open as it is currently and construct only the new stormwater runoff outfall pipe. The new discharge pipe would require an appropriately designed outfall to prevent erosion. Avoidance and mitigation measures described below address the potential for impacts from the proposed stormwater runoff outfall pipe.

Design Option 2: Culvert the drainage along its entire length within the Project site boundaries to reduce the long-term maintenance impacts. A new culvert would be connected to the existing culvert under Lawrence Street, convey runoff along the eastern side of the Project site, and discharge the runoff into the open channel to the north of the Project site. The new stormwater runoff drainage pipe needed for the Project would connect and discharge into this new culvert at a point along the channel extent within the Project site. This option assumes all riparian vegetation and open water habitat along the drainage channel would be removed within the Project site.

3 Regulatory Setting

Biological resources in California are protected under federal, state, and local laws. The laws that may pertain to the biological resources affected by the project are described in this section.

3.1 Federal

3.1.1 Federal Endangered Species Act

The Federal Endangered Species Act (FESA) of 1973, as amended, provides the regulatory framework for the protection of plant and animal species formally listed as endangered or threatened, as well as their designated critical habitats. While proposed and candidate species do not receive full statutory protections under FESA, they may be considered in planning processes to support proactive conservation and regulatory compliance. FESA has the following four primary components: (1) provisions for listing species, (2) requirements for consultation with the United States Fish and Wildlife Service (USFWS) and the National Oceanic and Atmospheric Administration's National Marine Fisheries Service (NOAA Fisheries), (3) prohibitions against "taking" (i.e., harassing, harming, hunting, shooting, wounding, killing, trapping, capturing, or collecting, or attempting to engage in any such conduct) of listed species, and (4) provisions for permits that allow incidental "take." FESA also discusses recovery plans and the designation of critical habitat for listed species.

Both the USFWS and NOAA Fisheries share the responsibility for administration of FESA. Section 7 requires federal agencies, in consultation with, and with the assistance of the USFWS or NOAA Fisheries, as appropriate, to ensure that actions they authorize, fund, or carry out are not likely to jeopardize the continued existence of threatened or endangered species or result in the destruction or adverse modification of critical habitat for these species. Non-federal agencies and private entities can seek authorization for take of federally listed species under Section 10 of FESA, which requires the preparation of an HCP.

3.1.2 U.S. Migratory Bird Treaty Act

The U.S. Migratory Bird Treaty Act (MBTA; 16 USC §§ 703 et seq., Title 50 Code of Federal Regulations [CFR] Part 10) states it is "unlawful at any time, by any means or in any manner, to pursue, hunt, take, capture, kill; attempt to take, capture or kill; possess, offer for sale, sell, offer to barter, barter, offer to purchase, purchase, deliver for shipment, ship, export, import, cause to be shipped, exported, or imported, deliver for transportation, transport or cause to be transported, carry or cause to be carried, or receive for shipment, transportation, carriage, or

export any migratory bird, any part, nest, or egg of any such bird, or any product, whether or not manufactured, which consists, or is composed in whole or in part, of any such bird or any part, nest or egg thereof…" In short, under the MBTA it is illegal to disturb a nest that is in active use, since this could result in killing a bird, destroying a nest, or destroying an egg. The USFWS enforces MBTA. The MBTA does not protect some birds that are non-native, or human introduced or that belong to families that are not covered by any of the conventions implemented by MBTA. A Department of Interior memo dated April 11, 2025, reinstated a 2017 interpretation of the MBTA (Solicitor's Opinion M-37050) determining that the MBTA does not prohibit accidental or incidental taking or killing of migratory birds. This interpretation does not exclude intentional take.

3.1.3 Clean Water Act

The Clean Water Act (CWA) is the primary federal law regulating water quality. The implementation of the CWA is the responsibility of the U.S. Environmental Protection Agency (EPA). However, the EPA depends on other agencies, such as the individual states and the USACE to assist in implementing the CWA. The objective of the CWA is to "restore and maintain the chemical, physical, and biological integrity of the Nation's waters." Section 404 and 401 of the CWA apply to activities that would impact waters of the U.S. The USACE enforces Section 404 of the CWA, and the California State Water Resources Control Board enforces Section 401.

Section 404. As part of its mandate under Section 404 of the CWA, the EPA regulates the discharge of dredged or fill material into "waters of the United States" (U.S.). In general, "Waters of the U.S." are navigable waters of the United States; interstate waters; all other waters where the use, degradation, or destruction of the waters could affect interstate or foreign commerce; tributaries to these waters that are relatively permanent standing or continuously flowing bodies of water; and wetlands adjacent to and with a continuous surface connection to these waters. Wetlands are defined as those areas "that are inundated or saturated by surface or groundwater at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions" (33 CFR 328.3(b)). The discharge of dredged or fill material into waters of the U.S. is prohibited under the CWA except when it complies with Section 404 of the CWA. Enforcement authority for Section 404 was given to the USACE, which it accomplishes under its regulatory branch. The EPA has veto authority over the USACE's administration of the Section 404 program and may override a USACE decision with respect to permitting.

Substantial impacts to waters of the U.S. may require an Individual Permit. Projects that only minimally affect waters of the U.S. may meet the conditions of one of the existing Nationwide Permits, provided that such permits' other respective conditions are satisfied. A Water Quality Certification or waiver pursuant to Section 401 (see below) of the CWA is required for Section 404 permit actions.

Section 401. Any applicant for a federal permit to impact waters of the U.S. under Section 404 of the CWA, including Nationwide Permits where pre-construction notification is required, must also provide to the USACE a certification or waiver from the State of California. The "401

Certification" is provided by the State Water Resources Control Board through the regional water quality control boards (RWQCB).

The RWQCB issues and enforces permits for discharge of treated water, landfills, stormwater runoff, filling of any surface waters or wetlands, dredging, agricultural activities and wastewater recycling. The RWQCB recommends the "401 Certification" application be made at the same time that any applications are provided to other agencies, such as the USACE, USFWS, or NOAA Fisheries. The application is not final until completion of environmental review under CEQA. The application to the RWQCB is similar to the pre-construction notification that is required by the USACE. It must include a description of the habitat that is being impacted, a description of how the impact is proposed to be minimized and proposed mitigation measures with goals, schedules, and performance standards. The RWQCB looks for mitigation that is on site and in-kind, with functions and values as good as or better than the water-based habitat that is being removed.

3.2 State

3.2.1 California Endangered Species Act

The California Endangered Species Act (CESA; Fish and Game Code 2050 et seq.) generally parallels FESA. It establishes the policy of the State to conserve, protect, restore, and enhance threatened or endangered species and their habitats. Section 2080 of the California Fish and Game Code prohibits the take, possession, purchase, sale, and import or export of endangered, threatened, or candidate species, unless otherwise authorized by permit or by the regulations. "Take" is defined in Section 86 of the California Fish and Game Code as to "hunt, pursue, catch, capture, or kill, or attempt to hunt, pursue, catch, capture, or kill." This definition differs from the definition of "take" under FESA. CESA is administered by CDFW. CESA allows for take incidental to otherwise lawful projects but mandates that State lead agencies consult with CDFW to ensure that a project would not jeopardize the continued existence of a candidate, threatened or endangered species.

3.2.2 California Fish and Game Code Sections 1600-1607

Sections 1600-1607 of the California Fish and Game Code require that a Notification of Lake or Streambed Alteration application be submitted to CDFW for "any activity that may substantially divert or obstruct the natural flow or substantially change the bed, channel, or bank of any river, stream, or lake." CDFW reviews the proposed actions in the application and, if necessary, prepares a Lake or Streambed Alteration Agreement (LSAA or SAA), that includes measures to protect affected fish and wildlife resources.

3.2.3 Native Plant Protection Act

The Native Plant Protection Act (NPPA) was created in 1977 with the intent to preserve, protect, and enhance rare and endangered plants in California (California Fish and Game Code sections 1900 to 1913). The NPPA is administered by CDFW, which has the authority to designate native plants as endangered or rare and to protect them from "take." CDFW maintains a list of plant species that have been officially classified as endangered, threatened, or rare. These special-

status plants have special protection under California law and projects that directly impact them may not qualify for a categorical exemption under CEQA guidelines.

3.2.4 Fully Protected Species and Species of Special Concern

The classification of California fully protected (CFP) species was CDFW's initial effort to identify and provide additional protection to those animals that were rare or faced possible extinction. Lists were created for fish, amphibians and reptiles, birds, and mammals. Most of the species on these lists have subsequently been listed under CESA and/or FESA. The Fish and Game Code sections (§5515 for fish, §5050 for amphibian and reptiles, §3511 for birds, §4700 for mammals) deal with CFP species and state that these species "…may not be taken or possessed at any time and no provision of this code or any other law shall be construed to authorize the issuance of permits or licenses to take any fully protected species" (CDFW Fish and Game Commission 1998). "Take" of these species may be authorized for necessary scientific research, for relocation to protect livestock, or under a natural community conservation plan (NCCP) or the project activities qualify for permitting under Section 2080.15 of the California Fish and Game Code. This language makes the CFP designation the strongest and most restrictive regarding the "take" of these species. In 2003, the code sections dealing with CFP species were amended to allow CDFW to authorize take resulting from recovery activities for state-listed species. On July 10, 2023, Governor Newsom signed Senate Bill 147, which allows for permits to take "fully protected" species for certain renewable energy and infrastructure projects (e.g., critical regional or local water agency infrastructure, and certain transportation projects). This law now establishes a permitting process for these species. Under this new law, all permits must be processed pursuant to provisions in the CESA that authorize CDFW to issue incidental permits and require permittees to minimize and fully mitigate impacts to the species. The law also requires permittees to satisfy "conservation standards" that essentially require permittees to exceed typical minimization and mitigation measures associated with permits under CESA.

California species of special concern (CSSC) are broadly defined as animals not listed under FESA or CESA, but which are nonetheless of concern to CDFW because they are declining at a rate that could result in listing or historically occurred in low numbers and known threats to their persistence currently exist. This designation is intended to result in special consideration for these animals by CDFW, land managers, consulting biologists, and others, and is intended to focus attention on the species to help avert the need for costly listing under FESA and CESA, and cumbersome recovery efforts that might ultimately be required. This designation also is intended to stimulate collection of additional information on the biology, distribution, and status of poorly known at-risk species, and focus research and management attention on them.

3.2.5 California Migratory Bird Protection Act

Fish and Game Code section 3513 prohibits taking or possessing all migratory birds (both game and nongame) designated in the MBTA as of January 1, 2025, and any additional migratory bird subsequently designated in the MBTA, except as provided by the Department of the Interior unless the federal rules or regulations are inconsistent with the Fish and Game Code. Section 3513 ensures that prohibitions against both intentional and incidental take provided under the

MBTA as of January 1, 2025, will remain in force in California. CDFW does not cite under federal law, including the MBTA, but may cite acts prohibited by CDFW regulations or Fish and Game Code sections 2000, 3513, or other applicable provisions.

3.2.6 Nesting Birds

Nesting birds, including raptors, are protected under California Fish and Game Code section 3503, which reads, “It is unlawful to take, possess, or needlessly destroy the nest or eggs of any bird, except as otherwise provided by this code or any regulation made pursuant thereto.” In addition, under California Fish and Game Code section 3503.5, “it is unlawful to take, possess, or destroy any birds in the orders Falconiformes or Strigiformes (birds-of-prey) or to take, possess, or destroy the nest or eggs of any such bird except as otherwise provided by this code or any regulation adopted pursuant thereto.” Passerines and non-passerine land birds are further protected under California Fish and Game Code section 3513. As such, CDFW typically recommends surveys for nesting birds that could potentially be directly (e.g., actual removal of trees/vegetation) or indirectly (e.g., noise disturbance) impacted by project-related activities. Disturbance during the breeding season could result in the incidental loss of fertile eggs or nestlings or otherwise lead to nest abandonment. Disturbance that causes nest abandonment and/or loss of reproductive effort is considered “take” by CDFW.

3.2.7 Non-Game Mammals

Sections 4150-4155 of the California Fish and Game Code protects non-game mammals, including bats. Section 4150 states “A mammal occurring naturally in California that is not a game mammal, fully protected mammal, or fur-bearing mammal is a nongame mammal. A non-game mammal may not be taken or possessed except as provided in this code or in accordance with regulations adopted by the commission”. The non-game mammals that may be taken or possessed are primarily those that cause crop or property damage. Bats are classified as a non-game mammal and are protected under the California Fish and Game Code, in addition to being protected if they are a listed species (e.g., CSSC, CFP, state or federal threatened, or state or federal endangered).

3.2.8 Sensitive Vegetation Communities

Sensitive vegetation communities are natural communities and habitats that are either unique in constituent components, of relatively limited distribution in the region, or are of particularly high wildlife value. These communities may or may not necessarily contain special-status species. Sensitive natural communities are usually identified in local or regional plans, policies, or regulations, or by CDFW (i.e., CNDDB) or the USFWS. The CNDDB identifies several natural communities as rare, which are given the highest inventory priority (CNDDB 2025, CDFW 2025).

3.2.9 Porter-Cologne Water Quality Control Act

The intent of the Porter-Cologne Water Quality Control Act (Porter-Cologne) is to protect water quality and the beneficial uses of water, and it applies to both surface and ground water. Under this law, the State Water Resources Control Board develops statewide water quality plans, and the RWQCBs develop basin plans, which identify beneficial uses, water quality objectives, and

implementation plans. The RWQCBs have the primary responsibility to implement the provisions of both statewide and basin plans. Waters regulated under Porter-Cologne, referred to as “waters of the State,” include isolated waters that are not regulated by the USACE. Projects that require a USACE permit, or fall under other federal jurisdiction, and have the potential to impact waters of the State are required to comply with the terms of the Water Quality Certification Program. If a proposed project does not require a federal license or permit, any person discharging, or proposing to discharge, waste (e.g., soil) to waters of the State must file a Notice of Intent (NOI) or a Report of Waste Discharge and receive either waste discharge requirements (WDRs) or a waiver to WDRs before beginning the discharge.

3.2.10 State Requirements to Control Water Quality Impacts

The CWA has nationally regulated the discharge of pollutants to the waters of the U.S. from any point source since 1972. In 1987, amendments to the CWA added Section 402(p), which established a framework for regulating nonpoint source storm water discharges under the National Pollutant Discharge Elimination System (NPDES). The NPDES is a permitting system for the discharge of any pollutant (except for dredge or fill material) into waters of the U.S. In California, this permit program is administered by the RWQCBs.

Waste Discharge Requirements for Construction. The NPDES General Construction Permit requirements apply to clearing, grading, and disturbances to the ground such as excavation. Construction activities on one or more acres are subject to a series of permitting requirements contained in the NPDES General Construction Permit. This permit requires the preparation and implementation of a Stormwater Pollution Prevention Plan (SWPPP) that includes BMPs to be implemented during project construction. The project sponsor is also required to submit a Notice of Intent (NOI) with the State Water Resources Control Board Division of Water Quality. The NOI includes general information on the types of construction activities that would occur on the site.

Waste Discharge Requirements for Operation. In 1999, EPA promulgated Phase II storm water regulations, which requires the SWRCB to issue NPDES storm water permits to operators of Small MS4s within “urbanized areas,” and to Small MS4s located outside of urbanized areas serving jurisdictions with a population density of at least 1,000 people per square mile and a population of at least 10,000. The SWRCB’s Municipal Stormwater Program regulates stormwater discharges from municipal separate storm sewer systems (MS4s) throughout the state. Statewide Phase II Small MS4 NPDES General Permit Section E.12 Post Construction Storm Water Management Program requires facilities designed to evapotranspire, infiltrate, harvest/use, and treat storm water the amount of runoff specified in Numeric Sizing Criteria for Storm Water Retention and Treatment (WQO 2013-0001-DWQ and Amendments, or most current version). All newly constructed projects must be designed to meet either a volumetric or flow-based criteria (e.g., capture of runoff from an 85th percentile 24-hour storm runoff event or flow of runoff produced by a rain event equal to two times the 85th percentile hourly intensity as determined from local rainfall records). Projects must implement one or more of the following site design measures to reduce project site runoff:

- Stream Setbacks and Buffers
- Soil Quality Improvement and Maintenance
- Tree Planting and Preservation
- Rooftop and Impervious Area Disconnection
- Porous Pavement
- Green Roofs
- Vegetated Swales
- Rain Barrels and Cisterns

3.3 Local Regulations

3.3.1 Plumas County General Plan 2035

The Judicial Council, acting as the judicial branch of State government, is not subject to local land use regulations; however, the Judicial Council, as lead agency, considers local policies in evaluating whether the proposed Project's impacts would be significant.

Conservation and Open Space Element

GOAL 7.2 Biological Resources

7.2.1 Habitat Protection

The County shall protect areas that have significant habitat and wetland values, including riparian corridors, wetlands, grasslands, and creeks and rivers, from incompatible rural development. The County shall also support their protection as a method to provide carbon sequestration for greenhouse gas (GHG) emissions under applicable State programs.

7.2.2 Species and Habitat Avoidance

The County shall require new development projects to avoid or minimize adverse impacts to threatened, rare, or endangered species and critical, sensitive habitat, as defined by appropriate local, state, and federal agencies, through proper project location and design. In the event that avoidance is not feasible, the County shall require a "no-net-loss" of these sensitive natural plant or habitat communities. Wildlife habitat will be preserved and managed in a manner that will not lead to the listing of additional species as threatened and endangered or negatively impact listed threatened or endangered species.

7.2.4 Stream Corridor Development

The County shall only permit new development within stream corridors when there is no lesser environmentally damaging feasible alternative and where the best feasible mitigation measures have provided to minimize adverse environmental effects. This policy is not intended to affect the cleaning of stream channels to avoid the flooding or erosion of existing developed lands, stream restoration projects or permitted mining operations consistent with CEQA and the Surface Mining and Reclamation Act (SMARA).

7.2.6 No Net-Loss of Wetland Habitats

The County shall require new development that is subject to review under CEQA to achieve a “no-net-loss” of wetland habitat through avoidance or appropriate mitigation in consultation with the appropriate resource protection agencies.

7.2.7 Wetland and Riparian Habitat Buffers

The County shall require new development that is subject to review under CEQA to identify wetlands and riparian habitat areas and designate a buffer zone around each area sufficient to protect these habitats from degradation, encroachment, or loss. As appropriate, criteria for the development of buffer width standards shall be developed in coordination with all appropriate resource agencies and the County will continue to identify areas as Open Space and Significant Wetlands under the General Plan.

4 Methods

This section describes the methods used to complete the general biological resources assessment. The methods include a database and literature review, field survey, an assessment of plant communities and wildlife habitats and corridors, an assessment of sensitive habitats and aquatic features, and a habitat evaluation for special-status species.

4.1 Background Review

Available background information pertaining to the biological resources on and near the project site was reviewed prior to conducting field surveys. Information was compiled and subsequently compared against site conditions during the field survey. The following sources were consulted:

- California Natural Diversity Database (CNDDB) 9-USGS quadrangle record search including: *Quincy*, *Spring Garden*, *Taylorsville*, *Crescent Mills*, *Twain*, *Meadow Valley, Dogwood Peak, Onion Valley,* and *Blue Nose Mountain* (CNDDB 2025).
- California Native Plant Society (CNPS) Rare Plant Program *Inventory of Rare and Endangered Plants of California* 9-USGS quadrangle record search, including: *Quincy*, *Spring Garden*, *Taylorsville*, *Crescent Mills*, *Twain*, *Meadow Valley, Dogwood Peak, Onion Valley,* and *Blue Nose Mountain* (CNPS 2025).
- Calflora Database for information on California plants for education, research, and conservation (Calflora 2025).
- U.S. Fish and Wildlife Service (USFWS) Information for Planning and Consultation (IPaC) tool (USFWS 2025).
- eBird Database – Information on Distribution of Birds (Cornell Lab of Ornithology 2025).
- Other relevant scientific literature, technical reports, technical databases, resource agency reports, and Federal Register notices and other information published by USFWS and National Marine Fisheries Service (NMFS) to assess the current distribution of special-status plants and animals in the project region.

4.2 Field Survey

A reconnaissance field survey of the project site was conducted by MIG senior biologist David Gallagher, M.S., on September 25 and 26, 2025. The survey was conducted to provide a project-specific impact assessment for the Project as described in the project description. Specifically, the survey was conducted to (1) assess existing vegetation communities, land cover types, and habitats in the project site, and (2) assess the project site for its potential to support special-status species.

4.3 Sensitive Vegetation Communities

All vegetation communities observed on the Project site were evaluated to determine if they are considered sensitive. Sensitive natural communities are communities that are especially diverse; regionally uncommon; or of special concern to local, state, and federal agencies.

4.4 Wetlands and Other Waters

The Project site was also inspected for the presence of wetlands, drainages, streams, coastal waterways, and other aquatic features, including those that support stream-dependent (i.e., riparian) vegetation communities that could be subject to jurisdiction by the USACE, RWQCB, and/or CDFW.

5 Environmental Setting

5.1 General Project Site Description

The Project site is in downtown Quincy, California and is surrounded by commercial and residential urban development, including a bike path along a former railroad alignment and a defunct, former wastewater treatment plant to the north. The Project site is mostly developed. Ranch lands are also present north of the Project site. Quincy is in the American Valley and is surrounded by the Plumas National Forest. An unnamed drainage channel flows along the east side of the parcel south to north and empties into an unnamed tributary to Spanish Creek, which then flows into the East Branch of the North Fork of the Feather River. Spanish Creek is approximately 0.44 miles north of the Project site. The Project site is situated in the *Quincy* U.S. Geological Survey (USGS) 7.5-minute quadrangle. The Project site ranges in elevations from approximately 3,418 feet to 3,423 feet North American Vertical Datum of 1988 (NAVD88) (Google Inc. 2025).

The climate at the Project site is a warm-summer Mediterranean, with most precipitation falling in the winter and spring. Summer months are dry, and warm. Snow is common in the winter months. Climate conditions in the area include a 30-year average of approximately 42 inches of annual precipitation and 35.7 inches of annual snowfall with an average temperature range from 35.7ºF to 67.6ºF (Deters 2025).

5.2 Existing Vegetation Communities, Habitats, and Land Cover Types

The Project site is located within the Northern Sierra Nevada Foothills District of the Sierra Nevada Region, both of which are contained within the larger California Floristic Province (Baldwin et al. 2012). Where applicable, vegetation communities were mapped using CDFW's

Vegetation Classification and Mapping Program's (VegCAMP) currently accepted list of vegetation alliances and associations (CDFW 2025a). The field survey on September 25 and 26, 2025 identified three vegetation communities/land cover type on the Project site, which are summarized in Table 1, and their distribution is depicted in Appendix A, Figure 3.

Table 1. Summary of Vegetation Communities, Land Cover Types, and Habitats in the Project Site.

Vegetation Communities and Land Cover Types	Area (acres)
Wild Oats and Annual Brome Grassland Alliance	0.81
Developed	1.76
Lemmon's Willow Thickets Alliance (includes freshwater aquatic habitat)	0.30
Project Site Total	**2.87**

Wild Oats and Annual Brome Grasslands. This vegetation community is dominated by non-native annual grasses and forbs that are characteristic of disturbed areas. In the Project site, *Wild Oats and Annual Brome Grasslands* are the dominant vegetation community (Appendix B, Photo 1). Non-native grasses observed included wild oats (*Avena barbata*) and velvet grass (*Holcus lanatus)*. Native grasses observed included blue wildrye (*Elymus glaucus*). Non-native herbaceous species observed included curlycup gumweed (*Grindelia squarrosa*), tansy (*Tanacetum vulgare*), chicory (*Cichorium intybus*), field mustard (*Brassica rapa*), black medick (*Medicago lupulina*), prickly wild lettuce (*Lactuca serriola*), sweet pea (*Lathyrus latifolius*), English plantain (*Plantago lanceolata*), and woolly mullein (*Verbascum thapsus).* Native herbs observed included Canada horseweed (*Erigeron canadensis*) and California poppy (*Eschscholzia californica*).

Lemmon's Willow Thickets. This native riparian vegetation community is growing along the drainage channel, and the shrub layer is dominated by Lemmon's willow (*Salix lemmonii*) (Appendix B, Photo 2). At the time of the field visit, water was flowing in the channel. The depth of the water was shallow (less than 12 inches) and the width of the channel was approximately 5 feet to 8 feet. *Lemmon's Willow Thickets* occur along stream banks, lake shores, seeps, and mesic meadows in the middle to high Sierra Nevada and Cascades. *Carex* species (sedges) are regularly associated with *Lemmon's Willow Thickets* and represent the highest cover of the herbaceous layer. Other native trees, shrubs, and vines observed included black cottonwood (*Populus trichocarpa*), Oregon oak (*Quercus garryana*), chokecherry (*Prunus virginiana*), blueberry (*Vaccinium uliginosum*), bitter cherry (*Prunus emarginata*), and California wild grape (*Vitis californica*). Non-native trees and shrubs observed included Himalayan blackberry (*Rubus armeniacus*), paradise apple (*Malus pumila*), and catalpa (*Catalpa* sp.). Understory vegetation observed included non-native spearmint (*Mentha spicata*), teasel (*Dipsacus fullonum*), sweet pea, woolly mullein, velvet grass, and tansy. Native understory species observed included blue wild rye, sedge (*Carex* sp.), and willowherb (*Epilobium* sp.).

Developed. Developed land cover includes the buildings, paved areas, and ornamental plantings adjacent to buildings. Ornamental vegetation observed included Norway maple (*Acer platanoides*) and common lilac (*Syringa vulgaris*) (Appendix B, Photo 3).

Non-native Invasive Plant Species. Invasive plants degrade habitat quality for native plants and animals by altering vegetative structure and often reducing specific food and structural resources required by native animals. As a result, invasion of native habitats by non-natives results in adverse effects on both the native plants being displaced and native animals that would otherwise use those habitats. Because many invasive plants can easily colonize recently disturbed areas and/or tolerate repeated disturbance better than many natives, Project construction activities, such as clearing and grading, could create conditions suitable for spreading of invasive plant species. In addition, bare upland soils left after construction of temporary staging areas could encourage growth of weedy species; and mulching or erosion control mixes could include and thus introduce invasive, non-native plant species.

Five invasive species classified as highly or moderately invasive by the California Invasive Plant Council (Cal-IPC) were identified in the Project site within the *Wild Oats and Annual Brome Grasslands* and *Lemmon's Willow Thickets* vegetation communities (Table 2).

Table 2. Summary of Invasive Plants Identified in the Project Site.

Species	Cal-IPC Rating
Common Velvetgrass (*Holcus lanatus*)	Moderate
Himalayan Blackberry (*Rubus armeniacus*)	High
Tansy (*Tanacetum vulgare*)	Moderate
Teasel (*Dipsacus fullonum*)	Moderate
Wild oats (*Avena barbata*)	Moderate

6 Special-Status Species and Sensitive Habitats

For this analysis, special-status species are defined below. Impacts on these species are regulated by federal and state laws described under the Regulatory Setting in Section 3.

- Listed under the Federal Endangered Species Act (FESA) as threatened, endangered, proposed threatened, proposed endangered, or a candidate species.
- Listed under the California Endangered Species Act (CESA) as threatened, endangered, rare, or a candidate species.
- Listed by the CNPS as CRPR 1A, 1B, 2, 3, or 4.
- Designated by CDFW as a California species of special concern.
- Listed in the California Fish and Game Code as fully protected species (fully protected birds are provided in Section 3511, mammals in Section 4700, reptiles and amphibians in Section 5050, and fish in Section 5515).

6.1 Special-Status Plants

Calflora (2025), CNPS (2025), and the CNDDB (2025) identify 64 special-status plant species as occurring within the vicinity of the Project site. Of the 64 special-status species, 60 species are not expected to occur in the Project site because (1) a lack of specific habitat (e.g., coniferous woodland, chaparral, meadows, seeps, bogs or fens) and/or edaphic requirements (e.g., serpentine, alkaline, volcanic) for the species in question, (2) the geographic range of the

species does not overlap the Project site, (3) the species is known to be extirpated from the Project region, (4) the habitats within the Project site are too degraded to reasonably expect any special-status species to occur there, and/or (4) is isolated from the nearest known extant populations by development and therefore were excluded from the analysis. However, suitable habitat for four species is present on the Project site and are described in more detail below in Table 3. Expanded discussions of special-status species that may be present on the Project site are included after Table 3. The remaining 60 special-status plant species considered in this analysis are listed in Appendix C.

Table 3. Special-status Plant Species with Potential to Occur in the Project Site.

Common Name (*Scientific Name*)	Listing Status[1]	Habitat	Occurrence in the Project Site
Alder Buckthorn (*Rhamnus alnifolia*)	CRPR 2B.2	Wet meadow edges, seeps, and stream sides (riparian). Blooms May to July.	**May be present.** There is suitable habitat in the *Lemmon's Willow Thickets*. The closest documented occurrence of this species is from Brady's Campground in the Plumas National Forest in 2024, approximately 20 miles northeast of the Project site. There are five other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).
Castlegar Hawthorne (*Crataegus castlegarensis*)	CRPR 3	Stream sides in meadows, scrub, and forest (riparian). Blooms May to August.	**May be present.** There is suitable habitat in the *Lemmon's Willow Thickets.* The closest documented occurrence of this species is from Indian Creek near Crescent Falls from 2017, approximately 20 miles north of the Project site. There are three other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).
Obtuse Starwort (*Engellaria obtusa*)	CRPR 4.3	Moist areas in woodland, shaded edges of creeks (riparian). Blooms May to August.	**May be present**. There is suitable habitat in the *Lemmon's Willow Thickets.* The closest documented occurrence of this species is from the South Fork of the Feather River in 2012, approximately 22 miles south of the Project site. There are five other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).
Sheldon's Sedge (*Carex sheldonii*)	CRPR 2B.2	Mesic areas in lower montane coniferous forest, freshwater marshes, swamps, and riparian scrub. Blooms May to August.	**May be Present**. There is suitable habitat in the *Lemmon's Willow Thickets.* The closest documented occurrence of this species is from Poplar Creek near Sloat from 2023, approximately 25 miles southeast of the Project site. There are over 10 other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).

[1]Key to Status Abbreviations: Federally Endangered (FE); Federally Threatened (FT); State Endangered (SE); State Threatened (ST); California Rare Plant Rank (CRPR). CRPR 1A = Plants presumed extinct in California; CRPR 1B = Plants rare, threatened, or endangered in California and elsewhere; CRPR 2B = Plants rare, threatened, or endangered in California, but more common elsewhere; CRPR 3 = Plants about which information is needed-a review list; CRPR 4 = Plants of limited distribution-a watch list; 0.1 = seriously threatened in California; 0.2 = moderately threatened in California; 0.3 = not very threatened in California.

Alder Buckthorn. Alder buckthorn is a perennial deciduous shrub in the Rhamnaceae (buckthorn family) that is found in California and elsewhere. It occurs within wet meadow edges, seeps, and stream sides (riparian) in lower and upper montane coniferous forests. The blooming period for this species extends from May to July. It has a CRPR of 2B.2 (i.e., Rare, Threatened, or Endangered in California, But More Common Elsewhere; Moderately threatened in California). It is known from at least 69 occurrences in the last 20 years, from Lassen, Nevada, Placer, Plumas, and Sierra counties. Threats to this species include grazing and road maintenance (CNPS 2025).

Alder buckthorn may be present in the *Lemmon's Willow Thickets*. The closest documented occurrence of this species is from Brady's Camp Campground in the Plumas National Forest in 2024, approximately 20 miles northeast of the Project site. There are five other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).

Castlegar Hawthorne. Castlegar hawthorne is a perennial deciduous shrub in the Rosaceae (rose family) that is found in California and elsewhere. It occurs within stream sides (riparian) in meadows, scrub, and forest. The blooming period for this species extends from May to August. It has CRPR of 3 (Plants which more Information is needed, A Review List). More information is needed on status, rarity and threats in California. It is known from at least 19 occurrences in the last 20 years from Plumas, Modoc, and Shasta counties. Apparently widespread outside of California. Possibly threatened by logging, grazing, and recreational activities (CNPS 2025).

Castlegar hawthorne may be present in the *Lemmon's Willow Thickets*. The closest documented occurrence of this species is from Indian Creek near Crescent Falls from 2017, approximately 20 miles north of the Project site. There are three other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).

Obtuse Starwort. Obtuse starwort is a perennial rhizomatous herb in the Caryophyllaceae (pink family) that is found in California and elsewhere. It occurs within moist areas in woodland, and shaded edges of creeks (riparian) in lower and upper montane coniferous forest. The blooming period for this species extends from May to August. It has a CRPR of 4.3 (Plants of Limited Distribution, A Watch List; Not very threatened in California). It is known from at least 29 occurrences in the last 20 years from the Northern Sierra Nevada. It is also found in other counties in Northern California. Potentially threatened by logging, development, fire, trampling, grazing, and hydrological alterations (CNPS 2025).

Obtuse starwort may be present in the *Lemmon's Willow Thickets*. The closest documented occurrence of this species is from the South Fork of the Feather River in 2012, approximately 22 miles south of the Project site. There are five other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).

Sheldon's Sedge. Sheldon's sedge is a perennial rhizomatous herb in the Cyperaceae (sedge family) that is found in California and elsewhere. It occurs within wet areas, including marshes and swamps, in lower montane coniferous forest and riparian scrub. The blooming period for this species extends from May to August. It has a CRPR of 2B.2 (Plants Rare, Threatened, or Endangered in California, But More Common Elsewhere; Moderately threatened in California). It

is known from at least 39 occurrences in the last 20 years from Plumas, Placer, Lassen, and Modoc counties. Threats to this species include grazing and road maintenance (CNPS 2025).

Sheldon's sedge may be present in the *Lemmon's Willow Thickets*. The closest documented occurrence of this species is from Poplar Creek near Sloat from 2023, approximately 25 miles southeast of the Project site. There are over 10 other documented observations of this species from Plumas County since 2000 (Calflora 2025, CNPS 2025).

6.2 Special-status Animals

Based on a review of the USFWS (2025) and CNDDB (2025), eBird (Cornell Lab of Ornithology 2025), and Bumble Bee Watch (Xerces Society et al. 2025) databases; as well as species accounts and field guides (Hall 1981, Jennings and Hayes 1994, Shuford and Gardali 2008); the biologists' knowledge of sensitive species; and an assessment of the types of habitats within the Project site at the time of the site visit, it was determined that six special-status wildlife species could potentially occur within the Project site: western bumble bee (*Bombus occidentalis*), willow flycatcher (*Empidonax traillii*), yellow-breasted chat (*Icteria virens*), yellow warbler (*Setophaga petechia*), Townsend's big-eared bat (*Corynorhinus townsendii*), and western red bat (*Lasiurus frantzii)*.

Additionally, 14 other species may occasionally disperse across, forage, and/or fly over the Project site, but no suitable breeding or roosting habitat is present for these species on the site: monarch butterfly (*Danaus plexippus*), American goshawk (*Astur atricapillus*), bald eagle (*Haliaeetus leucocephalus*), black swift (*Cypseloides niger*), golden eagle (*Aquila chrysaetos*), grasshopper sparrow (*Ammodramus savannarum*), loggerhead shrike (*Lanius ludovicianus*), long-eared owl (*Asio otus*), northern harrier (*Circus hudsonius*), olive-sided flycatcher (*Contopus cooperi*), short-eared owl (*Asio flammeus*), Swainson's hawk (*Buteo swainsoni*), Vaux's swift (*Chaetura vauxi*), and yellow-headed blackbird (*Xanthocephalus xanthocephalus*).

Additionally, eight species are known in the Project vicinity but are considered absent or are not expected to occur on the Project site either because preferred habitat is absent, the species is considered extirpated from the Project region, the habitat is too fragmented, or potential dispersal barriers are present: northwestern pond turtle (*Actinemys marmorata*), foothill yellow-legged frog - Feather River Distinct Population Segment (DPS) (*Rana boylii*), Sierra Nevada yellow-legged frog (*Rana sierrae*), southern long-tailed salamander (*Ambystoma macrodactylum sigillatum*), California spotted owl (*Strix occidentalis occidentalis*), fisher (*Pekania pennanti*), gray wolf (*Canis lupus*), and Sierra Nevada mountain beaver (*Aplodontia rufa californica*).

This determination is based on an assessment of the presence of essential habitat requirements for the species, habitat connectivity with documented occurrences in the region, and/or the Project site's location within the species' known range of distribution. The legal status and likelihood of occurrence of all special-status animal species considered for their potential occurrence on the Project site are discussed in Table 4 and expanded discussions of special-status species that may be present on the Project site follow Table 4.

Western Bumble Bee. Federal Listing Status: none; State Listing Status: Candidate for Listing. The western bumble bee was historically common throughout California, including the Project region but has declined throughout much of its' range. The western bumble bee has not been detected in much of its range since the 1970s and is now considered to only occur in high elevation sites in the Sierra Nevada (Xerces Society 2018).

The western bumble bee has an annual lifecycle, which means most individuals in the colony live about one year or less and reproductive females are the only individuals that overwinter. Western bumble bee nests have been found in cavities, including in abandoned rodent burrows and above ground locations including in logs among railroad ties. Overwintering sites have generally been found underground, most often in shaded areas near trees as well as in banks without dense vegetation and in areas with tree litter, moss, or in bare patches within short grass. Western bumble bees are generalist foragers and will forage for pollen on both native and non-native plant species. Because they do not depend on any one species, they are excellent pollinators and are known to pollinate many commercial crops. Floral resource availability within a landscape is required for nesting success. However, western bumble bees likely do not require flowering resources in the immediate vicinity of their nests and may forage 300 feet or more from the entrance of the nest (Xerces Society 2018).

This species may forage and nest in the *Wild Oats and Annual Brome Grasslands* vegetation community on the Project site. This species was observed in downtown Quincy in 2014; near Butterfly Creek in 2013, approximately 5 miles northwest of the Project site; and near Pine Creek, approximately 10 miles southeast of the Project site in 2021. There are an additional 11 documented occurrences in Plumas County from 2019 to 2024 (Xerces Society et al. 2025).

Townsend's Big-eared Bat. Federal Listing Status: none; State Listing Status: Species of Special Concern. Townsend's big-eared bat is a medium-sized bat with extremely long, flexible ears, and small yet noticeable lumps on each side of the snout. They are found in a variety of habitats from forests to desert scrub. They prefer to roost in open caves. However, they will use a variety of other roost types, particularly abandoned buildings or buildings with minimal human activity, mines, tunnels, bridges, and tree cavities. When roosting they prefer large open areas and do not tuck themselves into cracks and crevices like many other bat species. This species is sensitive to disturbance, and it has been documented that they will abandon roost sites after human interference (Zeiner et al. 1988-1990).

Townsend's big-eared bat hibernates throughout its range during winter months when temperatures are between 0°C and 11.5 degrees Celsius (32-53 degrees Fahrenheit). While hibernating, it hangs alone or in small groups in the open, with fur erect to provide maximum insulation and with ears coiled back. These bats emerge late in the evening to forage and are swift, highly maneuverable fliers. Prey items include small moths, flies, lacewings, dung beetles, and sawflies (Zeiner et al. 1988-1990).

Table 4. Special-status Animal Species with Potential to Occur in the Project Site.

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
		Invertebrates	
Monarch Butterfly (*Danaus plexippus*)	FPT	Roosts in wind protected tree groves (eucalyptus, Monterey pine, cypress) with nectar and water sources nearby. Requires milkweeds (*Asclepias* spp.) host plants for breeding.	**Not Expected.** There are no overwintering sites in Plumas County, and monarchs are not expected to breed on the Project site since no *Asclepias* spp. were observed during the field visit in late September. In late winter and early spring, Monarchs migrate inland from coastal overwintering sites across the western United States, including Plumas County (Xerces Society 2025).
Western Bumble Bee (*Bombus occidentalis*)	SC	Grassland and scrub habitats with small mammal burrows for nesting and abundant floral resources for foraging.	**May be Present.** There is suitable foraging and nesting habitat in the *Wild Oats and Annual Brome Grasslands* on the Project site. The western bumble bee was historically common throughout California, including the Project region, but has declined throughout much of its' range. The species has not been detected in much of its range since the 1970s and is now considered to only occur in high elevation sites in the Sierra Nevada (Xerces Society et al. 2018). This species was observed in downtown Quincy in 2014, near Butterfly Creek in 2013, approximately 5 miles northwest of the Project site; and near Pine Creek, approximately 10 miles southeast of the Project site in 2021. There are an additional 11 documented occurrences in Plumas County from 2019 to 2024 (Xerces Society et al. 2025).
		Reptiles	
Northwestern Pond Turtle (*Actinemys marmorata*)	FPT, CSSC	Slow-moving ponds, streams, storm drain channels and other wetland habitats. Nest sites are in upland habitats, in clay or silty soils in unshaded areas such as grassland or sparsely vegetated shrubby habitats. Requires basking sites within/adjacent to aquatic habitat.	**Not Expected.** There are no documented occurrences of pond turtle from Plumas County (CNNDB 2025). There is suitable aquatic habitat in the drainage channel and there is potential upland nesting habitat in the *Wild Oats and Annual Brome Grassland* in the Project site, but pond turtle is not expected to occur in the Project site since there are no documented occurrences from Plumas County.

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
		Amphibians	
Foothill Yellow-legged Frog - Feather River DPS (*Rana boylii*)	FT, ST	Partially shaded to unshaded, rocky perennial streams and rivers, intermittent creeks, and ponds at low to moderate elevations in Pacific Coast drainages as well as the lower western slopes of the Sierra Nevada mountains. For breeding they require low gradient streams with riffles containing cobble-sized or larger rocks as substrate to be used as egg laying sites.	**Not Expected.** The closest documented observations of foothill yellow-legged frog are from Wapaunise Creek, Spanish Creek, and Rock Creek, as recently as 2017, approximately 4 miles west of Quincy in the Plumas National Forest. There is a historic occurrence from Quincy from 1899, but foothill yellow-legged frogs are considered extirpated from this site (CNNDB 2025). There is no suitable breeding habitat in the drainage channel. However, the drainage channel provides potential foraging and refugia habitat, but since there are no documented occurrences near the Project site, this species is not expected to occur on the Project site.
Sierra Nevada Yellow-legged Frog (*Rana sierrae*)	FE, ST	Inhabits lakes, ponds, meadow streams, isolated pools, and sunny riverbanks in the Sierra Nevada Mountains. Usually found in or very close to water. Egg-laying sites must be connected to permanent lakes or ponds that do not freeze to the bottom in winter.	**Not Expected.** The closest documented observations of foothill yellow-legged frog are from the Plumas National Forest, including the East Branch of Rock Creek in 2024, approximately 4 miles Southwest of Quincy; Bean Creek in 2024, approximately 7 miles northwest of Quincy; and from near Gasner Creek, approximately 1.5 miles southwest of Quincy in 2020. There are many other documented occurrences from the Plumas National Forest (CNNDB 2025). There is no suitable breeding habitat in the drainage channel. However, the drainage channel provides potential foraging and refugia habitat, but since there are no documented occurrences near the Project site, this species is not expected to occur on the Project site.
Southern Long-tailed salamander (*Ambystoma macrodactylum sigillatum*)	CSSC	Inhabits alpine meadows, high mountain ponds, and lakes in the northern Sierra Nevada south to Garner Meadows and Spicer Reservoir, and in Trinity and Siskiyou counties near the Trinity Alps. It also occurs in southwestern Oregon.	**Absent.** There are no documented occurrences in the Project region and there is no suitable habitat for this species on the Project site (CNDDB 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
		Birds	
American Goshawk (*Astur atricapillus*)	CSSC (nesting)	Breeds in North Coast Ranges through Sierra Nevada, Klamath, Cascade, and Warner Mountains. Prefers middle and higher elevations, and mature, dense conifer forests. Forages in wooded areas.	**Absent as Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally fly over the site. There are several documented occurrences for this species from Quincy since 2020 (Cornell Lab of Ornithology 2025).
Bald Eagle (*Haliaeetus leucocephalus*)	SE, FP	Breeds in large, old-growth trees or snags. Nest usually located near a permanent water source.	**Absent as a Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally fly over the site. There are many documented occurrences for this species from Quincy since 2008 (Cornell Lab of Ornithology 2025).
Black Swift (*Cypseloides niger*)	CSSC (nesting)	Breeds very locally in the Sierra Nevada and Cascade Range. Nests on cliffs behind, or adjacent to, waterfalls in deep canyons. Forages widely over many habitats.	**Absent as a Breeder.** The Project site is not in the known breeding range for this species and there is no suitable breeding habitat on the Project site. However, this species may occasionally forage over the site. This species was observed along Spanish Creek near Feather River College in 2022 (Cornell Lab of Ornithology 2025).
California Spotted Owl (*Strix occidentalis occidentalis*)	FPT, CSSC	An uncommon, permanent resident in dense, old-growth, multi-layered mixed conifer, redwood, and Douglas-fir habitats, from sea level up to approximately 7600 feet. Usually nests in tree or snag cavity, or in broken top of large tree near water. In winter, roosts in oak woodland habitats.	**Absent as Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally fly over the site. There are documented occurrences for this species from the Plumas National Forest in the Quincy area (Cornell Lab of Ornithology 2025).
Golden Eagle (*Aquila chrysaetos*)	FP	Breeds on cliffs or in large trees (rarely on electrical towers) and forages in open areas.	**Absent as a Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally fly over the site. There are many documented occurrences for this species from Quincy from 2011 to 2023 (Cornell Lab of Ornithology 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
Grasshopper Sparrow (*Ammodramus savannarum*)	CSSC (nesting)	Nests and forages in grasslands, meadows, fallow fields, and pastures. Thick cover of grasses and forbs is essential for concealment of nests.	**Absent as a Breeder.** The Project site is not in the known breeding range for this species and there is no suitable breeding habitat on the Project site. However, this species may occasionally forage on the site as a migrant. There is a documented occurrence for this species from 2023 near Quincy Junction Road, approximately 1.25 miles northeast of the Project site (Cornell Lab of Ornithology 2025).
Loggerhead Shrike (*Lanius ludovicianus*)	CSSC (nesting)	Nests in tall shrubs and dense trees; forages in grasslands, marshes, and ruderal habitats.	**Absent as a Breeder.** There is potential nesting habitat on the Project site in the *Lemmon's Willow Thickets*, but the Project site is not in the known breeding range for this species. Therefore, this species is absent as a breeder from the Project site. However, this species may occasionally forage on the site as a migrant. There are documented occurrences for this species from 2021 to 2023 along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site and other locations in Quincy (Cornell Lab of Ornithology 2025).
Long-eared Owl (*Asio otus*)	CSSC (nesting)	Nests in conifer, oak, riparian, pinyon-juniper, and desert woodlands that are either open or are adjacent to grasslands, meadows, or shrublands.	**Absent as a Breeder.** There is potential nesting habitat on the Project site in the *Lemmon's Willow Thickets*, but the Project site is not in the known breeding range for this species. Therefore, this species is absent as a breeder from the Project site. However, this species may occasionally forage on the site as a migrant. There is a documented occurrence for this species from 2021 in Gansner Park, approximately 0.65 miles northwest of the Project site (Cornell Lab of Ornithology 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
Northern Harrier (*Circus cyaneus*)	CSSC (nesting)	Nests on the ground, mostly within patches of dense, often tall, vegetation in undisturbed areas in a wide range of habitats, including freshwater marshes, brackish and saltwater marshes, wet meadows, weedy borders of lakes, rivers and streams, annual and perennial grasslands.	**Absent as a Breeder.** The Project site is not in the known breeding range for this species and there is no suitable breeding habitat on the Project site. However, this species may occasionally fly over the site as a migrant. There are many documented occurrences for this species from 2012 to 2023 in Quincy (Cornell Lab of Ornithology 2025).
Olive-sided Flycatcher (*Contopus cooperi*)	CSSC (nesting)	Nests in mature forests with open canopies, along forest edges in more densely vegetated areas, in recently burned forest habitats, and in selectively harvested landscapes.	**Absent as a Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally fly over the site. There are many documented occurrences for this species from Gansner Park, approximately 0.65 miles northwest of the Project site; and from 2009 to 2025 and other locations in Quincy (Cornell Lab of Ornithology 2025).
Short-eared Owl (*Asio flammeus*)	CSSC (nesting)	Nests in perennial grasslands, prairies, dunes, meadows and both fresh and saline water wetlands.	**Absent as a Breeder.** The Project site is not in the known breeding range for this species and there is no suitable breeding habitat on the Project site. However, this species may occasionally fly over the site as a migrant. There are documented occurrences for this species from 2025 along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site; and from 2020 near Quincy Junction Road and Bell Lane, approximately 1.75 miles northeast of the Project site (Cornell Lab of Ornithology 2025).
Swainson's Hawk (*Buteo swainsoni*)	ST	Swainson's hawks in California are strongly associated with riparian habitats, although they also are found in oak woodlands and other open habitats. Prime breeding habitat for Swainson's hawk encompasses riparian draws or clumps of trees surrounded by open grassland or oak savannah for foraging.	**Absent as a Breeder.** The Project site is not in the known breeding range for this species and there is no suitable breeding habitat on the Project site. However, this species may occasionally fly over the site as a migrant. There are documented occurrences for this species from 2022 to 2025 along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site; and from other locations in the Quincy area (Cornell Lab of Ornithology 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
Vaux's swift (*Chaetura vauxi*)	CSSC (nesting)	This species is a summer resident of northern California. Breeds in the Coast Ranges from Sonoma County. north, and very locally south to Santa Cruz County and in the Sierra Nevada. Nests in redwood and Douglas-fir habitats with nest-sites in large hollow trees and snags, especially tall, burned-out stubs; occasionally, in chimneys. Forages aerially over many habitats.	**Absent as a Breeder.** There is no suitable nesting habitat on the Project site. This species may occasionally forage over the site. There are many documented occurrences for this species from 2015 to 2021 in the Quincy area (Cornell Lab of Ornithology 2025).
Willow Flycatcher (*Empidonax traillii*)	SE	This species breeds in dense riparian and mesic upland thickets, usually near standing water in California, including the American Valley. In the spring and fall, willow flycatchers are common transients throughout California's riparian willow habitats.	**May be Present as a Breeder.** There is potential nesting habitat on the Project site in the *Lemmon's Willow Thickets.* Given that there are nearby observations during the breeding season, this species may be present as a breeder in the *Lemmon's Willow Thickets.* There are documented occurrences for this species from 2022 and 2023 during fall migration along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site and other locations from 2008 to 2024, including spring and fall migration observations from Gansner Park, approximately 0.65 miles northwest of the Project site; and the Quincy-East Quincy Wastewater Treatment Plant, approximately 0.55 miles northeast of the Project site. There are two observations from the wastewater treatment plant and Gansner Park during the breeding season from 2011 and 2024, respectively (Cornell Lab of Ornithology 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
Yellow-breasted Chat (*Icteria virens*)	CSSC (nesting)	An uncommon summer resident and migrant in coastal California and in the foothills of the Sierra Nevada. Nests in dense stands of willow and other riparian habitat.	**May be Present as a Breeder.** There is potential nesting habitat on the Project site in the *Lemmon's Willow Thickets.* Given that there are nearby observations during the breeding season, this species may be present as a breeder in the *Lemmon's Willow Thickets.* There are documented occurrences for this species during the breeding season from 2010 to 2024 in Gansner Park, approximately 0.65 miles northwest of the Project site; and near the Quincy-East Quincy Wastewater Treatment Plant, approximately 0.55 miles northeast of the Project site; and from Dillinger Pond, approximately 0.55 miles from the Project site (Cornell Lab of Ornithology 2025).
Yellow-headed Blackbird (*Xanthocephalus xanthocephalus*)	CSSC (nesting)	Breeds commonly, but locally, east of Cascade Range and Sierra Nevada, and in the Central Valley. Nests in fresh emergent wetland with dense vegetation and deep water, often along borders of lakes or ponds. Nests are always located over water. Forages in emergent wetland and moist, open areas, especially cropland and muddy shores of lakes and ponds.	**Absent as a Breeder.** There is no suitable breeding habitat on the Project site. However, this species may occasionally forage in the *Lemmon's Willow Thickets*. There are documented occurrences for this species from 2021 along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site; and from 2008 to 2014 from near Quincy-East Quincy Wastewater Treatment Plant, approximately 0.55 miles northeast of the Project site; as well as other locations in the Quincy area (Cornell Lab of Ornithology 2025).
Yellow Warbler (*Setophaga petechia*)	CSSC (nesting)	Nests in dense stands of willow and other riparian habitat.	**May be Present as a Breeder.** There is potential nesting habitat on the Project site in the *Lemmon's Willow Thickets.* Given that there are nearby observations during the breeding season, this species may be present as a breeder in the *Lemmon's Willow Thickets.* There are documented occurrences for this species during the breeding season from 2011 to 2025 from the unnamed tributary to Spanish Creek, just northeast of the Project site, including a 2018 observation approximately 100 feet outside of the Project site. There are also many other documented observations for this species from the Quincy area during breeding season (Cornell Lab of Ornithology 2025).

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
		Animals	
Townsend's Big-eared Bat (*Corynorhinus townsendii*)	CSSC	Townsend's big-eared bat is found throughout California, but the details of its distribution are not well known. This species is found in all but subalpine and alpine habitats and may be found at any season throughout its range. Natural roost habitat includes caves and large basal hollows of large trees. Also, roosts in abandoned buildings or buildings with minimal human activity, mines, and bridges (Kunz 1982, Pierson et al. 2006, Szewczak 2013).	**May be Present.** This species may roost and breed in the old Quincy Lumber and Supply building, which is open in the front and back; and there are numerous other openings on the outside of the building that bats can use to get inside. This species may also roost in the open garage structure. Currently, there appears to be no substantial human activity occurring in the structure other than a small office space, occupied by a business, at the front of the building, which is closed off from the open areas of the building, and for storage of a large RV. There have been 21 documented occurrences of this species from Plumas County since 2001, with the closest occurrence approximately 5 miles northwest of the Project site along Blackhawk Creek Road in 2002 (CNDDB 2025). Even though evidence of roosting bats was not detected during the site visit, the Quincy Lumber and Supply building and open garage structure provides suitable roosting and breeding habitat. Therefore, this species may occupy these structures in the future.
Western Red Bat *(Lasiurus frantzii)*	CSSC	The western red bat is locally common in riparian habitats of California, from Shasta County to the Mexican border, west of the Sierra Nevada/Cascade crest, and deserts. The winter range includes western lowlands and coastal regions south of San Francisco Bay. Roost sites are often in tree foliage along the edges of mature riparian habitats. May also roost in urban riparian habitats (Kunz 1982, Pierson et al. 2004, Szewczak 2013, Solick et al. 2020).	**May be Present.** There is one documented occurrence of this species from 2000, approximately 15 miles east of the Project site near Little Grizzly Creek in the Plumas National Forest (CNDDB 2025). Even though there is only one documented occurrence from Plumas County, there is suitable roosting and possible breeding habitat in *the Lemmon's Willow Thickets*. Therefore, this species may be present.

Common Name	Regulatory Status[1]	Habitat	Potential For Occurrence
Fisher (*Pekania pennanti*)	CSSC	Uncommon permanent resident of the Sierra Nevada, Cascades, and Klamath mountains. Occurs in intermediate to large-tree stages of coniferous forests and deciduous-riparian habitats with a high percent canopy closure.	**Absent.** There are six documented observations of this species from Plumas County, five of which are older than 40 years. There is one documented occurrence from 2015, approximately 30 miles northwest from the Project site near Little Grizzly Campground in Plumas National Forest. There is no habitat for this species present or adjacent to the Project site, therefore this species is considered absent from the Project site.
Gray Wolf (*Canis lupus*)	FE, SE	Gray wolves have a circumpolar range including North America, Europe and Asia. The wide range of habitats in which wolves can thrive includes temperate forests, mountains, tundra, taiga, grasslands, and deserts. Most of the known wolf activity and packs occur in the northeastern portion of the state, including Plumas County. Wolf packs can generally have territories of up to 200 square miles. Dispersing wolves can also travel long distances.	**Absent.** Gray Wolves have been confirmed active in the eastern Plumas and southern Lassen County areas, including the Quincy area (Beyem Seyo and Diamond packs). From 2011 to 2024, 132 individual wolves have been detected in California. However, this species is not expected to regularly occur or take up permanent residence in the urban areas of Quincy and is therefore considered absent from the Project site (CDFW 2025b).
Sierra Nevada Mountain Beaver (*Aplodontia rufa californica*)	CSSC	Permanent resident in the Cascade, Klamath, and Sierra Nevada ranges. Populations are localized and uncommon in the Sierra Nevada. Mountain beavers occur in dense riparian-deciduous and open, brushy stages of most forest habitats.	**Absent.** There are 11 documented occurrences of this species from Plumas County since 2000, with the closest occurrence near Deanes Valley Campground in the Plumas National Forest, approximately 9 miles southwest of the Project site in 2000. While the drainage channel and the *Lemmon's Willow Thickets* provide marginal habitat for the species, mountain beavers are not expected to make substantial use of these habitats in and adjacent to the Project site due to the urban setting of the Project site. Therefore, this species is considered absent on the Project site.

[1]Key to Status Abbreviations: Federally Listed as Endangered (FE); Federally Listed as Threatened (FT); Federal Candidate for Listing (FC), Federal Proposed Threatened (FPT); State Listed as Endangered (SE); State Listed as Threatened (ST); State Candidate for Listing (SC); State Fully Protected (FP); California Species of Special Concern (CSSC)

Even though evidence of roosting bats in buildings and structures was not detected during the site visits, the Quincy Lumber and Supply building and open garage structure provides suitable roosting and breeding habitat for Townsend's big-eared bat. Therefore, this species may occupy these structures in the future. There have been 21 documented occurrences of this species from Plumas County since 2001, with the closest occurrence approximately 5 miles northwest of the Project site along Blackhawk Creek Road in 2002 (CNDDB 2025).

Western Red Bat. Federal Listing Status: none; State Listing Status: Species of Special Concern. The western red bat is locally common in some areas of California, occurring from Shasta County to the Mexican border, west of the Sierra Nevada/Cascade crest and deserts. The winter range includes western lowlands and coastal regions south of San Francisco Bay. There is migration between summer and winter ranges, and migrants may be found outside the normal range (Pierson et al. 2004).

The western red bat roosts primarily in tree foliage, especially in cottonwood, sycamore, and other riparian trees or orchards, specifically walnut trees. The bat prefers habitat edges and mosaics with trees that are protected from above and open below with open areas for foraging, including grasslands, shrublands, and open woodlands. They are solitary by nature but will gather in larger nursery roosts during the summer. Known to occur up to 8,250 feet but breeding females primarily occur in low-elevation cottonwood/sycamore and oak dominated riparian habitats, with many breeding records from the Central Valley at elevations below 700 feet (Pierson et al. 2004). Western red bats have also been detected in riparian habitats in urban areas (Krauel and LeBuhn 2016).

This species may possibly roost and possibly breed in the *Lemmon's Willow Thickets*. There is one documented occurrence of this species from 2000, approximately 15 miles east of the Project site near Little Grizzly Creek in the Plumas National Forest. (CNDDB 2025).

Willow Flycatcher. Federal Listing Status: None; State Listing Status: Endangered. Historically, the willow flycatcher nested throughout California wherever thickets of riparian deciduous shrubs, primarily willow (*Salix* spp.) occurred (Grinnell and Miller 1944). The species is typically associated with broad, open river valleys or large mountain meadows with extensive growth of shrubby willows. Dense willow thickets are required for nesting and roosting, while low exposed branches are used for singing posts and hunting perches (Zeiner et al. 1988-1990).

In the last four decades, breeding populations have been extirpated from most of the lower elevation riparian areas in California because of cowbird parasitism and habitat destruction. Habitat destruction and degradation have been caused by a variety of activities including livestock grazing, and agricultural and urban development.

The Willow Flycatcher now occurs only in small numbers as a summer resident, primarily at scattered wet meadows and montane riparian habitats above 4,000 feet in the Sierra Nevada and southern Cascades, and along a few waterways in the arid southwestern portion of the state. The Sierra Nevada–southern Cascades population in California is especially vulnerable, with fewer than 200 pairs remaining. The Little Truckee River watershed and nearby locations in Sierra and Nevada counties represent one of only a few remaining strongholds for the species

in California, with a cluster of meadows that collectively retained approximately 30 territories at least until 2000 (Loffland et al. 2022).

In the Sierra Nevada, willow flycatcher breeding season occurs from late May or early June (territory establishment) to the middle of September (fledgling independence). The nesting period lasts approximately 14 days. Most young fledge between July 15 and August 31, and fledglings remain in the territory for 2 to 3 weeks post-fledging. Willow flycatchers feed primarily on insects, many of which have aquatic larval stages (Sanders and Flett 1989).

Willow flycatcher may nest in the *Lemmon's Willow Thickets*. There are documented occurrences for this species from 2022 and 2023 during fall migration along an unnamed tributary to Spanish Creek, approximately 700 feet northeast of the Project site and other locations from 2008 to 2024, including spring and fall migration observations from Gansner Park, approximately 0.65 miles northwest of the Project site; and the Quincy-East Quincy Wastewater Treatment Plant, approximately 0.55 miles northeast of the Project site. There are two observations from the wastewater treatment plant and Gansner Park during the breeding season from 2011 and 2024, respectively (Cornell Lab of Ornithology 2025).

Yellow-breasted Chat. Federal Listing Status: None; State Listing Status: Species of Special Concern (nesting). The yellow-breasted chat is a summer resident in California from March to September and breeds from April through August. It mainly breeds in early successional riparian habitat with a well-developed, dense shrub layer and open canopy. It winters in the tropics, where it is found in open scrub and woodland edges in lowland areas. It forages by searching among foliage among dense low tangles or by perching to eat insects and berries. Habitat loss and degradation are most likely the greatest threat to this species (Comrack 2008).

This species may nest in the *Lemmon's Willow Thickets.* There are documented occurrences for this species during the breeding season from 2010 to 2024 in Gansner Park, approximately 0.65 miles northwest of the Project site; and near the Quincy-East Quincy Wastewater Treatment Plant, approximately 0.55 miles northeast of the Project site; and from Dillinger Pond, approximately 0.55 miles from the Project site (Cornell Lab of Ornithology 2025).

Yellow Warbler. Federal Listing Status: None; State Listing Status: Species of Special Concern (nesting). The yellow warbler is a widespread neotropical migrant that inhabits wet deciduous forests throughout North America (Lowther et al. 1999). In California, yellow warblers occupy wooded riparian habitats along the coast, on both eastern and western slopes of the Sierra Nevada, and throughout the northern portion of the state (Heath 2008). Their range has remained relatively stable over time, but populations have declined substantially in many localities due to habitat loss and expansion of the brood-parasitic brown-headed cowbird (*Molothrus ater*) (Cain et al. 2003, Heath 2008). Ideal nesting habitat for yellow warblers consists of riparian corridors with dense, shrubby understory and open canopy (Lowther et al. 1999; Cain et al. 2003; Heath 2008). Yellow warblers nest from early May through early August and construct open cup nests in upright forks of shrubs or trees in dense willow thickets or other dense vegetation (Lowther et al. 1999).

This species may nest in the *Lemmon's Willow Thickets*. There are documented occurrences for this species during the breeding season from 2011 to 2025 from the unnamed tributary to Spanish Creek, just northeast of the Project site, including a 2018 observation approximately 100 feet outside of the Project site. There are also many other documented observations for this species from the Quincy area during breeding season (Cornell Lab of Ornithology 2025).

6.3 Nesting Birds

Nesting birds may occur on buildings, trees, shrubs, understory vegetation, and shallow scrapes on bare ground in and around the Project site. All migratory bird species are protected under California Fish and Game Code.

6.4 Bat Colonies

Bats tend to forage and roost near freshwater sources. The unnamed drainage provides a perennial source of freshwater within and adjacent to the Project site. Cavities within trees, foliage, tree bark, and structures in and adjacent to the Project site may provide suitable day and maternity roost habitat for many species of bats.

Roost sites play a critical role in mating, hibernation, rearing young, conserving energy, and protection from adverse weather and predators. Selection of roost sites is influenced by distribution and abundance of food resources, risks of predation, as well as the physical attributes of the roost itself. Roost selection is paramount to the success of a species, and the removal of roost habitat could adversely impact the survivorship of a species (Kunz 1982).

Depending upon species, maternity roosts can host from a few to thousands of reproductive female bats that congregate during spring and summer months to give birth and nurse their young. In California, maternity roosts may remain active from April through August. As a potentially uncommon and limited resource, maternity roosts may be the limiting resource for a local population of bats and thus may be essential to the survival of a local bat population. Maternity roosts tend to have sensitivity to disturbance, with documented instances of abandonment even during the presence of flightless young. As bats have a low reproductive rate of typically one pup per year, negative impacts to maternity roosts can have profound impacts on a local population of bats (Szewczak 2013).

The disturbance of roosting habitat of any bat species would be considered significant under CEQA guidelines. The Project site as well as adjacent areas contain potential suitable roosting habitat for Townsend's big-eared bat and western red bat (see Table 4). Other bat species that may roost in crevices in structures on the Project site include hoary bat (*Aeorestes cinereus*), big brown bat (*Eptesicus fuscus*), silver-haired bat (*Lasionycteris noctivagans*), California myotis (*Myotis californicus*), small-footed myotis (*Myotis ciliolabrum*), long-eared myotis (*Myotis evotis*), little brown myotis (*Myotis lucifugus*), fringed myotis (*Myotis thysanodes*), long-legged myotis (*Myotis volans*), and Yuma myotis (*Myotis yumanensis*).

6.5 Sensitive and Regulated Plant Communities and Habitats

Natural communities have been considered part of the Natural Heritage Conservation triad, along with plants and animals of conservation significance, since the state inception of the

Natural Heritage Program in 1979. CDFW determines the level of rarity and imperilment of vegetation types; and tracks sensitive communities in its Rarefind database (CNDDB 2025). Global rankings (G) of natural communities reflect the overall condition (rarity and endangerment) of a habitat throughout its range, whereas state (S) rankings reflect the condition of a habitat within California. Natural communities are defined using NatureServe's standard heritage program methodology as follows (CDFG 2007):

- G1/S1: Less than 6 viable occurrences or less than 2,000 acres
- G2/S2: Between 6 and 20 occurrences or 2,000 to 10,000 acres
- G3/S3: Between 21 and 100 occurrences or 10,000 to 50,000 acres
- G4/S4: The community is apparently secure, but factors and threats exist to cause some concern
- G5/S4: The community is demonstrably secure to ineradicable due to being common throughout the world (for global rank) or the state of California (for state rank)

State rankings are further described by the following threat code extensions:

- S1.1: Very threatened
- S1.2: Threatened
- S1.3: No current threats known

In addition to tracking sensitive natural communities, CDFW also ranks vegetation alliances, defined by repeating patterns of plants across a landscape that reflect climate, soil, water, disturbance, and other environmental factors (Sawyer et al. 2009). If an alliance is marked G1-G3, all the vegetation associations within it will also be of high priority (CDFG 2007). CDFW provides the Vegetation Classification and Mapping Program's (VegCAMP) currently accepted list of vegetation alliances and associations (CDFW 2025).

Natural Communities of Special Concern. There are no CDFW classified sensitive natural communities within the Project site.

Sensitive Vegetation Alliances. There is one sensitive vegetation association within the Project site, *Lemmon's Willow Thickets Alliance*, which is classified by CDFW as "G4 S3", which means that this community is at a moderate risk of extirpation throughout its range in California (Appendix A, Figure 3).

Waters of the U.S./State. The USACE and RWQCB would need to determine whether the drainage channel meets the definition of Waters of the U.S./State and would also need to determine if impacts to the drainage channel would require a permit. Waters of the State include waters of the U.S. and generally also extend to the top of bank (TOB), but RWQCB may also claim riparian habitat (*Lemmon's Willow Thickets*) that extends beyond the TOB and other areas within the 100-year flood plain. (Appendix A, Figure 3).

CDFW Stream/Riparian Habitat. As described above under Regulatory Setting, the California Fish and Game Code includes regulations governing the use of, or impacts to, many of the state's fish, wildlife, and sensitive habitats, including the bed and banks of rivers, lakes, and streams. The unnamed drainage and its associated riparian habitat (*Lemmon's Willow Thickets*)

are potentially subject to CDFW jurisdiction under Section 1600 et seq. of State Fish and Game Code (Appendix A, Figure 3).

Critical Habitat/Essential Fish Habitat (EFH). There is no Critical Habitat or EFH on the Project site.

7 Project Impacts on Sensitive Biological Resources and Avoidance and Minimization Measures

This section describes potential impacts to sensitive biological resources—including special-status plants and animals, and waters of the U.S. and the state—that may occur as a result of implementing the Project.

The CEQA Guidelines define which impacts are considered significant. The Act defines “significant effect on the environment” as “a substantial adverse change in the physical conditions which exist in the area affected by the proposed Project.” Potential impacts to biological resources were determined in accordance with Appendix G of the CEQA Guidelines. Impacts would be considered potentially significant if the proposed Project will:

a) "have a substantial adverse effect, either directly or through habitat modifications, on any species identified as a candidate, sensitive, or special status species in local or regional plans, policies, or regulations, or by the California Department of Fish and Game or U.S. Fish and Wildlife Service".
b) "have a substantial adverse effect on any riparian habitat or other sensitive natural community identified in local or regional plans, policies, regulations or by the California Department of Fish and Game or U.S. Fish and Wildlife Service".
c) "have a substantial adverse effect on state or federally protected wetlands (including, but not limited to, marsh, vernal pool, coastal, etc.) through direct removal, filling, hydrological interruption, or other means”.
d) "interfere substantially with the movement of any native resident or migratory fish or wildlife species, or with established native resident or migratory wildlife corridors, or impede the use of native wildlife nursery sites".
e) "conflict with any local policies or ordinances protecting biological resources, such as a tree preservation policy or ordinance".
f) "conflict with the provisions of an adopted Habitat Conservation Plan (HCP), Natural Community Conservation Plan (NCCP), or other approved local, regional, or state habitat conservation plan".

Direct take of a federally or state listed species is considered a significant impact. Per Section 3(18) of FESA, the term take means to harass, harm, pursue, hunt, shoot, wound, kill, trap, capture, or collect, or to attempt to engage in any such conduct. Temporary and/or permanent habitat loss is not considered a significant impact to sensitive species (other than for listed or candidate species under the FESA and CESA), unless a significant percentage of total suitable habitat throughout the species’ range is degraded or somehow made unsuitable, or areas supporting a large proportion of the species’ population are substantially and adversely

impacted. Potential impacts to nesting bird species and bat colonies would be considered significant due to their protection under California Fish and Game Code.

The Project proposes two design options as part of the post-construction treatment of stormwater runoff (Design Option 1 and Design Option 2 – see Section 2 for a description of each option). The design options share many of the following proposed mitigation measures, and conceptually the implementation of the measures is the same for both design options. However, Design Option 2 includes the removal of about 0.30 acres of *Lemmon's Willow Thickets,* including aquatic habitat, which would have greater potential for impacts to biological resources than Design Option 1 since the area of impact associated with a typical outfall for similar projects is substantially less. Therefore, Design Option 2 may face additional scrutiny from resources agencies (i.e., USACE, RWQCB, and/or CDFW) when applying for permits, and those agencies may deny the permits or impose greater mitigation requirements on the Project.

7.1 Impacts to Special-Status Plant Species

Design Option 1 or Design Option 2

If present, Project activities within the drainage channel and adjacent riparian habitat associated with the implementation of Design Option 1 or Design Option 2 may affect alder buckthorn, Castlegar hawthorn, Rocky Mountain chickweed, and Sheldon's sedge due to disturbance or destruction of individuals or suitable habitat. Direct impacts could include grading or filling areas supporting these species, trampling, or crushing of plants, and soil compaction. Indirect impacts could include increased mobilization of dust onto plants, which can affect their photosynthesis and respiration, or changes to hydrology supporting these plants due to grading or construction in nearby habitats.

Conservation of alder buckthorn and Sheldon's sedge, which are special-status species and considered fairly threatened in California, is important because even the smallest of populations contribute to preserving the genetic resources for these species and ensuring their persistence in Plumas County and the state. For plants on the watchlist or which have limited distribution in California (Castlegar hawthorn and obtuse starwort), conservation of populations of these species is also important since more current and accurate information is still needed on the distribution and ecology of these species.

With the implementation of Mitigation Measures BIO-1a through BIO-1c, potential impacts to these species will be ***less than significant with mitigation.***

Mitigation Measure BIO-1a. **Pre-Activity Focused Survey for Special-status Plants**. Prior to initial ground disturbance in the Project site, and during the appropriate blooming period for each species: alder buckthorn (May - July), Castlegar hawthorn (May - August), obtuse starwort (May - August), and Sheldon's sedge (May - August), focused surveys will be conducted by a qualified plant ecologist within suitable habitat in the Project site and a 50-foot buffer around the Project site, where feasible. A qualified plant ecologist is an individual who has minimum of a BA or BS in biological sciences or related discipline (e.g., environmental sciences) and professional work experience in biological sciences, including a minimum of two survey seasons conducting surveys for each special-status plant species that will be surveyed.

The purpose of the survey will be to assess the presence or absence of special-status species. If no special-status species are found in the Project site or in the 50-foot buffer, then no further mitigation will be warranted. The results of the survey will be documented. If a special-status species is found on the Project site, then Mitigation Measure BIO-1b will be implemented.

Mitigation Measure BIO-1b. **Avoidance Buffers**. To the extent feasible, and in consultation with a qualified plant ecologist, the Judicial Council and/or its contractorwill construct the Project to avoid impacts on all populations of special-status plant species within the Project site or within the identified buffer of the impact area described in Mitigation Measure BIO-1a. Avoided special-status plant populations will be protected by establishing and observing the identified buffer between plant populations and the impact area. All such populations located in the impact area or the identified buffer, and their associated designated avoidance areas, will be clearly depicted on any construction plans. In addition, prior to initial ground disturbance or vegetation removal, the limits of the identified buffer around special-status plants to be avoided will be flagged or fenced. The flagging will be maintained intact and in good condition throughout Project-related construction activities. If avoidance is not feasible then Mitigation Measure BIO-1c will be implemented.

Mitigation Measure BIO-1c. **Provide a Mitigation Plan for Impacts to Special-status Plants.** If the impact on special-status plants cannot be avoided, the Judicial Council shall comply with CDFW's determination of the appropriate measures to mitigate the Project's significant impacts on special-status plants. These measures may include preserving and enhancing existing populations, creation of off-site populations on Project mitigation sites through seed collection or transplantation, and/or restoring or creating suitable habitat in sufficient quantities to mitigate against loss.

7.2 Impacts to Western Bumble Bee

Design Option 1 or Design Option 2

Construction activities, including tree and shrub removal, clearing of downed woody debris, and grading activities could result in the destruction of active nests of western bumble bee, and result in the injury or death of adults, eggs, and larvae. However, with the implementation of Mitigation Measures BIO-2a to BIO-2c, potential impacts on western bumble bee will be ***less than significant with mitigation***.

Mitigation Measure BIO-2a: Pre-construction/Pre-disturbance Survey for Western Bumble Bee. Prior to the start of construction activities, including tree removal, staging of equipment, and/or grading activities, a qualified biologist shall conduct pre-construction surveys for western bumble bee nests. The qualified biologist shall have a degree in biological sciences, or similar degree; knowledge in the life history and ecology of western bumble bee and their identification; and have a minimum of two field seasons of experience conducting focused surveys with positive identification of western bumble bee.

Pre-construction surveys shall entail a minimum of three visual encounter surveys for foraging western bumble bees and their active nests. Surveys should be conducted during the height of the active flight season (April - September) when probability of detection is highest, and in the

same year that Project activities are planned to start. These surveys should be spaced 2 to 4 weeks apart to account for variability in resource use and availability. Surveys shall be conducted during dry conditions (i.e., when it is not raining, foggy, or drizzling), when temperatures are above 70° Fahrenheit, and during low wind speeds (i.e., less than 8 miles per hour) (CDFW 2023). If the pre-construction surveys do not identify western bumble bee nests, no additional surveys or mitigation is required. If western bumble bee nests are observed, then Mitigation Measure BIO-2b will be implemented.

Mitigation Measure BIO-2b: Prepare a Habitat Protection Plan for Western Bumble Bee. If western bumble bee nests are detected on the Project site, the qualified biologist shall prepare a plan to protect active nests and surrounding foraging areas and protect potential overwintering habitat within the Project site. The plan shall be implemented as part of the site activities. The plan shall include, but not be limited to, the following measures:

- Fencing or flagging to delineate no-disturbance buffers around active nest sites.
- Construction monitoring during initial ground disturbance activities.
- Avoidance of initial ground disturbance between November and February to protect potential overwintering queen western bumble bees.
- Retaining existing woody debris to support overwintering queen bumble bees.
- Where erosion control and/slope stabilization are required, prescription of seed mix composed of locally native flower species, known to be visited by western bumble bee.

Mitigation Measure BIO-2c: Obtain an Incidental Take Permit. If “take” or adverse impacts to western bumble bee cannot be avoided, then CDFW shall be consulted to determine if a CESA Section 2080 Incidental Take Permit (ITP) is required. If an ITP is required, the Project shall comply with any requirements of the ITP.

7.3 Impacts to Willow Flycatcher

Construction Disturbance

Design Option 1 or Design Option 2

Willow flycatchers are protected under CESA. Direct take of a state-listed species is considered a significant impact. Furthermore, willow flycatchers and their nests are protected under the Migratory Bird Treaty Act (MBTA) and California Fish and Game Code. Project activities must comply with CESA, and the provisions of the MBTA and California Fish and Game Code (i.e., avoid take of protected nesting birds).

Construction disturbance during the willow flycatcher breeding season (late May through mid-August) could result in the incidental loss of eggs or nestlings, either directly through the destruction or disturbance of active nests or indirectly by causing the abandonment of nests. In addition, noise and increased construction activity could temporarily alter foraging behavior, potentially resulting in the abandonment of nest sites. However, with the implementation of Mitigation Measure BIO-3 below, Project construction impacts on willow flycatcher will be ***less than significant with mitigation***.

Mitigation Measure BIO-3: Pre-Construction/Pre-Disturbance Protocol-level Surveys for Willow Flycatcher

Avoidance. To the extent feasible, construction activities, including mobilization and staging, surveying, clearing, grubbing, vegetation removal, fence installation, demolition, grading, and any other related activities, should be scheduled to avoid the nesting season. If construction activities are scheduled to take place outside the nesting season, all impacts to nesting birds protected under the MBTA and California Fish and Game Code would be avoided. The nesting season for willow flycatcher generally extends from late May through mid-August.

Pre-Construction Protocol-level Surveys. If construction and construction noise will occur within the avian nesting season (from late May to mid-August), all suitable habitats located within the Project's area of disturbance, including staging and storage areas plus a 250-foot buffer around these areas shall be thoroughly surveyed, as feasible, for the presence of active nests. The survey protocol (Bombay et al. 2003) requires the following:

- A minimum of two separate surveys in one year at each site; one during survey period 2 (June 15-25) and one during either survey period 1 (June 1-14), or survey period 3 (June 26-July 15) to document presence or absence of willow flycatchers in the survey year.
- To be considered a separate survey, visits must be at least 5 days apart; surveys done fewer than 5 days apart are not considered to be in separate survey periods.
- Follow-up visits are required when a flycatcher is detected and suspected but not confirmed to be a willow flycatcher.
- The surveys will be conducted by a qualified biologist. The qualified biologist shall have a degree in biological sciences, or similar degree; knowledge in the life history and ecology of the willow flycatcher; and have a minimum of two field seasons of experience conducting protocol-level surveys for willow flycatchers with positive identification of willow flycatchers. The qualified biologist will also have the necessary regulatory agency permits and be approved by CDFW to conduct willow flycatcher surveys.
- The results of the surveys shall be documented per the requirements of the protocol.

If the surveys result in the location of active nests, no site disturbance and/or mobilization of heavy equipment (including but not limited to equipment staging, fence installation, clearing, grubbing, vegetation removal, fence installation, demolition, grading, and soil stockpiling), shall take place within 250 feet of Willow Flycatcher nests unless smaller buffers are determined to be appropriate by the qualified biologist in consultation with CDFW.

Potential Loss of Habitat

<u>Design Option 1</u>

The installation of a stormwater outfall pipe that discharges into the existing drainage channel could impact willow flycatcher nesting and foraging habitat by removing or altering the *Lemmon's Willow Thickets*. The area of vegetation removal would be limited to the stormwater pipeline and outfall constructed zone and the loss of vegetation would not significantly reduce

the habitat available to willow flycatcher due to the small impact area and the presence of additional nearby nesting habitat. The impact is ***less than significant.***

Design Option 2

If the drainage channel is culverted, there would be a permanent loss of the *Lemmon's Willow Thickets* along the length of the drainage channel on the property, which may result in the loss of nesting and foraging habitat available to willow flycatcher*,* if present. Given the availability of higher quality nesting and foraging habitat in the Project region, the loss of willow flycatcher habitat from project removal of *Lemmon's Willow Thickets* will not be significant. Further, if the Project results in the permanent loss of *Lemmon's Willow Thickets*, CDFW may require mitigation for the loss of habitat (see Mitigation Measure BIO-8a in Section 7.8 below). The impact is ***less than significant.***

7.4 Impacts to Yellow-breasted Chat, Yellow Warbler, and Other Nesting Birds

Construction Disturbance

Design Option 1 or Design Option 2

All migratory bird species and their nests are protected under the Migratory Bird Treaty Act (MBTA) and California Fish and Game Code. Project activities must comply with the provisions of the MBTA and California Fish and Game Code (i.e., avoid take of protected nesting birds).

Construction disturbance during the avian breeding season (February 1 - September 15, for most species) could result in the incidental loss of eggs or nestlings, either directly through the destruction or disturbance of active nests or indirectly by causing the abandonment of nests. In addition, noise and increased construction activity could temporarily alter foraging behavior, potentially resulting in the abandonment of nest sites. However, with the implementation of Mitigation Measure BIO-4 below, impacts on yellow-breasted chat, yellow warbler, and other nesting birds will be ***less than significant with mitigation***.

Mitigation Measure BIO-4: Pre-Construction/Pre-Disturbance Survey for Nesting Birds.

Avoidance. To the extent feasible, construction activities, including mobilization and staging, surveying, clearing, grubbing, vegetation removal, fence installation, demolition, grading, and any other related activities, should be scheduled to avoid the nesting season. If construction activities are scheduled to take place outside the nesting season, all impacts to nesting birds protected under the MBTA and California Fish and Game Code would be avoided. The nesting season for most birds in Plumas County extends from February 1 to September 15.

Pre-Construction Surveys. If construction and construction noise occur within the avian nesting season (February 1 - September 15), all suitable habitats located within the Project's area of disturbance, including staging and storage areas plus a 250-foot (passerines) and 1,000-foot (raptor nests) buffer around these areas shall be thoroughly surveyed, as feasible, for the presence of active nests. The surveys shall be conducted by a qualified biologist no more than 5 days before commencement of any vegetation trimming, site disturbance activities and/or equipment mobilization. If Project activities are delayed by more than 5 days, an additional nesting bird survey shall be performed. Active nesting is present if a bird is building a nest,

sitting in a nest, a nest has eggs or chicks in it, or adults are observed carrying food to the nest. The results of the surveys shall be documented.

A qualified biologist is an individual who has minimum of a BA or BS in biological sciences or related discipline (e.g., environmental sciences) and professional work experience in biological sciences, including a minimum of two survey seasons conducting surveys for avian species in the Project region or in other areas with similar habitats.

If pre-construction nesting bird surveys result in the location of active nests, no site disturbance and/or mobilization of heavy equipment (including but not limited to equipment staging, fence installation, clearing, grubbing, vegetation removal, fence installation, demolition, grading, and soil stockpiling), shall take place within 250 feet of non-raptor nests and 1,000 feet of raptor nests, unless smaller buffers are determined to be appropriate by a qualified biologist. If work is required within the buffers, the qualified biologist will assess the level of disturbance from the planned work and determine if a smaller buffer is warranted (e.g., installation of sheet pile with an impact hammer would not warrant a smaller buffer, but minor grading and excavation may warrant a smaller buffer). If the qualified biologist determines that a smaller buffer is warranted, then the planned work may proceed. The qualified biologist will observe the behavior of the nesting bird(s) and/or chicks during the onset of the planned work and if the nesting bird(s) and/or chicks do not show signs of distress then work may resume within the smaller buffer. If the nesting bird(s) and/or chicks show signs of distress, then the planned work will cease within the smaller buffer and work may resume within the original buffer established. The buffer shall remain in place until the chicks have fledged. Monitoring by a qualified biologist will ensure compliance with MBTA and relevant California Fish and Game Code requirements. Monitoring dates and findings shall be documented.

Potential Loss of Habitat

Design Option 1

The installation of a stormwater outfall pipe that discharges into the existing drainage channel could impact the *Lemmon's Willow Thickets* by removal of vegetation. The area of vegetation removal would be limited to the stormwater pipeline and outfall constructed zone and the loss of vegetation would not significantly reduce the habitat available to yellow-breasted chat, yellow warbler, and other nesting birds due to the small impact area and the presence of additional nearby nesting habitat. The impact is ***less than significant***.

Design Option 2

If the drainage channel is culverted, there would be a permanent loss of up to 0.3 acres of the *Lemmon's Willow Thickets*, which may result in the loss of nesting and foraging habitat for yellow-breasted chat, yellow warbler and other nesting birds, if observed nesting in the *Lemmon's Willow Thickets.* Given the availability of higher quality nesting and foraging habitat in the Project region, these impacts will not be significant. However, CDFW may require mitigation for the permanent loss of *Lemmon's Willow Thickets* (see Mitigation Measure BIO-8a in Section 7.8 below). The impact is ***less than significant.***

7.5 Impacts to Migratory Birds

Avian Collisions with Windows

Design Option 1 or Design Option 2

Glass windows, including facades, have the potential to cause injury or mortality to birds when birds collide with these surfaces. Birds do not perceive glass as an obstruction in the same way that humans do. As a result, they may collide with glass walls or windows if the glass reflects the sky or nearby vegetation and is not perceived as an obstruction, when transparent glass appears to be a clear pathway, or when vegetation behind transparent glass (such as behind glass railings) appears unobstructed (Loss et al. 2014, Sheppard and Phillips 2015). Additionally, interior and exterior lighting, especially when pointed upward, can disorient birds and potentially attract them to buildings, increasing collision risks. These risks are highest for buildings in or near areas of high avian activity or movement, such as migratory corridors, large open spaces, large water bodies, and riparian habitats.

The *Lemmon's Willow Thickets* riparian corridor provides potential habitat for a variety of bird species, which could forage and travel through the Project site given the proximity of the *Lemmon's Willow Thickets* to the proposed location of the new building (Appendix A, Figure 2). Additionally, if the Project incorporates landscaping with trees, shrubs, and herbaceous vegetation around the building and parking areas, this vegetation will attract birds in the area and increase bird activity around the buildings. Therefore, following construction of the Project, birds using the on-site landscaping and flying between landscaped areas on the site and the unnamed drainage channel riparian corridor may collide with the building, resulting in the death of migratory and non-migratory species. Individual special-status bird species are not expected to make use of the landscaping on the Project site; however, all native migratory birds regardless of special status are protected under the Migratory Bird Protection Act (California Fish and Game Code 3513).

The most common bird strike zone is from the ground to 60 feet, and then again at 500 feet for skyscrapers (Loss et al. 2015) with glazing. Glazing starts to be a hazard to birds at about 24 square feet in size. Since detailed building specifications will be developed during the design-build process, it is conservatively assumed that building glass will not be made with patterns or light reflectance values that would be more visible to birds and thereby reduce the likelihood of collision with the glass.

The Project will be designed and constructed in accordance with the California Trial Court Facility Standards, which include lighting strategies to reduce glare and light pollution such as LED luminaires compliant with International Dark-Sky Association requirements and exterior lighting levels reduced during nighttime hours of inactive periods. The 2025 California Green Building Standards Code (CALGreen) Nonresidential Voluntary Measures (found in Title 24, Part 11, Appendix A5, Section A5.107) include bird-friendly design provisions for new construction and major alterations. These voluntary standards specify that a portion of a building's facade is treated to reduce bird collisions. The Facilities Standards do not incorporate these voluntary measures.

The proposed building will be adjacent to a riparian corridor that may attract a variety of birds including migratory birds, regardless of whether the Project implements Design Option 1 or Design Option 2. The proposed building could result in a cumulatively significant loss of birds over time when considered alongside other similar buildings in the Project area. However, the implementation of Mitigation Measure BIO-5 would minimize the loss of birds by window strike to less than a significant level. The impact is ***less than significant with mitigation***.

Mitigation Measure BIO-5: Standards for Bird Safe Buildings. The Project shall implement the applicable bird-friendly design standards from the 2025 California Green Building Standards Code A5.107 (ICC 2025), which may include the following building specifications:

- At least 90% of glazing on building elevations between grade and 40 feet high, and at least 60% of glazing above 40 feet above grade will use bird-friendly mitigation strategies.
- Glazing with visual markers shall include, but is not limited to, the following:
    - Etched or fritted glass with patterns of elements on the exterior.
    - Interior or exterior glazing film with 2 × 2 visual markers.
    - Laminated glass with 2 × 2 visual markers, patterned ultraviolet (UV) coating or use of contrasting patterned UV-absorbing and UV-reflecting films.
    - Glass block or channel glass.
    - Developed glazing technologies documented to reduce bird strikes.
- Glazing protected by exterior features that create a visible barrier in front of the glazing, may include, but not be limited to:
    - Horizontal or vertical slats, grills, netting or sunshades.

Additionally, the Project shall implement the applicable bird-friendly design options for landscaping and lighting from *Reducing Bird Collisions with Buildings and Buildings Glass Best Practices* (USFWS 2021), which may include the following:

Lighting

- Avoid unnecessary lighting, including perimeter lighting.
- Install motion sensors on all lights (both interior and exterior) that activate only when people are present.
- Ensure all exterior lighting is “fully shielded”, so that all light is only emitted downward below the lowest light emitting part of the fixture.
- Ensure that any lights that are not motion-activated are turned off at night, especially architectural lighting, interior lighting, and lobby or atrium lighting.

Landscaping

- Avoid using glass in supplemental structures (e.g., bus shelters, guard rails, glass walls, etc.). If unavoidable, use glass with visual markers or exterior features listed above.
- Avoid planting trees and shrubs adjacent to, seen through, or reflected in any glass structures. If unavoidable, use glass with visual markers or exterior features listed above.
- Avoid placing indoor plants adjacent to clear glass windows or move them far enough away so that they can't be seen from the outside.

For all measures intended to avoid and minimize the likelihood of bird strikes at the Project, the relevant guidance documents should be consulted for detailed discussion and descriptions of the applicable design specifications.

Additionally, the proposed design specifications to minimize bird strikes will be approved by a qualified biologist with experience in both avian ecology and analyzing bird strike potential from buildings.

7.6 Impacts on Townsend's Big-eared Bat, Western Red Bat, and Bat Colonies

Design Option 1 or Design Option 2

Bats may roost in the old Quincy Lumber and Supply building, other structures/buildings, and trees within the Project site. Pre-construction and construction activities, including abatement, demolition, use of heavy equipment, removal of vegetation, and other pre-construction and construction activities may result in the injury or mortality of individuals. Additionally, noise from generators, powerpacks, heavy equipment, and other construction activities could result in the disturbance of active maternity or day roosts, disrupt foraging and dispersal behavior of bats, and may result in roost abandonment.

Therefore, Project-related impacts to roosting bats would be considered potentially significant. However, with the implementation of Mitigation Measures BIO-6a to BIO-6c below, impacts to roosting bats will be reduced to less than significant. The impact is ***less than significant with mitigation***.

Mitigation Measure BIO-6a: Avoidance and Minimization of Impacts to Special-Status Bats and Sensitive Bat Colonies. No less than 6 months prior to Project initiation, a habitat assessment for roosting bats shall be conducted for all buildings and trees on the Project site and within 100 feet of the site, as access allows. A qualified bat biologist will conduct the survey and will look for evidence of bat use in buildings and trees.

A qualified bat biologist is defined as a biologist with a degree in biology, ecology, zoology, or related degree, is knowledgeable in life histories of bat species, can correctly identify bat species, has demonstrable experience conducting field surveys/assessments with positive findings and mitigation planning (i.e., avoidance, minimization, compensatory) for bats and is familiar with survey protocols, and is knowledgeable of state and federal laws protecting sensitive species.

If evidence of use is observed, or if roost sites are present in areas where evidence of bat use might not be detectable (such as crevices), an evening survey that utilizes bat acoustic detectors will be conducted to determine if bats are roosting on the site, the species, and the location of the roost. The evening survey must be conducted during the appropriate time of year when bats are detectable in the region (March 15 - September 15, or as determined by the qualified biologist). If an active roost of special-status bats, maternity colony, or winter hibernacula of non-special-status bats is detected, construction activities will be modified or revised to avoid disturbance of the roost. If an active roost of special-status bats, maternity colony, or winter hibernacula of non-special-status bats cannot be avoided, removal or disturbance of the roost will be scheduled to take place outside the maternity roost season (April 15 - September 15), and winter hibernacula season (October 15 - March 1). If special-status bats, maternity colony, or winter hibernaculum is detected and construction work cannot be modified or revised to avoid removal or disturbance of the occupied roost, the qualified bat biologist shall develop a bat mitigation plan (see Mitigation Measure BIO-6b).

Mitigation Measure BIO-6b: Bat Mitigation Plan. At a minimum, the bat mitigation plan will include methods for humane bat exclusion, including the timing of the exclusion, type of exclusion devices to be used, and no-disturbance buffers around any sensitive roosts adjacent to the Project area. Acceptable timing for exclusion is September 15 - October 15 or March 1 - April 15. The timing may be adjusted by the qualified biologist based on regional weather patterns.

The bat mitigation plan shall also prescribe replacement bat roost habitat that is specific to the type of roost and the species being displaced. The plan will describe (1) the type of roost habitat being removed, (2) type of replacement habitat structure to be constructed/installed, (3) location of the replacement habitat, (4) performance standards for the use of the habitat by the displaced species, and (5) timeline for monitoring the use of the habitat, and (6) the credentials of the biologist performing/overseeing the exclusion. This plan will be implemented at least 30 days prior to eviction of bats from the roost.

Mitigation Measure BIO-6c: Tree Removal.-To minimize impacts on individual roosting western red bats, trees without a maternity colony or winter hibernacula may be removed September 15 - October 15 or March 1 - April 15. Additionally, trees shall be removed when evening temperatures are above 45° F, daytime temperatures are at least 65°F, and there is no forecasted rain for 48 hours before or after tree removal activities. Once these conditions have been met, the following process shall be followed to remove trees with potential roost habitat.

- Remove trees in two steps over a period of 2 days where portions of the trees containing no habitat are removed on the first day and the remaining portion of the tree with habitat is removed on the second day. All branch removal shall be conducted using chainsaws or similar handheld equipment.
- When removing the tree on the second day, work should be conducted in a sensitive manner, and where reasonably practicable, so that the cut tree is lowered to the ground and left for at least 48 hours to allow any existing bats to leave the tree unharmed.

- A qualified bat biologist shall be present to point out potential roost habitat to the tree removal contractor and to monitor tree removal.

7.7 Impacts on Sensitive Vegetation Communities

The *Lemmon's Willow Thickets* is classified as a sensitive community by CDFW and may be regulated by the RWQCB and/or CDFW under Section 1600 of the California Fish and Game Code because it is also considered riparian habitat. Permits from the RWQCB and CDFW may require additional conservation and mitigation measures than what are described below.

Artificial Lighting

Many animals, including special-status species, are sensitive to light cues, which influence their physiology and influence their behaviors, particularly during the breeding season (de Molenaar et al. 2006). It is known that photoperiod (the relative amount of light and dark in a 24-hour period), is an essential cue triggering physiological processes such as growth, metabolism, development, breeding behavior, and molting in birds, mammals, and many other taxa, suggesting that increases in ambient light may interfere with these processes across a wide range of species and result in impacts on wildlife populations (Beier 2006; de Molenaar et al. 2006).

Artificial lighting may also indirectly affect mammals and birds by increasing the nocturnal activity of predators like owls, hawks, and mammals (Negro et al. 2000, Longcore and Rich 2004, DeCandido and Allen 2006, Beier 2006). The presence of artificial light may influence habitat use by rodents and by breeding birds (Beier 2006; de Molenaar et al. 2006) by causing avoidance of well-lit areas, resulting in a net loss of habitat availability and quality.

<u>Design Option 1</u>

The Lemmon's Willow Thickets on the project site occur in a narrow band of drainage channel within an urban setting. Under Design Option 1, the existing riparian habitat including the Lemmon's Willow Thickets sensitive community would remain along the drainage channel and could be illuminated by Project outdoor lighting. If the proposed Project implements Design Option 1 and includes the installation of lighting that illuminates the *Lemmon's Willow Thickets* and drainage channel, such lighting could potentially have adverse effects on wildlife species present in these habitats.

Facilities Standards require LED lights with motion sensors in parking lots and dimmed lighting during inactive periods with an exemption for nighttime security lighting. The Facilities Standards prohibit light emissions beyond the property but do not include restrictions that would specifically prevent illumination of the sensitive riparian habitat along the property drainage channel. To avoid significant impact, lighting should be low intensity, directed inward to the Project site rather than directing any lighting toward the *Lemmon's Willow Thickets* and drainage channel, and downward toward the ground for any permanent lighting. CalGreen Code A5.203.1.1.1.1 specifies that newly installed outdoor lighting power shall be no greater than 90% of Allowed Outdoor Lighting Power and shall have a color temperature no higher than 3000K which is consistent with the Dark Sky Association requirements. CalGreen Code A5203.1.1.1.2 specifies that outdoor pole-mounted and arm-mounted luminaires should be

installed with tilting not greater than 10 degrees, or the outdoor luminaires shall be installed with arm-mount or tenon-mount capable of tilting less than or within 10 degrees. The Facilities Standards do not incorporate these voluntary measures. With Mitigation Measure BIO-7, implementation of the CalGreen voluntary measures and specification of dimmed lights during inactive periods without exemption would reduce the illumination impact on Lemmon's Willow Thickets and riparian habitats to a less than significant level. Therefore, the impact of artificial light on sensitive communities and riparian habitat is ***less than significant with mitigation incorporated*.**

Mitigation BIO-7: Outdoor Lighting Plan. The Project shall implement an outdoor lighting plan that includes reduced lighting in parking areas during inactive periods specified in Facilities Standards 16.C.1.h.

The outdoor lighting plan shall also incorporate design standards from the 2025 CalGreen Code A5.203, which shall include the following specifications:

- A5.203.1.1.1 Newly installed outdoor lighting power shall be no greater than 90 percent of the Allowed Outdoor Lighting Power, and general hardscape lighting within the scope of Title 24, Part 6, Section 140.7(b)1 shall have a color temperature no higher than 3000K. The Allowed Outdoor Lighting Power calculation is specified in Title 24, Park 6, Section 140.7, Requirements for Outdoor Lighting.
- A5.203.1.1.1.2 Outdoor pole mounted luminaries shall be installed with tilting not greater than 10 degrees, or the outdoor luminaires shall be installed with arm-mount or tenon-mount capable of tilting less than or within 10 degrees.

Design Option 2

If the Project implements Design Option 2 and the drainage channel is culverted, the *Lemmon's Willow Thickets* would be removed. With the permanent loss of the *Lemmon's Willow Thickets*, there would be **no impact** of artificial lighting on the *Lemmon's Willow Thickets* and associated riparian habitat.

Loss of Vegetation

Design Option 1

Ground clearance and excavation activities to install the stormwater outfall pipe that discharges stormwater into the existing drainage channel could impact the *Lemmon's Willow Thickets* in the Project area and may require permits from the RWQCB and/or CDFW.

Examples of significant permanent impacts that may require CDFW authorization include removal of trees and other woody vegetation, grading, and placement of fill (e.g., rip rap, concrete, shotcrete). Examples of significant temporary impacts that may also require authorization from CDFW, include removal of understory herbaceous vegetation, creation of temporary access points, and substantial tree trimming.

Additionally, the presence of Himalayan blackberry, which is classified as highly invasive by Cal-IPC and four other species classified as moderately invasive at the Project site creates a threat of spreading invasive weeds into areas of the *Lemmon's Willow Thickets* disturbed by the Project (See Table 2 for a complete list of invasive species observed).

If the Project impacts the *Lemmon's Willow Thickets*, the area of vegetation removal would be limited to the stormwater pipeline and outfall construction zone. Designing the outfall to minimize or avoid permanent loss of vegetation and replanting the disturbed area after installation would minimize the impact to the *Lemmon's Willow Thickets*. The vegetation loss would mostly be temporary and any permanent loss of this vegetation community would be minimal or avoided. Replacement of vegetation through implementation of Mitigation Measures BIO-8a and BIO-8c, would reduce impacts to the *Lemmon's Willow Thickets* to a less-than-significant level. As a result, the impact to sensitive communities under Design Option 1 is ***less than significant with mitigation incorporated***.

Design Option 2

If the drainage channel is culverted, ground clearance and excavation activities to install the culvert would result in a permanent loss of up to 0.3 acres of the *Lemmon's Willow Thickets* in the Project site and may require permits from the RWQCB and/or CDFW. Replacement of vegetation through implementation of Mitigation Measure BIO-8a would be needed to reduce impacts to the *Lemmon's Willow Thickets* to a less-than-significant level. With implementation of Mitigation Measure BIO-8a, the impact to sensitive communities under Design Option 2 is ***less than significant with mitigation incorporated***.

Mitigation Measure BIO-8a: A Habitat Mitigation and Monitoring Plan (HMMP). For Design Option 1 or Design Option 2, an HMMP shall be prepared and implemented to replace and protect sensitive native habitats (including aquatic habitat – see Section 7.9 below) in the Project site. Onsite restoration will include replacement and/or habitat enhancement ratios at a minimum 1:1 mitigation ratio for temporary and permanent impacts on *Lemmon's Willow Thickets* as well as aquatic habitat. If on-site restoration is not feasible, then offsite in-kind restoration or preservation will also be at a minimum 1:1 mitigation ratio, unless an applicable regulatory agency requires a higher or lower restoration or preservation mitigation ratio. Specific recommendations are provided below.

- identify the responsible parties.
- describe Project impacts to habitat types and functions and values.
- identify specific sites for restoration and identify the amount and type of habitat restored in each site.
- set goals and performance standards for the restoration.
- set goals and performance standards for the control of invasive weeds with a Cal-IPC Inventory rating of moderate or high.
- provide a detailed implementation plan, including a schedule for completing and monitoring the restoration, financial assurances, construction drawings for a planting/restoration plan, an irrigation plan if appropriate, and maintenance requirements.
- specify monitoring requirements and a minimum monitoring period of 5 years, with annual reports.
- identify contingency and adaptive management measures if restoration does not meet performance standards.

The HMMP may be included with any permit applications to the USACE, RWQCB, and CDFW, and the ultimate details will be refined pending agency comments. Permit requirements related to the HMMP shall be incorporated into the final HMMP that is implemented.

Mitigation Measure BIO-8b: Construction Measures to Minimize Invasive Plant Infestations. For Design Option 1, the following measures shall be taken during construction to minimize invasive plant infestation and potential impacts of invasive plants on sensitive vegetation communities:

- All ground disturbing equipment used adjacent to native habitats will be washed (including wheels, tracks, and undercarriages) both before and after being used at the Project site. Worker personal gear, including boots, should also be cleaned and clear of plant material prior to entering the Project site work area.
- All seeds and straw materials used on Project site shall be weed-free rice straw, and all gravel and fill material shall be certified weed free.
- The Project will implement erosion control measures to reduce stormwater runoff which can carry the seed of invasive plants to sensitive vegetation habitats (see Section 7.9 below).
- All disturbed soils within sensitive habitats will be stabilized and planted in accordance with the restoration plan prepared for the Project (see Mitigation Measure BIO-8a).
- Soil and vegetation removed from weed-infested areas will not be used in general soil stockpiles and will not be redistributed as topsoil cover for the newly filled areas. All weed-infested soil will be disposed of off-site at a landfill or buried at least 2.5 feet below final grade.

Mitigation Measure BIO-8c: Long-term Riparian Protection Measures. To ensure appropriate long-term maintenance of and avoidance of impacts to the *Lemmon's Willow Thickets* as well as aquatic habitat for Design Option 1, the Judicial Council will implement a notification process for all future Judicial Council site managers such that no vegetation management along the banks of or in the unnamed drainage channel would occur without consultation with a qualified biologist if work would occur within the banks of the drainage channel.

7.8 Impacts on Jurisdictional Waters and Wetlands

The drainage channel (aquatic habitat) has not been evaluated by USACE for agency determination of whether it meets the definition of Waters of the U.S. Impacts to the drainage channel are potentially subject to jurisdiction by the USACE, RWQCB, and CDFW. Permits from the USACE, RWQCB, and/or CDFW may require additional conservation and mitigation measures than what are described below.

Additionally, construction projects in California causing land disturbances that are equal to 1.0 acre or greater must comply with State requirements to control the discharge of stormwater pollutants under National Pollutant Discharge Elimination System (NPDES)/Construction General Permit. Prior to the start of construction/demolition, a Notice of Intent must be filed with

the State Water Board describing the Project. A Storm Water Pollution Prevention Plan (SWPP) must be developed and maintained during the Project, and it must include the use of BMPs to protect water quality until the site is stabilized. Standard permit conditions under the NPDES/Construction General Permit require that the applicant utilize various measures including on-site sediment control best management practices, damp street sweeping, temporary cover of disturbed land surfaces to control erosion during construction, and utilization of stabilized construction entrances and/or wash racks, among other methods. The NPDES General Permit also requires projects be designed to evapotranspire, infiltrate, harvest/use, and treat storm water prior to discharge. These regulatory requirements address the water quality of stormwater pollutants potentially discharged to the drainage channel.

Design Option 1

The installation of a stormwater outfall pipe that discharges stormwater into the existing drainage channel could impact the drainage channel in the Project site and may require permits from USACE, RWQCB, and/or CDFW.

Examples of significant permanent impacts that may require authorization include removal of trees and other woody vegetation, installation of a stormwater outfall, grading, placement of fill (e.g., rip rap, concrete, shotcrete). Examples of significant temporary impacts that may also require authorization include removal of understory herbaceous vegetation, creation of temporary access points, and substantial tree trimming, and degradation of surface or ground water quality due to erosion and transport of fine sediments and contaminants into the channel and downstream aquatic habitat, which could adversely affect fish and wildlife within this habitat.

If the Project implements Design Option 1, implementation of Mitigation Measures BIO-8a and BIO-8b (see Section 7.8 above) and compliance with the requirements to control the discharge of stormwater pollutants under the NPDES Construction General Permit would reduce impacts to potential Waters of the U.S./state to ***less than significant with mitigation incorporated***.

Design Option 2

If the drainage channel is culverted, there will be a permanent loss of aquatic habitat in the Project site, which may require permits from the USACE, RWQCB, and/or CDFW.

If the Project implements Design Option 2, implementation of Mitigation Measures BIO-8a and BIO-8b (see Section 7.8 above) and compliance with the requirements to control the discharge of stormwater pollutants under the NPDES Construction General Permit would reduce impacts to Waters of the U.S./state to ***less than significant with mitigation incorporated***.

7.9 Impacts on Wildlife Movement

Design Option 1 or Design Option 2

Continuous riparian buffers also provide important wildlife migration corridors, which are critical “movement highways” for terrestrial species such as mammals and reptiles as well as for water dependent species such as amphibians and waterfowl. Wildlife corridors play an important role in countering habitat fragmentation. A wildlife corridor is a landscape element which serves as a linkage between historically connected habitats or landscapes that are otherwise separated and

is meant to provide avenues along which wildlife can travel, migrate, and find mates; plants can propagate; genetic interchange can occur; populations can move in response to environmental changes and natural disasters; and individuals can re-colonize habitats from which populations have been locally extirpated. Corridors can consist of a sequence of stepping-stones across the landscape (i.e., discontinuous areas of habitat such as isolated wetlands and roadside vegetation), continuous lineal strips of vegetation and habitat (e.g., riparian strips and ridge lines), or they may be parts of larger habitat areas of known or likely importance to local wildlife.

The unnamed drainage channel, including associated riparian habitat may function as a wildlife movement corridor for a variety of terrestrial and aquatic species given its connectivity to tributaries of Spanish Creek. However, since the Project site is surrounded by commercial and residential development and is not adjacent to any natural open space areas, the Project site likely functions as an isolated corridor primarily for wildlife that are commonly found in developed or urban areas. Furthermore, urban adapted species may also breed within and around the Project site, but no regionally important wildlife nursery areas are present in the Project site or would be impacted by the Project.

Grading and other construction activities could restrict some wildlife species from moving between suitable habitat patches during construction within and adjacent to the Project site. In addition, noise and disturbance associated with construction activities could impact habitat connectivity within the site during construction for species that commonly use habitats in the Project site. If dewatering of the unnamed drainage channel is required during construction, the movement of aquatic species will be temporarily impeded during construction. Furthermore, if Project construction also occurred at night, when many nocturnal mammals, reptiles, and amphibians are active, use of the Project site by dispersing nocturnal animals would be limited during construction

After Project completion, based on the current conceptual plans including the implementation of Design Option 1 or Design Option 2 for the Project, there would be a permanent loss of dispersal habitat due to the loss of vegetation communities, i.e., *Wild Oats and Annual Brome Grasslands*, but will likely be limited to common species that are regionally abundant. Thus, the restriction of movement across the site during construction and after Project completion is not expected to have a substantial impact on their regional populations. Therefore, impacts to the movement of wildlife are ***less than significant***.

7.10 Impacts due to Conflicts with Local Policies

Design Option 1 or Design Option 2

While the Judicial Council is not subject to local land use regulations and ordinances, the Judicial Council considered local policies and ordinances intended to protect biological resources in evaluating the Project’s impacts. Relevant local policies are identified above in section 3.3.

The Project would not conflict with the Plumas County Conservation and Open Space Element. While the Project Design Option 2 proposes the removal of riparian habitat, such removal would not be incompatible with rural development because the drainage channel is already culverted up to the Project's boundary (Policy 7.2.1). With Mitigation Measures BIO-1 through BIO-8, the

Project will avoid or minimize impacts to threatened, rare, and endangered species, and sensitive habitat, and will not conflict with Policy 7.2.2. The Project is proposed for a previously developed site, and to the extent the drainage might be considered a stream corridor the Project is not new development and does not conflict with Policy 7.2.4 relating to flooding, erosion, and stream restoration projects; and the County has expressed support for Design Option 2 (R. Thorman, personal. Communication, March 20, 2026). Although Design Option 2 would remove wetland habitat along the drainage channel, as described in Sections 7.3 and 7.4, that habitat is of limited value and higher quality nesting and foraging habitat already exists in the Project region. Under Mitigation Measure BIO-8a, the Project would provide for no net loss of habitat. If the relevant permitting agency requires additional no-net-loss or habitat enhancement, the Project would comply with any permit conditions. Thus, the Project would not conflict with Policy 7.2.6. Under Design Option 1, which would preserve the riparian habitat, the Project site is already fully developed and Project development will not encroach further onto the habitat. The existing buffer would remain intact, and the Project would not conflict with Policy 7.2.7. Impacts to special-status species and sensitive habitats would also be avoided or minimized through Mitigation Measures BIO-1 through BIO-8.

With implementation of the mitigation measures outlined in this report, the Project's impact on biological resources does not conflict with any local policies protecting biological resources in the Plumas County General Plan 2035 (Plumas County 2013).

7.11 Impact due to Conflicts with an Adopted Habitat Conservation Plan

Design Option 1 or Design Option 2

The Project site is not within an area covered by an HCP or NCCP. As a result, the Project would have ***no impact*** related to a conservation plan.

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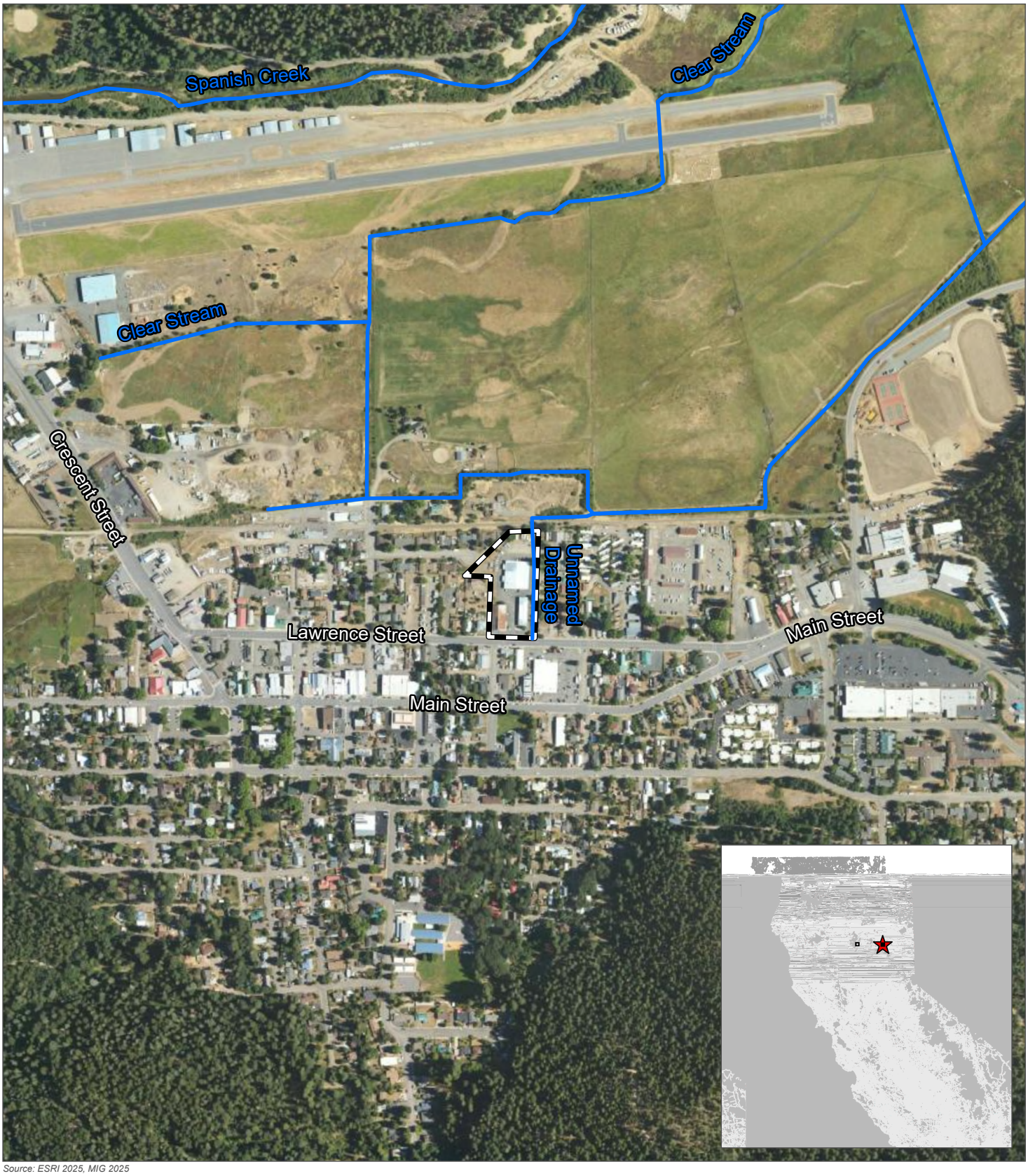
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Appendix A Figures



Source: ESRI 2025, MIG 2025

Project Site

US Feet
0 250 500 1,000

Figure 1 Project Location

New Quincy Courthouse Project

MIG



Source: ESRI 2025, Plumas County 2025, MIG 2025

Unnamed Drainage

Project Site

Proposed Building

Proposed Parking

0 62.5 125 250 US Feet

Figure 2 Proposed Building Footprint

New Quincy Courthouse Project

MIG



Source: ESRI 2025, MIG 2025

Vegetation Communities and Land Cover Types

- Wild Oats and Annual Brome Grassland Alliance
- Lemmon's Willow Thickets Alliance
- Developed

Base Map Features

- Unnamed Drainage
- Project Site

0 62.5 125 250 US Feet

Figure 3 Vegetation Communities and Land Cover Types

New Quincy Courthouse Project

MIG

Appendix B Photographs



Photo 1. *Wild Oats and Annual Brome Grasslands* vegetation community within the Project site.



Photo 2. *Lemmon's Willow Thickets* and drainage channel along the eastern boundary of the Project site.



Photo 3. Developed land cover in the Project site.

Appendix C Special-status Plants

Scientific Name	Common Name	Lifeform	Regulatory Status	Habitat
Arctostaphylos mewukka ssp. *truei*	True's manzanita	perennial evergreen shrub	4.2	Chaparral, Lower montane coniferous forest
Astragalus webberi	Webber's milk-vetch	perennial herb	1B.2	Broadleafed upland forest, Lower montane coniferous forest, Meadows and seeps
Astragalus whitneyi var. *lenophyllus*	woolly-leaved milk-vetch	perennial herb	4.3	Alpine boulder and rock field, Subalpine coniferous forest (rocky)
Azolla microphylla	Mexican mosquito fern	annual/perennial herb	4.2	Marshes and swamps (ponds, slow water)
Boechera constancei	Constance's rockcress	perennial herb	1B.1	Chaparral, Lower montane coniferous forest, Upper montane coniferous forest
Botrychium minganense	Mingan moonwort	perennial rhizomatous herb	4.2	Bogs and fens, Lower montane coniferous forest, Meadows and seeps (edges), Upper montane coniferous forest
Brasenia schreberi	watershield	perennial rhizomatous herb (aquatic)	2B.3	Marshes and swamps (freshwater)
Bruchia bolanderi	Bolander's bruchia	moss	4.2	Lower montane coniferous forest, Meadows and seeps, Upper montane coniferous forest
Carex buxbaumii	Buxbaum's sedge	perennial rhizomatous herb	4.2	Bogs and fens, Marshes and swamps, Meadows and seeps (mesic)
Carex geyeri	Geyer's sedge	perennial rhizomatous herb	4.2	Great Basin scrub, Lower montane coniferous forest
Carex lasiocarpa	woolly-fruited sedge	perennial rhizomatous herb	2B.3	Bogs and fens, Marshes and swamps (freshwater, lake margins)
Carex limosa	mud sedge	perennial rhizomatous herb	2B.2	Bogs and fens, Lower montane coniferous forest, Marshes and swamps, Meadows and seeps, Upper montane coniferous forest
Carex petasata	Liddon's sedge	perennial herb	2B.3	Broadleafed upland forest, Lower montane coniferous forest, Meadows and seeps, Pinyon and juniper woodland
Carex scabriuscula	Siskiyou sedge	perennial rhizomatous herb	4.3	Lower montane coniferous forest, Meadows and seeps, Upper montane coniferous forest
Carex scoparia var. *scoparia*	pointed broom sedge	perennial herb	2B.2	Marshes and swamps (freshwater)
Ceanothus fresnensis	Fresno ceanothus	perennial evergreen shrub	4.3	Cismontane woodland (openings), Lower montane coniferous forest
Chenopodium simplex	large-seeded goosefoot	annual herb	4.3	Lower montane coniferous forest (openings, disturbed areas) , PJWld (carbonate)
Clarkia mildrediae ssp. *lutescens*	golden-anthered clarkia	annual herb	4.2	Cismontane woodland, Lower montane coniferous forest (openings)
Clarkia virgata	Sierra clarkia	annual herb	4.3	Cismontane woodland, Lower montane coniferous forest
Claytonia palustris	marsh claytonia	perennial herb	4.3	Marshes and swamps, Meadows and seeps (mesic), Upper montane coniferous forest
Corallorhiza trifida	northern coralroot	perennial rhizomatous herb (achlorophyllous)	2B.1	Lower montane coniferous forest, Meadows and seeps (edges)
Cypripedium californicum	California lady's-slipper	perennial rhizomatous herb	4.2	Bogs and fens, Lower montane coniferous forest
Cypripedium fasciculatum	clustered lady's-slipper	perennial rhizomatous herb	4.2	Lower montane coniferous forest, North Coast coniferous forest
Cypripedium montanum	mountain lady's-slipper	perennial rhizomatous herb	4.2	Broadleafed upland forest, Cismontane woodland, Lower montane coniferous forest, North Coast coniferous forest
Darlingtonia californica	California pitcherplant	perennial rhizomatous herb (carnivorous)	4.2	Bogs and fens, Meadows and seeps
Eleocharis torticulmis	California twisted spikerush	perennial rhizomatous herb	1B.3	Bogs and fens, Lower montane coniferous forest, Meadows and seeps
Epilobium luteum	yellow willowherb	perennial stoloniferous herb	2B.3	Lower montane coniferous forest (seeps, Streambanks), Meadows and seeps
Eremogone cliftonii	Clifton's eremogone	perennial herb	1B.3	Chaparral, Lower montane coniferous forest, Upper montane coniferous forest
Erigeron lassenianus var.*deficiens*	Plumas rayless daisy	perennial herb	1B.3	Lower montane coniferous forest
Erigeron petrophilus var. *sierrensis*	northern Sierra daisy	perennial rhizomatous herb	4.3	Cismontane woodland, Lower montane coniferous forest, Upper montane coniferous forest
Eriogonum umbellatum var. *ahartii*	Ahart's buckwheat	perennial herb	1B.2	Chaparral, Cismontane woodland
Eriophorum gracile	slender cottongrass	perennial rhizomatous herb (emergent)	4.3	Bogs and fens, Meadows and seeps, Upper montane coniferous forest
Eurybia merita	subalpine aster	perennial herb	2B.3	Upper montane coniferous forest

Scientific Name	Common Name	Lifeform	Regulatory Status	Habitat
Frangula purshiana ssp. *ultramafica*	Caribou coffeeberry	perennial deciduous shrub	1B.2	Chaparral, Lower montane coniferous forest, Meadows and seeps, Upper montane coniferous forest
Hackelia amethystina	amethyst stickseed	perennial herb	4.3	Lower montane coniferous forest, Meadows and seeps, Upper montane coniferous forest
Hartmaniella sierrae	Sierra starwort	perennial rhizomatous herb	4.2	Chaparral, Cismontane woodland, Lower montane coniferous forest, Upper montane coniferous forest
Ivesia webberi	Webber's ivesia	perennial herb	1B.1, FT	Great Basin scrub (volcanic ash), Lower montane coniferous forest, Pinyon and juniper woodland
Lewisia cantelovii	Cantelow's lewisia	perennial herb	1B.2	Broadleafed upland forest, Chaparral, Cismontane woodland, Lower montane coniferous forest
Lewisia kelloggii ssp. *hutchisonii*	Hutchison's lewisia	perennial herb	3.2	Upper montane coniferous forest
Lupinus dalesiae	Quincy lupine	perennial herb	4.2	Chaparral, Cismontane woodland, Lower montane coniferous forest, Upper montane coniferous forest
Lycopus uniflorus	northern bugleweed	perennial herb	4.3	Bogs and fens, Marshes and swamps
Meesia triquetra	three-ranked hump moss	moss	4.2	Bogs and fens, Meadows and seeps, Subalpine coniferous forest, Upper montane coniferous forest (mesic)
Mielichhoferia elongata	elongate copper moss	moss	4.3	Broadleafed upland forest, Chaparral, Cismontane woodland, Coastal scrub, Lower montane coniferous forest, Meadows and seeps, Subalpine coniferous forest
Monardella follettii	Follett's monardella	perennial shrub	1B.2	Lower montane coniferous forest (rocky, serpentine)
Oreostemma elatum	tall alpine-aster	perennial herb	1B.2	Bogs and fens, Meadows and seeps, Upper montane coniferous forest
Orthocarpus bracteosus	rosy orthocarpus	annual herb	2B.2	Meadows and seeps
Peltigera gowardii	western waterfan lichen	foliose lichen (aquatic)	4.2	Riparian forest
Penstemon personatus	closed-throated beardtongue	perennial herb	1B.2	Chaparral, Lower montane coniferous forest, Upper montane coniferous forest
Piperia colemanii	Coleman's rein orchid	perennial herb	4.3	Chaparral, Lower montane coniferous forest
Piperia leptopetala	narrow-petaled rein orchid	perennial herb	4.3	Cismontane woodland, Lower montane coniferous forest, Upper montane coniferous forest
Poa sierrae	Sierra blue grass	perennial rhizomatous herb	1B.3	Lower montane coniferous forest
Potamogeton epihydrus	Nuttall's ribbon-leaved pondweed	perennial rhizomatous herb (aquatic)	2B.2	Marshes and swamps (shallow freshwater)
Pyrrocoma lucida	sticky pyrrocoma	perennial herb	1B.2	Great Basin scrub, Lower montane coniferous forest, Meadows and seeps
Rhynchospora alba	white beaked-rush	perennial rhizomatous herb	2B.2	Bogs and fens, Marshes and swamps (freshwater), Meadows and seeps
Rhynchospora capitellata	brownish beaked-rush	perennial herb	2B.2	Lower montane coniferous forest, Marshes and swamps, Meadows and seeps, Upper montane coniferous forest
Schoenoplectus subterminalis	water bulrush	perennial rhizomatous herb (aquatic)	2B.3	Bogs and fens, Marshes and swamps (montane lake margins)
Sedum paradisum ssp. *subroseum*	Plumas stonecrop	perennial herb	1B.2	Lower montane coniferous forest, Upper montane coniferous forest
Solidago lepida var. *salebrosa*	Rocky Mountains Canada goldenrod	perennial rhizomatous herb	3.2	Marshes and swamps (lake margins, streambanks), Meadows and seeps (mesic)
Stachys pilosa	hairy marsh hedge-nettle	perennial rhizomatous herb	2B.3	Great Basin scrub (mesic), Meadows and seeps
Utricularia intermedia	flat-leaved bladderwort	perennial stoloniferous herb (carnivorous) (aquatic)	2B.2	Bogs and fens, Marshes and swamps (lake margins), Meadows and seeps (mesic), Vernal pools

[1]Key to Status Abbreviations: Federally Endangered (FE); Federally Threatened (FT); State Endangered (SE); State Threatened (ST); California Rare Plant Rank (CRPR). CRPR 1A = Plants presumed extinct in California; CRPR 1B = Plants rare, threatened, or endangered in California and elsewhere; CRPR 2B = Plants rare, threatened, or endangered in California, but more common elsewhere; CRPR 3 = Plants about which information is needed-a review list; CRPR 4 = Plants of limited distribution-a watch list; 0.1 = seriously threatened in California; 0.2 = moderately threatened in California; 0.3 = not very threatened in California

APPENDIX D

Historic Resources Study and Archaeological Resources Report

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New Quincy Courthouse Project
Quincy, California

Historical Resources Study (FINAL)



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March 2026

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1 Introduction

This Historical Resources Study (HRS) was prepared by MIG on behalf of the Judicial Council of California (Judicial Council), in partial fulfillment of environmental review requirements for a property in Quincy, California.

The subject property contains three extant buildings and structures, one of which is more than 50 years old. This study assesses all three buildings to determine whether any potential historical resources are present. The presence of one or more potential historical resources would initiate further research and evaluation under state and national criteria and a determination of eligibility in a Historic Resource Evaluation (HRE) report.

The purpose of this report is to provide a preliminary constraints analysis for the property relating to historical resources. This HRS does not include a complete historic context for the subject property or a full assessment of historic significance under state or national criteria. Chapter 4, *Conclusions*, provides a professional opinion as to the likelihood of historical resources at the site based on a desktop review of available background documentation and field verification of existing conditions.

This HRS concludes that no potential historical resources are present at the subject property, and that no further research or documentation is necessary regarding the historic significance of the extant buildings and structures. This report does not consider the potential for archaeological or tribal cultural resources at the subject property.

1.1 Project Location and Description

The project site consists of three contiguous, privately-owned parcels in the unincorporated town of Quincy in Plumas County. Addresses include 253 Lawrence Street (APN 115-031-055), 287 Lawrence Street (APN 115-031-052), and 293-295 Lawrence Street (APN 115-031-054). The project site is approximately 2.86 acres (Figure 1).

The Judicial Council proposes purchasing the three parcels from the current owners to construct a new courthouse and to relocate the Superior Court operations that are currently housed in the Plumas County Courthouse located at 520 Main Street. The construction of the new courthouse building would include demolition of the existing buildings and structures and construction of new courtrooms with support spaces, administrative and operations areas, and an entry plaza. The project would also include site improvements, including new on-site surface parking lots and drive aisles, and new or rerouted utility connections.

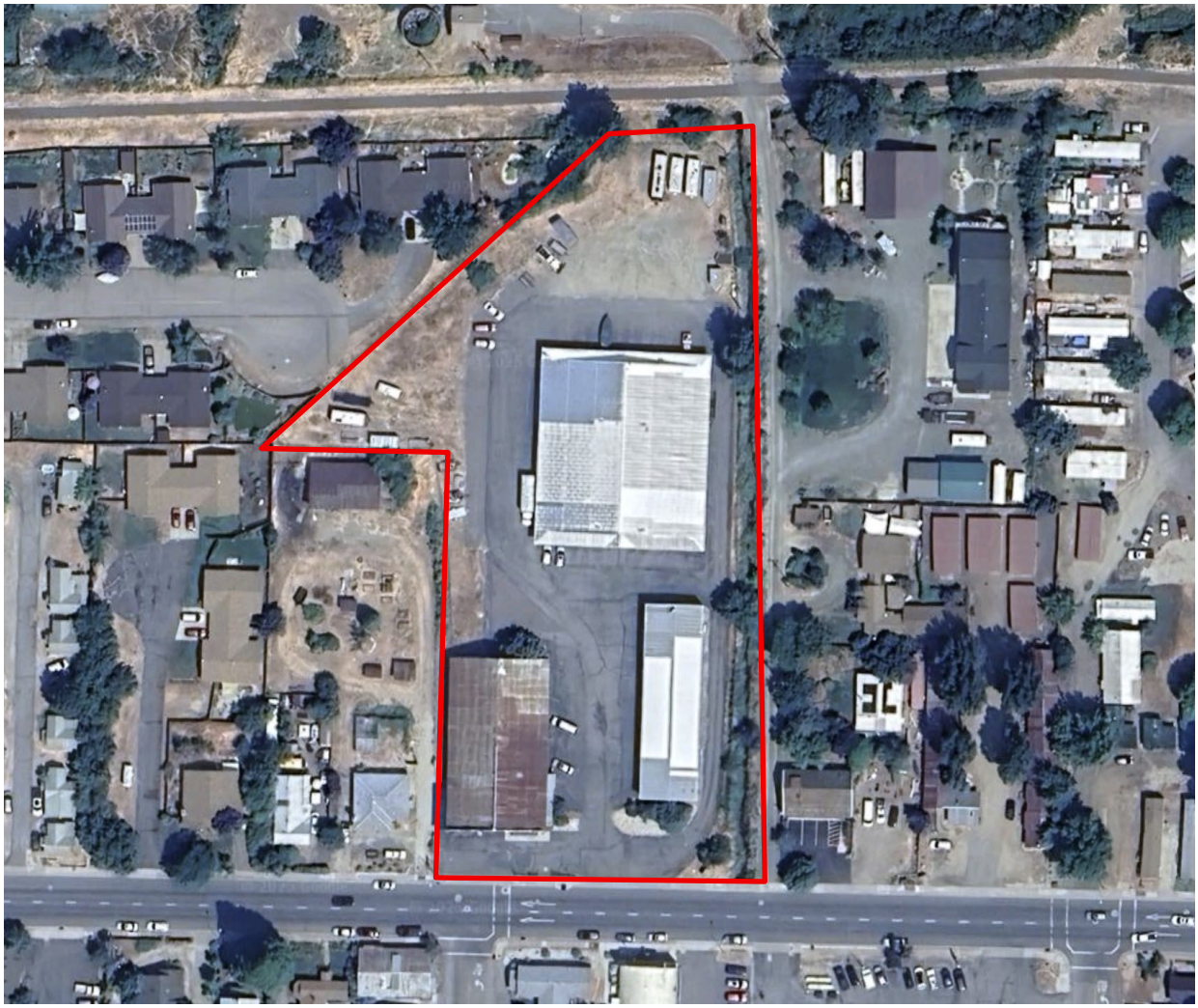


FIGURE 1. THE SUBJECT PROPERTY, COMPRISED OF THREE PARCELS, IS OUTLINED IN RED, NORTH IS UP. (SOURCE: GOOGLE EARTH, EDITED BY MIG.)

1.2 Methodology

This section describes the methods used to complete HRS. Methods include research, field survey, and a preliminary assessment of potential historical resources.

1.2.1 Records Review

Available background information pertaining to known and potential historical resources on the subject property was reviewed prior to and during field survey. The following sources were consulted:

- Relevant historic maps and photographs in the on-site archives at the Plumas County Museum.

- Digital newspaper articles, both historical and contemporary, available online at the California Digital Newspapers Collection, Newspapers.com, and PlumasNews.com (online edition of the Feather Publishing's Plumas County Newspapers).
- Online databases and repositories, including the National Register of Historic Places, the Cal. State University Chico Digital Collections, HistoricAerials.com, and Calisphere.org.
- Plumas County Assessor's Office records for the three parcels within the subject property.

1.2.2 Field Survey and Archival Research

Field survey of the project area was conducted by MIG senior preservation specialist Eleanor Cox, M.S., on September 25, 2025. Existing conditions were recorded via digital photography and field notes. Review of archival materials was conducted on September 26, 2025, at the Plumas County Museum in downtown Quincy.

1.2.3 Preparer's Qualifications

The analysis outlined in this report was prepared by Eleanor Cox, who meets the Secretary of the Interior's Professional Qualifications Standards in the areas of History and Architectural History.

1.3 Historical Resources Summary

1.3.1 Historic Status

The buildings and structures within the subject property have not been previously evaluated for historic significance or eligibility for the National Register of Historic Places, the California Register of Historical Resources, or any local surveys.[1] However, one of the buildings at the property is more than 50 years old, raising the question as to its potential historic significance.

[1] An inventory of historic properties in the downtown areas was completed in support of the California Mainstreet Feasibility Study for Chester, Greenville, Portola, and Quincy in 1988. Printed copies of the inventory forms (California Parks and Recreation Department A forms) are on file with the Plumas County Museum. Properties listed in the study are generally considered potential historical resources by the County, unless otherwise noted in the form. The Plumas County Museum also maintains a Historic Building Inventory list, a Historic House Properties list, and a Heritage Walk brochure that describe historic architecture in Quincy, which are consulted during planning and development projects in the town.

The building known as Quincy Lumber & Supply (293-295 Lawrence Street, APN 115-031-054) is mentioned in the Historic Building Inventory as "Quincy Lumber & Supply 291 Lawrence Street" with a construction date of 1932. No determination of historic status is provided. The other buildings and structures at the subject property are not mentioned in any of the inventories. This information was provided by Paul Russel, Director of the Plumas County Museum at 500 Jackson Street in Quincy, CA.

1.3.2 Historical Resources Assessment

Based on the preliminary analysis completed in this HRS, MIG concludes that no potential historical resources are located within the subject property. Although the building known as Quincy Lumber & Supply (293-295 Lawrence Street) was constructed more than 50 years ago, it does not appear to rise to a level of significance associated with historic patterns of development or its architectural design to qualify for listing in state or national registers.

Further discussion on potential historical resources is located in Chapter 4, *Conclusions*.

1.4 Report Contents

1.4.1 Report Organization

The information included in this report is organized as follows:

Chapter 1 The first chapter outlines the purpose and methodology of the HRS and includes a summary of findings.

Chapter 2 The second chapter includes a description of existing conditions at the subject property. The description focuses on extant buildings and structures at the site.

Chapter 3 The third chapter includes a high-level chronology of physical development at the subject property, based on in-person and desktop research completed for the HRS.

Chapter 4 The last chapter provides a preliminary assessment of the potential for historical resources on the site.

References References lists resources consulted in the preparation of this HRS.

1.4.2 A Note on Naming Conventions

The three buildings and structures at the subject property are referred to throughout this technical report by their current names: the Quincy Lumber & Supply building (293-295 Lawrence Street), the Feather Publishing Co. building (287 Lawrence Street), and the carport.

The only exception is found in Chapter 3, *Development Chronology*, where the Quincy Lumber & Supply building, which was constructed in 1937, is referred to by what it was called at the time it is being described. For example, the building is referred to as the Diamond Match Co. lumber yard when discussing the years 1937 – 1955, during which time it was occupied by that business. To avoid confusion, a timeline of the building's names is provided at the beginning of the chronology.

2 Existing Conditions

The subject property includes two buildings and one structure associated with light-industrial/commercial operations at the site. Overviews of their present condition are described and illustrated below. All photos were taken by MIG on September 25, 2025, unless otherwise noted.

2.1 Site

The 2.86-acre subject property is located at the northeast edge of downtown Quincy. The immediate area is comprised of a mix of residential, institutional, and commercial buildings. A bike path runs along the north boundary of the subject property following a former railroad alignment, and a drainage forms the property's east boundary (Figure 5). A town sidewalk fronts the subject property on its south boundary on Lawrence Street, and the east boundary intersects with neighboring developed properties. A view south along Church Street, towards Main Street, connects the property to Quincy's downtown commercial hub (Figure 7).

The irregularly shaped subject property is divided into three privately-owned parcels, all accessed via a shared driveway from Lawrence Street. The driveway leads to surface parking, paved with asphalt, at the geographic center of the property. Three buildings and structures are located to the west, north, and east of the central parking area (Figures 4, 8). The remainder of the property is paved in gravel (Figures 9, 10). Storage containers and oversized vehicle parking are located at the rear and northwest edges of the property, behind the buildings. A commercial sign and patches of mixed vegetation mark the southeast corner of the property and line the drainage along the east boundary (Figures 3, 6).

The parcels, with building addresses, include:

- APN 115-031-052: The north parcel (Figure 2, Parcel 1), occupied by the Feather Publishing Co. (287 Lawrence Street)
- APN 115-031-054: The southwest parcel (Figure 2, Parcel A), occupied by the Quincy Lumber & Supply building (293-295 Lawrence Street)
- APN 115-031-055: The southeast parcel (Figure 2, Parcel B), occupied by a carport and the property sign (253 Lawrence Street)

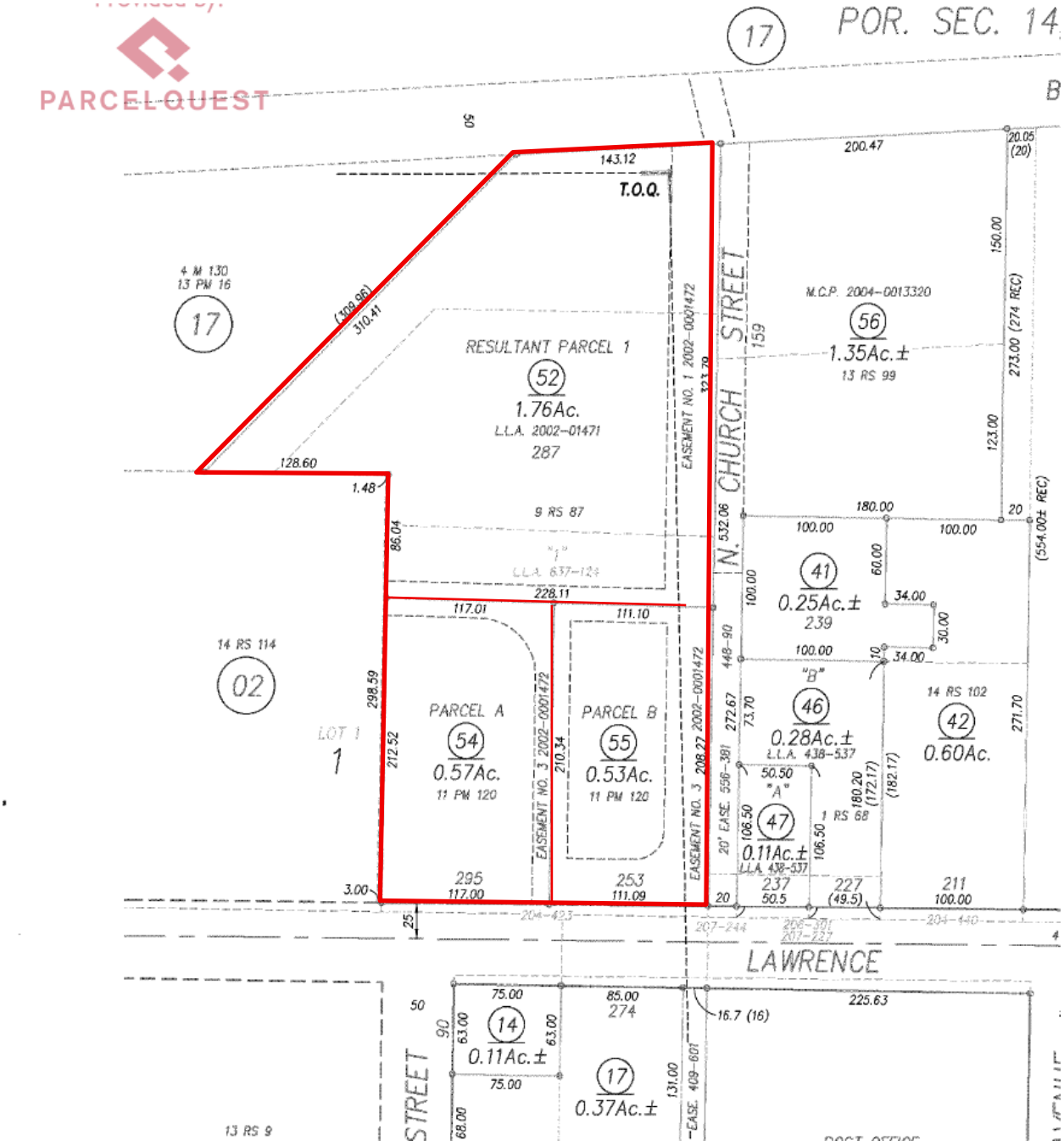


FIGURE 2. PARCEL MAP WITH DIVIDED PARCELS AT THE SUBJECT PROPERTY OUTLINED IN RED. NORTH IS UP. LAWRENCE STREET FORMS THE SOUTHERN BOUNDARY, A BIKE PATH/RAILWAY ALIGNMENT FORMS THE NORTH BOUNDARY, A DRAINAGE FORMS THE EAST BOUNDARY (LABELED HERE AS "EASEMENT NO. 3" AND "EASEMENT NO. 1"). (SOURCE: PLUMAS COUNTY ASSESSOR'S MAP, BOOK 115, PAGE 3, VIA PARCELQUEST, 2023. RED OUTLINES ADDED BY AUTHOR.)



FIGURE 3. VIEW OF THE SUBJECT PROPERTY, WITH SIGN AT FOREFRONT, LOOKING NORTHWEST FROM LAWRENCE STREET.



FIGURE 4. VIEW OF THREE EXTANT BUILDINGS AND STRUCTURES AROUND CENTRAL PARKING AREA, LOOKING NORTH FROM LAWRENCE STREET.



FIGURE 5. VIEW OF THE DRAINAGE THAT RUNS UNDER LAWRENCE STREET AND FORMS THE EAST BOUNDARY OF THE SUBJECT PARCEL, LOOKING SOUTHWEST.



FIGURE 6. MIXED VEGETATION AT THE SOUTHEAST CORNER OF THE LOT, LOOKING NORTH ALONG THE DRAINAGE.



FIGURE 7. VIEW SOUTH FROM SUBJECT PARCEL ALONG CHURCH STREET.



FIGURE 8. PAVED SURFACE PARKING, LOOKING SOUTH TOWARDS LAWRENCE STREET FROM FEATHER PUBLISHING CO.



FIGURE 9. GRAVEL TURNAROUND AND VEHICLE STORAGE AT THE REAR OF THE PROPERTY, LOOKING SOUTHWEST FROM THE EAST BOUNDARY.



FIGURE 10. VIEW LOOKING NORTH FROM THE NORTH END OF THE PROPERTY.

2.2 Quincy Lumber & Supply (293-295 Lawrence Street; APN 115-031-054)

A building known as Quincy Lumber & Supply is located at the southwest corner of the subject property, facing south towards Lawrence Street. The wood-frame building is rectangular in plan with a front-gabled roof that is capped in corrugated metal sheeting; the roof extends approximately one foot beyond the east and west façades and features exposed eaves. The building sits on a concrete slab foundation and features a central aisle that spans the length of the building from the front (south) to the rear (north) façades. The majority of the building was painted red with white trim at an unknown date, and the words “Quincy Lumber & Supply” are painted on the false front and on the roof ridge.

The primary façade (south) of the building features a false front with a stepped parapet that obscures the gable end. The façade is clad in horizontal wood siding and includes two commercial office spaces that flank the aisle entrance, forming three bays (Figures 11, 12). The

commercial spaces are each articulated by storefronts comprising a wood “barn”-style door set within a system of fixed wood windows. The commercial spaces were inaccessible during survey, although the space in the east bay appears vacant. The storefronts are surmounted by shallow hipped roofs capped in asphalt shingles. A white picket fence spans the opening to the central aisle; there is no door. Six wood divided-lite windows form a row above the entrance in the center bay.

Moving clockwise around the building, the west façade features two types of untreated wood siding: the south end near the front of the building features board and batten siding before transitioning to flush vertical siding at the north end of the building (Figure 13). It is the only façade that is not painted red. It is devoid of fenestration with the exception of two sliding doors on metal rails located towards the north end; they are rusted shut and no longer operable (Figure 14). A wood-framed lean-to, covered in a tarp, extends from the south end of the façade, protecting an air-conditioning wall unit and a propane tank (Figure 15).

The rear (north) façade features the termination of the central aisle (Figure 16). The opening is the same width as the opening on the south façade but rises to a greater height. It may have been enlarged overtime, as an extant sliding barn door remains fixed in an open position and hanging from a metal rail to the left (west) of the opening, but is only half the height of the current entrance. A chain-link fence spans the door opening. The façade contains no other fenestration. It is clad in flush vertical siding; the outline of a former rear extension that has been removed is visible due to a change in paint color. A wood ladder is affixed to the façade to the immediate right (west) of the opening (Figure 19). A maple tree grows to the immediate east of the opening in front of the inoperable sliding barn door.

The east façade features the most variation in siding and fenestration (Figure 17). Starting at the south end, the commercial storefront in the east bay wraps around the corner of the building via a ramp to provide an accessible entrance. The secondary entrance, not original to the building, comprises a single glazed door with wood side-lites set within a raised porch under a shed roof that is capped in an extension of the corrugated metal panels from the main roof. The shed roof is supported by square wood columns with Y-braces. The south section of the façade, near the front of the building, is clad in horizontal wood siding like the primary façade, and features four windows that are associated with the interior commercial office space: two tripartite aluminum sliding windows that form an extension of the storefront system, and two wood double-hung windows of different sizes that appear to date from the original construction (Figure 18). Another window between the double-hung windows has been removed and the opening patched with wood siding. The north end of the façade features flush vertical wood siding and two divided-lite windows; these windows match the fenestration in the front gable end but are deteriorated and boarded over with no extant glazing.

The interior of the Quincy Lumber & Supply building features an exposed wood truss system under the roof, and expansive shelving and storage space on either side of the central aisle that rises to three levels in height (Figures 21, 24). The upper levels are accessed via a combination of built-in wood ladders and floating staircases. Plank walkways line the second and third levels

on both sides of the aisle (Figure 20). An office is built into the second level of the east bay, featuring a sliding aluminum window and a plywood door. The storage labels remain extant, marking the types and sizes of lumber stacked in each bay; some sections are enclosed with plywood or wood siding (Figures 22, 23). A pedestrian door connects the central aisle to the commercial office space in the east bay of the building.



FIGURE 11. VIEW OF THE PRIMARY FAÇADE OF THE QUINCY LUMBER & SUPPLY BUILDING, LOOKING NORTH FROM LAWRENCE STREET.



FIGURE 12. DETAIL VIEW OF THE COMMERCIAL STOREFRONT ON THE PRIMARY FAÇADE, LOOKING NORTHWEST.



FIGURE 13. VIEW OF THE WEST FAÇADE OF THE QUINCY LUMBER & SUPPLY BUILDING, LOOKING EAST FROM THE ADJACENT PROPERTY.



FIGURE 14. DETAIL VIEW OF THE SLIDING BARN DOORS LOCATED AT THE WEST FAÇADE, LOOKING EAST.



FIGURE 15. THE LEAN-TO LOCATED AT THE SOUTH END OF THE WEST FAÇADE.



FIGURE 16. VIEW OF THE REAR FAÇADE, LOOKING SOUTH. THE DISCOLORATION ON THE RIGHT (WEST) BAY INDICATES WHERE THE REAR EXTENSION USED TO BE ATTACHED TO THE BUILDING.



FIGURE 17. VIEW OF THE EAST FAÇADE, LOOKING WEST FROM THE CENTRAL PARKING AREA.



FIGURE 18. DETAIL VIEW OF THE SECONDARY ENTRANCE AND FENESTRATION ASSOCIATED WITH THE COMMERCIAL OFFICE SPACE AT THE FRONT OF THE QUINCY LUMBER & SUPPLY BUILDING.



FIGURE 19. DETAIL VIEW OF THE REAR ENTRANCE OPENING, WITH LADDER AFFIXED TO THE RIGHT OF THE OPEN DOORWAY.

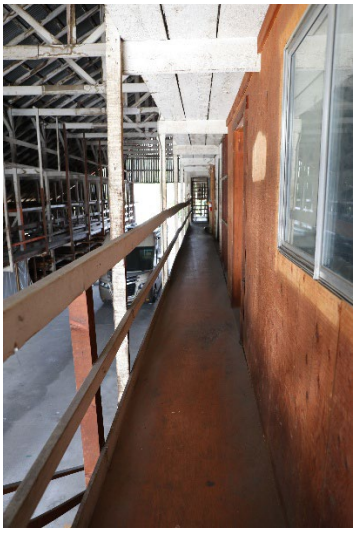


FIGURE 20. THE WALKWAY AT THE SECOND LEVEL OF THE EAST BAY ON THE INTERIOR, LOOKING NORTH. A FORMER OFFICE SPACE IS VISIBLE TO THE RIGHT.

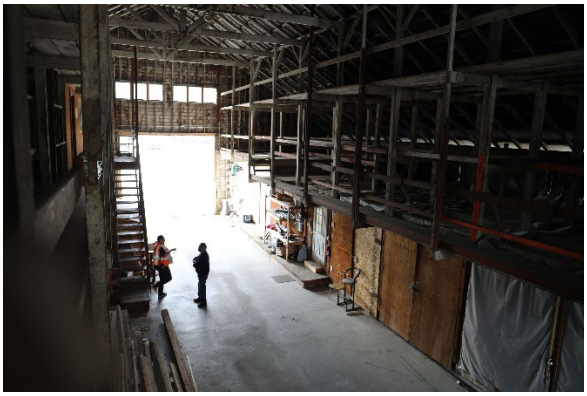


FIGURE 21. THE CENTRAL AISLE AT THE INTERIOR OF THE QUINCY LUMBER & SUPPLY BUILDING, LOOKING SOUTH TOWARDS THE MAIN ENTRANCE FROM THE SECOND LEVEL.



FIGURE 22. DETAIL VIEW OF LUMBER STORAGE LABELS.



FIGURE 23. THE INTERIOR CONNECTION BETWEEN THE LUMBER STORAGE AND COMMERCIAL OFFICE SPACES. A PILE OF LEFTOVER LUMBER IS VISIBLE AT THE FOREFRONT.

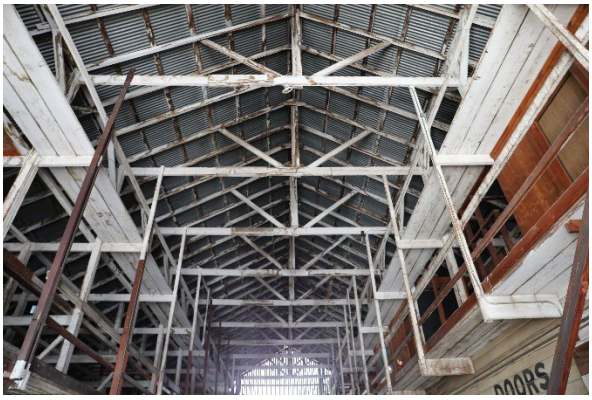


FIGURE 24. THE TRUSS ROOF SYSTEM, LOOKING NORTH FROM THE MAIN ENTRANCE.

2.3 Feather Publishing Co. Inc. (287 Lawrence Street; APN 115-031-052)

Built ca. 1992-1994, the square plan building that houses the Feather Publishing Co. faces south towards the central parking area. It is set back from Lawrence Street, at the rear of the subject property.

The building is two stories in height, capped in a front-gabled metal roof. The 15,020 sq. ft. building is constructed of wood over a concrete foundation, with full-width arcades spanning the front (south) and rear (north) façades. The façades are clad in flush vertical siding, while the primary façade features a rusticated concrete block finish at the base. The arcades are supported by square columns formed of rusticated concrete blocks.

The primary façade (south) features the main entrance, formed by a wood storefront system comprising a pair of metal glazed doors and fixed windows, that provides access to the interior office space for the publishing company. Three signs are affixed to the building in a row above the arcade roof that read from left to right: Plumas – Lassen CONNECTION, FEATHER PUBLISHING CO. INC., and THE PRINT SHOP (Figures 25, 26).

The west and east façades of the building feature minimal fenestration and deep overhanging closed eaves. Two sets of wood doors with metal veneer are located in the west façade: the southernmost set features a pair of doors and the northernmost door is a single pedestrian door (Figures 27, 28, 29). The east façade features three sets of aluminum sliding windows (Figure 32).

The rear (north) façade features multiple openings (Figure 30). Oversized roll-top doors are located near each end. A pedestrian door and one set of metal sliding windows are located near

the center of the building (Figure 31). The second story features four sets of metal sliding windows above the arcade roof.

The interior of the Feather Publishing Co. includes a mix of office and light industrial uses to support the publication of regional newspapers. Offices are located on the first and second floors at the center of the building, while printing operations are located at the east and west ends of the first story and accessed via the roll-top doors at the rear façade (Figures 33, 34). The physical archives of the printed newspapers are stored in the second story (Figure 35).



FIGURE 25. VIEW OF PRIMARY FAÇADE OF THE FEATHER PUBLISHING CO. BUILDING, LOOKING NORTH FROM THE PARKING AREA AT THE CENTER OF THE SUBJECT PROPERTY.



FIGURE 26. DETAIL VIEW OF THE MAIN ENTRANCE AT THE CENTER OF THE PRIMARY (SOUTH) FAÇADE OF THE FEATHER PUBLISHING CO.



FIGURE 27. VIEW OF THE WEST FAÇADE, LOOKING NORTH. THE VIEW WAS PARTIALLY OBSTRUCTED BY PARKED OVERSIZED VEHICLES.



FIGURE 28. DETAIL VIEW OF PAIRED DOORS ON THE WEST FAÇADE.



FIGURE 29. VIEW OF THE WEST FAÇADE OF THE FEATHER PUBLISHING CO. BUILDING, LOOKING EAST FROM THE WEST EDGE OF THE PROPERTY.



FIGURE 30. VIEW OF THE REAR (NORTH) FAÇADE OF THE FEATHER PUBLISHING CO., LOOKING SOUTH FROM THE NORTH EDGE OF THE PROPERTY.



FIGURE 31. DETAIL VIEW OF TWO DOORS ON THE REAR FAÇADE.



FIGURE 32. VIEW OF THE EAST FAÇADE OF THE FEATHER PUBLISHING CO., LOOKING NORTH/NORTHEAST.



FIGURE 33. PRINTING MACHINES AT THE INTERIOR OF THE FEATHER PUBLISHING CO.



FIGURE 34. PRINTING EQUIPMENT AT THE INTERIOR OF THE FEATHER PUBLISHING CO.



FIGURE 35. PHYSICAL ARCHIVES OF LOCAL AND REGIONAL PAPERS STORED IN THE SECOND STORY OF THE FEATHER PUBLISHING CO.

2.4 Carport (253 Lawrence Street; APN 115-031-055)

A carport built ca. 1981, is located at the southeast corner of the subject property (Figure 36). The structure includes seven bays under a shallow gable roof (Figure 37). The six bays at the front (south end) are formed via steel columns and bracing. The seventh (rear) bay is partially enclosed with vertical wood siding and was inaccessible during field survey (Figure 38). The enclosed bay features fenestration comprised primarily of fiberglass or aluminum windows and metal doors (Figure 39). The structure's columns are anchored in concrete piers, and the floor is gravel. The roof is capped in corrugated metal panels. The exposed bays are used for vehicle or boat storage. The enclosed bay appears to function as an office or for operations or storage.



FIGURE 36. VIEW OF THE CARPORT FRONTED BY MIXED VEGETATION, LOOKING NORTH FROM THE LAWRENCE STREET SIDEWALK.



FIGURE 37. VIEW OF THE CARPORT, LOOKING NORTHWEST FROM THE SOUTHWEST CORNER OF THE SUBJECT PROPERTY.



FIGURE 38. THE PARTIALLY ENCLOSED BAY, LOOKING NORTHWEST FROM THE EAST EDGE OF THE SUBJECT PROPERTY.



FIGURE 39. THE PARTIALLY ENCLOSED BAY, LOOKING SOUTHEAST FROM THE PARKING AREA AT THE CENTER OF THE SUBJECT PROPERTY.

3 Development Chronology

The following chronology outlines events that shaped the development of the subject property. This chronology is not comprehensive; it provides a high-level historical framework to contextualize when and why the buildings and structures at the subject parcel were constructed, and whether they are part of a larger or significant pattern in history.

The information herein was gathered via desktop research in digital repositories and archival research at the Plumas County Museum. The chronology includes some gaps in information that would be included in a full HRE. Additional in-depth research at the Plumas County Assessor's Office and Building Department, and at Cal. State University Chico would reveal a more complete historic context for the subject property, including a full record of permitted alterations and a complete timeline of ownership and occupancy.

Although the Quincy Lumber & Supply building has consistently served as a lumber and building supply store since it was constructed in 1937, it has undergone several changes in ownership and has been referred to with different names over time. The building is referred to in the chronology by its contemporaneous name. A rough timeline of the building's names since construction through the present is presented here to avoid confusion. These names generally align with but do not consistently include the commercial shops that occupied the storefronts:

- 1937 – 1955: Diamond Match Co. Lumber Yard
- 1955 – 1960: Atkins Lumber and Supply Co.
- 1960 – 1970: *unconfirmed*
- 1970 – 2025: Quincy Lumber & Supply Co.

3.1 Chronology

1848-1850	The California Gold Rush spurs immigration to and settlement in the region.
1854	Plumas County is formed and Quincy is established as the County Seat.
	Local industry includes mining and agriculture. The mining industry attracts thousands of Chinese American laborers to the region, and the Quincy Chinatown is established where the Quincy High School is currently located.
1859	The first permanent County Courthouse is constructed in Quincy.
Ca. 1850s	Early iterations of the Diamond Match Company form in Delaware.
1866	The Feather River Bulletin is founded as the Plumas National newspaper.

1880s Mr. O.C. Barber of Ohio purchases the company that later came to be known as Diamond Match Co. They produce matches and other timber products.

1892 The Plumas National newspaper moves to a building on West Main Street in Quincy after merging with the Greenville Bulletin.[2] It rebrands as the Plumas National Bulletin (Figure 40).

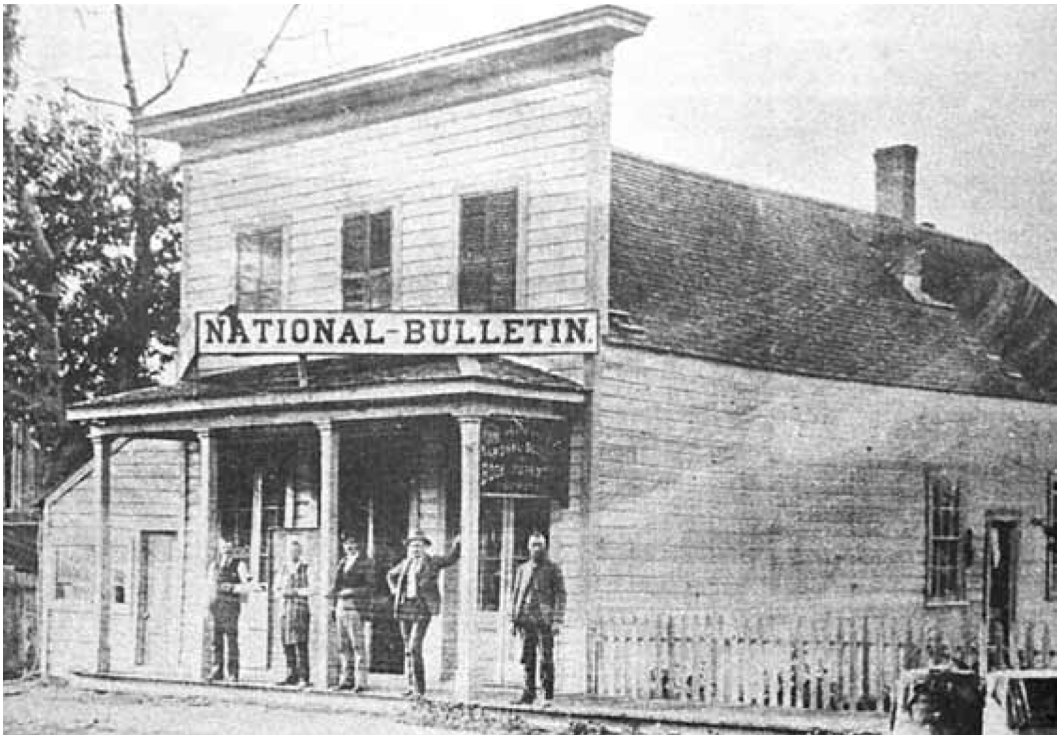


FIGURE 40. THE FEATHER RIVER BULLETIN'S CA. 1892 OFFICES ON WEST MAIN STREET IN DOWNTOWN QUINCY (NON-EXTANT). (SOURCE: *FEATHER RIVER BULLETIN: 1866 -2016*)

19th century The subject parcel is owned by Mr. Agassiz and Mr. Shaw. It is part of a large acreage that follows the Spanish Creek in a map entitled "Sketch showing the Vacant Land joining the property of Messrs Agassiz and Shaw near American Valley" (n.d.) on file with

[2] *Feather River Bulletin: 1866-2016*. Pg. 3.
The location of the ca. 1892 publishing offices are described as both West Main Street and on Buck's Lake Road in the Feather River Bulletin anniversary edition. Two plaques are located on the current brick building at the corner of Main Street and Crescent Street commemorating the Feather Publishing Co. and local journalism. The Plumas County Assessor's Office: Map Portal states that the brick building was constructed in 1976 and the building date is verified through analysis of historic aerial photographs. The original building that housed the Plumas National Bulletin, later the Feather Publishing Co., was likely located near this intersection and demolished in the early 1970s. However, the publishing company continued to operate out of the new building at that location until they built and moved into their current building at 287 Lawrence Street (subject property) between 1992 and 1994.

	the Plumas County Museum. The subject property forms the southernmost leg of the acreage and is located just outside of the area marked as the Quincy "town site". The vacant land on the map is largely composed of small ranches.
Ca. 1901-1904	Mr. Barber opens a Diamond Match Co. mill in Sterling City, CA and a plant in Chico, CA. Rail lines are constructed by Southern Pacific Railroad between the plant and the mill, and later expanded to other company operations in greater Lassen and Plumas counties.
Early 20th Century	The Diamond Match Co. built dozens of lumber yards, mills, factories, and sales offices across northern California in the first half of the 20th century.[3]
Ca. 1906	The subject property is sold and incorporated into the developing town of Quincy. It is part of an L-shaped parcel owned by B.F. Chandler, who is associated with several parcels in the vicinity along the north edge of the town site (Figure 41). The properties to its west and south are also being subdivided for development.

[3] Cal State Chico maintains an archive of Diamond Match Co. photos and other materials in the Meriam Library's Special Collections.

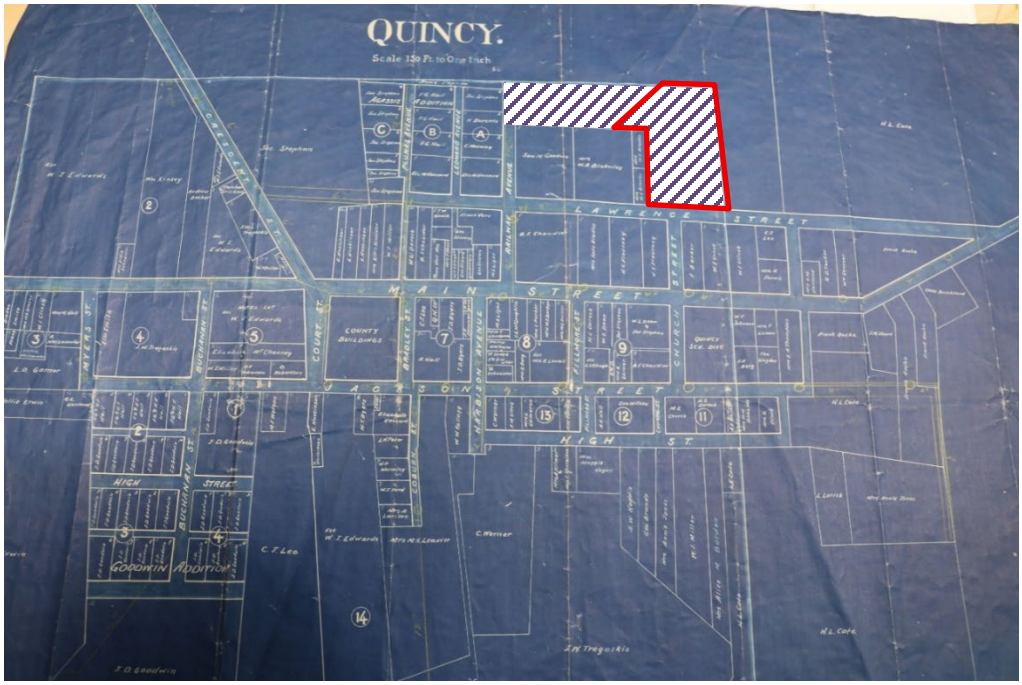


FIGURE 41. A PLAT MAP FROM 1906 ILLUSTRATING OWNERSHIP IN THE TOWN OF QUINCY, NORTH IS UP. THE SUBJECT PROPERTY, OWNED BY MR. CHANDLER IS LOCATED AT THE NORTHEAST EDGE OF TOWN (EDITED BY AUTHOR. THE L-SHAPED OUTLINE OF THE CHANDLER PROPERTY IS NOTED IN PURPLE HATCH AND THE APPROXIMATE OUTLINE OF THE SUBJECT PROPERTY IS NOTED IN RED). (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

1909-1910	The Western Pacific Railroad plans and constructs a railway line through the town of Quincy, later called Quincy Junction. The railroad facilitates the transportation of timber and lumber products in and out of the region.
1913	Quincy Lumber Company commences milling operations in the area. They are located to the east of the Quincy town site.
Ca. 1910s-1920s	Mr. Chandler subdivides the L-shaped parcel into two parcels, forming the current irregular footprint of the subject property. Both parcels are sold but remain under agricultural use. The subject property is utilized for grazing and enclosed with wood fencing. The parcel does not contain any buildings or structures (Figure 42).
1919	The current County Courthouse replaces the original county courthouse at the west end of Main Street, across from the Feather River Bulletin offices.

1926 The Powell Lumber Company purchases the Quincy Lumber Company but retains the mill's name.

The growing California lumber industry and the local mills fuel immigration from the American south to the region's small mill towns, including thousands of African American laborers fleeing segregation in the southern states (Figures 42 and 43).[4]



FIGURE 42. THE TOWN OF QUINCY AS REPRESENTED IN A POSTCARD FROM 1929, LOOKING SOUTHWEST NINE YEARS BEFORE ANY BUILDINGS OR STRUCTURES WERE BUILT ON THE SUBJECT PROPERTY. THE PARCEL IS PARTIALLY VISIBLE AT THE RIGHT (OUTLINED IN RED), ENCLOSED WITH A WOOD PERIMETER FENCE. THE LAND WAS USED FOR GRAZING OR GROWING GRAIN CROPS, AND THE SURROUNDING LANDS TO THE NORTH AND EAST ARE SIMILARLY AGRICULTURAL IN CHARACTER. DOWNTOWN QUINCY IS LOCATED TO THE SOUTH (LEFT). THE QUINCY LUMBER COMPANY MILL (AND MILL POND) ARE VISIBLE IN THE FOREGROUND OF THE PHOTO, FEATURING STACKS OF MILLED LUMBER. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

[4] https://blackpast.org/african-american-history/working-quincy-mill-african-american-lumber-mill-workers-northern-california-1926-1955/, accessed in November of 2025.

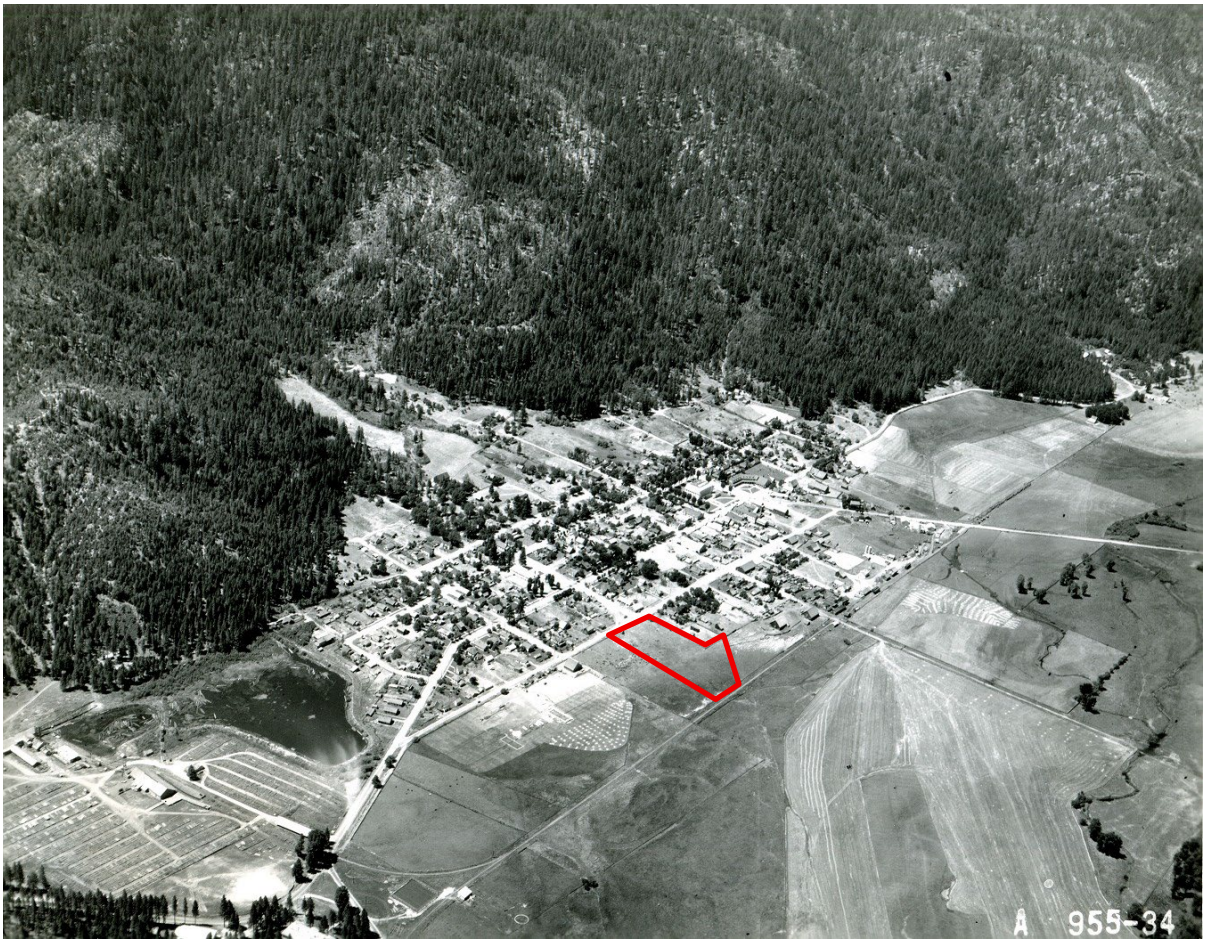


FIGURE 43. AN AERIAL VIEW OF QUINCY FROM THE EARLY 1930S LOOKING SOUTHWEST, WHEN THE U.S. FOREST SERVICE BUILDING WAS UNDER CONSTRUCTION. THE SUBJECT PARCEL REMAINS LARGELY UNDEVELOPED, ALTHOUGH A SMALL-SCALE AGRICULTURAL STRUCTURE (NON-EXTANT) IS LOCATED AT THE SOUTH EDGE ALONG LAWRENCE STREET. THIS VIEW PROVIDES A REGIONAL CONTEXT FOR THE TOWN OF QUINCY, WITH THE AGRICULTURAL SETTING VISIBLE TO THE NORTH (RIGHT), THE RAILROAD ALIGNMENT CUTTING THROUGH THE LANDSCAPE TO THE QUINCY LUMBER COMPANY AND FORMING THE REAR BOUNDARY OF THE SUBJECT PROPERTY, AND THE EXPANSIVE ACREAGE OF THE QUINCY LUMBER COMPANY TO THE EAST (BOTTOM LEFT). (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

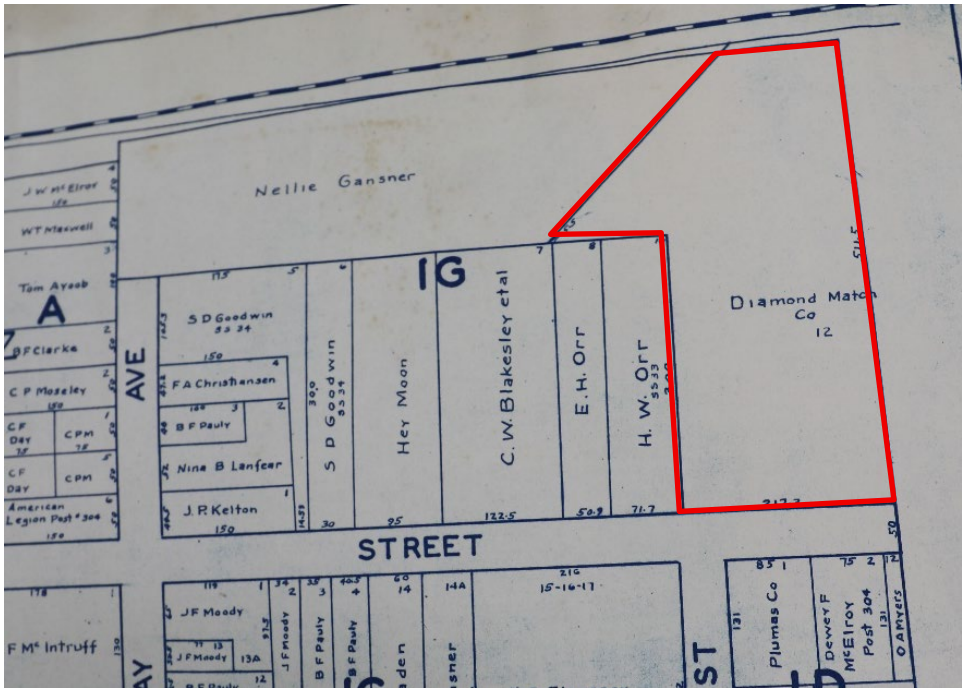


FIGURE 44. AN UNDATED PLAT MAP (ESTIMATED TO BE FROM THE 1930S OR 1940S) ILLUSTRATES DIAMOND MATCH CO.'S OWNERSHIP OF THE FULL SUBJECT PARCEL (OUTLINED IN RED). ANOTHER PARCEL ON THE BLOCK WAS OWNED BY HEY MOON, A PROMINENT BUSINESSMAN IN QUINCY AND THE LOCAL CHINESE AMERICAN COMMUNITY. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

Ca. 1920s-1930s Diamond Match Co. purchases the subject property at an unconfirmed date (Figure 44).

Ca. 1931 Feather River Bulletin newspaper begins publication under the Plumas National Bulletin banner.

1937 The Diamond Match Co. constructs a commercial lumber yard on Lawrence Street in Quincy (Figure 45).[5] The lumber store is the only building on the subject property. The building was painted white with black signage and included an office/storefront space at the front (Figures 46, 47, 50). A shed lean-to is built at the rear (Figures 48, 49). Stacks of lumber are located adjacent to the building (Figures 47, 49). The north end of the subject property is still used for grazing or grain crops; it is separated from the lumber yard via a wood post fence.

An article in the Feather River Bulletin notes that the Diamond Match Co. owns 57 lumber yards in Northern California, although it

[5] Plumas County Assessor's Office, Map Portal: Parcel Query. https://mangomap.com/plumasgis/maps/47398/parcel-query.

does not appear that they were built according to standard specifications or plans.

Construction of the new lumber yard in Quincy is managed by local contractor H.C. Conklin. Contemporaneous newspaper articles describe the interior finishes as “Beaver Insulation Board”. The building is electrified by the Feather River Electric Shop, and plumbing is installed by McCoys Plumbing and Sheet Metal Shop.

The Diamond Match Co. sells lumber and other building materials to local customers, including cement, plaster, composition roofing, paint, and hardware.



Diamond Match Company Opens New Plant in Quincy

A NEW CHAPTER in the progress of Quincy is being written today. A new industry finds its niche in Quincy's growing business district.

The Diamond Match Company formally opens the doors of its retail lumber yard to Quincy and Plumas County.

Has Confidence in Quincy

Quincy welcomes this enterprising firm, realizing that it is welcoming an organization that is as progressive in its business as Quincy is as a community — a firm that is as enterprising in its dealings with its customers as Quincy is in its desire to enlist new business within its confines.

The Diamond Match Company brings to Quincy, after months of careful study, planning and building, a retail lumber yard that is modern, attractively designed and constructed to give efficient customer service. Everett Pierce, local manager, has extended an invitation to all to inspect this modern plant at their earliest convenience.

Located on Lawrence street, the operations are compactly housed under one building 68 feet by 123 feet, with ample yard space for the storage of materials not required

(Continued on Page 2)

The Diamond Match Compnay's sawmill at Stirling City, where 40 million board feet of lumber is cut annually.

FIGURE 45. A NEWSPAPER CLIPPING FROM THE FEATHER RIVER BULLETIN IN AUGUST OF 1937 HERALDING THE OPENING OF THE NEW DIAMOND MATCH CO. LUMBER YARD IN QUINCY. THE GENERAL MANAGER IS LISTED AS EVERETT PIERCE. THE PHOTOGRAPH HIGHLIGHTS THE DIAMOND MATCH FACTORY AND HEADQUARTERS IN CHICO, CA. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

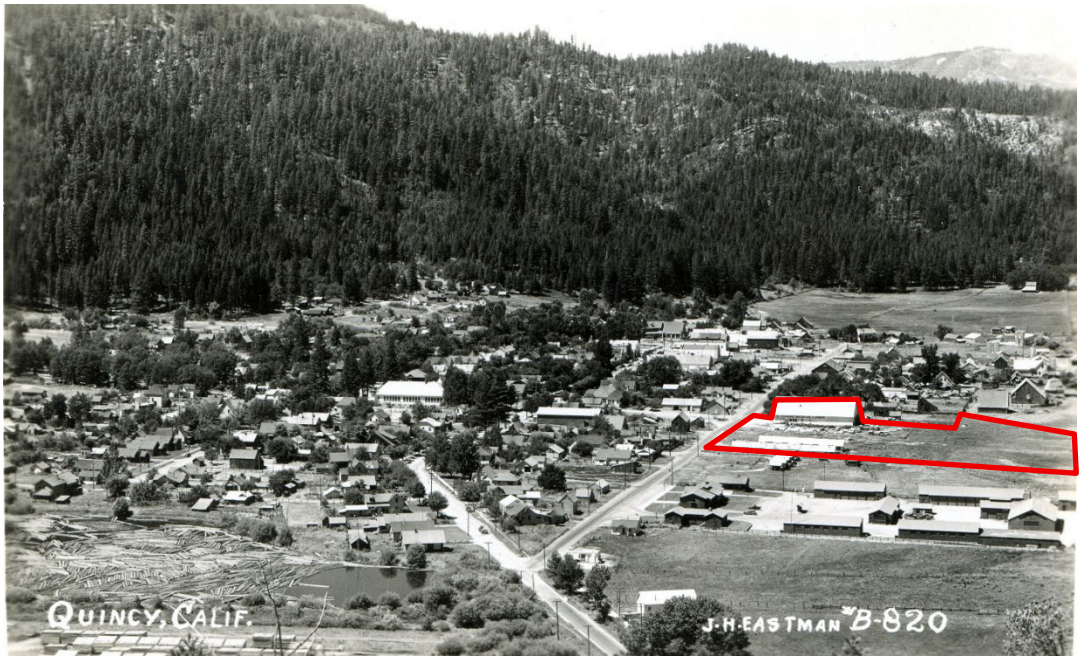


FIGURE 46. THE TOWN OF QUINCY REPRESENTED IN A 1938 POSTCARD, LOOKING SOUTHWEST. THE SUBJECT PROPERTY IS VISIBLE AT THE RIGHT; THE DIAMOND MATCH CO. BUILDING IS PAINTED WHITE WITH BLACK SIGNAGE. THE U.S. FOREST SERVICE CAMPUS IS VISIBLE IN THE FOREGROUND, BUT THE REMAINDER OF LAWRENCE STREET REMAINS AGRICULTURAL IN CHARACTER, FEATURING NUMEROUS BARNS AND OTHER FARM-RELATED STRUCTURES. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)



FIGURE 47. DETAIL VIEW OF SUBJECT BUILDING CROPPED FROM THE AERIAL PHOTOGRAPH TAKEN IN 1938. THE ORIGINAL FENESTRATION AT THE EAST AND REAR FAÇADES, INCLUDING THE ORIGINAL SIZE OF THE REAR DOOR, AND THE ORIGINAL LEAN-TO (NON-EXTANT) IS VISIBLE. MILLED LUMBER IS STACKED IN THE YARD. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

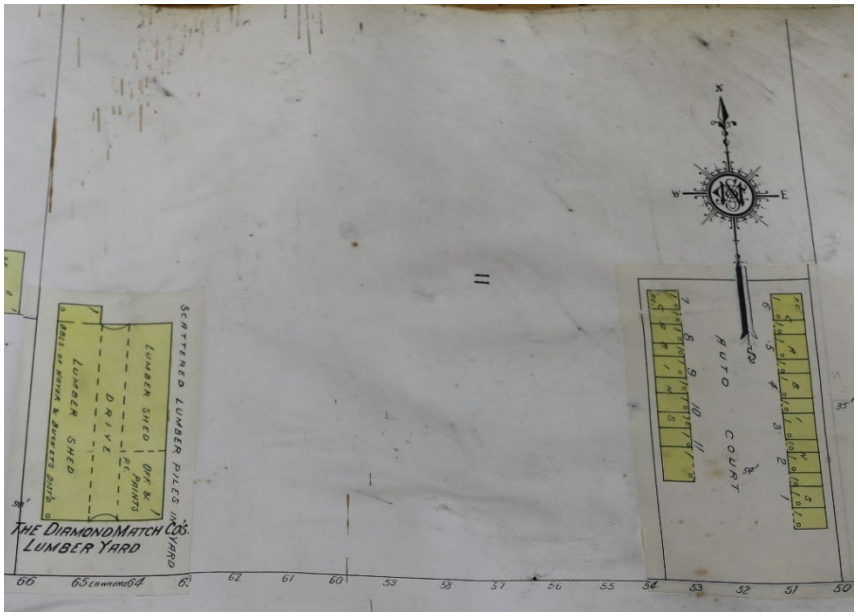


FIGURE 48. THE 1938 UPDATE TO THE 1929 SANBORN MAP FOR THE TOWN OF QUINCY INCLUDES THE DIAMOND MATCH CO. LUMBER YARD AT THE SUBJECT PROPERTY, VISIBLE AT THE LEFT OF THE IMAGE . (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)



FIGURE 49. A DETAIL OF THE DIAMOND MATCH CO. LUMBER YARD BUILDING IN THE 1938 SANBORN MAP. THE MIDDLE BAY IS LABELED AS "DRIVE". THE OFFICE IS NOTED IN THE BOTTOM RIGHT CORNER OF THE BUILDING, AND THE REMAINDER OF THE BUILDING IS DEDICATED TO LUMBER SHELVING AND STORAGE. THE OTHER COMMERCIAL STOREFRONT IS BELIEVED TO HAVE BEEN INCLUDED IN THE ORIGINAL CONSTRUCTION BUT IS NOT NOTED HERE. THE LEAN-TO IS INCLUDED AT THE REAR AND LUMBER PILES ARE NOTED TO THE IMMEDIATE EAST OF THE BUILDING. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

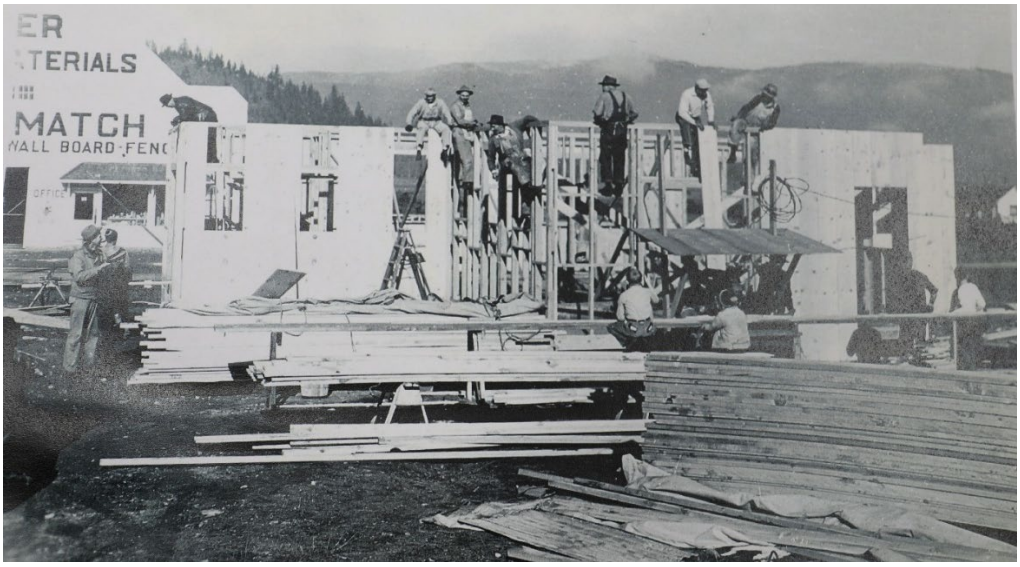


FIGURE 50. A PHOTO TAKEN FROM ACROSS THE STREET, DURING THE CONSTRUCTION OF THE LOCAL YOUTH CENTER IN 1945, CAPTURES THE ORIGINAL CONFIGURATION OF THE STOREFRONT SYSTEM AT THE DIAMOND MATCH CO. LUMBER YARD'S OFFICE. THE DOOR WAS SITUATED AT THE LEFT SIDE OF THE STOREFRONT SYSTEM. THE AISLE IS VISIBLE AT THE EDGE OF THE PHOTO AND IS THE SAME HEIGHT AS THE STOREFRONT SYSTEM. A WOODEN GATE SPANS THE AISLE OPENING. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM, BOX 77 F)

Ca. 1938-1946	The rear lean-to is demolished, and an extension is constructed at the rear of the Diamond Match Co. lumber yard building to accommodate additional storage. The extension is two stories in height but is smaller in scale than the main building. It features a gabled roof, and open storage bays (Figures 51, 54).
Ca. 1945-1966	The front aisle opening is enlarged and rises above the storefront systems. It's possible the rear door was enlarged at the same time (Figure 54).
1955	Atkins Lumber and Supply Co. purchases the subject property from Diamond Match Co. The company is managed by J.R. Atkins. The Quincy operation is their third branch. Before founding Atkins Lumber and Supply Co., Mr. Atkins worked for the Quincy Lumber Company (Figure 51). The signage at the lumber yard office is updated to reflect new ownership. Lawrence Street has been developed in the post-WWII era and no longer exhibits an agricultural character (Figures 49, 50).
Ca. 1950s	A secondary building is constructed at the rear of the parcel. It is one story in height with a shed roof (Figures 52, 53).

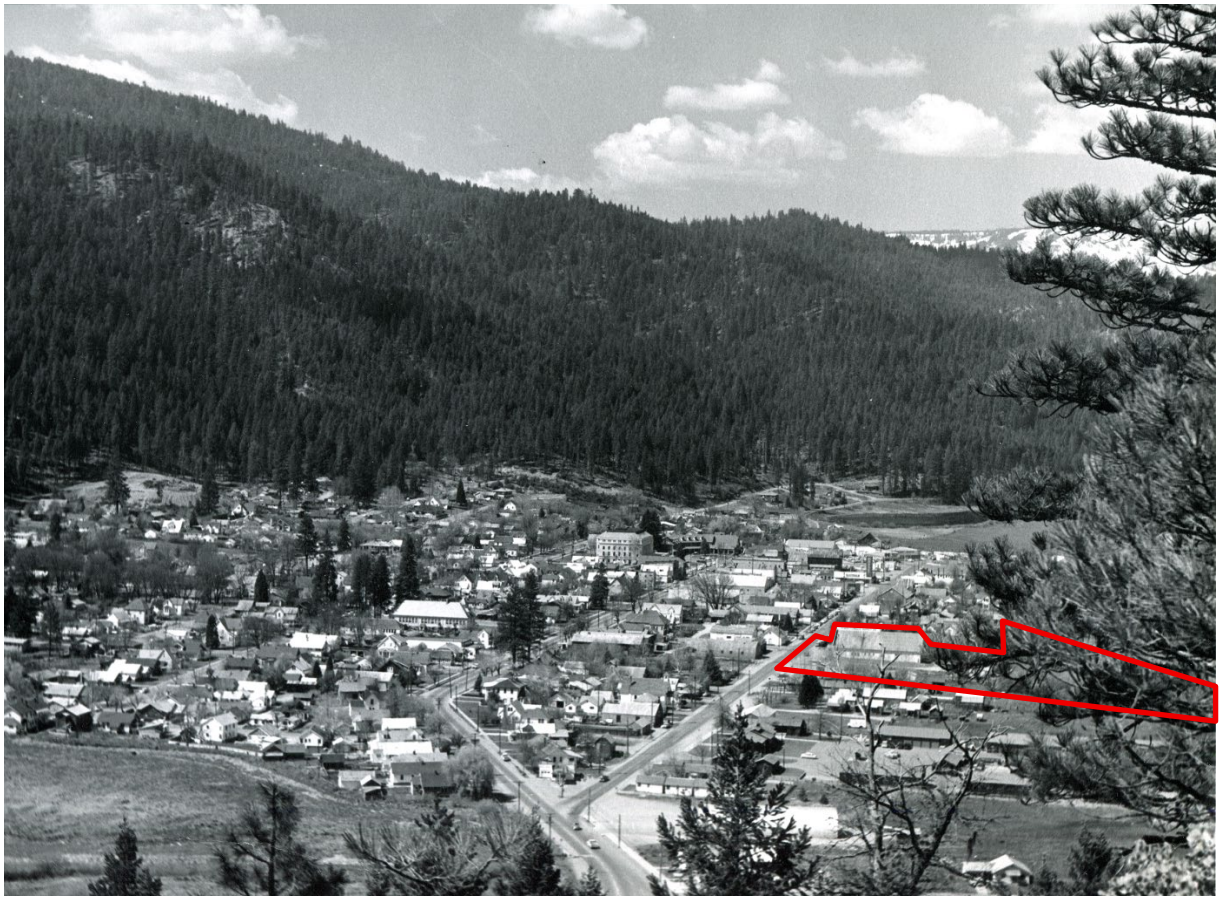


FIGURE 51. THE TOWN OF QUINCY CA. LATE 1950S, LOOKING SOUTHWEST. THE ATKINS LUMBER AND SUPPLY CO. BUILDING IS VISIBLE AT THE RIGHT. IT IS STILL PAINTED WHITE WITH BLACK SIGNAGE. THE U.S. FOREST SERVICE CAMPUS IS VISIBLE IN THE FOREGROUND AND THE COURTHOUSE IS VISIBLE IN THE BACKGROUND. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)



FIGURES 52 AND 53. HISTORIC AERIAL PHOTOGRAPHS OF THE SUBJECT PROPETY. THE PHOTOGRAPH ON THE LEFT WAS TAKEN IN 1946 AND SHOWS THE COMPLETED CONSTRUCTION OF THE REAR EXTENSION AT THE DIAMOND MATCH CO. LUMBER YARD BUILDING. THE PHOTO ON THE RIGHT WAS TAKEN IN 1963 AND SHOWS THE PERIMETER FENCE AROUND THE EXTENT OF THE LUMBER YARD. IN BOTH PHOTOS THE NORTH HALF OF THE SUBJECT PROPERTY REMAINS UNDEVELOPED. (SOURCE: HISTORICAERIALS.COM; FOR EDUCATIONAL USE ONLY, NOT FOR PUBLICATION)



FIGURE 54, THE TOWN OF QUINCY IN 1966, LOOKING WEST. THE SUBJECT PROPERTY IS VISIBLE AT THE RIGHT. THE BUILDING IS STILL PAINTED WHITE WITH BLACK SIGNAGE. THE REAR EXTENSION WITH OPEN STORAGE BAYS IS VISIBILE. A SHED BUILDING (NON-EXTANT) IS LOCATED AT THE REAR OF THE SUBJECT PROPERTY. THE DOWNTOWN AND RESIDENTIAL NEIGHBORHOODS TO THE SOUTH (LEFT) HAVE CONTINUED TO FILL IN DURING THE POST-WWII ERA, BUT THE FORMER AGRICULTURAL PARCELS TO THE NORTH REMAIN LARGELY UNDEVELOPED. THE RAILROAD DEPOT IS VISIBILE IN THE BACKGROUND. (SOURCE: PLUMAS COUNTY MUSEUM, ARCHIVES ROOM)

1960	Atkins Lumber and Supply Co. liquidates and auctions off their remaining supply inventory.
1963	A fence has been constructed around the lumber yard. The north end of the property remains undeveloped (Figure 52).
1967	Advertisements for Quincy Lumber & Supply Co. (sometimes listed as Quincy Lumber & Supply) begin to appear in the Feather River Bulletin, but the address is either not specified or listed as 320 Lawrence Street.

1970	Advertisements in the Feather River Bulletin indicate that Quincy Lumber & Supply Co. have established operations at 291 Lawrence Street (an address sometimes associated with the subject property). The proprietor is listed as O.E. Abel. The signage is likely updated to reflect the contemporaneous occupants around this time.
Ca. early 1970s	Feather Publishing Co. Inc. is established by the Bey-Taborski family. They take over operation of the Feather River Bulletin and other local newspapers. The small-scale shed building at the rear of the subject property is demolished.
1975	Sierra Pacific Industries, one of the largest lumber producers in the U.S., purchases the Quincy Lumber Company.[6]
Ca. 1981	The carport is constructed at the southeast corner of the lot.[7]
1992	The subject property is divided into three parcels and sold to two different owners.
Ca. 1992-1994	The Feather Publishing Co. purchases the northernmost parcel on the subject property and constructs a new headquarters building on the lot.[8] The company relocates their operations from Main Street in downtown Quincy.
Ca. 1998-2005	The rear extension is demolished at the Quincy Lumber & Supply building. The secondary ramp entrance and porch are added to the east façade of the Quincy Lumber & Supply building.
2009	Quincy Lumber & Supply Co. closes commercial operations at the subject property, but the signage remains and the building retains its name in public consciousness.
2012	A computer repair shop is operating out of the commercial space in the west bay of the Quincy Lumber & Supply Co. building.

[6] Sierra Pacific Industries is the largest private employer in Plumas County. https://www.plumasnews.com/spi-continues-to-demonstrate-its-commitment-to-the-community-with-its-latest-investment/, Accessed in November, 2025.
[7] Plumas County Assessor's Office, Map Portal: Parcel Query. https://mangomap.com/plumasgis/maps/47398/parcel-query, Accessed in November, 2025
[8] Plumas County Assessor's Office, Map Portal: Parcel Query. https://mangomap.com/plumasgis/maps/47398/parcel-query, Accessed in November, 2025

	The original wood gate that spanned the aisle entrance was replaced at an unknown time with a metal gate topped in barbed wire.
2013	The Quincy Paint Center operates out of the commercial space in the east bay of the Quincy Lumber & Supply building. The ramp and secondary entrance were added at an unknown date after 1966.
2016	The Feather River Bulletin celebrates its 150th anniversary at Feather Publishing Co. All four weekly newspapers in Plumas County are published by Feather Publishing Co.[9]
2022	A metal gate spanning the center aisle opening on the primary (south) façade of the Quincy Lumber & Supply building is replaced with a white picket fence.
2024	The wood lean-to structure is attached to the west façade of the Quincy Lumber & Supply building.
	Quincy Paint Center ceases operations.

[9] *Feather River Bulletin: 1866-2016*. Pg. 4.

4 Conclusions

This section provides an assessment as to the presence of potential historical resources at the subject property. This assessment considers historic development patterns and themes in the town of Quincy and the broader region.

4.1 Assessment Approach

The development chronology outlined in Chapter 3 highlights specific events and themes with which the subject property may be historically associated. These include:

- Agriculture
- The early development of downtown Quincy
- The lumber milling industry in Plumas and Lassen counties
- The Diamond Match, Atkins Lumber and Supply, and Quincy Lumber & Supply companies
- The Feather River Bulletin and the Feather Publishing Co.
- Architecture and design

Because only one building at the subject property was constructed more than 50 years ago, which is a national standard maintained by the Secretary of the Interior for allowing enough time to pass for historians and scholars to understand historic significance, this assessment focuses on that building's association with the bulleted themes above before briefly considering the other buildings and structures on the property.[10]

Other important themes highlighted in the development chronology include mining, the railroad, Chinese American and African American communities, labor, and the establishment of Quincy as the county seat and the associated construction of the first and second permanent County Courthouses. Although critical to understanding the history of the town of Quincy, these themes do not share a strong association with the subject property and are not explored further in this HRS.

This assessment does not include a full evaluation of historic significance under the California Register of Historical Resources or the National Register of Historic Places. It provides preliminary screening for potential historical resources on the subject property.

[10] Although the California Register of Historical Resources does not specify the same 50-year rule for eligibility that the National Register of Historic Places relies on, guidance from the California State Historic Preservation Office indicates an overall alignment between the two sets of criteria for evaluation of historical significance.

4.1.1 Overview of Evaluation Criteria

The criteria used to determine whether a property is eligible for listing in the National or California Registers is listed below. While a full discussion under each criterion is not included in this HSR, it's helpful to review them as a framework for the preliminary analysis.

To be eligible for listing in either register, a property must demonstrate significance under one or more of the following criteria and also retain historical integrity:

- **Criterion A/1 (Events)**: Resources that are associated with events that have made a significant contribution to the broad patterns of local, California, or national history.
- **Criterion B/2 (Persons)**: Resources that are associated with the lives of persons important to local, California, or national history.
- **Criterion C/3 (Design/Construction)**: Resources that embody the distinctive characteristics of a type, period, region, or method of construction, or represent the work of a master, or possess high artistic values.
- **Criterion D/4 (Information Potential)**: Resources that have yielded, or have the potential to yield, information important to the prehistory or history of the local area, California, or the nation.

In addition, the California Public Resource Code, Section 5024, requires a state agency to maintain a master list of agency-owned buildings and properties that are listed as or eligible for listing as a California Historic Landmark (CHL). The CHL criteria largely align with state and national criteria for significance, but they are bolstered by an assumption of heightened local or state importance. The criteria for eligibility as a CHL include properties that are:

- **First, Last, or Most Significant in its Region**
- **Associated with Important Individuals or Groups**
- **Prototypes or Outstanding Examples of Architecture or Design**

4.2 Preliminary Assessment

This section analyzes the site and each of the extant buildings and structures at the subject property for their potential historic significance under applicable state and federal criteria. Current names and addresses are used for each building.

4.2.1 Site

Before the current buildings and structures at the subject property were constructed, the land was part of a larger parcel that served an agricultural purpose. The subject property has been subdivided numerous times and is no longer agricultural in use or character; it does not appear to be wholly representative of the earlier agricultural era or any influential agricultural operations in the American Valley. Furthermore, the subject property never housed any major agricultural

outbuildings or residences. A barn associated with the larger agricultural operations was located on an adjacent parcel to the immediate east (non-extant, see Figures 43 and 46 in Chapter 3, *Development Chronology*).

The town of Quincy developed along Main Street to the south of the subject property during the later part of the 19th century and the early decades of the 20th century. Early plat maps indicate that the subject property was outside the initial town limits and later incorporated into town planning documents during the early 20th century, but it remained under agricultural use until the Diamond Match Co. built a lumber yard in 1937.

Although prominently located at the intersection with Church Street, the subject property was not among the earliest parcels to be developed in downtown Quincy or along Lawrence Street. Both the courthouse and other early businesses, such as the Feather River Bulletin offices, were located at the west end of Main Street. The construction of the second permanent courthouse in that location in 1929 solidified the town's commercial hub several blocks to the southwest of the subject property almost a decade prior to the construction of the first permanent building at the subject property.

As such, the subject property does not appear to be representative of either the region's agricultural heritage or the early development of the town of Quincy.

4.2.2 Quincy Lumber & Supply Co. (293-295 Lawrence Street; APN 115-031-054)

The most important themes that influenced the modern development of the subject property are the rise of the local lumber industry via the extension of the Western Pacific Railroad and the arrival of the Diamond Match Co. in Lassen and Plumas counties.

In 1937 the Diamond Match Co. built what is now known as the Quincy Lumber & Supply building to serve as storage, retail, and office space for a lumber yard. It was the first permanent building constructed on the subject property. It was located adjacent to the Western Pacific Railway, but it does not appear that a spur or loading dock was ever installed on the property.

The Diamond Match Co. operated a much larger factory and lumber yard in Chico, CA, for several decades (Figure 55). They built dozens of lumber mills and yards across northern California (Figures 56, 57). Each yard was built to local specifications, and the Quincy Lumber & Supply building appears to have been a relatively small-scale retail operation. Although it was intentionally built to accommodate lumber storage, with oversized doors and open storage systems, this was already a common aesthetic for building and farm supply stores at the time and was not architecturally distinctive. At some point after the 1960s the building was painted red with white trim and barn-style doors were installed in the storefronts to recall a farm or barn motif.

Diamond Match Co. is the most prominent lumber company to have occupied the subject property, but the Quincy Lumber Company, who established and operated a large mill in east Quincy, appears to have cornered the local market on lumber milling and sales. This is

evidenced by the fact that even though Diamond Match Co. built the lumber yard, they only remained in Quincy for 18 years. The Diamond Match Co. sold the lumber yard to a local competitor, Atkins Lumber and Supply, in 1955. Atkins liquidated in 1960, and another retail lumber supply company by the name of Quincy Lumber & Supply moved into the building ca. 1970. Quincy Lumber & Supply closed in 2009, but its signage remains extant and the building retains the name in local vernacular.

Diamond Match Co. was a prominent national company, with regional headquarters in Chico, that influenced economic and development patterns in Lassen and Plumas counties. However, the Quincy Lumber & Supply building does not appear to represent the scale and scope of that business. Buildings or landscapes that are associated with Diamond Match Co.'s regional hubs in Chico or Sterling City provide better representations of the company's historic operations (Figure 55, 56). Quincy Lumber Company, in east Quincy, appears to have had a larger impact on the lumber industry's development in Quincy. It commenced local operations more than two decades before Diamond Match Co. and was directly connected with the Quincy Junction railway line. Based on this preliminary research and analysis, it is unlikely that the Quincy Lumber & Supply building is eligible as a historical resource in state or local registers for its associations with the lumber milling industry, the railroad, or Diamond Match Co. themes.

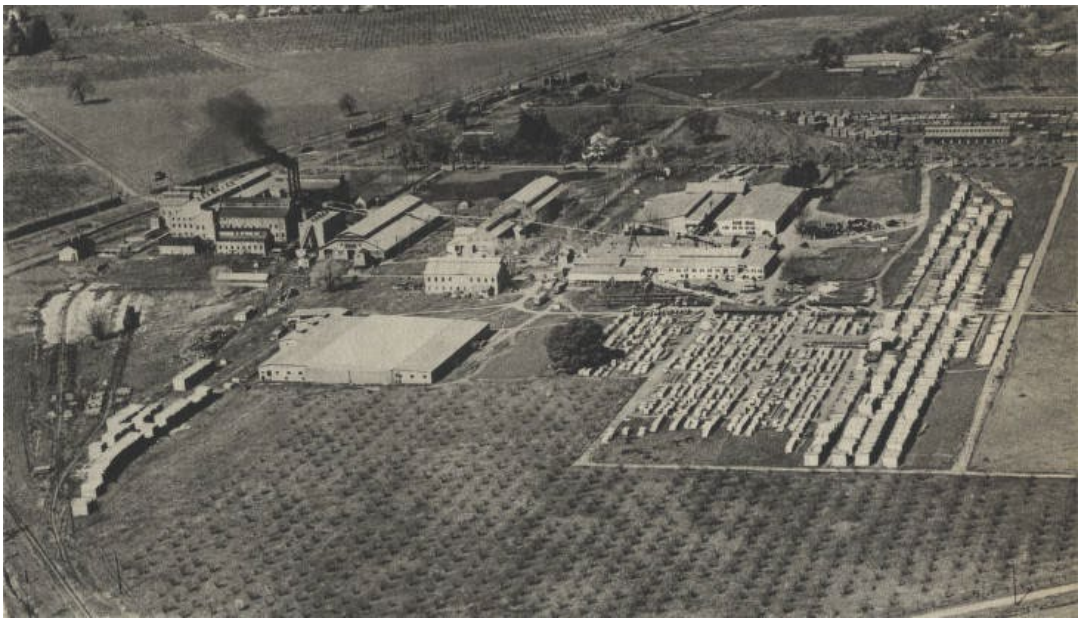


FIGURE 55. DIAMOND MATCH HEADQUARTERS IN CHICO, CA, CA. 1939, TWO YEARS AFTER THE CONSTRUCTION OF THE QUINCY LUMBER & SUPPLY BUILDING. THE CAMPUS INCLUDES MULTIPLE BUILDINGS AND ACRES OF STACKED LUMBER. IT IS ACCESSED VIA ROADS AND RAIL LINES. THE LARGE BRICK FACTORY AT THE LEFT EDGE OF THE CAMPUS WAS ONE OF THE FIRST DIAMOND MATCH CO. BUILDINGS IN CALIFORNIA. (SOURCE: CSU CHICO DIGITAL COLLECTIONS)

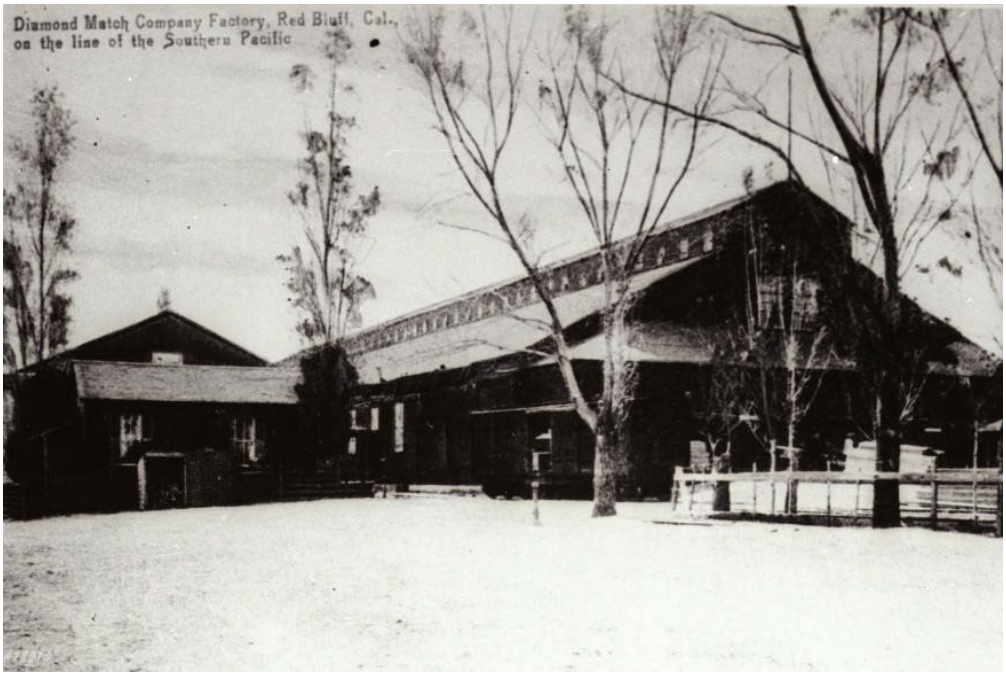


FIGURE 56. EARLY (N.D.) THE DIAMOND MATCH FACTORY IN RED BLUFF, CA. LOCATED NORTH OF CHICO, THIS PROPERTY DOES NOT MATCH THE HEADQUARTERS IN TERMS OF SCALE BUT EXHIBITS THE INVESTMENT THE COMPANY PUT INTO BUILDING ACROSS THE STATE. (SOURCE: CSU CHICO DIGITAL COLLECTIONS)



FIGURE 57. DIAMOND MATCH LUMBER YARD IN CHICO, CA, CA. 1915. ALTHOUGH THE DIAMOND MATCH LUMBER YARDS DO NOT APPEAR TO HAVE BEEN BUILT ACCORDING TO STANDARD SPECIFICATIONS, THIS HIGHLIGHTS SOME ARCHITECTURAL SIMILARITIES WITH THE QUINCY LUMBER & SUPPLY BUILDING'S HISTORIC DESIGN: WHITEWASHED WOOD BUILDING, WITH BLACK SIGNAGE AND FALSE FRONTS. (SOURCE: CSU CHICO DIGITAL COLLECTIONS)

4.2.3 Feather Publishing Co. (287 Lawrence Street; APN 115-031-052)

The Feather Publishing Co. is a prominent local institution that was established in the early 1970s and took over the management of multiple regional weekly newspapers that were published under various banners. The company purchased the northernmost parcel at the subject property and purpose-built a new building to house the administration, sales, and publishing operations ca. 1992-1994.

Before Feather Publishing Co. constructed the building at 287 Lawrence Street, they retained offices on Main Street in downtown Quincy. A marker was placed on a brick building near the intersection of Main Street and Crescent Street in 1978 and a second plaque was added in 1990; both markers commemorate more than a century of journalism in Plumas County (Figures 58, 59).[11] One of the newspapers, the Feather River Bulletin, was established in 1866 under the name the Plumas National News and celebrated its 150th anniversary in 2016.

The current Feather Publishing Co. building on the subject property does not represent the impact of the company nor any of its publications during their peak years of operation. Due to the stature of the Feather River Bulletin in the community, the publishing company's former offices on Main Street may have qualified as a local or state landmark had they not been demolished in the early 1970s. Additionally, the Feather Publishing Co. building is less than 50 years old and does not exhibit architectural distinction that would elevate it to exceptional importance under the National Register of Historic Places criteria for evaluation.[12]

[11] The Plumas County Assessor's Office: Map Portal states that the brick building was constructed in 1976. It appears that the building that housed Feather Publishing Co. was demolished and the plaque was placed to mark or mitigate the loss. However, the publishing company continued to operate out of that location until they built and moved into the current building at 287 Lawrence St ca. 1992-1994.

[12] National Register of Historic Places Criteria Consideration G covers properties that have achieved significance within the last fifty years. For more information on Criteria Consideration G, refer to National Register Bulletin 22: Guidelines for Evaluating and Nominating Properties that Have Achieved Significance Within the Last Fifty Years. https://www.nps.gov/subjects/nationalregister/upload/NRB22-Complete.pdf



FIGURE 58. DETAIL OF THE HISTORICAL MARKERS COMMEMORATING THE FEATHER PUBLISHING CO. AT THE CORNER OF MAIN STREET AND CRESCENT STREET. (SOURCE: HISTORICAL MARKER DATABASE, HMDB.ORG)



FIGURE 59. THE CA. 1976 BUILDING WHERE THE HISTORICAL MARKERS COMMEMORATE THE FEATHER PUBLISHING CO. AT THE CORNER OF MAIN STREET AND CRESCENT STREET. (SOURCE: HISTORICAL MARKER DATABASE, HMDB.ORG)

4.2.4 Carport (253 Lawrence Street; APN 115-031-055)

The carport, built in 1981, does not appear to be associated with any important themes associated with the development of Quincy or the region, nor does the structure exhibit engineering or architectural distinction.

4.3 Conclusion

The buildings or structures located at the subject property do *not* appear significant under state or national criteria for historic significance. They are not exemplary of the historical themes identified in Chapter 3, *Development Chronology* and listed at the beginning of this chapter. Although agricultural and lumber milling were important economic drivers in the region historically, and both the Diamond Match Co. and the Feather Publishing Co. are important regional and local (respectively) institutions, these patterns of development are not represented by any of the extant buildings. As such, no potential historical resources are present.

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ARCHAEOLOGICAL RESOURCES ASSESSMENT REPORT

NEW QUINCY COURTHOUSE REPLACEMENT
QUINCY, PLUMAS COUNTY, CALIFORNIA

FOR

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MAY 2026

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CHRIS/NEIC SEARCH RESULTS

SEARCH	CHRIS/NEIC File # NE 25-434 dated October 7, 2025 (No Confidential Information)

1.0 INTRODUCTION

This *Archaeological Resources Assessment Report* (ARAR) provides a review of the Project site for the proposed new Quincy Courthouse Project (Project) to be located at 253, 287, and 293 Lawrence Street, unincorporated Quincy, Plumas County. The existing courthouse building, located approximately 0.2 miles southwest of the Project site, is substantially out of compliance with regulatory safety, seismic, and accessibility codes, and Judicial Council of California (Judicial Council) space standards. The new courthouse will relocate Superior Court operations and courtrooms to a new, permanent facility. The existing county-owned historic courthouse would remain in place under County ownership. The Judicial Council is currently unaware of the County's plans for the existing courthouse following transition of operations to the new courthouse.

This ARAR is based on available archival and literature resources and a field inventory and provides recommended programmatic mitigation measures to avoid potentially significant impacts to recorded and potential archaeological resources in accordance with the California Environmental Quality Act (CEQA) and the Judicial Council's planning requirements.

2.0 LOCATION AND DESCRIPTION

The 2.86-acre Project site includes three contiguous, privately-owned parcels in the unincorporated town of Quincy located at 253 Lawrence Street (APN 115-031-055), 287 Lawrence Street (APN 115-031-052), and 293 Lawrence Street (APN 115-031-054). The Project site is bounded by Lawrence Street/SR 70/89 to the south, multi-family and single-family residential land uses to the west, a bike path along a former railroad alignment and a defunct, former wastewater treatment plant to the north, and multi-family residential and commercial land uses to the east (T 24N, R 9E, S ½ of Section 14, USGS Quincy, CA 1994) [Figs. 1-3].

The Project consists of the construction of a new courthouse to relocate Superior Court operations that are currently housed in the Plumas County Courthouse, 520 Main Street, to the Project site. The new courthouse, a one-story approximately 23,097 square foot building, will provide a permanent state-owned facility that is accessible to the public and can provide enhanced services to the public. The courthouse building will include construction of new courtrooms with support spaces, and administrative and operations areas. The Project also includes site improvements, including new on-site surface parking lots and drive aisles, and rerouted existing utility connections to serve the new building.

The existing on-site commercial buildings and hardscape along with any subsurface utilities will be abandoned or removed and the site prepared for new construction.

3.0 REGULATORY

The Judicial Council, acting as the judicial branch of State government, is not subject to local land use regulations; however, the Judicial Council, as lead agency, considers local policies in evaluating whether the Project's impacts would be significant.

Cultural resources include pre-contact and post-contact historic archaeological sites, districts, and objects; standing historic structures, buildings, districts, and objects; and locations of

important historic events or sites of traditional and/or cultural importance to various groups. The analysis of cultural resources can provide valuable information on the cultural heritage of both local and regional populations. Cultural resources may be determined significant or potentially significant in terms of national, state, or local criteria either individually or in combination.

This report has been prepared to provide information for the Project's CEQA analysis and the Judicial Council's planning analysis. The Judicial Council, as the CEQA lead agency, must review the potentially significant impacts of the Project on historical and unique archaeological resources, and tribal cultural resources. If potentially significant impacts may occur, the Judicial Council must identify whether feasible mitigation measures or Project alternatives can minimize adverse impacts on cultural resources.

3.1 STATE OF CALIFORNIA

Public agencies under CEQA must consider the effects of a proposed project on both "historical resources" and "unique archaeological resources." Pursuant to California Public Resources Code (PRC) Section 21084.1, a "project that may cause a substantial adverse change in the significance of an historical resource is a project that may have a significant effect on the environment" (14 Cal. Code of Regulations (CEQA Guidelines) Section 15064.5(b)). PRC 21083.2 requires agencies to determine whether a proposed project would have a significant effect on "unique" archaeological resources.

Historical Resources

An historical resource includes a resource listed in or determined to be eligible for listing in the California Register of Historical Resources (CRHR) (PRC 21084.1 and CEQA Guidelines Section 15064.5(a)). The CRHR includes resources listed in or determined eligible for listing in the National Register of Historic Places (NRHP) or the CRHR as well as some California State Landmarks and Points of Historical Interest.

Historical resources included in a local register of historical resources (PRC 5020.1(k)), or identified as significant in a historical resources survey (PRC 5024.1(g)), are presumed to be historical resources under CEQA unless a preponderance of the evidence demonstrates otherwise (PRC 21084.1 and CEQA Guidelines Section 15064.5(a)).

In addition, the lead agency has discretion to treat an object, building, structure, site, area, place, record, or manuscript as a historical resource for CEQA purposes if the lead agency has substantial evidence showing that such a resource is historically significant or significant in the architectural, engineering, scientific, economic, agricultural, educational, social, political, military, or cultural annals of California. (PRC 21084.1 and CEQA Guidelines Section 15064.5(a)(3)). Generally, a lead agency may determine a resource to be "historically significant" if the resource meets the criteria for listing on the CRHR, including the following:

1. Is associated with events that have made a significant contribution to the broad patterns of California's history and cultural heritage;
2. Is associated with the lives of persons important in our past;
3. Embodies the distinctive characteristics of a type, period, region, or method of

construction, or represents the work of an important creative individual, or possesses high artistic values; or,

4. Has yielded, or may be likely to yield, information important in prehistory or history (CEQA Guidelines Section 15064.5(a)(3)).

The fact that a resource is not listed or determined to be eligible for listing in the CRHR, or not included in a local register of historical resources (pursuant to PRC Section 5020.1(k)), or identified in an historical resources survey meeting the criteria in PRC Section 5024.1(g) does not preclude a lead agency from determining that the resource may be a historical resource (PRC 21084.1 and CEQA Guidelines Section 15064.5(a)(4)).

A project that may cause a substantial adverse change in the significance of a historical resource is a project that may have a significant effect on the environment (PRC Section 21084.1). A "substantial adverse change" in the significance of a historical resource means physical demolition, destruction, relocation, or alteration of the resource or its immediate surroundings such that the significance of a historical resource would be materially impaired (CEQA Guidelines Section 15064.5(b)(1)).

Unique Archaeological Resources

CEQA also distinguishes between two classes of archaeological resources: archaeological sites that meet the definition of a historical resource, as described above, and "unique archaeological resources." Under CEQA, an archaeological resource is considered "unique" if it can be clearly demonstrated that, without merely adding to the current body of knowledge, there is a high probability that the resource meets any of the following criteria:

1. Contains information needed to answer important scientific research questions and there is a demonstrable public interest in that information;

2. Has a special and particular quality such as being the oldest of its type or the best available example of its type; or,

3. Is directly associated with a scientifically recognized important prehistoric or historic event or person (PRC 21083.2(g)).

Archaeological resources meeting the definition of a historical resource must be treated as a historical resource. If the site is not a historical resource, but meets the definition of a unique archaeological resource, it must be treated in accordance with the provisions of PRC 21083.2. PRC Section 21083.2 states that if it can be demonstrated that a project will cause damage to a unique archaeological resource, the lead agency may require reasonable efforts to be made to permit any or all of these resources to be preserved in place or left in an undisturbed state. Examples of that treatment, in no order of preference, may include, but are not limited to:

(1) Planning construction to avoid archaeological sites.

(2) Deeding archaeological sites into permanent conservation easements.

(3) Capping or covering archaeological sites with a layer of soil before building on the sites.

(4) Planning parks, greenspace, or other open space to incorporate archaeological sites.

If the lead agency does not preserve the unique archaeological resource in place or leave it undisturbed, the lead agency must require mitigation measures, as specified in PRC 21083.2.

Tribal Cultural Resources

Several PRC sections added by Assembly Bill 52 (Gatto 2014) provide protections for tribal cultural resources.[1] Prior to the release of a negative declaration, mitigated negative declaration, or environmental impact report for a project, lead agencies must begin consultation with each traditionally and culturally affiliated California Native American tribe that has requested consultation (PRC 21080.3.1). Lead agencies must consult with tribes regarding the potentially significant impacts of a project on tribal cultural resources and feasible project alternatives or mitigation measures (PRC 21080.3.2). Under PRC Section 21074, tribal cultural resources include sites, features, places, cultural landscapes, sacred places, or objects that are of cultural value to a California Native American tribe eligible or listed on the CRHR or a local historic register, or that the lead agency has determined to be a significant tribal cultural resource while considering the significance of the resource to the tribe. A project that may cause a significant adverse change in the significance of a tribal cultural resource would have a significant effect on the environment (PRC 21084.2).

Other California Laws and Regulations

Other state-level requirements for cultural resources management appear in PRC Chapter 1.7, Section 5097.5 "Archaeological, Paleontological, and Historical Sites," and Chapter 1.75 beginning at Section 5097.9 "Native American Historical, Cultural, and Sacred Sites" for lands owned by the state or a state agency.

The disposition of Native American burials is governed by Section 7050.5 of the California Health and Safety Code and PRC Sections 5097.94 and 5097.98 and falls within the jurisdiction of the Native American Heritage Commission (NAHC).

4.0 BACKGROUND CONTEXT

4.1 ENVIRONMENTAL SETTING

Plumas County is located at the northern terminus of the granitic Sierra Nevada at its intersection with the volcanic Cascade Range. The county is one of the most rural counties in the state with an area of approximately 2,613 square miles of which about 65% consists of public lands managed by the U.S. Forest Service with another 6% owned and managed by other public agencies (e.g., State of California and County of Plumas) and about 29% privately owned.

The county boasts diverse mineral resources, forestlands and the largest high elevation valley-meadow complex in California along with a network of streams and rivers that are part of the Feather River Watershed – the largest in the Sierra Nevada. Elevation ranges from 1,800 to 8,376

1. AB 52 amended Section 5097.94 of, and added Sections 21073, 21074, 21080.3.1, 21080.3.2, 21082.3, 21083.09, 21084.2 and 21084.3 to, the California Public Resources Code.

feet. Valleys with known pre-contact Native American occupation present between 3,500 and 5,500 feet elevation include Big Meadows (present-day Lake Almanor), American Valley in which the town of Quincy is located, Genesee Valley, and Indian Valley (Kowta 1988:8; see Fariss and Smith 1988 [1882]; *Plumas County General Plan 2035*).

4.2 NATIVE AMERICAN – Pre-contact

Early occupation of Northeastern California appears to date from 13,400 to 8,850 cal B.P.[2] The lifeway of these mobile, early peoples focused on hunting and the resources offered by lacustrine and marshland environments. Subsequent cultural change and the emergence of regional archaeological patterns appear to have been local responses to available environmental opportunities influenced by climatic change and impacts of other groups/tribes/cultures through time.

Researchers have developed various archaeological chronologies for Northeastern California using limited data usually based on excavation (e.g., Kowta 1988:Fig. 1; Moratto 1984:Fig. 7.6; McGuire 2007:169, Table 11.1; Hull 2007:Fig. 12-4). The archaeological data indicates at least 11,000 years of occupation culminating with the ethnographic Mountain Maidu who occupied villages that persisted until displaced by the influx of EuroAmericans, Chinese, and other parties during the mid-19th century Gold-Rush followed by permanent settlement.

A summary chronology presented by McGuire (2007:169, Table 11.1) suggests changes in material culture complexity with a concomitant increase over time in the pre-contact Native American population and provides information on the complexity of the evolving material culture as well as aspects of settlement patterns and evidence of trade systems over time and space.[3]

Early Holocene	5000+ cal B.C. [ca. 11,500 - 9500 ca B.C.; Clovis-like projectile points; highly mobile over a large geographic area]
Post-Mazama	5000-300 cal. B.C.[Northern side-notched projectile points; generalized hunting and gathering with a focus on intensive exploitation of plant resources]
Early Archaic	3000-1500 cal. B.C. [Martis Complex or Tradition; diversified artifact assemblages; hunting and gathering with focus on varied plant resources; semi-permanent villages]
Middle Archaic	1500 cal B.C – cal. A.D. 700 [large semi-sedentary villages with

2. "Cal BP" (calibrated years Before Present) refers to radiocarbon ages adjusted using calibration curves (e.g., often tree-ring data) to match actual calendar years, with "Present" defined as AD 1950. Calibration converts raw radiocarbon years into historically accurate dates, allowing for direct comparison with calendar years. Dates presented as Cal BP have not been converted into current usage which uses BCE/CE (Before Common Era/Comma Era) which is a secular alternative to BC/AD (Before Christ/After Christ). The BCE/CE notation is increasingly common in literature over the past 25 years.

3. Archaeologists theorize that pre-contact populations increased prior to the arrival of EuroAmericans with a concomitant increase in social and material culture complexity. McGuire (2007) provides summaries of notable social and material culture traits (e.g., change in projectile point types, presence of larger villages, and other observations).

	house structures; increased material culture complexity; trade and exchange networks]
Late Archaic	cal. A.D. 700-1400 [Rose Spring and Gunther series projectile points; large villages with short duration occupation; scattered smaller occupation sites; changes in subsistence and settlement organization; major changes possibly linked to warmer/dryer climate change A.D. 900-1400]
Terminal Prehistoric	cal. A.D. 1400 – historic contact [Desert side-notched and Cottonwood series projectile points; population shifts and dispersals due arrival of Numic groups; transition to smaller occupation sites from large seasonal or semi-permanent settlements; shift to smaller material culture and less specialized material culture assemblages; possible interpersonal conflicts between Numic and other groups; introduced European disease epidemics may have resulted in Native population losses]

4.3 NATIVE AMERICAN - Ethnographic

The Project site is within the territory of Native Americans identified as the *Maidu,* also known as the *Mountain Maidu* or *Northeastern Maidu,* who occupied drainages of the American and Feather rivers of the northern Sierra. The Mountain/Northeastern Maidu family of languages is classified as within the California Penutian Stock. The "American Valley" dialect, one of the four Mountain/Northeastern Maidu dialects, would have been spoken in the Project area and vicinity.

The Mountain/Northeastern Maidu lived in mountain valleys with permanent settlements located near water, often near streams or on ridges or knolls with southern exposure. They "built along the edges overlooking the valley, with the pine timbered highland on one side of them and the open level on the other in order to avoid the snow and later, mushy meadows. The general Project area appears to have been an "optimal zone" for prehistoric subsistence and settlement.

The American Valley in which the Project site is located, was named *Silo-nt-koyo*, that is "Silo valley" or "silo land," with six known pre-contact villages. Each settlement consisted of two to three houses or six to seven houses for an approximate total of 18-23 within the valley. The pre-contact occupation site nearest to the Project site was *Nukuti* (see Kroeber 1925) located "where the high school has since been erected,"[4] that is approximately 0.3 mile to the east of the proposed new courthouse location.[5] This village had two to three houses and was not the "most populous village" but had the largest "sweat house" or ceremonial chamber of the four sweat houses/chambers known within the American Valley. Its large size "probably means that the man who had the most authority within the group [the American Valley] and was its spokesman

4. Quincy Junior/High School, in existence since 1910, is located at 6 Quincy Junction Road (Web, 10/20/2025). Reportedly, the Quincy Chinatown was also located on school property (Plumas County Museum Association [PCMA] 2025d).

5. All four recorded sites that are located east of Quincy Junction Road in the vicinity of Quincy Junior/High School consist of historic scatters. No "informal prehistoric resources" have been noted in the vicinity (NEIC File # NE-424).

lived here" (Kroeber 1925:393, 396-398, Plate 37; Riddell 1978:370-371, Fig. 1; Moratto 1984:290).

The discovery of gold with the influx of non-native populations, introduced disease and forced relocations resulted in an extraordinary decline in the population of the Maidu, Konkow and Nisenan from an estimated 8,000 in 1864 to 1,100 in 1910 and 40 in 1941 (Riddell 1978:386; Heizer 1978:Table 1). For a more extensive review of the Maidu see Dixon (1905), Kroeber (1925), and Riddell (1978).

4.4 POST-CONTACT HISTORIC PERIODS

The post-contact history of the general area can be divided into the Hispanic Period (1769-1848) and the American Period (1848-onward). During the Hispanic Period, Spanish government policy in northwestern New Spain was directed at the founding of presidios (forts), missions, and pueblos (secular towns), with the land held by the Crown. Later, Mexican policy (1822-1846) stressed individual ownership of the land with grants of vast tracts of land to individual citizens (Hart 1987). The American Period focused on development and growth, a pattern that continues into the 21st Century. The Project site is located within the American Valley which later became part of Plumas County.

4.4A Hispanic Period (1769-1848)

The northern Sacramento Valley region was explored and lightly settled late in the Spanish-Mexican colonial era. The most northerly Spanish expeditions were the 1820 expedition of Luis Arguello, credited with exploring and naming "El Rio de las Plumas," (the river of feathers), and his 1821 expedition that is known to have proceeded along the west bank of the Sacramento River reaching Cottonwood Creek (15 miles south of present-day Redding) and then following the Trinity, Eel, and Russian rivers (Beck and Haase 1974:#18; Kyle 2002:281**).**

None of the presidios, missions, secular towns or Spanish or Mexican grants were located within what later became Plumas County (Beck and Haase 1974).

4.4B American Period (1848-Present)

The first wave of settlement in the region occurred during the Gold Rush, beginning in 1848 with a tapering by the mid-1850s. Numerous mining camps sprang up along the Sacramento River and its tributaries, giving rise to permanent towns. The Lassen Emigrant Trail to California dates to 1848 and traveled through what was to become Plumas County to Big Meadows (present-day Lake Almanor) and on to the Sacramento River. A second trail soon followed. James Pierson Beckwourth, namesake of Beckwourth Pass[6] over the High Sierra Nevada, led a prospecting expedition in 1851 that discovered the pass. He proposed and constructed a wagon road through the pass down to American Valley in which the Project site is located. The existing pack trail between American Valley and Bidwell Bar, was subsequently widened and eventually reached Marysville, the supply center for the northern mines. By August 1851 the first emigrants were entering California via the Beckwourth Trail, but by 1855 other routes into California superseded

6. California State Landmark #336 (CAL/OHP 1990:154).

the trail. Beckwourth built a cabin[7] in 1852, the first in the Sierra Valley, that functioned as a hotel and trading post just west of present-day Beckwourth on SR 70 (Kyle 2002:281-282).

Gold was reportedly discovered on the American Ranch[8] (future Quincy) in the early 1850s (Gudde 1975:280). Plumas County was organized in 1854 from part of Butte County and a portion of Lassen County. The town of Quincy, situated within Plumas Township, is strategically located within American Valley about equidistant from the East Branch of the North Fork of the Feather River (and south Spanish Creek) and the Middle Fork of the Feather River (Coy 1973:202-203; Gudde 1975:Map 3; Keddie 1886). The town of Quincy has been the only county seat.

The "Quinsy" post office (also known as American Ranch) was established December 17, 1855, when it was moved from the larger Elizabethtown (about opposite Quinsy on the north side of the East Branch tributary) (see Patera 1991:174, 283 [map]; Gudde 1975:Map 3). The importance of both is demonstrated by their presence on Goddard's 1857 *Map of the State of California,* but by 1882 Elizabethtown was no longer extant (see Keddie's 1882 map of *Map of Plumas County, California, and portions of Lassen, Sierra, Nevada, Yuba, Butte, Tehama and Shasta Counties, California, and Roop and Washoe Counties, Nevada*).

The Town of Quincy was laid out by James H. Bradley, one of the three commissioners instrumental in the creation of Plumas County, after his farm in Illinois so named for John Quincy Adams, sixth President of the United States. In addition, he constructed a building for a temporary courthouse, described as a "rude shake building" in the rear of his hotel placed at 355 Main Street, about a block south and west of the Project site. Furthermore, he and Joseph Greena [*sic*] and George W. Sharpe provided the public square that was the site for a future courthouse. The first county courthouse was built in 1859 while the current courthouse was built in 1920 (CAL/OHP 1976:68; Plumas County General Plan 2013/2023:4, Fig. 3; Kyle 2002:286).

The 1860 census lists a population of 191 white residents and 1 Free Colored in Quincy of the county population of 4,042. No Asiatic persons were resident within the town although the American Valley had 207 white residents and 31 Asiatic persons. Reportedly none of the 399 Chinese who arrived Plumas County in the 1850s resided in Quincy but were present in the American Valley (31), Fillmore township (144), and Mineral (78) with smaller populations elsewhere in the county. The Chinese focused on streambed gravel gold mining and other marginal "diggings" and by the 1880s were the majority of miners in the county. The Chinese developed their own communities in Greenville just west of the town; China Alley on the east side of town; Taylorsville on the south had a small Chinese neighborhood; and, Quincy had a small Chinatown that was present until the early 1900s. Silver Creek west of Spanish Ranch about 7 miles from Quincy was the largest Chinese settlement of over 500 residents. The location of the Quincy Chinatown is now occupied by the Quincy Junior Senior High School

7. State of California Black Ethnic Site (CAL/OHP 1988:90-91, 95 #10).

8. California State Landmark #479, Site of American Ranch and Hotel is located at 355 Main Street (CAL/OHP 1990:154; Kyle 2002:286). Site listed in *The California History Plan* and *California Inventory of Historic Resources* (CAL./OHP 1973:124; CAL/OHP 1976:249).

(Fariss and Smith 1988 [1882]:138-139, 277-278; Plumas County General Plan 2013/2023:4, Fig. 3; PCMA 2025d).[9]

During the 1870s, the area experienced an economic boom from hydraulic mining, attracting large numbers of miners including significant numbers of Chinese immigrants. By 1882 the town was thriving "surrounded by good farms, and in the midst of a mineral region that is [was] rapidly being developed." At the time, the town included two hotels (Plumas and Quincy House), seven stores, two livery stables, five saloons, a meat market, wagon shop, several blacksmiths, a shoemaker, barber and jeweler along with a church, school-house, courthouse and jail, post-office, a Wells Fargo & Company express office (including banking), telegraph office, I.O.O.F hall, Masonic hall, town hall, and a weekly newspaper. A narrow-gauge railroad to Reno, Nevada was anticipated and at the time travel to Reno relied on stages to Indian Valley and Susanville, to Oroville to La Porte, and to Sierra Valley and Reno. Quincy was also one of the stations of Whiting and Company's Dog Express that in the early years brought mail over the snows of the Sierra (1858-1865) until replaced by the horse snowshoe. The rich, arable land within American Valley produced wheat, oats, barley, potatoes with a variety of vegetables and stock. Dairies were also an important component. Two saw-mills provided the "large quantities of lumber used in building and in the mining claims." (Kyle 2002:286; Fariss and Smith 1988 [1882]:275-276, 281; Plumas County 2013/2023:156).

The completion of the Western Pacific Railroad (WPRR) in 1910 opened opportunities for the timber industry, which became the region's dominant economic force.[10] The lumber boom saw the relocation of African-Americans from Louisiana to work in the industry from the 1930-1950s with many of the workers and families remaining after the closure of the mills.

The completion of State Route 70 in 1937 connected the town to the Sacramento Valley and fostered subsequent development along the highway and residential growth. The economic shift in the mid-1990s from a historic dependence on timber led to the development of tourism and outdoor recreation. The diversified economy of the town and county includes a focus on government and commercial services, education and the timber industry although with less prominence than in the past due to sustainable forest management policies. The current population of Quincy is approximately 1,600.

4.4C Historic Map Review

Mora (2023) reviewed selected historic maps (USGS topographic maps 1951-2021); survey plats (General Land Office 1872); aerial photographs (1947-2002); and, Sanborn Fire Insurance maps (1902, 1912) for the Project site and adjacent areas. The 1902 and 1912 Sanborn Fire Insurance maps show Lawrence Street on the southern boundary of the Project site but indicate no or minimal development within the site and adjacent areas. Construction of a single building (293 Lawrence Street) occurred in the mid-1930s with additional buildings/structures added in 1981 and 1993-1998 along with other improvements.

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9. The Quincy Chinese American Cemetery is located just beyond the 1.0 mile search radius. It is a State of California Chinese Ethnic Site (CAL/OHP 1988:155 #66).

10. The Quincy Western Railroad began construction in 1909 and operated for over a decade providing service to the Western Pacific Railroad at Quincy Junction until 1917. The Quincy Railroad, incorporated the same year took over the tracks and is now owned by Sierra Pacific Industries. It still is in service.

5.0 RESEARCH PROTOCOLS AND RESULTS

Two archival records and literature searches for a 1.0 mile radius of the Project site were completed in 2025 by the California Historical Resources Information System, Northeast Information Center (CHRIS/NEIC) for: (1) Ascent Environmental (IC File NE22-25, January 27, 2025 addressed to Alta Cunningham) and, (2) Basin Research Associates (IC File NE 25-434, October 7, 2025). An earlier search of a 0.5 miles radius was completed by Ascent Environmental (IC File # NE23-202, May 12, 2023) and resulted in a Memo to File (see Mora 2023) (see also Hagel 2025a-b).

In addition, reference material available on the internet, the Bancroft Library at the University of California, Berkeley, and Basin Research Associates was also consulted. Sources included:

California History Plan (CAL/OHP 1973);

California Inventory of Historic Resources (CAL/OHP 1976);

Five Views: An Ethnic Sites Survey for California (CAL/OHP 1988);

National Register of Historic Places (NRHP) listings in Plumas County (USNPS 2025-c);

Built Environment Resources Directory (BERD) for Plumas County (CAL/OHP 2025a;

California Historical Resources for Plumas County (CAL/OHP 2025b);

Archaeological Determinations of Eligibility for Plumas County [ADOE] (CAL/OHP 2025c); and;

Other relevant sources (see References Cited and Consulted).

5.1 RECORDS SEARCH RESULTS (see Tables 5.1-5.2)

There are no cultural resources studies within or adjacent to the Project site on file with the CHRIS/NEIC. There are 31 studies within a 1.0 mile radius of the Project site (see Table 5.1).

The records search was negative for recorded archaeological sites, built environment resources, and/or reported cultural resources within or adjacent to the Project site. No precontact sites have been recorded within the 1.0 mile radius search buffer. A total of 16 Historic Era resources have been recorded within 1.0 mile of the Project site including two historic buildings. Post-contact historic archaeological sites include: six trash scatters/deposits; two water ditches (Mill Creek Ditch and Old Powerhouse Pipeline Ditch); two cabin sites, two prospecting pits/adits, the Plumas County Cemetery and segments of the Beckwourth Trail. The majority of the recorded resources have not been evaluated for the National Register of Historic Places (NRHP) and/or the California Register of Historical Resources (see Table 5.2).

TABLE 5.1
STUDIES IN/ADJACENT TO OR WITHIN 1.0 MILE OF THE PROJECT SITE

Report #	Author	Date	Title	Study Type	Comments	Resources In/Adjacent
In or Adjacent						
None						
Within 1.0 Mile						
NEIC-000193	Henry O. Bass	1974	Environmental Impact Report for the Proposed Reconstruction of California State Route 70 through the Town of Quincy, Plumas County	Archaeological, Field study	Negative	None
NEIC-000209	Charles D. James	1976	Archaeological Clearance Investigations Medical Clinic Building Project; Plumas Hospital District, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-000212	Janet P. Friedman	1976	Archaeological Reconnaissance of Gansner and Beckwourth Airports, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-000229	Kevin Buchanan	1979	Archaeological Reconnaissance of the Quincy Sewage Treatment and Disposal Project, Plumas County, California, S.W.R.C.B. Project #C-06-1179-010	Archaeological, Field study	Negative	None
NEIC-001579	Brian Wayland	1996	Archaeological and Historical Resources Survey and Impact Assessment: Peppard Flat THP	CF MOU	One resource outside of the 1.0 mile search area	None
NEIC-001967	Brian Wayland	1997	Confidential Archaeological Addendum for Timber Operations on Non-Federal Lands in California: Blanchard THP	CF MOU	Negative	None
NEIC-002555	Brian Wayland	1995	Archaeological and Historical Resources Survey and Impact Assessment: Plumas County Cemetery THP	CF MOU	P-32-001442 is within the 1.0 mile search area	None
NEIC-004852	Richard Jenkins	1988	5100 Forest Regulation 5130 Timber Harvesting Plans THP 2-88-121 PLU Archaeological Review	Archaeological, Field study	P-32-002463 is within the 1.0 mile search area	None
NEIC-005033	Brian Wayland	2002	Confidential Archaeological Addendum for Timber Operations on Non-Federal Lands in California: Boyle Ravine THP	CF MOU	Negative	None
NEIC-005408	Richard Jenkins	1988	5100 Forest Regulation 5130 Timber Harvesting Plans THP 2-88-116 PLU Archaeological Review	Archaeological, Field study	Negative	None
NEIC-006295	Diane McCombs	2005	Heritage Resource Survey for the 3.4 Acre Spanish Creek Dyrr Bank Stabilization Project, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-007595	Brian Wayland	2005	An Archaeological Survey Report for the Cemetery Hill Timber Harvesting Plan Plumas County, California	CF MOU	Negative	None
NEIC-007605	Dawn Henrici	1979	Proposed Division of 6.18 Acres into Two Parts for Commercial Use	Archaeological, Field study	Negative	None
NEIC-007610	Dawn Henrici	1979	Proposed Zone Change of 11.77 Acres from CG and 6A-FP-2 Districts to C-2 District	Archaeological, Field study	Negative	None
NEIC-007611	Dawn Henrici	1979	Archaeological Reconnaissance of the Christenson and Barlow Minor Lot-Line Adjustment	Archaeological, Field study	Negative	None
NEIC-007616	Dawn Henton	1982	An Archaeological Reconnaissance of the County Owned Property on the Western Edge of American Valley	Archaeological, Field study	Negative	None
NEIC-007618	Peak & Associates	1983	Cultural Resource Assessment of a Proposed Small Hydroelectric Development near Quincy, Plumas County, California	Archaeological, Field study	Negative	None

TABLE 5.1, con't
STUDIES IN/ADJACENT TO OR WITHIN 1.0 MILE OF THE PROJECT SITE

Report #	Author	Date	Title	Study Type	Comments	Resources In/Adjacent
Within 1.0 Mile, con't						
NEIC-007622	David Rhode	1990	Beskeen Property Survey, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-009485	Diane McCombs	2008	Heritage Resource Survey for the American Valley Gansner Park River Parkway. 6.3 acres in Quincy	Archaeological, Field study	Negative	None
NEIC-009913	Wayne H. Bonner	2008	Cultural Resources Record Search and Site Visit Results for T-Mobile Candidate SC55476 (Quincy), 677 Radio Hill Road, Quincy, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-009914	Diane McCombs	2008	Heritage Resource Survey for the Quincy Community Services District Wetland Project, 50 Acres in American Valley, Plumas County, California	Archaeological, Field study	One resource outside of the 1.0 mile search area	None
NEIC-009914	Diane McCombs	2010	Heritage Resource Survey for the Quincy Community Services District Wastewater Treatment Discharge Project, 16 acres in American Valley, Plumas County, California [Revised]	Archaeological, Field study	Negative	None
NEIC-010593	Gregory Henton	1994	An Archaeological Reconnaissance of the East Quincy Services District Force Sewer Main, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-010972	Susan Rose	1979	Archaeological Reconnaissance Report for the Proposed Airport Land Exchange Project, Plumas County, California	Archaeological, Field study	Negative	None
NEIC-011578	Heath Browning	2012	Cultural Resources Inventory for the Caribou-Plumas 60kV Reliability Project-Phase 2: Elizabethtown Junction to Quincy, Plumas County, California. PG&E PM. No. 30828169	Archaeological, Field study	P-32-003909, -10, -11, -12 within the 1.0 mile search area; three resources outside of the search area	None
NEIC-013087	Melinda Button and Heath Browning	2016	Cultural Resources Inventory for the Highway 70 Hazardous Fuel Reduction Project, Plumas County, California	Archaeological, Field study	Four resources outside of the 1.0 mile search area	None
NEIC-013367	Dewey Robbins	2014	An Archaeological Survey Report for the Icky Thump Timber Harvesting Plan Plumas County, California	CF MOU	P-32-005693 is within the 1.0 mile search area; three resources outside of the search area	None
NEIC-013402	Melinda Button and Heath Browning	2016	Cultural Resources Inventory for the East Quincy Hazardous Fuel Reduction Project Plumas County, California	Archaeological, Field study	Four resources outside of the 1.0 mile search area	None
NEIC-014322	Danielle Bradfield	2017	An Archaeological Survey Report for the Porterfield Timber Harvest Plan, Plumas County, California	CF MOU	Negative	None
NEIC-014575	John W. Jones	2020	Claremont Heritage Resource Inventory Plumas County, California	Archaeological, Field study	Many resources outside of the 1.0 mile search area	None
NEIC-015443	Robert McCann	2020	NRCS California 19FY323_0003	Archaeological, Field study	Negative	None

TABLE 5.2
CULTURAL RESOURCES WITHIN OR WITHIN 1.0 MILE OF THE PROJECT SITE

Resource	Type	Recorded by	Eligibility NRHP/CRHR	Comment
In/adjacent				
None				
Within 0.25 mile				
P-32-000459 CA-PLU-459H	Historic; Site; Mill Creek Ditch	1980 (S. Rose, P. Preschutti, M. Ramos, P. Hines, Plumas National Forest); 1990 (Susan Rose, Plumas National Forest); 2009 (T. Whetstone, Plumas National Forest)	Unevaluated	[redacted]
P-32-001442 CA-PLU-1442H	Historic; Site; Plumas County Cemetery	1995 (R. Stine and B. Wayland)	Unevaluated	[redacted]
P-32-001635 CA-PLU-1635H	Historic; Site; Beckwourth Trail	Numerous segments recorded by various researchers	Unknown	[redacted]
P-32-002463	Historic; Site; Cabin Site, Carson THP	2003 (Brian Wayland, Wayland Resource Management)	Unevaluated	[redacted]
P-32-003808 CA-PLU-3808H	Historic; Building; Quincy Motor Sales	2010 (Diane McCombs, McCombs Archaeology)	6Z DPR	[redacted]
P-32-003909 CA-PLU-3909H	Historic; Site; historic refuse scatter	2012 (R. Heath Browning, Cardno Entrix)	Unevaluated	[redacted]
P-32-003910 CA-PLU-3910H	Historic; Site; historic refuse scatter and deposit	2012 (R. Heath Browning and Jay Baker, Cardno Entrix)	Unevaluated	[redacted]
P-32-003911 CA-PLU-3911H	Historic; Site; small historic refuse scatter	2012 (R. Heath Browning and Jay Baker, Cardno Entrix)	Unevaluated	[redacted]
P-32-003912 CA-PLU-3912H	Historic; Site; sparse historic refuse scatter	2012 (R. Heath Browning and Jay Baker, Cardno Entrix)	Unevaluated	[redacted]
P-32-005379 CA-PLU-5379H	Historic; Site; prospecting pit	2016 (Heath Browning, Melinda Button, Browning Cultural Resources)	Unevaluated	[redacted]
P-32-005623	Historic; Building; Outbuilding at 227 Oddie Way	2016 (T. Vaughan and B. Davidson, Coyote & Fox Enterprises)	6Z DPR	[redacted]
P-32-005693 CA-PLU-5693H	Historic; Site; Old Powerhouse Pipeline Ditch	2014 (Dewey Robbins, Jefferson Resource Co.)	Unevaluated	[redacted]
P-32-006540	Historic; Site; PDH Cabin Site	2021 (Madison Thomson, California Department of Forestry and Fire Protection)	Unevaluated	[redacted]
P-32-006717	Historic; Site; historic refuse scatter	2023 (Daniel Elliott, Elliott CRM)	Unevaluated	[redacted]
P-32-006718	Historic; Site; two shallow adits	2023 (Daniel Elliott, Elliott CRM)	Unevaluated	[redacted]
P-32-006720	Historic; Site; several refuse deposits	2023 (Daniel Elliott, Elliott CRM)	Unevaluated	[redacted]

6Z Found ineligible for NR, CR or Local designation through survey evaluation.

6.0 INDIVIDUALS, GROUP AND AGENCY PARTICIPATION

No individuals, public agencies, historical societies, etc. were contacted about potential resources or concerns by Basin Research Associates due to the information available on the Project from previous research. The Native American Heritage Commission (NAHC) review of the Sacred Lands File (SLF) was positive for sacred sites at the Project and vicinity (M. Carlos to A. Cunningham, Ascent Environmental, January 21, 2025). On June 17, 2025, the Judicial Council sent letters by certified mail to the tribes on the NAHC list inviting them to consult pursuant to Public Resources Code section 21080.3.1. The Mooretown Rancheria of Maidu Indians of California replied that they were not aware of any cultural resources on the Project site. Follow-

up emails were sent July 2, 2025, and July 9, 2025. No request for consultation was received from any tribe. A closure letter dated August 13, 2025 was sent certified mail.

7.0 ARCHAEOLOGICAL FIELD REVIEW [Figs. 3-11]

Mr. Christopher Canzonieri (MA, RPA), completed an archaeological field review of the Project site on September 25, 2025 (253, 287, and 293 Lawrence Street, Quincy (APNs 115-031-052, 115-031-054, and 115-031-055)).[11] The majority of the Project site, with the exception of the side along Lawrence Street, is enclosed by a chain-link fence. The Project site is currently occupied by three commercial structures (two buildings and one overhead canopy structure). These include the Feather Publishing Co., Inc. (287 Lawrence Street, constructed 1993-1998) [Figs. 3, 5, 8]; a storage facility for boats and recreational trailers (253 Lawrence Street, constructed 1981) [Figs. 3, 6-7]; and, the Quincy Paint Center and The2Mic (amplification supplies for guitars) (293 Lawrence Street) [Figs. 3-4], the latter of which was previously occupied by Quincy Lumber & Supply.[12] Asphalt pavement, including parking areas and drive aisles, surround the onsite structures and cover a large portion of the Project site. The north and northwest portions of the site contain unpaved gravel surfaces. There is an unnamed channelized drainage (creek) originating from Boyle Ravine to the south forming the eastern boundary of the Project site.

Field transects were oriented north-south and spaced 1-2 meters apart in open areas. Visibility was fair, with 50% of the surface observable in the areas where hardscape was not present.

Observed sediment consisted of yellowish brown sandy loam with gravels in the northwest and north end of the Project site without hardscape. No native soils, precontact or post-contact historic archaeological material or culturally modified sediments were observed.

8.0 FINDINGS

The research and field inventory completed for the ARAR was undertaken with the objective of identifying both prehistoric and historic archaeological resources to meet the legal requirements of the California Environmental Quality Act (CEQA) (Public Resources Code 21000 et seq.) of 1970, as amended, and Judicial Council planning requirements.

> The records search was negative for recorded archaeological sites, built environment resources, or reported resources within the Project site. Two buildings and 14 post-contact historic era resources have been recorded within 1.0 mile of the Project site.
>
> No known Native American ethnographic villages appear to have been located within or adjacent to the Project site.
>
> No known Hispanic Period expeditions, adobe dwellings, or other structures, features, etc. have been identified in or adjacent to the Project site.

11. Landowners Cobie Brown (Feather Publishing Co.) and William (Bill) Siebold (owner 253 and 293 Lawrence Street) were present.

12. The building may have been constructed by Diamond Match/Lumber circa 1937. The County Assessor's property record indicates a date of 1938.

No known American Period archaeological sites have been recorded or reported within the Project site.

The archaeological field review of the Project site was negative. No surface indicators of potential archaeological material or culturally modified sediments was observed.

No unique archaeological resource(s), historic properties listed, determined eligible or potentially eligible for inclusion on the NRHP and/or the CRHR have been identified within or adjacent to the Project site.

No State of California landmarks or points of interest or local archaeological, historical, and/or architectural resources have been identified within or immediately adjacent to the Project site.

A low potential for the discovery of subsurface prehistoric and/or historic archaeological materials within the Project site is suggested due to the lack of development prior to 1935; no previous discoveries related to building development and the installation of infrastructure (water, sewage, communications, etc.) over the past 80-90 years; and, lack of reported and/or recorded pre-contact and historic archaeological sites within or adjacent to the Project site. In addition, no pre-contact or historic resources have been reported during ongoing development and infrastructure maintenance of the area over the past 50+ years. It is possible that isolated pre-contact and historic finds may be present within the Project site and may be exposed during demolition and future construction although the available information strongly indicates a low potential for the discovery of significant buried archaeological materials.

9.0 IMPACTS AND MITIGATION MEASURES

9.1 DEFINITION AND USE OF SIGNIFICANCE CRITERIA

This section analyzes the impacts related to archaeological resources that could result from future use or development within the Project site. Programmatic mitigation measures are recommended pertinent to the archaeological sensitivity.

The following criteria have been established for determining the significance of potential impacts on historic resources and archaeological (cultural) resources, based on the CEQA Guidelines environmental checklist. Implementation of the Project would have a significant impact on cultural resources if it would:

- Cause substantial adverse change in the significance of a historical resource as defined in CEQA Guidelines Section 15064.5(b) (see also Section 15064.5(c)(1) in regard to archaeological cultural resources). Substantial adverse changes include physical demolition, destruction, relocation, or alteration of the resource or its immediate surroundings such that the significance of the historical resource would be materially impaired;
- Affect a unique archaeological resource as defined in CEQA Guidelines 21083.2(g); and,
- Disturb any human remains, including those interred outside of formal cemeteries.

9.2 GENERAL IMPACTS

As a general principle, ground-disturbing construction activities have the potential to impact archaeological resources in the Project area by disturbing both surface and subsurface soils. The results from each search and site investigation were negative for historical or archeological resources. Thus, there is no substantial evidence that the Project may have a significant impact on historical or archaeological resources. A general inference may be made that ground disturbance anywhere could produce a unique archaeological discovery, however unlikely. Project impacts on buried and unknown archaeological resources could be significant.

9.3 POTENTIAL IMPACTS AND MITIGATION MEASURES

Impact CUL-1 Ground-disturbing activities associated with building demolition and future development within the Project site could directly or indirectly damage buried and unknown unique archaeological resources pursuant to CEQA Guidelines §15064.5 and 21083.2.

Significance: Less Than Significant with Mitigation

Analysis - Archival research has determined that no significant historical resources or unique archaeological sites have been recorded within the Project site. Construction of a single building occurred in the mid-1930s with additional buildings added in 1981 and 1993-1998 along with other improvements. A field review identified no indications of surface or subsurface cultural resources. As yet unknown subsurface archaeological resources could potentially be present and have important research values; and therefore, could be potential unique archaeological resources under CEQA (Guidelines 21083.2).

While the presence of subsurface archaeological resources within the Project site cannot be discounted, the analysis of the available archival data indicates a low archaeological sensitivity for the Project site due to: (1) the Project site's location outside of the historic core of Quincy and the lack of historic development until the mid-1930s with two other buildings following in the early 1980s and 1990; (2) the installation of related infrastructure (water, sewage, communications, etc.) over the past 80+ years; and, (3) lack of reported and/or recorded prehistoric and historic archaeological sites within or adjacent to the Project site. In addition, no discoveries of pre-contact or post-contact historic resources have been reported during ongoing development and infrastructure maintenance of the immediate area over the past 50+ years.

MM CUL 1 Should any pre-contact or post-contact historic cultural materials[13] be

13. Significant prehistoric cultural materials may include:
    a. Human bone - either isolated or intact burials.
    b. Habitation (occupation or ceremonial structures as interpreted from rock rings/features, distinct ground depressions, differences in compaction (e.g., house floors).
    c. Artifacts including chipped stone objects such as projectile points and bifaces; groundstone artifacts such as manos, metates, mortars, pestles, grinding stones, pitted hammerstones; and, shell and bone artifacts including ornaments and beads.
    d. Various features and samples including hearths (fire-cracked rock; baked and vitrified clay), artifact caches, faunal and shellfish remains (which permit dietary reconstruction), distinctive changes in soil stratigraphy indicative of prehistoric activities.

exposed during ground disturbing activities, all such activities shall stop within a 50-foot radius of the discovery, and a qualified archaeologist shall be retained to determine whether the find is a unique archaeological resource. The archaeologist shall perform data recovery on any unique archaeological resource, unless the archaeologist recommends and the Judicial Council determines that other methods of mitigation are more culturally appropriate under the circumstances of the discovery.

***Level of Significance After Mitigation*:** Mitigation Measure CUL-1 would reduce impacts to archaeological resources to a less-than-significant level.

Impact CUL-2 *Ground-disturbing activities associated with development within the Project site could disturb human remains, including those interred outside of formal cemeteries.*

Significance: Less Than Significant with Mitigation

Analysis - Archival research has determined that no human remains have been reported within the Project area or within a 1.0 mile radius. Similar to archeological resources there remains the potential for the Project to disturb human remains, however unlikely. Implementation of existing law, described in Mitigation Measure CUL-2 would reduce impacts to human remains to a less-than-significant level.

MM CUL 2 If pre-contact or post-contact historic human remains and associated or unassociated funerary objects are exposed, work within 50 feet of the discovery will be halted and the resource protected in compliance with applicable state law.

The Judicial Council or its designee shall immediately notify the Plumas County Coroner. If the Coroner determines that the human remains are Native American remains, the Coroner shall notify the Native American Heritage Commission (NAHC) to determine the Most Likely Descendant (MLD) (Health & Safety Code 7050.5; PRC 5097.98). Additional statutory requirements apply depending on the nature of the discovery.

---

e. Isolated artifacts

Significant historic cultural materials may include finds from the late 19th through early 20th centuries. Objects and features associated with the Historic Period can include.

f. Structural remains or portions of foundations (bricks, cobbles/boulders, stacked field stone, postholes, etc.).
g. Trash pits, privies, wells and associated artifacts.
h. Isolated artifacts or isolated clusters of manufactured artifacts (e.g., glass bottles, metal cans, manufactured wood items, etc.).
i. Human remains.

In addition, cultural materials including both artifacts and structures that can be attributed to Hispanic, Asian and other ethnic or racial groups are potentially significant. Such features or clusters of artifacts and samples include remains of structures, trash pits, and privies.

***Level of Significance After Mitigation*:** Mitigation Measure CUL-2 would reduce impacts to human remains exposed within the Project site to a less-than-significant level.

9.4 CUMULATIVE IMPACTS AND MITIGATION MEASURES

The potential for subsurface pre-contact and historic archaeological resources within the Project site cannot be completely discounted as the area has been occupied for at least 11,000 years.

However, as described above there are no known or anticipated archaeological deposits on the Project site. The Project's impacts on any buried and unknown unique archaeological deposits will be mitigated under CUL-1, and impacts on unknown and buried human remains will be mitigated under CUL-2. Since the potential impact of buried and unknown unique archaeological resources, or human remains, is purely speculative, the Project will have no known cumulative impacts.

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Abbreviations

n.d. no date v.d. various dates N.P. no publisher noted
n.p. no place of publisher noted

CHRIS/NEIC is used for material on file at the California Historical Resources Information System, Northeast Information Center, Chico.

ATTACHMENTS

FIGURES

FIGURE 1	General Project Location (ESRI World Street Map)
FIGURE 2	Project Location - T24N R9E Sec 14 (USGS Quincy, CA 1994)
FIGURE 3	Project Site with Photo View Locations
FIGURE 4	293 Lawrence Street, Quincy Lumber building – view to northwest from Lawrence Street
FIGURE 5	287 Lawrence Street, Feather Publishing Company – view to northwest
FIGURE 6	253 Lawrence Street, open-storage garage – view to southwest
FIGURE 7	253 Lawrence Street, enclosed north end of open-storage garage – view to southwest
FIGURE 8	View south from the northeast corner of the Project site
FIGURE 9	View southwest from the northeast corner of the Project site
FIGURE 10	View northeast along the northwest Project boundary
FIGURE 11	View north along the west side of the Project site from north end of the Quincy Lumber building

CHRIS/NWIC SEARCH RESULTS

SEARCH	CHRIS/NEIC File # NE 25-434 dated October 7, 2025 (No Confidential Information)



Figure 1: General Project Location (ESRI World Street Map)

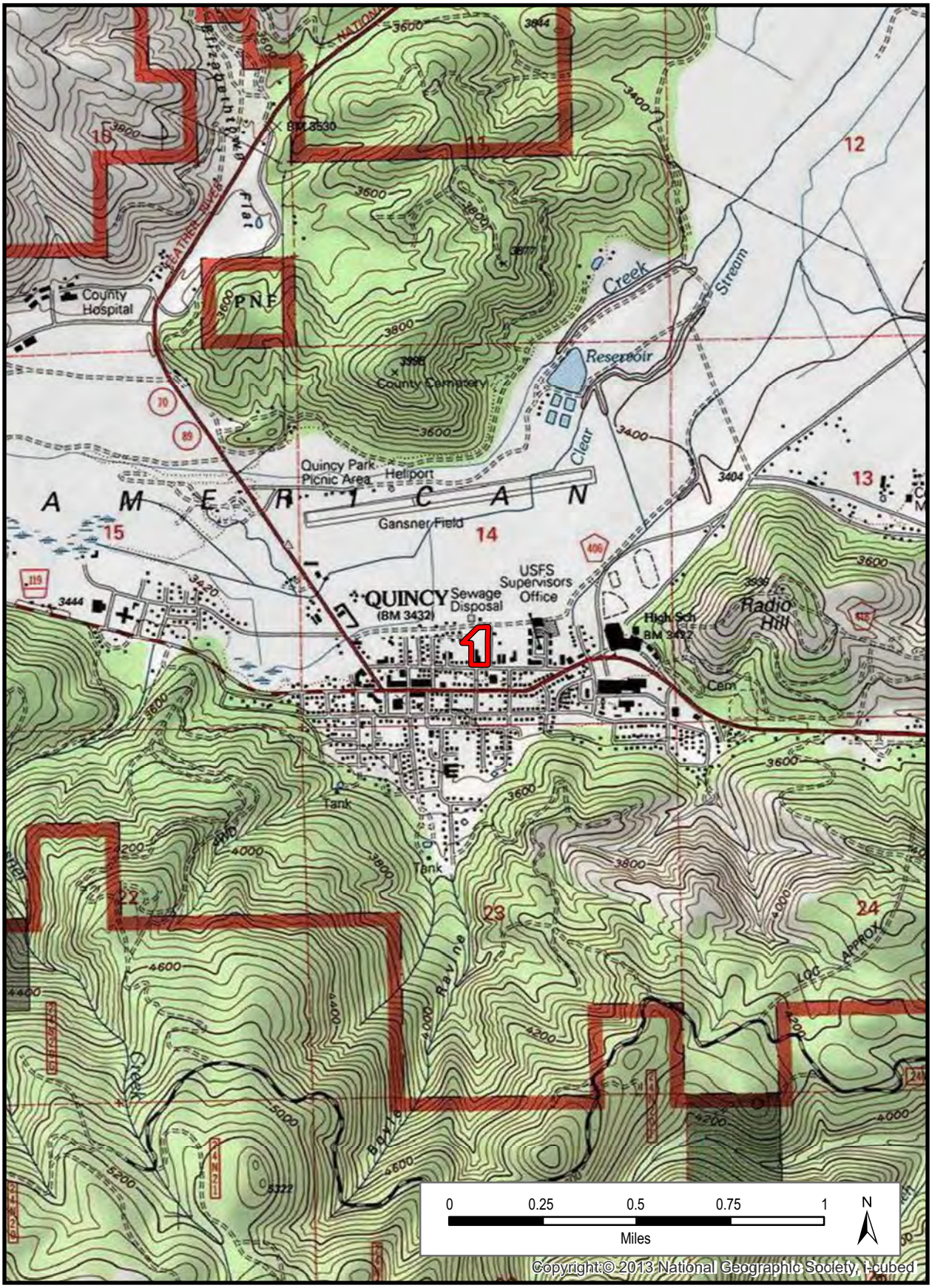


Figure 2: Project Location - T24N R9E Sec 14 (USGS Quincy, CA 1994)



Figure 3: Project Site with Photo View Locations



Figure 4: 293 Lawrence Street, Quincy Lumber building – view to northwest from Lawrence Street



Figure 5: 287 Lawrence Street, Feather Publishing Company – view to northwest



Figure 6: 253 Lawrence Street, open-storage garage – view to southwest



Figure 7: 253 Lawrence Street, enclosed north end of open-storage garage – view to southwest



Figure 8: View south from the northeast corner of the Project site



Figure 9: View southwest from the northeast corner of the Project site



Figure 10: View northeast along the northwest Project site boundary



Figure 11: View north along the west side of the Project site from north end of the Quincy Lumber building

California Historical Resources Information System

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October 7, 2025

Donna M. Garaventa
Basin Research Associates
1933 Davis Street, Suite 214
San Leandro, CA 94577

IC File # NE25-424
Data Request - Standard

RE: Quincy Courthouse
T24N, R09E, Section 14 MDBM
USGS Quincy 7.5' (1975) & Quincy 15' (1951) quadrangle maps
Approximately 2.9 acres (Plumas County)

Donna M. Garaventa:

In response to your request, a records search for the project cited above was conducted by examining the official maps and records for cultural resources and reports in Plumas County. Please note, the search includes the requested 1-mile radius surrounding the project area.

RESULTS:

Resources within project area:	None listed
Resources within 1-mile radius:	P-32-000459, P-32-001442, P-32-001635, P-32-002463, P-32-003808, P-32-003909, P-32-003910, P-32-003911, P-32-003912, P-32-005379, P-32-005623, P-32-005693, P-32-006540, P-32-006717, P-32-006718, P-32-006720
Reports within project area:	None listed
Reports within 1-mile radius:	NEIC-000193, NEIC-000209, NEIC-000212, NEIC-000229, NEIC-001579, NEIC-001967, NEIC-002555, NEIC-004852, NEIC-005033, NEIC-005408, NEIC-006295, NEIC-007595, NEIC-007605, NEIC-007610, NEIC-007611, NEIC-007616, NEIC-007618, NEIC-007622, NEIC-009485, NEIC-009913, NEIC-009914,

	NEIC-010593, NEIC-010972, NEIC-011578, NEIC-013087, NEIC-013367, NEIC-013402, NEIC-014322, NEIC-014575, NEIC-015443

As indicated on your data request form, the locations of resources and reports are provided in the following format: ☒ Custom Maps ☐ GIS Data ☐ N/A

Resource Database Printout (list):	☒ enclosed	☐ not requested	☐ nothing listed
Resource Database Printout (details):	☒ enclosed	☐ not requested	☐ nothing listed
Resource Digital Database Records:	☐ enclosed	☒ not requested	☐ nothing listed
Report Database Printout (list):	☒ enclosed	☐ not requested	☐ nothing listed
Report Database Printout (details):	☒ enclosed	☐ not requested	☐ nothing listed
Report Digital Database Records:	☐ enclosed	☒ not requested	☐ nothing listed
Other Reports: *	☐ enclosed	☒ not requested	☐ nothing listed
Resource Record Copies:	☐ enclosed	☒ not requested	☐ nothing listed
Report Copies:	☐ enclosed	☒ not requested	☐ nothing listed
Built Environment Resources Directory:	☐ enclosed	☐ not requested	☒ nothing listed
Archaeological Determinations of Eligibility:	☒ enclosed	☐ not requested	☐ nothing listed
CA Inventory of Historic Resources (1976):	☐ enclosed	☒ not requested	☐ nothing listed
Caltrans Bridge Survey:	☐ enclosed	☒ not requested	☐ nothing listed
Ethnographic Information:	☐ enclosed	☒ not requested	☐ nothing listed
Historical Literature:	☐ enclosed	☒ not requested	☐ nothing listed
Historical Maps:	☐ enclosed	☒ not requested	☐ nothing listed
Local Inventories:	☐ enclosed	☒ not requested	☐ nothing listed
GLO and/or Rancho Plat Maps:	☐ enclosed	☒ not requested	☐ nothing listed
Shipwreck Inventory:	☐ enclosed	☒ not requested	☐ nothing listed

Notes: *These are classified as studies that are missing maps or do not have a field work component.

Please refer to the NRCS Soil Survey website for current soil survey information:

https://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm

Please forward a copy of any resulting reports from this project to the office as soon as possible. Due to the sensitive nature of archaeological site location data, we ask that you do not include resource location maps and resource location descriptions in your report if it is for public distribution.

The provision of California Historical Resources Information System (CHRIS) Data via this records search response does not in any way constitute public disclosure of records otherwise exempt from disclosure under the California Public Records Act or any other law, including, but not limited to, records related to archaeological site information maintained by or on behalf of, or in the possession of, the State of California, Department of Parks and Recreation, State Historic

Preservation Officer, Office of Historic Preservation (OHP), or the State Historical Resources Commission.

Not all known cultural resources have been recorded and submitted to the OHP, so this record search should not be considered an exhaustive list of all cultural resources present in your project area. DPR forms and reports that are used for recording and evaluating sites and individual resources are submitted to the Northeast Information Center by private and public agencies. Please note that the Northeast Information Center is not responsible for misinformation of coordinates presented on the submitted DPR forms. If a discrepancy is found, please contact the lead agency for more information.

Due to processing delays and other factors, it is possible that not all reports and resource records that have been submitted to the OHP are available via this records search. Additional information may be available through the federal, state, and local agencies that produced or paid for cultural resource management work in the search area. Additionally, Native American tribes have cultural resource information not in the CHRIS Inventory, and you should contact the California Native American Heritage Commission for information on local/regional tribal contacts.

An invoice will follow from Chico State Enterprises for billing purposes. Thank you for your concern in preserving California's cultural heritage, and please feel free to contact us if you have any questions or need any further information.

Sincerely,



Casey Hegel, M.A.
Senior Research Associate
Northeast Information Center
(530) 898-6256

APPENDIX E

Geotechnical Engineering and Geohazard Study

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GEOTECHNICAL ENGINEERING AND GEOHAZARD STUDY

NEW QUINCY COURTHOUSE

253, 287, and 295 Lawrence Street
Quincy, California 95971

PREPARED FOR:

Judicial Council of California (JCC)
Superior Court of California, County of Plumas
C/O BKF Engineers
980 9th Street, Suite 2300
Sacramento, California 95814

PREPARED BY:

Atlas Technical Consultants LLC
9085 Aero Drive, Suite B
San Diego, CA 92123

December 15, 2025

9085 Aero Drive, Suite B
San Diego, CA 92123
(877) 215-4321 | oneatlas.com

December 15, 2025

Atlas No. 91-65859-PW
Report No. 2

JUDICIAL COUNCIL OF CALIFORNIA (JCC)
SUPERIOR COURT OF CALIFORNIA, COUNTY OF PLUMAS
ATTN: MR. JIM MCCURDY, PE
SENIOR ASSOCIATE PRINCIPAL
C/O BKF ENGINEERS
980 9th STREET, SUITE 2300
SACRAMENTO, CALIFORNIA 95814

Subject: **Geotechnical Engineering and Geohazard Study**
New Quincy Courthouse
253, 287, and 295 Lawrence Street
Quincy, California 95971
APNs 115031052000, 115031054000, and 115031055000

Dear Mr. McCurdy:

This report presents the results of the final geotechnical investigation performed for the proposed new courthouse to be located north of Lawrence Street in central Quincy, California. As part of the feasibility and site selection study for the proposed courthouse, a preliminary geotechnical engineering and geohazard study was performed in 2023. It is our understanding that the proposed single-story courthouse will be 23,100 gross square feet with no below-grade (basement) level. This study was performed in general conformance with the scope of work presented in Exhibit A, Phase II of our contract dated April 28, 2023. In general, this investigation was performed to provide design-level geotechnical conclusions and recommendations regarding the proposed structure at the subject site. Based on the results of our investigation, we consider the planned development feasible from a geotechnical standpoint, provided the recommendations of this report are followed.

We appreciate the opportunity to be of service on this project. Should you have any questions related to this report, please contact the undersigned at your convenience.

Respectfully submitted,
Atlas Technical Consultants LLC

Jalal Fatemi, PE C94820
Senior Engineer

Kyle Hahn, PG 10397
Project Geologist

Erick Aldrich, GE 2565
Principal Engineer

Doug Skinner, CEG 2472
Principal Geologist

KBH:JF:SD:DS:EA:ji
Distribution: Addressee via email at jmccurdy@bkf.com

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EXECUTIVE SUMMARY

This report presents the results of our final geotechnical engineering study for the proposed new Courthouse in Quincy, California. The subject site is located in central Quincy on the north side of Lawrence Street, opposite Church Street. The 2.86-acre site consists of three combined parcels (253, 287 and 295 Lawrence Street), is irregularly shaped and relatively level, descending slightly toward the northern end of the site. The site is bound by Lawrence Street on the south, a residential property on the west, a paved pathway on the north, and a small, open creek channel on the east. The site is currently developed with three significant structures and surrounding asphalt pavement.

We understand the current improvements within the project site would be demolished and removed, and a new single-story courthouse building will be constructed along with a new paved parking lot and a driveway entrance from Lawrence Street. The proposed location of the courthouse building is on the southwest corner of the site with the access driveway east of the building. The paved parking area is currently planned to be located to the rear of the site to the north.

As part of the feasibility and site selection study for the proposed courthouse, a geotechnical investigation was initially performed in 2023 (Atlas, 2023) which included drilling a total of six borings to depths ranging from 10 to 50 feet below the ground surface. For the current study, we performed an additional five borings and four cone penetration test (CPT) soundings with depths ranging from 11.5 to 80.0 feet The subsurface conditions below the site as encountered in our borings consisted of stratified lacustrine deposits consisting of interbedded loose to dense, silty to clayey sands and gravels, and medium stiff to stiff sandy clay. Possible fill materials were identified within the uppermost 3 to 10 feet throughout property. The near-surface clayey soils were found to have a generally low plasticity and low expansion potential. Bedrock was not encountered in our borings within the depth explored. Free groundwater was encountered in the borings at depths ranging from 6 to 16 feet below the existing ground surface.

The main geotechnical consideration affecting the proposed construction is the presence of undocumented fills, compressible deposits in the upper 25 feet, and shallow groundwater. Remedial grading will need to be performed to reduce the potential for distress to the proposed structure and other proposed improvements. Based on the results of our investigation and our understanding that no below-grade levels are proposed for the building, we anticipate that the building can be supported on a mat foundation with bottom levels bearing entirely on compacted fill; or shallow spread footings bearing on improved ground.

This summary omits details that may be contained within the body of this report.

1. INTRODUCTION

This report presents the results of the final geotechnical engineering and geohazard study Atlas performed for the proposed new single-story, 23,100 gross-square-foot building and associated improvements. We understand that Atlas performed an initial study as part of the feasibility and site selection in 2023 (Atlas, 2023). The purpose of our work was to provide update conclusions and recommendations regarding the geotechnical aspects of the subject site. The findings and **recommendations provided in this report supersede findings and recommendations provided in our previous geotechnical report (Atlas, 2023).** Figure 1 shows the approximate location of the site.

2. SCOPE OF WORK

We conducted this investigation in general conformance with the scope of work presented in Exhibit A, Phase II of our contract dated April 28, 2023.

2.1 Subsurface Investigation

2.1.1 Current Investigation

Prior to mobilization, an Atlas representative visited the site to mark the proposed exploratory boring and CPT locations for underground utility clearance. Atlas notified Underground Service Alert (USA), as required by law, prior to the commencement of field activities. Additionally, a private utility locator was used to identify utilities detectable by geophysical methods to clear the proposed exploration locations for potential conflicts.

On September 17, 2025, Atlas further explored the subsurface conditions by drilling five exploratory borings to depths of about 11.5 to 41.5 feet below the existing ground surface (bgs) using a truck-mounted drill rig equipped with a solid-stem auger. An Atlas geologist logged the borings and collected soil samples for examination and geotechnical laboratory testing. Soils were logged and classified according to the Unified Soil Classification System (USCS) as presented on the boring logs provided in Appendix I.

On September 16, 2025, four cone penetration test (CPT) soundings were advanced at the site to a maximum depth of about 80.0 feet below the existing ground surface. CPT subsurface data was collected by pushing an integrated electronic cone system into the soil by means of a truck-mounted hydraulic ram. Measurements of cone bearing resistance, pore water pressure, and sleeve friction were collected at approximately 2.5-centimeter intervals. Shear wave measurements were obtained at 5-foot increments at two of the CPT locations. Dissipation tests were performed at different depths in accordance with ASTM D6067. The CPT sounding was backfilled, and the pavement surface patched to match the existing surrounding area. The logs of the CPT soundings are presented in Appendix II. Figure 2 presents the approximate locations and depths of the borings and CPT soundings.

2.1.2 Previous Investigation

Atlas previously performed a geotechnical investigation in 2023 by drilling six borings to depths ranging from 10 and 50 feet below existing grade using a truck-mounted drill rig equipped with solid-stem augers. One boring was converted to a percolation test to assist the project design engineer with evaluation of the infiltration feasibility and rate. Previous Atlas borings are shown on Figure 2. The boring logs are provided in Appendix I.

The percolation hole was drilled on June 5, 2023, using a drill rig equipped with a 6-inch diameter solid stem auger and terminated at a depth of about 5 feet. Following drilling, the bottom of the hole was filled with at least 2 inches of ¾-inch drain rock to prevent scouring of the native materials when water was added. The hole was then filled with water before the test was conducted on June 9, 2023. The percolation test was conducted by refilling the hole with water up to 5 feet and measuring the water level drop at 15-minute time intervals, and after each interval the hole was refilled, and the test was repeated until the water level drop stabilized over at least two successive readings. The estimated vertical infiltration rate of the soil was calculated from the field percolation rate adjusted with the correction formula according to the Porchet Method, which accounts for percolation occurring out the side of the hole. Following the performance of the test, the hole was backfilled with auger soil cuttings. The result of the field percolation test is presented in Table 1.

Table 1: Percolation Test Result

Location	Depth (feet)	Corrected Infiltration Rate (in/hr)
B-2	5	1.78

2.2 Laboratory Testing

Selected samples obtained from the borings were tested to evaluate pertinent soil classification and engineering properties and enable development of geotechnical conclusions and recommendations. The laboratory tests consisted of in situ moisture and density, grain size distribution, percent finer than no. 200 sieve, Atterberg limits, maximum density, R-value, corrosivity, expansion index, consolidation, unconsolidated-undrained (UU) triaxial, and consolidated-undrained (CU) triaxial tests. The results of the laboratory tests and brief explanations of the test procedures are presented in Appendix III. Results of the laboratory tests permed as part of the Phase I study are also provided in this Appendix.

2.3 Environmental Analytical Testing

A total of three composite soil samples were collected and transported, under appropriate chain-of-custody protocols, to Enthalpy Analytical, a State of California accredited laboratory, for environmental testing and analysis at the request of our client. Environmental laboratory tests included:

- CA Title 22 Metals by EPA Method 6010/7471

- Total Petroleum Hydrocarbons (TPHs) by EPA Method 8015M, and
- Asbestos by PLM EPA Method 600/R-93/116.

The results of the environmental testing are provided in Appendix VI. The interpretation of the test results will be performed by others.

2.4 Analysis and Report

The results of the field and laboratory tests were evaluated to develop conclusions and recommendations regarding:

- Subsurface conditions beneath the site, including groundwater levels, if encountered,
- Potential geologic hazards
- Criteria for seismic design in accordance with the 2025 California Building Code (CBC),
- Site preparation, grading, and drainage,
- Temporary excavations and shoring,
- Excavation characteristics,
- Allowable bearing capacity,
- Appropriate alternatives for foundation support along with geotechnical engineering criteria for design of the foundations,
- Resistance to lateral loads,
- Estimated foundation settlements,
- Support for concrete slabs-on-grade,
- Suitability of excavated materials for use as bedding and backfill,
- Pavement recommendations, and
- Soil corrosivity.

3. SITE DESCRIPTION

The subject site is located north of Lawrence Street in Quincy, California. The irregularly-shape, 2.86-acre site consists of three parcels with physical addresses 253, 287, and 295 Lawrence Street. The site is bound by Lawrence Street to the south, residential property to the west, a creek channel to the east, and a paved pathway to the north.

The site descends gently toward the north, with elevations ranging from approximately 3420 to 3412 feet (NAVD88 datum) between the south and north property boundaries, respectively, based on the preliminary topographic survey (BKF Engineers, 2023).

The site is occupied by three commercial and industrial structures and surrounding asphalt concrete (AC). The northern parcel contains an industrial building, Feather River Publishing Company, the southwestern parcel contains a retail building occupied by Quincy Lumber Supply, and the southeastern parcel is occupied by an overhead canopy structure used for storage. The creek channel is approximately 2 to 4 feet below property elevation, drains toward the north, and accommodates upstream flows passing through a buried culvert below Lawrence Street.

4. PROPOSED DEVELOPMENT

We understand the current structures and improvements within the project site will be demolished and a new single-story courthouse building will be constructed. The proposed location of the building is shown in Figure 2. Pavement, flatwork, and new utilities are also anticipated. Design details such as foundation structural loads and final grade elevations were not available at the time of preparing this report. We anticipate that the new building pad grade will be similar to that of the existing buildings; therefore, cuts and fills outside the building pad should be relatively minor (less than 2 feet) as required to establish new positive site drainage.

5. GEOLOGY AND SUBSURFACE CONDITIONS

The project site is located near the northern end of the Sierra Nevada geomorphic province of California, just south of the Cascade Range Province, and near the boundary with the Basin and Range Province to the northeast. According to CGS, the Sierra Nevada (Sierra) is a tilted fault block nearly 400 miles long. Its east face is an eroded high, rugged group of multiple scarps created by thrust faulting, contrasting with the gently sloping western slope that disappears under sediments of the Great Valley. Deep river canyons are cut into the western slope of the Sierra. The upper courses of these canyons, especially in the massive granites of the higher Sierra, are modified by glacial sculpturing, forming such scenic features as Yosemite Valley. The high crest of the Sierra culminates in Mt. Whitney near the southern end of the range. The northern Sierra boundary is marked where bedrock disappears under the Cenozoic volcanic cover of the Cascade Range near Mount Lassen. The southern boundary of the Sierra is near the Tehachapi Mountains of the Transverse Ranges geomorphic province.

The Sierra Nevada range is primarily composed of Cretaceous-period granitic rock, older remnants of Paleozoic and Mesozoic metavolcanics and metasedimentary rocks intruded by the younger granitic rock, and Cenozoic volcanic and sedimentary rocks. The eastern portion of Plumas County is dominated by the Diamond Mountains, which were formed by a series of tilted fault blocks, which formed a series of parallel elongated valleys between low elevation ridges. Many of the lower valley features contained lakes that existed until recent geologic time and have formed a vast alluvial system of meadows forming the headwaters of the Feather River.

The project site is situated within central Quincy within the flood plain area of Spanish Creek, a headwaters tributary of the east branch of the north fork of the Feather River located to the northwest of Quincy. The site is immediately underlain by fill and local recent alluvium deposits along the southern edge of American Valley, which is mapped on the very small scale (1:250,000) CGS Geologic Map of the Chico Quadrangle (Saucedo and Wagner, 1992) as Holocene-epoch Lake Deposits associated with the lower valleys. Descriptions of the materials are presented below. Figure 3 illustrates the regional geology of the project site. Figure 4 presents a geologic cross-section extending through the site.

- **Fill (Af)**: Undocumented fill was encountered in Borings B-1, B-2, B-4, B-7, B-8, B-9, and B-11 from the existing ground surface to a depth of about 3 to 7 feet. As encountered, the

fill consists of yellowish brown to brown to reddish brown to dark gray, dry to moist, fine to coarse grained, clayey sand with gravel, silty sand with gravel, and silty gravel with sand.

- **Lake Deposits (Ql)**: Lake deposits were encountered beneath fill to the maximum explored depth of 50 feet below the existing grade. As encountered, the lacustrine deposits consists of soft to very stiff, dark gray to yellowish brown, moist to wet sandy lean clay with gravel and sandy lean clay, and loose to very dense, yellowish brown, moist to wet, clayey gravel with sand, clayey sand with gravel, poorly graded gravel with sand and clay, poorly graded sand with gravel, and sandy silt with gravel.
- **Groundwater**: Groundwater was encountered in Borings B-1 through B-8 and all CPTs between a depth of 6 to 17 feet below existing grade. Groundwater levels may fluctuate in the future due to rainfall, irrigation, broken pipes, or changes in site drainage. Because groundwater rise or seepage is difficult to predict, such conditions are typically mitigated if and when they occur. Table 2 provides a summary of the groundwater data obtained during the subsurface exploration.

Table 2: Groundwater Summary Data

Exploration Identification	Groundwater Depth (ft)	Groundwater Elevation (ft)	Date Measured
B-1	6.0	3407.0	6/5/2023
B-2	6.0	3408.0	6/5/2023
B-3	7.0	3408.0	6/5/2023
B-4	7.0	3409.0	6/6/2023
B-5	12.5	3406.5	6/5/2023
B-6	12.0	3406.0	6/6/2023
B-7	10.0	3406.0	9/17/2025
B-8	16.0	3402.0	9/17/2025
B-9	Not Encountered	-	-
B-10	Not Encountered	-	-
B-11	Not Encountered	-	-
CPT-01	12.5	3403.5	9/16/2025
CPT-02	15.0	3404.0	9/16/2025
CPT-03	10.3	3405.7	9/16/2025
CPT-04	12.5	3402.5	9/16/2025

6. GEOLOGIC HAZARDS

A discussion of geologic hazards, which may impact the proposed project, is presented below.

6.1 Faulting and Surface Rupture

The subject site is situated in an area of low to moderate seismic activity but is susceptible to infrequent, major earthquakes in the greater area. According to CGS publications, the site does not lie near any identified Alquist-Priolo Fault Zone (Hart and Bryant, 1997). Also, according to published mapping by CGS, no known active or potentially active fault traces cross the site, and no evidence of surface ground rupture was noted during our site reconnaissance. The probability of fault rupture is considered low.

The closest mapped active faults within an Alquist-Priolo Fault Zone are associated with the Honey Lake Fault, located approximately 34 miles northeast of the project site, and the Fort Sage Fault, located approximately 46 miles east northeast of the project site. In addition, the active Cleveland Hills Fault is located approximately 41 miles southwest of the site at its closest point. Local faults, which are all considered to be inactive or potentially active, are shown on Figure 5, California Fault Activity Map and include the Indian Valley Fault and the Mohawk Valley Fault, located approximately 10.3 miles northeast and east of the site, respectively.

The approximately 60-mile-long Honey Lake Fault zone consists of en echelon, northwest trending faults that form the boundary of the Sierra Nevada and Great Basin geomorphic provinces in northeastern California and is at the northern end of the Sierra Nevada Fault system along the eastern boundary of the range and is also part of the Walker Lane of Nevada. The Sierra Nevada Fault system itself extends south to the Death Valley area and has produced historic earthquakes as large as M 7.8 (e.g., Owens Valley Earthquake of 1872).

The Honey Lake and related faults in the western margin of the Basin and Range exhibit vertical as well as right lateral motion that also accommodates some of the right-lateral motion between the Pacific and North American plates in addition to the San Andreas Fault system to the southwest. In the Honey Lake Valley, the fault forms an over 30-mile-long zone of landforms typical of active strike slip faults. Based on right-lateral offset of an incised stream channel in the area, the Holocene slip rate of the Honey Lake Fault is estimated to be between 1.1 and 2.6 mm/year (Wills and Borchardt, 1993). An M 6.2 earthquake occurred in the Honey Lake area on January 24, 1875. More recently, the M 5.6 Fort Sage Mountain Earthquake occurred on December 14, 1950, along the Fort Sage Fault, a related normal fault spanning

6.2 Ground Shaking

The site will likely experience low to moderate ground shaking from earthquakes originating from a nearby fault such as the Mohawk Valley Fault. Earthquake intensities could vary depending upon the magnitude of the earthquake, the distance of the site from the causative fault, the type of materials underlying the site and other factors. The following section provides a site-specific ground motion hazard analysis of the site.

6.2.1 Site-Specific Ground Motion Hazard Analysis

The proposed structures on the project site should be designed to resist the seismic forces generated by earthquake ground motions in accordance with 2025 California Building Code (CBC, 2025) and ASCE 7-22. As part of the scope of this project, Atlas was tasked to perform a site-specific ground motion hazard analysis based on the provisions of Chapters 11 and 21 of ASCE 7-22.

The shear wave velocity of the site in the upper 100 feet (Vs30) was estimated to be 1100 ft/s (335 m/s) which classifies the site as Site Class CD. This estimate is based on the tabulation of the shear wave velocity measurements obtained from SCPT soundings. Since the shear wave velocity measurements did not reach 100 feet due to the SCPT refusal, Vs30 was estimated using Boore (2004). The site location was identified using the following coordinates:

- Latitude = 39.938239°
- Longitude = -120.943783°

The site-specific ground motion study for this project consisted of performing probabilistic and deterministic risk-targeted Maximum Considered Earthquake (MCE_R) and calculating site-specific MCE_R and design response spectra per guidelines of Chapter 21 of ASCE 7-22. As part of the site-specific analysis, ground motions were evaluated in conjunction with both a Probabilistic Seismic Hazard Analysis (PSHA) and a Deterministic Seismic Hazard Analysis (DSHA) to characterize earthquake ground shaking that may occur at the site during future seismic events.

The PSHA is based on an assessment of the recurrence of earthquakes on potential seismic sources in the region and on ground motion prediction models of different seismic sources in the region. The United States Geological Survey (USGS) Earthquake Hazard Toolbox-Dynamic Hazard Curves (USGS, 2025) was used to develop the uniform hazard ground motion (UHGM) and the risk targeted ground motion (RTGM) to analyze ground motions for corresponding periods. Maximum direction scale factors, based on Section 21.2 of ASCE 7-22, were applied to the resulting spectral acceleration to increase the motions to the maximum response.

The DSHA is represented by the 84th percentile of the spectral accelerations at different periods. The spectral accelerations were calculated using USGS Earthquake Hazard Toolbox-Response Spectra (USGS, 2025). Ground motion models Abrahamson, Silva, and Kamai (2014), Boore, Stewart, Seyhan, and Atkinson (2014), Campbell and Bozorgnia (2014), and Chiou and Young (2014) with equal weights were considered. The active fault system that contributes to the seismic hazard at the site is the Mohawk Valley Fault based on the disaggregation of the hazard at PGA and 1.0 second periods. The hazard disaggregation is provided in Appendix IV. The fault's characteristic parameters were obtained from the USGS Uniform California Earthquake Rupture Forecast, Version 3 (UCERF3) model, and USGS Earthquake Scenario Map (BSSC 2014), and are presented in Table 3.

The site-specific, risk-targeted MCE_R was taken as the lesser of the spectral response accelerations from the PSHA and DSHA. The design response spectrum and design acceleration parameters were calculated in accordance with the procedures of ASCE 7-22. The mapped and site-specific spectral acceleration parameters are presented in Table 3. Figure 3 in Appendix IV provides the site-specific MCE_R and design spectra with the mapped two-period and multi-period MCE_R and design spectra. Table 4 presents the mapped and site-specific seismic parameters. Details of the site-specific ground motion hazard analysis along with tabulated values and graphical plots are included in Appendix IV.

Table 3: DSHA Input Parameters

Mohawk Valley Fault	
M_W	7.13
Mechanism	Strike-slip
Rake (°)	180
Z_{TOR} (km)	1.47
Dip (°)	90
Width (km)	13.2
R_X (km)	16.3
R_{RUP} (km)	16.6
R_{JB} (km)	16.6

Table 4: 2025 CBC / ASCE 7-22 Site-Specific Seismic Parameters

Site Coefficients and Spectral Acceleration Parameters	Values	
Latitude, Longitude	39.938239°, -120.943783°	
Site Class	CD	
Mapped Spectral Response Acceleration at Short Period, S_S	1.43	
Mapped Spectral Response Acceleration at 1-Second Period, S_1	0.38	
	Mapped	Site-Specific
Design Spectral Acceleration at Short Period, S_{DS}	1.06	1.070
Design Spectral Acceleration at 1-Second Period, S_{D1}	0.51	0.538
MCE_R Design Spectral Acceleration at Short Period, S_{MS}	1.59	1.606
MCE_R Spectral Acceleration at 1-Second Period, S_{M1}	0.76	0.807
Peak Ground Acceleration, PGA_m	0.56	0.560

6.3 Liquefaction and Dynamic Settlement

Research and historical data indicate that soil liquefaction generally occurs in saturated, loose granular soil (primarily fine to medium-grained, clean sand deposits) during or after strong seismic ground shaking and is typified by a loss of shear strength in the affected soil layer, thereby causing

the soil to flow as a liquid. However, because of the higher inter-granular pressure of the soil at greater depths, the potential for liquefaction is generally limited to the upper 50 feet of the soil. Potential hazards associated with soil liquefaction below or near a structure include loss of foundation support, lateral spreading, sand boils, and areal and differential settlement. Dry sand settlement is a phenomenon where loose, relatively clean sandy soil located above the water table densified from vibratory loading, typically from seismic shaking or vibratory equipment.

Atlas performed a liquefaction hazard analysis using data obtained from the CPT soundings. To analyze liquefaction settlement, we utilized the CLiq v 2.3.1.15 software, developed by Geologismiki. Calculation of soil resistance against liquefaction is performed according to the Robertson (Youd et al., 2001) procedure and as recommended on CGS Special Publication 117A (CGS, 2008). The procedure used in the software slightly differs from the one originally published in NCEER-97-0022 (Youd and Idriss, 1997).

The CPT soundings identified some lacustrine layers as susceptible to potential seismic settlement through liquefaction or dry sand settlement. For analysis purposes, ASCE 7-22 specifies the use of Geometric Mean Peak Ground Acceleration, PGA_M, for use in liquefaction analysis. A PGA_M value of 0.56g, based on the results of site-specific ground motion hazard analysis, was used in our calculation. We also used a Modal Moment Magnitude of 5.5 based on the hazard disaggregation of PGA for a return period of 2,475 years (probability of exceedance of 2 percent in 50 years) using the USGS Earthquake Hazard Toolbox (USGS, 2025). Per SP117A guidelines, we also assumed a Factor of Safety (FS) of 1.3 below which liquefaction settlement occurs. For this analysis, groundwater during the earthquake event was assumed to be at 10 feet below the ground surface. Liquefaction results based on the CPT soundings indicated less than one inch of liquefaction-induced settlement and less than a quarter of an inch of dry settlement. Table 5 summarizes the results of the liquefaction analysis.

Based on the overall subsurface conditions such as the encountered soil types and their densities, groundwater level at the site, and the magnitude of a potential seismic event, our liquefaction analysis indicates that there is potential for occurrence of liquefaction within some relatively loose discontinuous layers at the site; however, the potential for extensive liquefaction that could adversely affect the structures at the site is considered low. Liquefaction analysis results are presented in Appendix V.

Table 5: Seismic Settlement Analysis Results

CPT No.	Calculated Liquefaction Settlement (inches)	Calculated Dry Sand Settlement (inches)	Calculated Total Seismic Settlement (inches)
CPT-01	0.4	0.1	0.5
CPT-02	0.75	0	0.75
CPT-03	0.4	0	0.4
CPT-04	0.6	0	0.6

6.4 Lateral Spreading

Lateral spreading involves both vertical and lateral ground movement, with some vertical component, occurring as a result of liquefaction. In addition to liquefaction, a free face or slope is necessary in most cases for lateral spreading to occur. Lateral spreading can occur on relatively flat sites with slopes less than 2 percent under certain circumstances and manifest itself at the ground surface in the form of cracking and settlement. Lateral spreading can occur in areas located within close proximity to an open face which are supported by underlying liquefiable soil under or close to the open face. Under a lateral spreading condition, soils which liquefy lose strength and the slope moves towards the open face. Any structures or improvements located within close proximity to the slope can also move and possibly be destabilized.

The project site is not in the vicinity of a slope or a free face that can cause lateral spreading in a liquefaction event. Additionally, the potential for the liquefaction of an extensive soil layer at the site is low. Therefore, it is our opinion that the potential for lateral spreading at the site is low.

6.5 Landslides and Slope Stability

Evidence of landslides or slope instability was not observed during our investigation and site topography is generally flat. Therefore, the potential for landslides and slope instability to occur is considered low.

6.6 Tsunamis, Seiches, and Flooding

The site is not located within a mapped area on the State of California Tsunami Inundation Maps based on the California Governor's Office of Emergency Services (Cal OES) (CGS, 2022); therefore, damage due to tsunamis is considered negligible. Seiches are periodic oscillations in large bodies of water such as lakes, harbors, bays, or reservoirs. The site is not located adjacent to any confined bodies of water; therefore, the potential for a seiche to affect the site is low.

The site is not located within areas mapped as susceptible to dam inundation (CDWR, 2025); therefore, damage due to dam inundation is considered negligible.

According to a published Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for Plumas County that covers the site, as shown on Figure 6, the southwestern portion of the project site, including the Quincy Lumber parcel, is mapped as within an area with a 0.2% annual chance flood hazard and area of 1% annual chance flood with average depth of less than 1 foot (Zone X). The portion of the site containing the overhead structure as well as the Feather River Publishing building, are within a mapped area of minimal flood hazard except for the northernmost edge of the site, which is mapped as within a special flood hazard area subject to inundation by the 1% annual chance flood hazard (Zone AE) (FEMA, 2005). The flood hazard of the site should be confirmed by the project Civil Engineer, and a flood specialist should be contacted if a more in-depth flooding analysis is desired.

6.7 Subsidence

The project is not located in an area of known subsidence associated with fluid withdrawal such as groundwater or petroleum (USGS, 2025). The potential for subsidence is considered low at the site.

6.8 Hydro-Consolidation

Hydro-consolidation can occur in recently deposited sediments (less than 10,000 years old) that were deposited in a semi-arid environment. Examples of such sediments are eolian sands, axial-channel deposits, and mudflow sediments deposited during flash floods. The pore spaces between the particle grains can re-adjust when inundated by groundwater, causing the material to consolidate. Considering the existing lake deposits and the shallow groundwater at the site, the potential for the proposed development to be affected by hydro-consolidation is low.

6.9 Other Geologic Hazards

Due to the site's location and geology, subsurface soil conditions, groundwater levels and land use factors, based on readily available maps, the site is not subject to the potential geologic hazards of Radon-222 gas, naturally occurring asbestos (NOA), and volcanism.

7. CONCLUSIONS

The main geotechnical consideration affecting the proposed construction is the presence of undocumented fills, compressible deposits in the upper 25 feet, and shallow groundwater. Remedial grading will need to be performed to reduce the potential for distress to the proposed structure and other proposed improvements. Remedial grading recommendations are provided in the following sections of this report. Based on the results of our investigation and our understanding that no below-grade levels are proposed for the building, we anticipate that the building can be supported on a mat foundation with bottom levels bearing entirely on compacted fill; or shallow spread footings bearing on improved ground. If below-grade (basement) levels are considered, Atlas will need to be contacted to provide recommendations regarding groundwater consideration during construction and alternative foundation systems.

The recommendations presented herein may need to be updated once final plans are developed.

8. RECOMMENDATIONS

8.1 Site Preparation and Grading

8.1.1 General Grading, Preparation and Drainage

If needed, site grading should be performed in accordance with these recommendations. A pre-construction meeting should be held at the jobsite with representatives from the owner, general contractor, grading contractor, and Atlas prior to starting the clearing operations at the site. Site grading is expected to consist of excavations and backfills to construct the new building pad; finish grading to establish site grades and positive drainage away from the building, utility trench

excavation and backfills, preparation of supporting subgrades for parking areas, sidewalks and flatwork, including aggregate base (base rock) sections for pavement and/or flatwork.

8.1.2 Site Preparation

The site should be cleared of the existing structures, concrete flatwork, undocumented loose or soft fill, and other deleterious materials within the proposed development area. The grading contractor should be aware of buried objects and underground utilities at the site which are to be removed or abandoned appropriately. Holes resulting from the removal of possible underground obstructions or root balls from trees that would extend below the proposed finish grade should be cleaned down to firm soil as approved by our office and backfilled with properly compacted engineered fill or other material approved by Atlas. If loose or soft soil or unsuitable fill soil is encountered, these soils should be removed to expose firm soil and backfilled with engineered fill. Removed fill soil may be evaluated by Atlas for possible reuse and placement as engineered fill. Our representative should observe and confirm the adequacy of site clearing operations during construction prior to engineered fill placement and observe and confirm backfilling operations for excavations to remove deleterious material.

Grading and backfill should be performed in accordance with the grading sections of this report. Our representative should observe and approve the adequacy of site clearing operations during construction, prior to placement of engineered fill.

8.1.3 Compressible Soils

Beneath the planned structures, settlement sensitive improvements and areas to receive new fill, the existing undocumented fill and upper loose deposits should be removed and replaced as recommended in the following sections.

Horizontally, the excavations should extend to a distance equal to the excavation depth for building foundations or at least 5 feet outside the planned perimeter foundations, whichever is greater. Excavations for planned hardscape and pavements should extend at least 2 feet outside the foundation or improvement, or up to existing improvements, whichever is less. If a lesser horizontal extent is over-excavated due to property line interference, the over-excavation should be backfilled with slurry from the bottom of the over-excavation to the bottom of the footing. An Atlas representative should observe conditions exposed in the bottom of excavations to determine if additional removals are required.

8.1.4 Compacted Fill

We anticipate that the on-site granular soils (sand and gravel) are suitable to be used as compacted fill. However, additional testing should be performed during the construction to confirm the suitability of the soils before using them as compacted fill.

An Atlas representative should observe the conditions exposed in the bottom of excavations to determine if additional excavation is required. The surface exposed at the bottom of excavations should be scarified to a depth of 8 inches, moisture conditioned to near optimum moisture content

and compacted to at least 90% relative compaction. Compacted fill should be moisture conditioned to near optimum moisture content and compacted to at least 90% relative compaction. Compacted fill should be thoroughly mixed and placed in horizontal lifts at a thickness appropriate for the equipment spreading, mixing, and compacting the material, but generally should not exceed 8 inches in loose thickness. The maximum dry density and optimum moisture content for evaluating relative compaction should be determined in accordance with ASTM D1557. Utility trench backfill beneath structures, pavements, and hardscape should be compacted to at least 90% relative compaction. The top 12 inches of subgrade beneath pavements should be compacted to at least 95%.

8.1.5 Grading Flatwork Areas

Flatwork or pavement areas should be excavated at least 2 feet below the planned subgrade elevation. The bottom of excavations should be scarified to a depth of 8 inches, moisture-conditioned to near optimum moisture content, and compacted to at least 90 percent relative compaction.

An Atlas representative should observe the conditions exposed in the bottom of excavations to determine if additional excavation is required.

8.1.6 Expansive Soil

Based on our investigation, the expansion potential of the on-site near-surface soils is expected to be very low. However, if localized areas of soils with an expansion index greater than 20 are encountered, these materials should be removed to a minimum depth of 2 feet and replaced with compacted fill materials having an expansion index of 20 or less.

8.1.7 Excavation Characteristics

It is anticipated that excavations can be achieved with conventional earthwork equipment in good working order. The contractor should anticipate caving conditions to be encountered in unconsolidated sandy and gravely portions of the undocumented fill and the lake deposits. Difficult excavation in localized areas with gravel and cobbles may be encountered. Contract documents should specify that the contractor may need to mobilize equipment capable of excavating and compacting materials with gravel and cobbles.

8.1.8 Oversized Material

Excavations may generate oversized material. Oversized material is defined as rocks or cemented clasts greater than 6 inches in largest dimension. Oversized material should be broken down to no greater than 3 inches in largest dimension for use in fill, used as landscape material, or disposed of offsite.

8.1.9 Temporary Excavations

Temporary excavations 4 feet deep or less can be made vertically, if possible. Temporary excavations deeper than 4 feet should not be steeper than 1½:1 (horizontal: vertical), per Cal/OSHA Type C soil classification. The faces of temporary slopes should be inspected daily by the contractor's "competent person" before personnel are allowed to enter the excavation. Zones of potential instability, sloughing, or raveling should be brought to the attention of the engineer and corrective action implemented before personnel begin working in the trench.

Slopes steeper than those described above will require shoring. Additionally, temporary excavations that extend below a plane inclined at 1½:1 (horizontal:vertical) downward from the outside bottom edge of existing structures or improvements will require shoring.

Soldier piles and lagging, corrugated metal pipe, internally braced shoring systems such as trench boxes or speed shoring may be used. If trench boxes or corrugated metal pipes are used, the soil immediately adjacent to the shoring is not directly supported. Ground surface deformations adjacent to the excavation could be greater when these methods are used compared to other methods of shoring leading to distress to overlying improvements.

Excavated soils should not be stockpiled behind temporary excavations within a distance equal to the depth of the excavation. Atlas should be notified if other surcharge loads are anticipated so that lateral load criteria can be developed for the specific situation.

If temporary slopes or open trenches are to be maintained during the rainy season, berms or other measures are recommended along the tops of the slopes and trenches to reduce the potential for runoff water to enter the excavation.

8.1.10 Temporary Shoring

For design of cantilevered shoring, an active soil pressure equal to a fluid weighing 45 pounds per cubic foot (pcf) above groundwater, and 20 pcf plus hydrostatic pressure below the groundwater can be used for level retained ground. The surcharge loads on the shoring from traffic and construction equipment adjacent to the excavation should also be considered by assuming an additional 2 feet of soil behind the shoring. The additional surcharge from adjacent structures within a distance equal to the retained height of the shoring system will also need to be accounted for. Deflection of the shoring system should be limited such that it will not adversely affect the adjacent structures, improvements and/or utilities.

For the design of soldier piles, use a passive earth pressure of 350 pounds per square foot (psf) per foot of embedment above groundwater and 200 psf per foot of embedment below the groundwater. Passive pressure should be applied over twice the pile diameter up to a maximum of 4,200 psf (2,400 psf below groundwater) can be used. The values above are for level backfill and do not include a factor of safety. Appropriate factors of safety should be incorporated into the design. Soldier piles should be spaced at least three pile diameters, center to center. Continuous lagging will be required throughout. The soldier piles should be designed for the full anticipated

lateral pressure; however, the pressure on the lagging will be less due to arching in the soils. For design of lagging, the earth pressure can be limited to a maximum value of 450 psf.

Piles should be filled with concrete immediately after drilling. The concrete should be pumped to the bottom of the drilled holes using the tremie method. If casing is used, the casing should be removed as the concrete is placed, keeping the level of the concrete at least 5 feet above the bottom of the casing at all times.

8.1.11 Temporary Dewatering

Groundwater seepage was encountered during drilling and should be anticipated in excavations. Excavations extending near or below groundwater will require temporary construction dewatering of the site to lower and maintain depressed groundwater levels during construction. A registered civil engineer experienced in dewatering system design should design the dewatering system. We anticipate that a system of dewatering wells will be required to lower and maintain the groundwater level below the excavation in order to provide a stable excavation during construction. Dewatering rates, water volumes, drawdown time, radius of influence, and equipment requirements should be considered in the design. Pumping tests to evaluate the hydraulic parameters for the dewatering system design may be required. An NPDES permit from the Regional Water Quality Control Board will have to be obtained by the contractor for discharge of the dewatering effluent.

Groundwater should be drawn down at least 3 feet below the bottom of the deepest planned excavation to reduce the possibility of wet, unstable soils. Groundwater must remain at this depressed level during construction until structure loads and uplift resistance are sufficient to counteract buoyant forces with groundwater at historic levels. The contractor should provide at least one groundwater observation well within the excavation to verify that groundwater levels have been adequately lowered before excavation commences and to ensure that depressed groundwater levels are maintained during construction. Additional observation wells should be installed as needed outside the shored area so the contractor can monitor the radius of influence and evaluate the potential for settlements induced by the lowered groundwater levels. Nuisance groundwater that enters the excavation may be removed by a gravel sump pump collection system. The dewatering system should be integrated with the shoring system.

Dewatering the excavation area will affect the water level outside the excavation. Lowering the water table will result in effective stress increases of the soil supporting nearby structures or improvements, which may result in ground settlement and distress to those structures or improvements. We recommend that adjacent structures and improvements be surveyed by the contractor prior to dewatering and monitored during construction.

8.1.12 Imported Soil

Imported select soil should have an expansion index of 20 or less, Plasticity Index of 12 or less, and an R-Value greater than 40. Imported general fill soil for mass grading should be at least of comparable quality as the existing onsite soils, and in any case should be tested and approved

by Atlas prior to use on the project. Imported materials should be free of environmental contaminants, organic materials and debris, and should not contain rocks or lumps greater than 3 inches in maximum size.

8.1.13 Surface Drainage

Final surface grades around structures should be designed to collect and direct surface water away from the structure and toward appropriate drainage facilities. The ground around the structure should be graded so that surface water flows rapidly away from the structure without ponding. In general, we recommend that the ground adjacent to the structure slope away at a gradient of at least 2%. Densely vegetated areas where runoff can be impaired should have a minimum gradient of at least 5% within the first 5 feet of the structure. Roof gutters with downspouts that discharge directly into a closed drainage system are recommended on structures. Drainage patterns established at the time of fine grading should be maintained throughout the life of the proposed structures. Site irrigation should be limited to the minimum necessary to sustain landscape growth. Should excessive irrigation, impaired drainage, or unusually high rainfall occur, saturated zones of perched groundwater can develop.

8.1.14 Grading Plan Review

Atlas should review the grading plans and earthwork specifications to ascertain whether the intent of the recommendations contained in this report have been implemented and that no revised recommendations are needed due to changes in the development scheme.

8.2 Foundations

8.2.1 Shallow Spread Footings with Ground Improvement

In order to provide higher bearing capacity values so that shallow spread footings can be used for the proposed building and to reduce the potential for distress to the settlement sensitive planned improvements, we recommend performing ground improvement to a depth of at least 30 feet below the existing ground surface as an alternative to deep foundations. Drilled displacement columns, and rammed aggregate piers have been used successfully for similar geologic conditions in the past. Ground improvement design and methods should be provided by a specialty contractor experienced in ground improvement design and utilizing the data in this report.

The objective of ground improvement is to alter the mechanics of the existing soils to meet performance requirements, which generally include increasing bearing capacity, reducing settlement, and increasing resistance to liquefaction. In-situ testing, such as CPTs, should be performed after ground improvement to assess the properties of the improved soils and to verify the performance goals are met.

When ground improvement is performed, we recommend excavating fill within 2 feet of spread footings, grade beams, and slabs-on-grade and 1 foot of structural slabs and replacing with compacted fill. Horizontally, the excavations should extend, at least 2 feet outside the planned

improvements, or up to existing improvements, whichever is less. The bottom of over-excavated areas should be scarified to a depth of 8 inches, moisture conditioned near optimum, and recompacted to 90% relative compaction (ASTM D1557) prior to receiving new fill.

When ground improvement techniques are applied to the appropriate depth, the planned structural improvements can be supported on shallow spread footings with grade beams on compacted fill. Footings should extend at least 18 inches below the lowest adjacent finished grade that exists within 5 feet of the perimeter of the foundation edge. Continuous footings should be at least 18-inches wide, and isolated or wall footings should be at least 24-inches wide. The allowable bearing capacity of the improved ground will depend on the ground improvement design by the specialty contractor; however, it is anticipated that an allowable bearing capacity of 3,000 psf or higher (possibly up to 6,000 psf depending on the design) can be achieved. The bearing value can be increased by ⅓ when considering the total of all loads, including wind or seismic forces.

8.2.2 Mat Foundation

The planned building may be supported on a mat foundation bearing on compacted fill. The over-excavation depth for the mat foundation should be 5 feet below the existing grades or 3 feet below the planned mat foundation bottom elevation, whichever is deeper. Horizontally, the over-excavation should extend at least 5 feet outside the planned footing perimeter or up to existing improvements, whichever is less. Following the overexcavation, bottom of the excavations should be scarified to a depth of at least 8 inches, moisture conditioned as needed and compacted to at least 90% relative compaction. The completed pad surface should be firm and unyielding and should be protected from damage caused by traffic or weather. Soil subgrades should be kept moist during construction.

The mat foundation may be designed for an allowable bearing capacity of 1,500 psf. This value can be increased by ⅓ when considering the total of all loads, including wind or seismic forces. Thickness and reinforcement of the mat foundation should be in accordance with the recommendations of the project structural engineer. Mat foundations typically experience some deflection due to loads placed on the mat and the reaction of the soils underlying the mat. A design modulus of subgrade reaction, K, of 90 pounds per cubic inch (pci) may be used for the subgrade soils in evaluating such deflections. This value is based on an area of one square foot and should be adjusted for larger mats. Adjusted values of the modulus of subgrade reaction, K_v, can be obtained from the following equation for square mats of various widths:

$$K_v = K\left[\frac{B+1}{2B}\right]^2$$

Where B is the width of the mat in feet.

Adjusted values of the modulus of subgrade reaction, K', can be obtained from the following equation for rectangular mats:

$$K' = K_v \left[\frac{1 + 0.5(B/L)}{1.5} \right]$$

Where, B is width the and L is the length of the mat.

8.2.3 Resistance to Lateral Loads

Lateral loads will be resisted by friction between the bottoms of footings and passive pressure on the faces of footings and other structural elements below grade. An coefficient of friction of 0.30 can be used. Passive pressure can be computed using a lateral pressure of 350 psf per foot of depth below the ground surface for level ground conditions. The passive pressure can be increased by ⅓ when considering the total of all loads, including wind or seismic forces. The values above are for level backfill and do not include a factor of safety. Appropriate factors of safety should be incorporated into the design. The upper 1 foot of soil should not be relied on for passive support unless the ground is covered with pavements or slab.

8.2.4 Settlement Characteristics

Total foundation static settlements are estimated to be less than 1 inch. Differential settlements between adjacent columns and across continuous footings are estimated to be less than 1 inch over a distance of 40 feet.

8.2.5 Foundation Excavation Observations

A representative from Atlas should observe the foundation excavations prior to forming or placing reinforcing steel.

8.2.6 Foundation Plan Review

Atlas should review the foundation plans to ascertain that the intent of the recommendations in this report has been implemented and that revised recommendations are not necessary as a result of changes after this report was completed.

8.3 Slabs-on-Grade

8.3.1 Interior Slab-on-Grade

New non-structural concrete slab-on-grade floors should generally be a minimum 5 inches thick and should be reinforced in accordance with the structural engineer's design requirements. Concrete floor slabs should be underlain by a minimum 6-inch thick base course consisting of compacted aggregate in order to provide a uniform, level base for slab construction. A modulus of subgrade reaction of 90 pounds per cubic inch (pci) can be used for design of slabs.

Slab-on-grade concrete floors with moisture sensitive floor coverings may require protection from moisture transmission through the slab from the underlying subgrade soils. Geotechnical engineers are not experts in the protection of floor coverings from underslab moisture, and if of significant importance, an expert in concrete slab construction familiar with moisture transmission

issues through concrete slabs should be consulted for specific slab moisture protection design. However, we provide the following general discussion on typical types of moisture protection used in local construction.

Primary protection from moisture transmission through floor concrete is typically provided by a moisture retarder consisting of a relatively impermeable vapor retarder placed between the subgrade soil and the bottom of the concrete slab. A capillary break consisting of at least 6 inches of free-draining gravel, such as ¾-inch, clean, crushed, uniformly graded gravel with less than 3 percent passing No. 200 sieve, or equivalent, has also been used by designers below the vapor retarder. The capillary break layer can replace the base course requirement mentioned above. The vapor retarder should be at least 10-mil thick and should conform to the requirements for ASTM E 1745 Class C Underslab Vapor Retarders (e.g., Griffolyn Type 65, Griffolyn Vapor Guard, Moistop Ultra C, or equivalent). If additional protection is desired by the owner, a higher quality vapor barrier conforming to the requirements of ASTM E 1745 Class A, and with a water vapor transmission rate less than or equal to 0.006 gr/ft2/hr (i.e., 0.012 perms) per ASTM E 96 (e.g., 15-mil thick “Stego Wrap Class A”), or to Class B (Griffolyn Type 85, Moistop Ultra B, or equivalent) may be used in place of a Class C retarder. The vapor barrier installation should comply with ASTM E1643.

8.3.2 Exterior Slabs-on-Grade

Exterior slabs not subjected to vehicular loads should be at least 4 inches thick underlain by at least 2 feet of compacted non-expansive granular material and reinforced with at least No. 3 bars at 18 inches on center each way. Slabs should be provided with weakened plane joints. Joints should be placed in accordance with the American Concrete Institute (ACI) guidelines. The project architect should select the final joint patterns. A 1-inch maximum size aggregate mix is recommended for concrete for exterior slabs. The corrosion potential of on-site soils with respect to reinforced concrete will need to be taken into account in concrete mix design. Coarse and fine aggregate in concrete should conform to the “Greenbook” Standard Specifications for Public Works Construction. Control joints should be spaced at intervals of no more than 15 feet.

8.4 Conventional Retaining Walls

The active earth pressure for the design of unrestrained retaining walls with level backfill can be taken as equivalent to the pressure of a fluid weighing 40 pounds per cubic foot (pcf). The at-rest earth pressure for the design of restrained retaining walls with level backfills can be taken as equivalent to the pressure of a fluid weighing 55 pcf. These values assume a granular and drained backfill condition. An increase in earth pressure equal to 100 psf applied uniformly along the walls can be used to account for surcharge loads from light traffic. The above values do not include a load factor (i.e., a factor of safety).

Walls with heights less than 6 feet do not need to be designed for seismic lateral earth pressures. Where applicable, the seismic lateral earth pressure on cantilever retaining walls with a level backfill can be taken as equivalent to the pressure of a fluid weighing 24 pcf. The seismic lateral

earth pressure is in addition to the un-factored, static active earth pressure. If other surcharge loads are anticipated, Atlas should be contacted for the necessary increase in soil pressure.

Wall backfill should consist of granular, free-draining material having an expansion index of 20 or less. The backfill zone is defined by a 1:1 plane projected upward from the heel of the wall. Expansive or clayey soil should not be used. We anticipate that the on-site soils will not be suitable for wall backfill due to the existing amount of fines. Additionally, backfill within 3 feet from the back of the wall should not contain rocks greater than 3 inches in dimension. Backfill should be compacted to at least 90% relative compaction. Backfill should not be placed until walls have achieved adequate structural strength. Compaction of wall backfill will be necessary to reduce settlement of the backfill and overlying settlement sensitive improvements. However, some settlement should still be anticipated. Provisions should be made for some settlement of concrete slabs and pavements supported on backfill. Additionally, utilities supported on backfill should be designed to tolerate differential settlement.

Retaining walls should be designed to resist hydrostatic pressures or be provided with a backdrain to reduce the accumulation of hydrostatic pressures. Backdrains can consist of a 1-foot-wide zone of ¾ inch crushed rock. The backdrain should be separated from the adjacent soils using a nonwoven filter fabric, such as Mirafi 140N or equivalent. Weep holes should be provided, or a perforated pipe should be installed at the base of the backdrain and sloped to discharge to a suitable storm drain facility. As an alternative, a geocomposite drainage system such as Miradrain 6000 or equivalent placed behind the wall and connected to a suitable storm drain facility can be used. The project design consultant should provide waterproofing specifications and details. Figure 7 presents typical conventional retaining wall backdrain details.

8.5 Pipelines

8.5.1 Thrust Blocks

For level ground conditions, a passive earth pressure of 350 psf per foot of depth below the lowest adjacent final grade can be used to compute allowable thrust block resistance. A value of 150 psf per foot should be used below groundwater level, if encountered.

8.5.2 Modulus of Soil Reaction

A modulus of soil reaction (E') of 1,000 pounds per square inch can be used to evaluate the deflection of buried flexible pipelines. This value assumes that granular bedding material is placed adjacent to the pipe and is compacted to at least 90% relative compaction.

8.5.3 Pipe Bedding

Pipe bedding as specified in Section 217 of "Greenbook" can be used. Bedding material, except for plastic pipe, shall be sand, gravel, crushed aggregate, or native free-draining granular material having a sand equivalent of not less than 20 or a coefficient of permeability greater than 1.5 inches/hour (37.5 mm per hour). For HDPE, PVC solid wall, and PE solid wall pipe the bedding material shall be crushed rock conforming to the requirements shown in Table 217-1.2 of the

"Greenbook". Bedding material should extend to at least 12 inches above the top of pipe. Alternative materials meeting the intent of the bedding specifications are also acceptable. Samples of materials proposed for use as bedding should be provided to the engineer for inspection and testing before the material is imported for use on the project. The on-site materials are not expected to meet "Greenbook" bedding specifications. The pipe bedding material should be placed over the full width of the trench. After placement of the pipe, the bedding should be brought up uniformly on both sides of the pipe to reduce the potential for unbalanced loads. No voids or uncompacted areas should be left beneath the pipe haunches. Ponding or jetting the pipe bedding should not be allowed.

8.5.4 Backfill

Utility trench backfill should conform to the minimum requirements of Section 217 of the "Greenbook" and local jurisdictions. Backfill should be placed in loose lifts not exceeding 6 to 8 inches in thickness, moisture conditioned to near optimum moisture content, and compacted to at least 90% relative compaction. The maximum dry density and optimum moisture content for the evaluation of relative compaction should be determined in accordance with ASTM D1557. On-site materials, except for soil containing roots, debris, and rock greater than 3 inches, can be used as non-structural trench backfill.

8.6 Pavement Section Recommendations

Atlas utilized the California Department of Transportation Highway Design Manual (Caltrans, 2020) and NAVFAC to prepare preliminary recommendations for flexible and rigid pavements. The pavement support characteristics of the soils encountered during our investigation are considered good. Laboratory testing was performed on a select sample, and results indicate an R-Value of 67. An R-value of 50 was used for the design of preliminary pavement sections. The support characteristics of actual subgrade soils should be determined after grading and final pavement sections are provided. Table 6 provides recommended flexible and rigid pavement structural sections for the assumed Traffic Indexes and subgrade R-value.

Table 6: Asphalt Pavement Sections

Traffic Type	Traffic Index (TI)	AC[1] over AB[2] (inches)	Full-Depth AC[1] (inches)	PCC[3] over AB[2] (inches)
Parking Bays	5.0	3 over 4	5	6 over 4
Drive Lanes	6.0	4 over 3	6	7 over 4
Fire Lanes	7.5	5 over 4	8	8 over 4

[1]AC – Asphalt Concrete
[2]AB – Class 2 Aggregate Base
[3]PCC – Portland Cement Concrete

PrThe top 12 inches of subgrade should be scarified, moisture conditioned to near optimum moisture content and compacted to at least 95% relative compaction. All soft or yielding areas should be removed and replaced with compacted fill or aggregate base. Aggregate base and asphalt concrete should conform to the Caltrans Standard Specifications or the "Greenbook" and

should be compacted to at least 95% relative compaction. Aggregate base should have an R-value of not less than 78. All materials and methods of construction should conform to good engineering practices.

8.7 Soil Corrosivity

Representative samples of the on-site soils were tested to evaluate corrosion potential. The test results are presented in Appendix III. The project design engineer can use the sulfate results in conjunction with ACI 318 to specify the water/cement ratio, compressive strength, and cementitious material types for concrete exposed to soil. A corrosion engineer should be contacted to provide specific corrosion control recommendations.

9. GEOTECHNICAL ENGINEERING DURING CONSTRUCTION

The geotechnical engineer should review project plans and specifications prior to bidding and construction to check that the intent of the recommendations in this report has been incorporated. Observations and tests should be performed during construction. If the conditions encountered during construction differ from those anticipated based on the subsurface exploration program, the presence of the geotechnical engineer during construction will enable an evaluation of the exposed conditions and modifications of the recommendations in this report or development of additional recommendations in a timely manner.

10. CLOSURE

Atlas should be advised of any changes in the project scope so that the recommendations contained in this report can be evaluated with respect to the revised plans. Changes in recommendations will be verified in writing. The findings in this report are valid as of the date of this report. Changes in the condition of the site can, however, occur with the passage of time, whether they are due to natural processes or work on this or adjacent areas. In addition, changes in the standards of practice and government regulations can occur. Thus, the findings in this report may be invalidated wholly or in part by changes beyond our control. This report should not be relied upon after a period of two years without a review by us verifying the suitability of the conclusions and recommendations to the site conditions at that time.

In the performance of our professional services, we comply with that level of care and skill ordinarily exercised by members of our profession currently practicing under similar conditions and in the same locality. The client recognizes that subsurface conditions may vary from those encountered at the boring locations and that our data, interpretations, and recommendations are based solely on the information obtained by us. We will be responsible for those data, interpretations, and recommendations, but shall not be responsible for interpretations by others of the information developed. Our services consist of professional consultation and observation only, and no warranty of any kind whatsoever, express or implied, is made or intended in connection with the work performed or to be performed by us, or by our proposal for consulting or other services, or by our furnishing of oral or written reports or findings.

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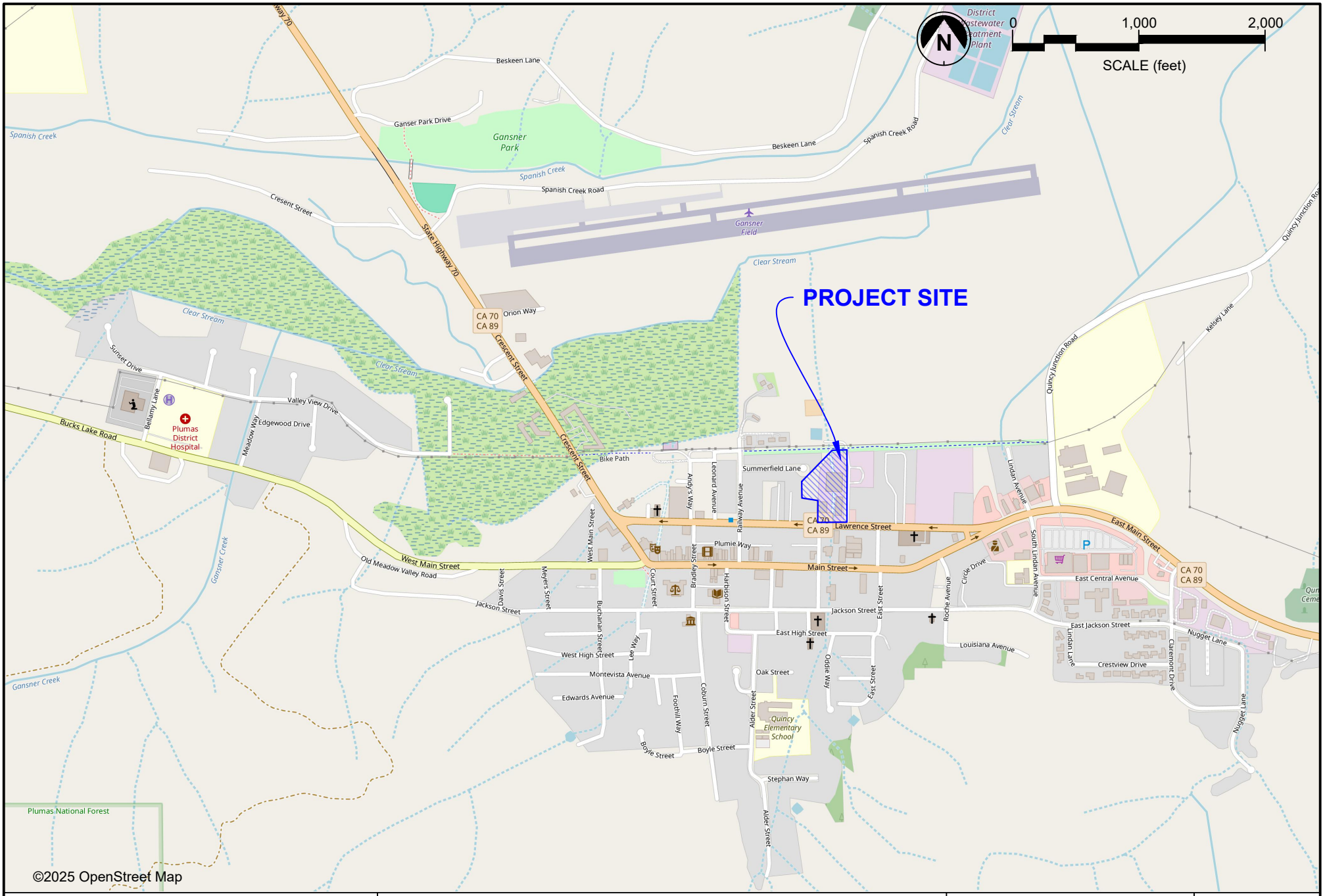
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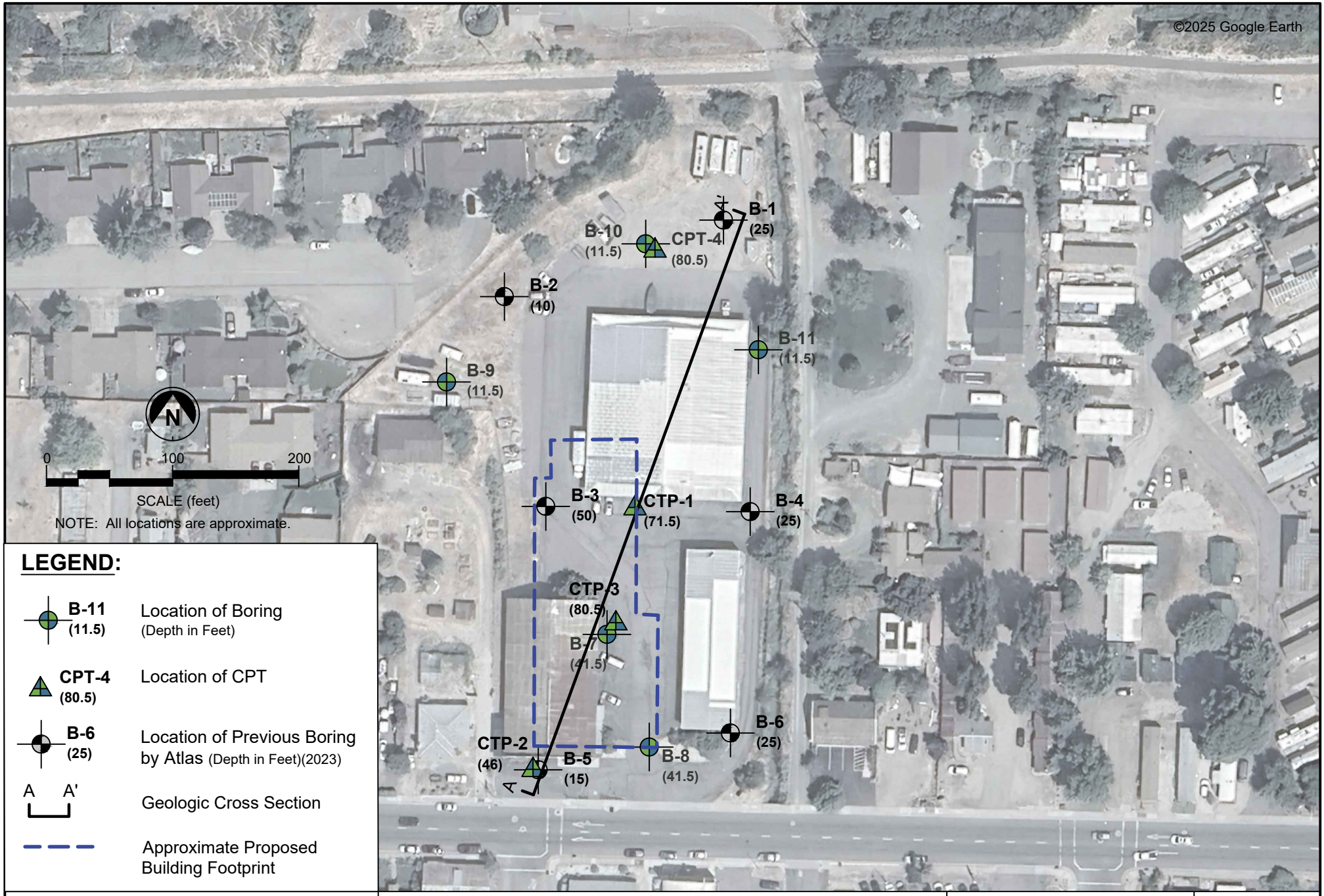
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Youd, T.L., Idriss, I.M., Andrus, R.D., Arango, I., Castro, G., Christian, J.T., Dobry, R., Finn, W.D.L., Harder, L.F. Jr., Hynes, M.E., Ishihara, K., Koester, J.P., Liao, S.S.C., Marcuson, W.F. III, Martin, G.R., Mitchell, J.K., Moriwaki, Y., Power, M.S., Robertson, P.K., Seed, R.B., and Stokoe, K.H. II, 2001, Liquefaction Resistance of Soils: Summary Report from the 1996 NCEER and 1998 NCEER/NSF Workshops on Evaluation of Liquefaction Resistance of Soils: ASCE Journal of Geotechnical and Environmental Engineering, Vol. 127, No. 10, October 2001, p. 817-833.

Youd, T.L. and Idriss, I.M. (1997), Proceeding of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils. Technical Report NCEER-97-0022. National Center for Earthquake Engineering Research, New York.



ATLAS	**SITE VICINITY MAP** Quincy Courthouse 253, 287, and 295 Lawrence Street Quincy, California 95971	Date: October, 2025 By: CGI Job No.: 91-65859-PW	Figure: 1



ATLAS

SUBSURFACE EXPLORATION MAP
Quincy Courthouse
253, 287, and 295 Lawrence Street
Quincy, California 95971

Date: October, 2025
By: CGI
Job No.: 91-65859-PW

Figure:
2



EXPLANATION:

QI	Lake deposits
PB^b	Pliocene Volcanic Rocks; basalt
PzMz	Metamorphic rocks of unknown age
Pzsf	Shoo Fly Complex SS - Sandstone, siltstone and slate

N

0 4,000 8,000

SCALE (feet)

NOTE: All locations are approximate.

Reference:
Saucedo, G.J. and Wagner, D.L. (1992), Geologic map of the Chico quadrangle, California, 1:250,000, California Division of Mines and Geology, Scale 1:250,000.

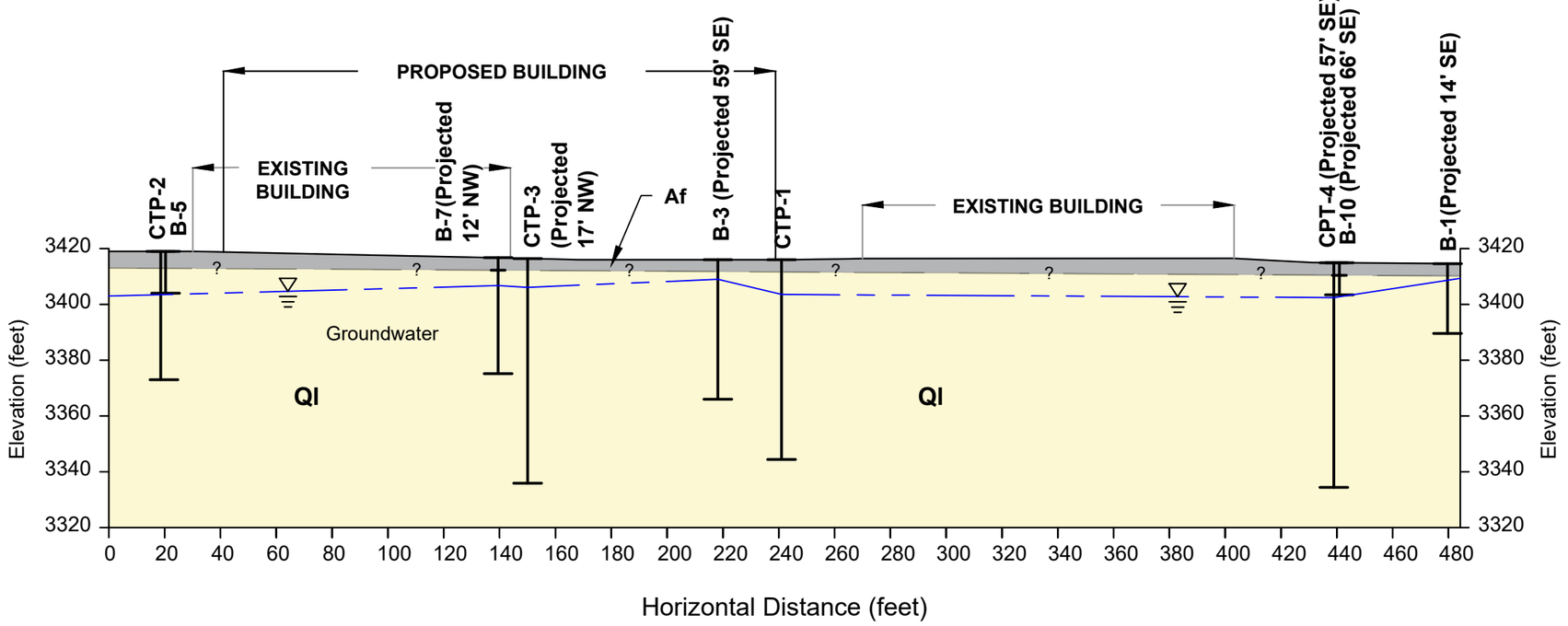
ATLAS

REGIONAL GEOLOGY MAP

Quincy Courthouse
253, 287, and 295 Lawrence Street
Quincy, California 95971

Date: October, 2025
By: CGI
Job No.: 91-65859-PW

Figure: 3



LEGEND:

B-2 — Location of Boring

—?— Geologic Contact, Queried Where Uncertain

Groundwater

Af — Fill

Ql — Lake deposits

0 50 100
SCALE (feet)

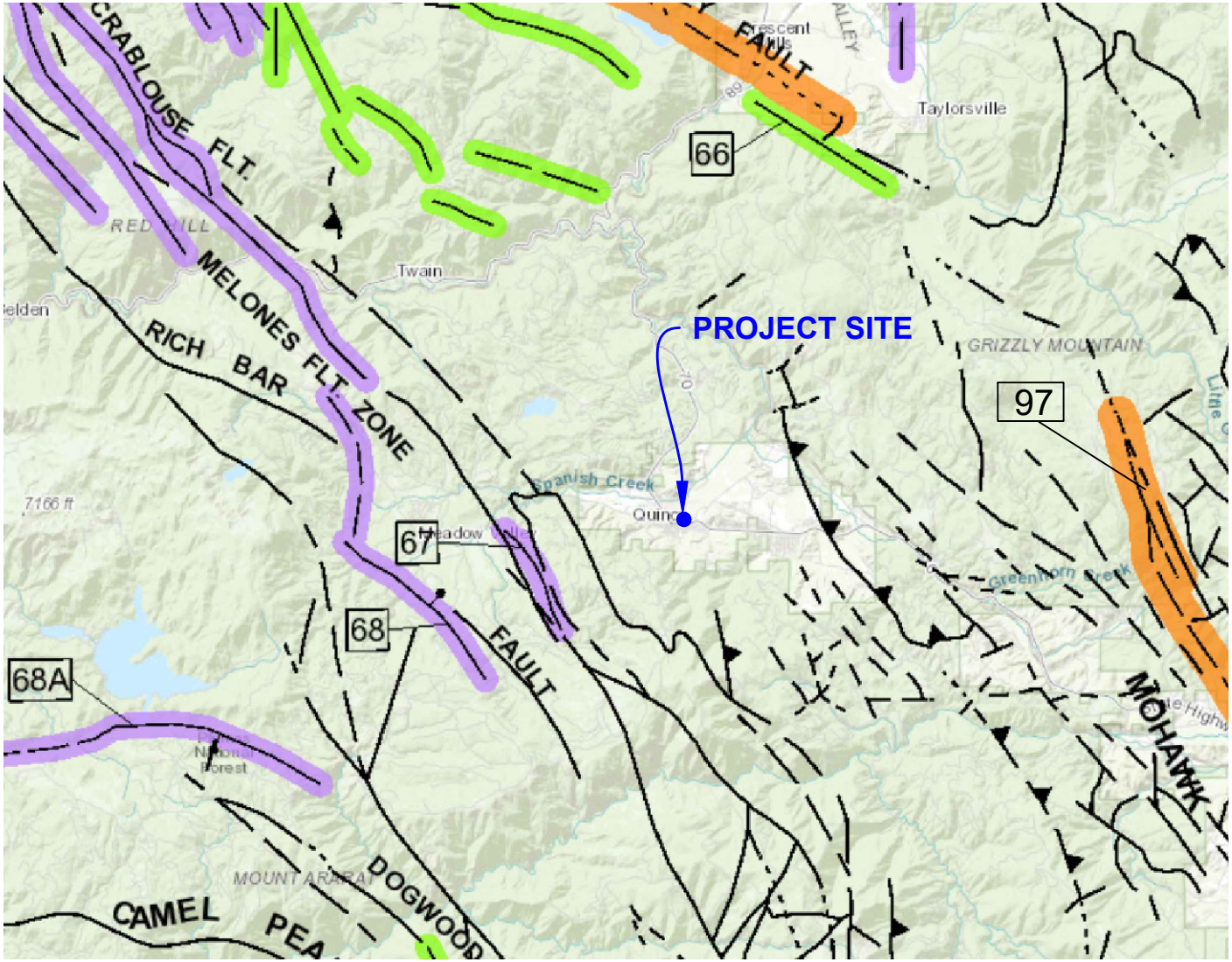
NOTE: All Locations are approximate.

Date: October,2025
By: CGI
Job No.: 91-65859-PW

GEOLOGIC CROSS-SECTION
Quincy Courthouse
Quincy, California

ATLAS

Figure:
4



EXPLANATION:

Fault along which historic (last 200 years) displacement has occurred

Holocene fault displacement (during past 11,700 years) without historic record.

Late Quaternary fault displacement (during past 700,000 years).

Quaternary fault (age undifferentiated).

Pre-Quaternary fault (older than 1.6 million years) or fault without recognized Quaternary displacement.

Low angle fault (barbs on upper plate).

66	Indian Valley fault - Indian Valley faultt zone (concealed)
67	Meadow Valley fault - Meadow Valley fault zone (certain)
68	Bottle Springs fault - Bottle Springs fault zone (certain)
68A	Haskins Valley fault- Haskins Valley fault zone (certain)
97	Mohawk Valley fault - Mohawk Valley fault zone (located)

N

0 4 8

SCALE (miles)

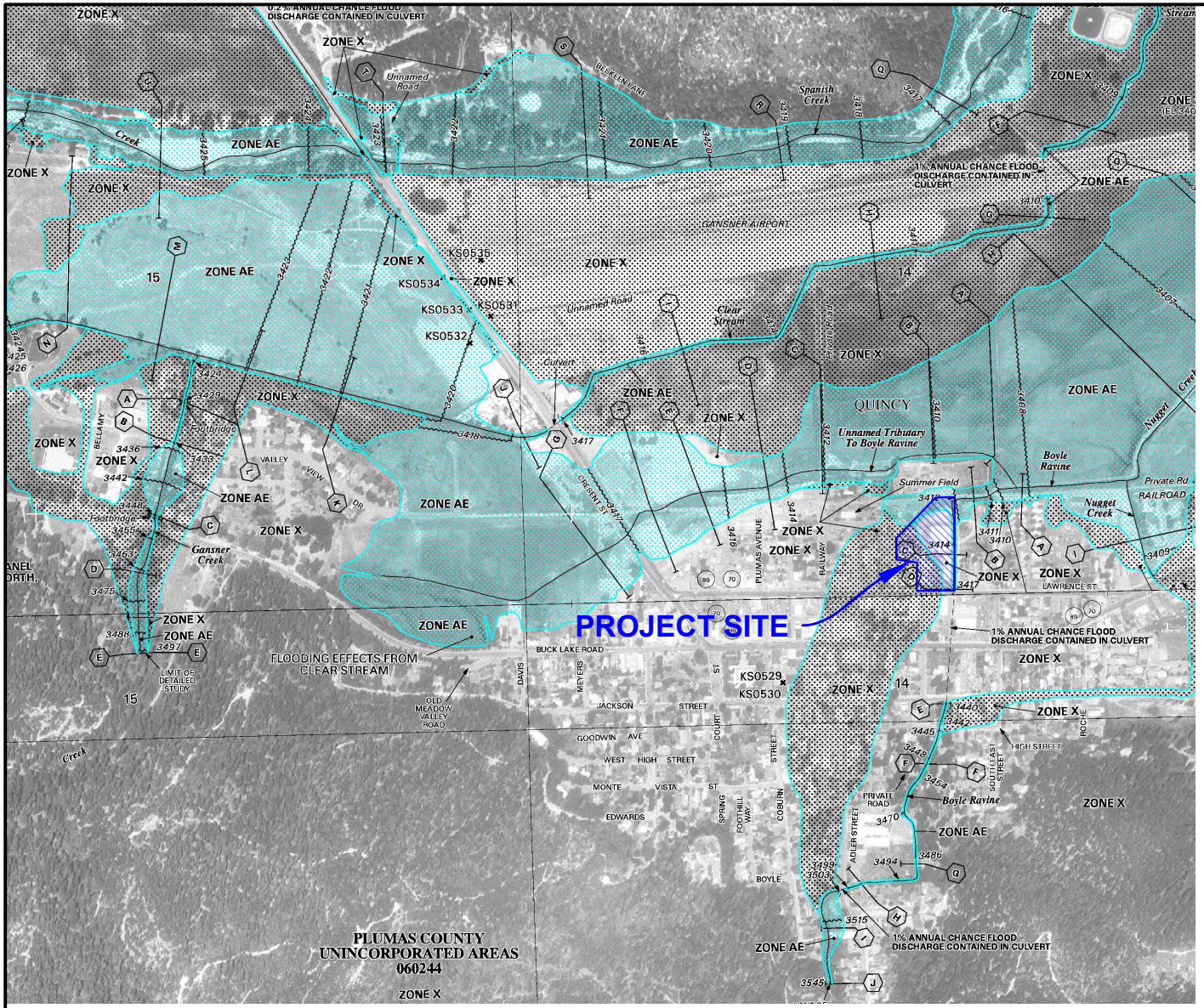
Reference:
Jennings, C.W., Bryant W.A., Fault Activity Map of California (2010), maps.conservation.ca.gov/cgs/fam; Accessed October, 2025

ATLAS

CALIFORNIA FAULT ACTIVITY MAP
Quincy Courthouse
253, 287, and 295 Lawrence Street
Quincy, California 95971

Date: October, 2025
By: CGI
Job No.: 91-65859-PW

Figure: 5



0 1,000 2,000

SCALE (feet)

Reference:
FEMA (2005), Flood Insurance Rate Map, Plumas County, California and Icorporated Areas, Map Number: 06063C0904E and 06063C0912E, Scale: 1":500'

EXPLANATION:

SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD EVENT

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water surface elevation of the 1% annual chance flood.

ZONE A No base flood elevations determined.

ZONE AE Base flood elevations determined.

ZONE AH Flood depths of 1 to 3 feet (usually areas of ponding); base flood elevations determined.

ZONE AO Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

ZONE AR Area of special flood hazard formerly protected from the 1% annual chance flood event by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood event.

ZONE A99 Area to be protected from 1% annual chance flood event by a Federal flood protection system under construction; no base flood elevations determined.

ZONE V Coastal flood zone with velocity hazard (wave action); no base flood elevations determined.

ZONE VE Coastal flood zone with velocity hazard (wave action); base flood elevations determined.

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance floodplain.

ZONE D Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

- 1% annual chance floodplain boundary
- 0.2% annual chance floodplain boundary
- Floodway boundary
- Zone D boundary
- CBRS and OPA boundary
- Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or velocities.
- 513 — Base Flood Elevation line and value; elevation in feet*
- (EL 987) — Base Flood Elevation value where uniform within zone; elevation in feet*

*Referenced to the North American Vertical Datum of 1988

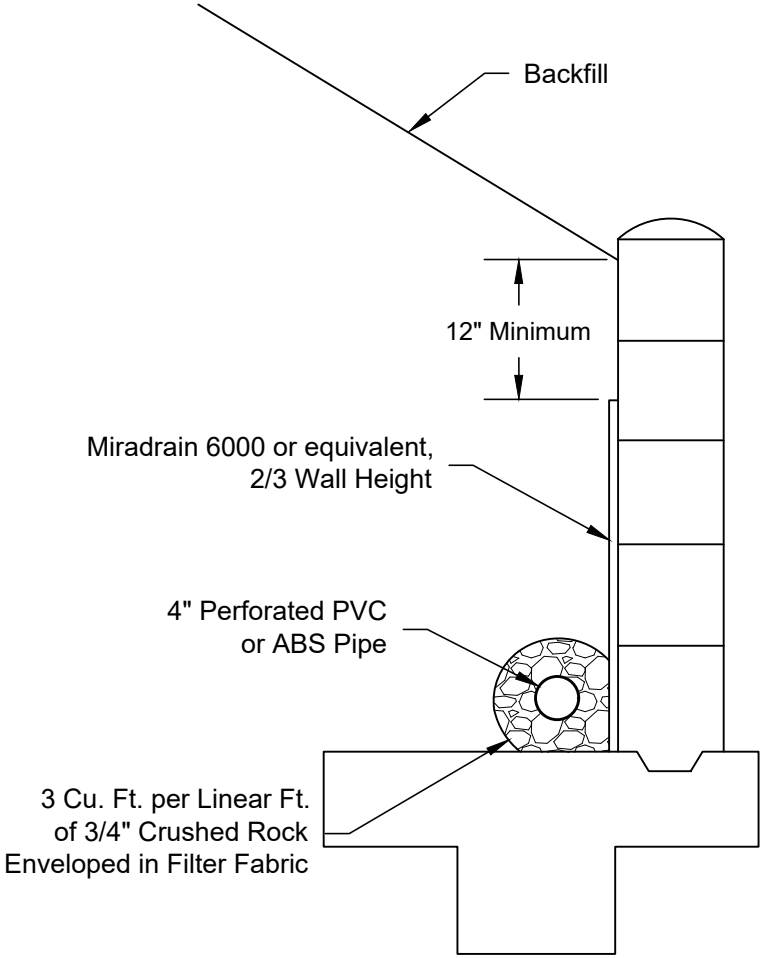
- A — A — Cross Section Line
- 23 — 23 — Transect Line
- 97°07'30", 32°22'30" — Geographic coordinates referenced to the North American Datum of 1983 (NAD 83)
- 4276000M — 1000-meter Universal Transverse Mercator grid values, zone 10
- 600000 FT — 5000-foot grid ticks
- DX5510 × — Bench mark (see explanation in Notes to Users section of this FIRM panel).
- M1.5 — River Mile

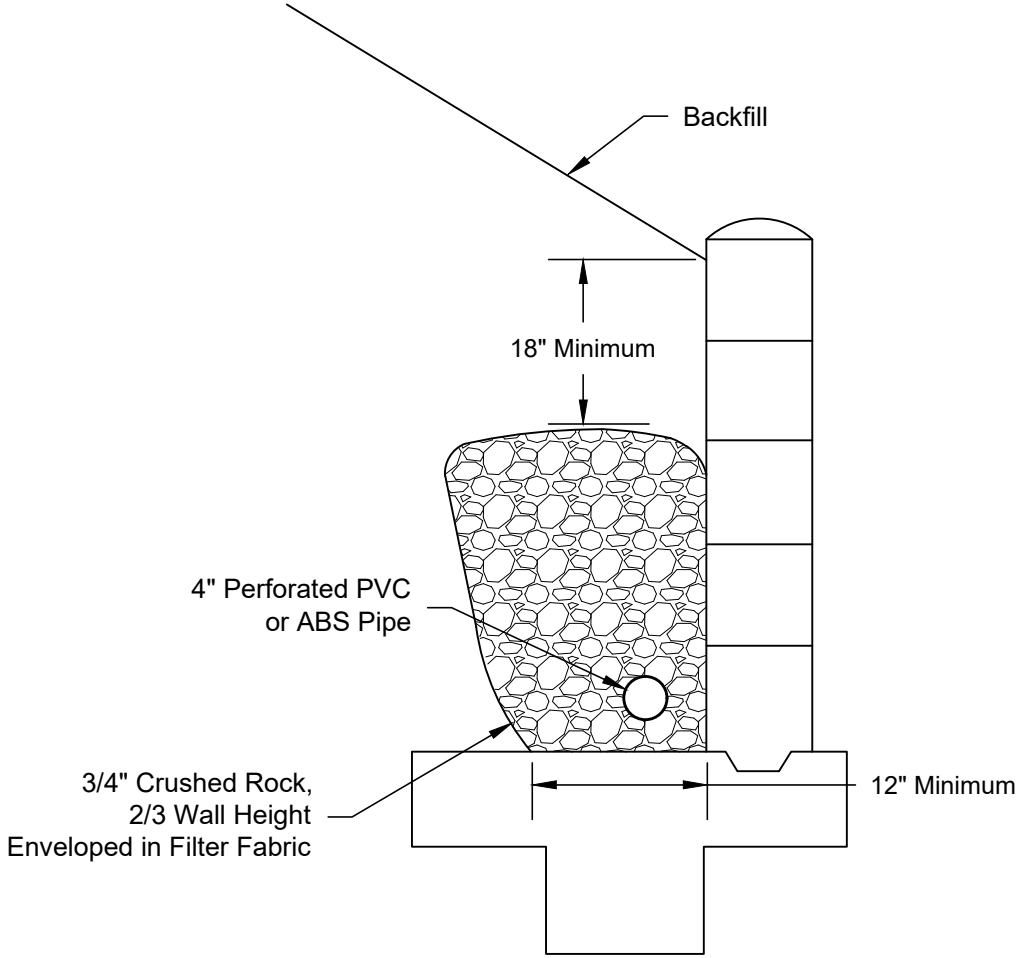
ATLAS

FLOOD MAP
Quincy Courthouse
253, 287, and 295 Lawrence Street
Quincy, California 95971

Date: October, 2025
By: CGI
Job No.: 91-65859-PW

Figure: 6





NOT TO SCALE

NOTES:

1) Dampproof or waterproof back of wall following architect's specifications.
2) 4" minimum perforated pipe, SDR35 or equivalent, holes down, 1% fall to outlet. Provide solid outlet pipe at suitable locations.
3) Drain installation and outlet connection should be observed by the geotechnical consultant.

ATLAS	**TYPICAL RETAINING WALL BACKDRAIN DETAILS** Quincy Courthouse 253, 287, and 295 Lawrence Street Quincy, California 95971	Date: October, 2025 By: CGI Job No.: 91-65859-PW	Figure: 7

APPENDIX I
BORING LOGS

Relatively undisturbed samples were obtained using a modified California (CAL) sampler, which is a ring-lined split tube sampler with a 3-inch outer diameter and 2½-inch inner diameter. Standard Penetration Tests (SPT) were performed using a 2-inch outer diameter and 1⅜-inch inner diameter split tube sampler. The CAL and SPT samplers were driven with a rope-and-cathead 140-pound weight dropping 30 inches. The number of blows needed to drive the samplers the final 12 inches of an 18-inch drive is noted on the boring logs as “Driving Resistance (blows/ft. of drive).” SPT and CAL sampler refusal was encountered when 50 blows were applied during any one of the three 6-inch intervals, a total of 100 blows was applied, or there was no discernible sampler advancement during the application of 10 successive blows. Disturbed bulk samples were obtained from the SPT sampler and the drill cuttings. The soils are classified in general accordance with the Unified Soil Classification System.

UNIFIED SOIL CLASSIFICATION (ASTM D-2487)

Material Types	Criteria for Assigning Soil Group Names			Group Symbol	Soil Group Names	Legend
Coarse Grained Soils	Gravels >50% of Coarse Fraction Retained on No. 4 Sieve	Clean Gravels <5% Fines	Cu≥4 and 1≤Cc≤3	GW	Well-Graded Gravel	
			Cu<4 and/or [Cc<1 or Cc>3]	GP	Poorly-Graded Gravel	
		Gravels with Fines >12% Fines	Fines Classify as ML or MH	GM	Silty Gravel	
			Fines Classify as CL or CH	GC	Clayey Gravel	
>50% Retained on No. 200 Sieve	Sands ≥50% of Coarse Fraction Passes on No. 4 Sieve	Clean Sands <5% Fines	Cu≥6 and 1≤Cc≤3	SW	Well-Graded Sand	
			Cu<6 and/or [Cc<1 or Cc>3]	SP	Poorly-Graded Sand	
		Sands and Fines >12% Fines	Fines Classify as ML or MH	SM	Silty Sand	
			Fines Classify as CL or CH	SC	Clayey Sand	
Fine Grained Soils	Silts and Clays Liquid Limits<50	Inorganic	PI>7 and Plots≥"A" Line	CL	Lean Clay	
			PI>4 and Plots<"A" Line	ML	Silt	
		Organic	LL (Oven Dried)/LL(not Dried <0.75)	OL	Organic Silt	
≥50% Passes No. 200 Sieve	Silts and Clays Liquid Limits≥50	Inorganic	PI Plots≥"A" Line	CH	Fat Clay	
			PI Plots<"A" Line	MH	Elastic Silt	
		Organic	LL (Oven Dried)/LL(Not Dried <0.75)	OH	Organic Clay	
Highly Organic Soils		Primarily Organic Matter, Dark in Color and Organic Odor		PT	Peat	

PENETRATION RESISTANCE (RECORDED AS BLOWS/0.5 FEET)

SAND AND GRAVEL		SILT AND CLAY		
RELATIVE DENSITY	N-VALUE (BLOWS/FOOT)*	CONSISTENCY	N-VALUE (BLOWS/FOOT)*	COMPRESSIVE STRENGTH
Very Loose	0 - 3	Very Soft	0 - 1	0 - 0.25
Loose	4 - 10	Soft	2 - 4	0.25 - 0.50
Medium Dense	11 - 29	Medium Stiff	5 - 7	0.50 - 1.0
Dense	30 - 49	Stiff	8 - 14	1.0 - 2.0
Very Dense	50+	Very Stiff	15 - 29	2.0 - 4.0
		Hard	30+	Over 4.0

SOIL MOISTURE

DESCRIPTOR	DESCRIPTION
Dry	Dry of Standard Proctor Optimum
Damp	Sand Dry
Moist	Near Standard Proctor Optimum
Wet	Wet of Standard Proctor Optimum
Saturated	Free Water in Sample

PARTICLES SIZES

COMPONENTS		SIZE OR SIEVE NUMBER
Boulders		Over 12 Inches
Cobbles		3 to 12 inches
Gravels	-Coarse	3/4 to 3 Inches
	-Fine	Number 4 to 3/4 Inch
Sand	-Coarse	Number 10 to Number 4
	-Medium	Number 40 to Number 10
	-Fine	Number 200 to Number 40
Fines (Silt and Clay)		Below Number 200

Grab Bulk Sample

Standard Penetration Test

2.5 Inch Modified California

Rock Core

Shelby Tube

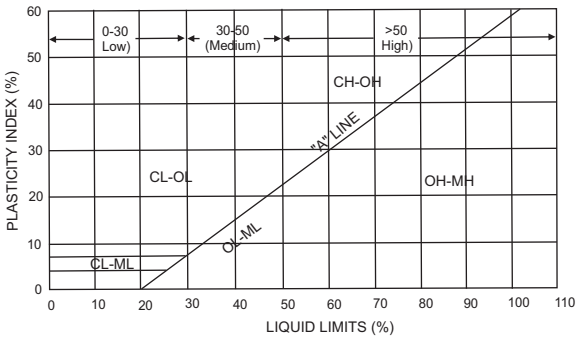
Initial Water Level Reading

Final Water Level Reading

Blow Count
The number of blows of the sampling hammer required to drive the sampler through each of three 6-inch increments. Less than three increments may be reported if more than 50 blows are counted for any increment. The notation 50/5" indicates 50 blows recorded for 5 inches of penetration.

N-Value
Number of blows 140 LB hammer falling 30 inches to drive a 2 inch outside diameter (1-3/8 inch I.D) split barrel sampler the last 12 inches of an 18 inch drive (ASTM-1586 Standard Penetration Test)

PLASTICITY CHART



CU -Consolidated Undrained triaxial test completed. Refer to laboratory results
DS - Results of Direct Shear test in terms of total cohesion (C, KSF) or effective cohesion and friction angles (C', KSF and degrees)
LL - Liquid Limit
PI - Plasticity Index
PP - Pocket Penetrometer test
TV - Torvane Shear Test results in terms of undrained shear strength (KSF)
UU - Unconsolidated Undrained triaxial test result in terms of undrained shear strength (KSF)
#200 - Percent passing number 200 sieve
Cu - Coefficient of Uniformity
Cc - Coefficient of Concavity

General Notes

1. The boring locations were determined by pacing, sighting and/or measuring from site features. Locations are approximate. Elevations of borings (if included) were determined by interpolation between plan contours or from another source that will be identified in the report or on the project site plan. The location and elevation of borings should be considered accurate only to the degree implied by the method used.

2. The stratification lines represent the approximate boundary between soil types. The transition may be gradual.

3. Water level readings in the drill holes were recorded at time and under conditions stated on the boring logs. This data has been reviewed and interpretations have been made in the text of this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, tides, temperature and other factors at the time measurements were made.

4. The boring logs and attached data should only be used in accordance with the report.

ATLAS

KEY TO EXPLORATORY BORING LOGS

%0! Ju icial Council of California (JCC)
#,"D* ! Ā0(> New Quincy Courthouse - Potential Site 2
#,"D* ! Ā0<> , 1- 859- PW
#, " D !Ā" !%" 0 70 Main St, Quincy, CA
1 !* Ā$(, ! 1 / / 23 " ># ! 1 / / 23
+,"<01Ā - ! %0 3413 ft /"& Ā$% 4"
1, % %0+ Ā"" 0!, !" , West Coast Exploration
+,"<01Ā . ! ,Ā - $2
1,% %0+ Ā- ! /"1 Solid Flight
▽ !Ā!%> Ā"ĀĀ1, % %0+ 8. ft / Elev 3405. ft
" ++ 1Ā= JL / @*1Ā CTD
▼ ! Ā 01 ĀA Ā1,% %0+ .0 ft / Elev 34 7.0 ft
0"! $ Elevations from Topo Map by BKF Engineers
A! ,Ā1,% %0+ ---

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS: LIQUID LIMIT	ATTERBERG LIMITS: PLASTIC LIMIT	ATTERBERG LIMITS: PLASTICITY INDEX	FINES CONTENT %)
		À Ā!" #$" %ĀĀ GC) Ā' Ā , - Ā%! / Ā$ 01 ĀĀ2Ā Dark yellow-brown, moist, dense. [FILL]	MC 1-1		19-12-18 3)		105					20
			MC 1-2		3-2-2 4)			21				
		CL) $(0 1 Ā Ā 46Ā 789: ;Ā2Ā Dark gray, very moist, soft. [FILL]				.						
		Becomes dark yellow brown and stiff.	MC 1-3		- 4-)							
10		GP-GC) Poorly graded GRAVEL with CLAY and SAND : Yellowish-brown, saturated, medium dense.										
			MC 1-4		- - 10 1)							10
15		CL) $ 01 Ā Ā. %/Ā+ ,(- Ā2Ā Yellowish-brown, wet, me ium stiff. UU @ 1 .5': Su = 0.7 ksf										
			MC 1-		3-3-4 7)							
20		Becomes saturate , very stiff, with trace gravel.				1.						
			MC 1-		7-8-12 2)			22				1
25		Bottom of borehole at 2 .0 feet.										

%0! Ju icial Council of California (JCC)
#,"D* ! Ā0(> New Quincy Courthouse - Potential Site 2
#,"D* ! Ā0<> , 1- 859- PW
#, " D !Ā" !%" 0 70 Main St, Quincy, CA
1 !* Ā$(, ! 1 / / 23 " ># ! 1 / / 23
+,"<01Ā - ! %0 3414 ft /"& Ā$% "
1, % %0+ Ā"' 0!, !" , West Coast Exploration
+,"<01Ā . ! ,Ā - $2
1,% %0+ Ā ! /"1 Solid Flight
▽ !Ā!%> Ā"ĀĀ1, % %0+ 7. ft / Elev 3407. ft
" ++ 1Ā= JL / @*1Ā CTD
▼ ! Ā 01 ĀA Ā1,% %0+ .0 ft / Elev 34 8.0 ft
0"! $ Elevations from Topo Map by BKF Engineers
A! ,Ā1,% %0+ ---

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS LIQUID LIMIT	ATTERBERG LIMITS PLASTIC LIMIT	ATTERBERG LIMITS PLASTICITY INDEX	FINES CONTENT %)
		Ā Ā!' #$" %ĀĀ										
		SP) Poorly graded SAND with GRAVEL : Yellowish brown, moist, medium dense. [FILL]	MC 2-1		- - 7 12)	1.						
		CL) $(01)Ā'&()ĀĀ2ĀĀ Yellowish-brown, moist, stiff. [FILL]										
		SC) Ā$(01Ā.%!/Ā+,(-*&ĀĀ2ĀĀ Yellow-brown, moist, loose.	MC 2-2		4-3-4 7)		120	14				28
		▼ ▽										
10			MC 2-3		3-3-3)							

Bottom of borehole at 1 .0 feet.

%0! Ju icial Council of California (JCC)
#,"D* ! Ā0(> New Quincy Courthouse - Potential Site 2
#,"D* ! Ā0<> , 1- 859- PW
#, " D !Ā" !%" 0 70 Main St, Quincy, CA
1 !* Ā$(, ! 1 / / 23 " ># ! 1 / / 23
+,"<01Ā - ! %0 3415 ft /"& Ā$% 4"
1, % %0+ Ā"' 0!, !" , West Coast Exploration
+,"<01Ā . ! ,Ā - $2
1,% %0+ Ā ! /"1 Solid Flight
▽ !Ā!%> Ā"ĀĀ1, % %0+ . ft / Elev 3406. ft
" ++ 1Ā= JL / @*1Ā CTD
▼ ! Ā 01 ĀA Ā1,% %0+ 7.0 ft / Elev 34 8.0 ft
0"! $ Elevations from Topo Map by BKF Engineers
A! ,Ā1,% %0+ ---

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. tsf)	DRY UNIT WT. pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS: LIQUID LIMIT	ATTERBERG LIMITS: PLASTIC LIMIT	ATTERBERG LIMITS: PLASTICITY INDEX	FINES CONTENT %)
		ĀÀĀĀĀĀ										
		GP) Ā Ā										
		SM) Ā$% Ā$ 01Ā. % Ā , - ĀĀĀdark brown, moist, medium dense.	MC 3-1		1 -8-7 1)		117	8				
		DS @ 2.0': C = 0; phi = 47.5 (est.)										
		SP) Poorly graded SAND with GRAVEL ĀĀ2ĀĀow-brown, moist, loose.	MC 3-2		- 4-)		104	8				
		▼										
		▽	MC 3-3		20-17-18 3)							
10		Becomes saturdate an dense.										
		SC) Ā$ 01Ā. % Ā , - ĀĀĀYellow-brown, wet, medium ense.	SPT 3-4		3- - 11)			22				42
15												
		CL) $ 01 Ā Ā. %/Ā+,(- ĀĀYellowish brown, wet, stiff.	SPT 3-		- - 8 14)							
20												
		SC) Ā' Ā$ 01Ā. % Ā , - ĀĀĀYellow-brown, wet, dense.	MC 3-		10-12-27 3)			8				20
25												
		Becomes me ium dense, gravel content increases.	SPT 3-7		- 7- / "			12				27
30												

%0 ! Ju icial Council of California (JCC) #,"D* ! Ā0(> New Quincy Courthouse - Potential Site 2

#,"D* ! Ā0<> , 1- 859- PW #, " D !Ā" !%" 0 70 Main St, Quincy, CA

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS LIQUID LIMIT	ATTERBERG LIMITS PLASTIC LIMIT	ATTERBERG LIMITS PLASTICITY INDEX	FINES CONTENT %)
30		SC) Ā' Ā$ 01Ā.% Ā-, - ĀĀĀĀellow-brown, wet, dense. Ä! "#$%&'-										
35		GC) Ā' Ā-, - Ā%! / Ā$ 01ĀĀĀYellow-brown, wet, medium ense.	SPT 3-8		7-13-1 28)							
40		Becomes very ense.	SPT 3-		11-29-44 73)			10				32
45			SPT 3-10		24- / "							
			SPT 3-11		42-25-29 4)							

Bottom of borehole at .0 feet.

%0! Ju icial Council of California (JCC)
#,"D* ! Ā(> New Quincy Courthouse - Potential Site 2
#,"D* ! Ā0<> , 1- 859- PW
#, " D !Ā" !%" 0 70 Main St, Quincy, CA
1 !* Ā$(, ! 1 / / 23 " ># ! 1 / / 23
+,"<01Ā - ! %0 3416 ft /"& Ā$% 4"
1, % %0+ Ā"' 0!, !" , West Coast Exploration
+,"<01Ā . ! ,Ā - $2
1,% %0+ Ā ! /"1 Solid Flight
▽ !Ā!%> Ā"ĀĀ1, % %0+ 8. ft / Elev 3408. ft
" ++ 1Ā= JL / @*1Ā CTD
▼ ! Ā 01 ĀA Ā1,% %0+ 7.0 ft / Elev 34 .0 ft
0"! $ Elevations from Topo Map by BKF Engineers
A! ,Ā1,% %0+ ---

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS LIQUID LIMIT	ATTERBERG LIMITS PLASTIC LIMIT	ATTERBERG LIMITS PLASTICITY INDEX	FINES CONTENT %)
		'ĀE ĀĀ2ĀĀ GM) **ĀĀLTY SAND with GRAVEL :** Dark brown, moist, medium dense. [FILL?]	MC 4-1		7-7-7 14)		100	14				29
		ML) **$(01)Ā$%&!Ā3456ĀGRAVELĀĀ2ĀĀ**llowish brown, moist, medium stiff.	MC 4-2		3-3-3)	1.	8	20	33	24		3
		GP) **Poorly graded GRAVEL with SANDĀ2ĀĀ**llow-brown, saturated, medium dense.	MC 4-3		- 8-10 18)							
10												
		CL) **$ 01 Ā Ā. %/Ā+,(- ĀĀĀ**Yellowish brown, saturate , stiff Consol test @ 14.5'	MC 4-4		2-3-7 1)		8	27				
15		SP) **Poorly graded SAND with GRAVELĀĀ2ĀĀ**llow-brown, saturated, loose.										
		CL) **$ 01 Ā Ā. %/Ā+,(- ĀĀĀ**Yellowish brown, saturate , stiff.	MC 4-		- - 11)			20				
20												
			MC 4-		4-4-)		113	17				
25												

Bottom of borehole at 2 .0 feet.

Ju icial Council of California (JCC)	New Quincy Courthouse - Potential Site 2
1- 859- PW	70 Main St, Quincy, CA
/ / 23	3419 ft 4"
West Coast Exploration	
Solid Flight	13. ft / Elev 3405. ft
JL / CTD	12. ft / Elev 3406. ft
Elevations from Topo Map by BKF Engineers	---

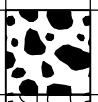
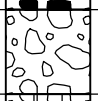
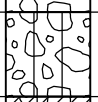
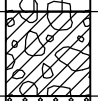
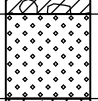
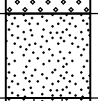
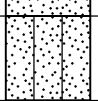
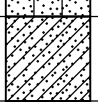
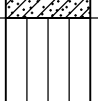
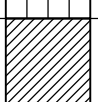
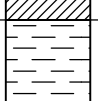
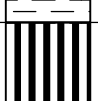
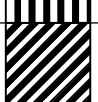
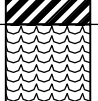
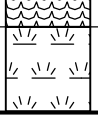
DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS LIQUID LIMIT	ATTERBERG LIMITS PLASTIC LIMIT	ATTERBERG LIMITS PLASTICITY INDEX	FINES CONTENT %)
		SM) dark yellow-brown, moist, me ium stiff.	MC - 1		3-3-3)	1.	100	19	36	26	10	39
		SC) yellow-brown, moist, loose.	MC - 2		2-3-2)		105	11				25
10		Becomes me ium ense.	MC - 3		- - 12 18)		118	10				
		CL) yellow-brown, wet, me ium stiff, with gravel.										
15			MC - 4		- 3-3)							

Bottom of borehole at 1 .0 feet.

Ju icial Council of California (JCC)	New Quincy Courthouse - Potential Site 2
1- 859- PW	70 Main St, Quincy, CA
/ / 23	3418 ft
/ / 23	4"
West Coast Exploration	
Solid Flight	12. ft / Elev 3406. ft
JL / CTD	12. ft / Elev 3406. ft
Elevations from Topo Map by BKF Engineers	---

DEPTH ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	Penetration Rate (sec./ft.)	SPT BLOW COUNTS N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	ATTERBERG LIMITS LIQUID LIMIT	ATTERBERG LIMITS PLASTIC LIMIT	ATTERBERG LIMITS PLASTICITY INDEX	FINES CONTENT %)
		CL) ark brown, moist, medium stiff. EI = 18 @ 2. '	MC - 1		4-3-3)	2.			33	24		
			MC - 2		2-3-3)							
		GM) ILTY GRAVEL with SAND ark brown, moist, medium dense.	MC - 3		8-11-12 23)		122					14
10												
		CL) ellowish-brown, wet, me ium stiff, with gravel. CU @ 14.5': Su = 3.68 ksf	MC - 4		3-3-3)			29				
15												
		SC) ellow-brown, saturated, medium ense.	MC -		- - 12 18)		128					14
20												
		Becomes ense.	MC -		3-18-3 48)							
25												

Bottom of borehole at 2 .0 feet.

MAJOR DIVISIONS					TYPICAL NAMES
COARSE-GRAINED SOILS MORE THAN HALF IS COARSER THAN NO. 200 SIEVE	GRAVELS MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE	CLEAN GRAVELS WITH LESS THAN 15% FINES	GW		WELL-GRADED GRAVELS WITH OR WITHOUT SAND
			GP		POORLY GRADED GRAVELS WITH OR WITHOUT SAND
		GRAVELS WITH 15% OR MORE FINES	GM		SILTY GRAVELS WITH OR WITHOUT SAND
			GC		CLAYEY GRAVELS WITH OR WITHOUT SAND
	SANDS MORE THAN HALF COARSE FRACTION IS FINER THAN NO. 4 SIEVE SIZE	CLEAN SANDS WITH LESS THAN 15% FINES	SW		WELL-GRADED SANDS WITH OR WITHOUT GRAVEL
			SP		POORLY GRADED SANDS WITH OR WITHOUT GRAVEL
		SANDS WITH 15% OR MORE FINES	SM		SILTY SANDS WITH OR WITHOUT GRAVEL
			SC		CLAYEY SANDS WITH OR WITHOUT GRAVEL
FINE-GRAINED SOILS MORE THAN HALF IS FINER THAN NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT 50% OR LESS		ML		INORGANIC SILTS OF LOW TO MEDIUM PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
			CL		INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
			OL		ORGANIC SILTS OR CLAYS OF LOW TO MEDIUM PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
	SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50%		MH		INORGANIC SILTS OF HIGH PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
			CH		INORGANIC CLAYS OF HIGH PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
			OH		ORGANIC SILTS OR CLAYS OF HIGH PLASTICITY WITH OR WITHOUT SAND OR GRAVEL
HIGHLY ORGANIC SOILS			PT		PEAT AND OTHER HIGHLY ORGANIC SOILS

LABORATORY SYMBOLS

AL - ATTERBERG LIMITS
CON - CONSOLIDATION
COR - CORROSIVITY TESTING
DS - DIRECT SHEAR
EI - EXPANSION INDEX
MAX - MAXIMUM DENSITY
RV - R-VALUE
PD - PARTICLE-SIZE DISTRIBUTION
UX - UNIAXIAL COMPRESSIVE STRENGTH
UC - UNCONFINED COMPRESSIVE STRENGTH
UU - UNCONSOLIDATED UNDRAINED
SE - SAND EQUIVALENT
COL - COLLAPSE
CBR - CALIFORNIA BEARING RATIO
CAI - CERCHAR ABRASIVITY
PLSI - POINT LOAD STRENGTH INDEX
WA - No. 200 WASH (% PASSING No. 200 SIEVE)

SAMPLE SYMBOLS

SAMPLE TYPES

Bulk Sample

CAL Modified California Sampler

SPT Standard Penetration Test

GROUNDWATER SYMBOLS

WATER LEVEL AT TIME OF EXCAVATION OR AS INDICATED

WHERE AN ASTERISK * EXISTS NEXT TO RQD VALUE - MEASURED INTACT PIECES DID NOT PASS FIELD SOUNDNESS TEST

RELATIVE DENSITY OF COHESIONLESS SOILS		CONSISTENCY OF COHESIVE SOILS		
RELATIVE DENSITY	SPT N60 BLOWS/FOOT	CONSISTENCY	SPT N60 BLOWS/FOOT	POCKET PENETROMETER MEASUREMENT (TSF)
VERY LOOSE	0 - 4	VERY SOFT	0 - 2	0 - 0.25
LOOSE	5 - 10	SOFT	3 - 4	0.25 - 0.50
MEDIUM DENSE	11 - 30	MEDIUM STIFF	5 - 8	0.50 - 1.0
DENSE	31 - 50	STIFF	9 - 15	1.0 - 2.0
VERY DENSE	OVER 50	VERY STIFF	16 - 30	2.0 - 4.0
		HARD	OVER 30	OVER 4.0

NUMBER OF BLOWS OF 140 LB HAMMER FALLING 30 INCHES TO DRIVE A 2 INCH O.D. (1-3/8 INCH I.D.) SPLIT-BARREL SAMPLER THE LAST 12 INCHES OF AN 18-INCH DRIVE (ASTM-1586 STANDARD PENETRATION TEST).
IF THE SEATING INTERVAL (1st 6 INCH INTERVAL) IS NOT ACHEIVED, N IS REPORTED AS REF.

COPY LEGEND NEW - - 4/18/25 14:23 - C:\USERS\CGARCIA\ONEDRIVE - ONEATLAS\DOCUMENTS\APP-1 238.GPJ

ATLAS
Atlas Technical Consultants LLC
9085 Aero Drive, Suite B
San Diego, California 92123
Telephone: (619) 280-4321

SUBSURFACE EXPLORATION LEGEND

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-7
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	1

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	41.5	3416

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING 10.00 ft / Elev 3406.00 ft

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
3415	0						**2 Inches of Asphalt Concrete (AC).** PID: 5.6ppm	
							FILL (Af): CLAYEY SAND with GRAVEL (SC); medium dense, brown, moist, fine to coarse grained.	
			CAL	18			PID: 31.3ppm	
	5						**QUATERNARY LAKE DEPOSITS (Ql):** CLAYEY SAND (SC); medium dense, brown, moist, fine to coarse grained, few GRAVEL. PID: 52.5 ppm	
3410			SPT	11				
			CAL	9			Loose, trace GRAVEL. PID: 10.0 ppm	PD
	10						▼	
3405			SPT	10			PID: 10.6 ppm	
							Poorly graded GRAVEL with SAND and CLAY (GP-GC); loose, brown, wet, fine to coarse grained.	
	15							
3400			SPT	6			PID: 1.9 ppm	PD
	20							
3395			SPT	13			SANDY SILT with GRAVEL (ML); loose, brown, moist, fine to medium grained. PID: 2.9 ppm	

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-1

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-7
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	2

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	41.5	3416

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING 10.00 ft / Elev 3406.00 ft

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
							SANDY SILT with GRAVEL (ML); loose, brown, moist, fine to medium grained. *(continued)*	
							CLAYEY SAND with GRAVEL (SC); medium dense, brown, wet, fine to coarse grained.	
	25							
3390			CAL	24			PID: 11.1 ppm	
	30							
3385			SPT	32			Dense.	PD
							SANDY lean CLAY with GRAVEL (CL) moderately bedded with thin interbeds of SANDY SILT (ML); very stiff, brown, moist, fine to coarse grained.	
	35							
3380			SPT	21			PID: 2.00 ppm PP = 3.00 tsf	
							CLAYEY GRAVEL with SAND (GC); medium dense, brown, wet, fine to coarse grained.	
	40							
3375			SPT	20			PID: 6.3 ppm	

BORING TERMINATED AT 41.5 FEET BGS.
GROUNDWATER ENCOUNTERED AT 10 FEET BGS.

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure
I-2

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-8
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	3

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	41.5	3418

DEPTH/ELEV. GROUND WATER (ft)
- AT TIME OF DRILLING ---
- AT END OF DRILLING ---
- AFTER DRILLING 16.00 ft / Elev 3402.00 ft

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	MOISTURE (%)	DRY DENSITY (pcf)	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
									2 Inches of Asphalt Concrete (AC). PID: 5.6ppm	
									FILL (Af): CLAYEY SAND with GRAVEL (SC); medium dense, brown, moist, fine to coarse grained.	RV COR
3415			CAL	13					PID: 9.5 ppm	
	5								SILTY GRAVEL with SAND (GM); medium dense, brown, moist, fine to coarse grained.	
			CAL	22					PID: 4.3 ppm	
									QUATERNARY LAKE DEPOSITS (Ql): SANDY SILT (ML); loose, grayish brown, moist, fine to medium grained.	
3410			SPT	7					PID: 4.5 ppm	AL
	10								PID: 5.8 ppm	
			CAL	18		15.0	113.2		SILTY SAND with GRAVEL (SM), medium dense, brown, moist, fine to medium grained. UU at 10 feet; Su = 2030 psf.	UU PD
3405										
	15								Loose, no GRAVEL, wet. PID: 8.7 ppm	
			SPT	8						
3400										
	20								SANDY SILT (ML); loose, grayish brown, moist, fine to medium grained.	
			CAL	13		22.6	106.6		PID: 3.0 ppm UU at 20 feet; Su = 1525 psf.	UU PD

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-3

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-8
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	4

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	41.5	3418

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING 16.00 ft / Elev 3402.00 ft

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	MOISTURE (%)	DRY DENSITY (pcf)	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
3395									SANDY SILT (ML); loose, grayish brown, moist, fine to medium grained. *(continued)*	
	25		SPT	6					LEAN CLAY with SAND (CL); medium stiff, brown, saturated, fine grained, trace GRAVEL. PP: 0.50 tsf PID: 11.3 ppm	
3390										
	30		CAL	13					No recovery.	
3385										
	35		SPT	17					SANDY SILT (ML); medium dense, brown, saturated, fine grained. PID: 2.5 ppm	
3380										
	40		CAL	19					CLAYEY GRAVEL with SAND (GC); medium dense, brown, wet, fine to coarse grained. PID: 2.0 ppm	
3375									**BORING TERMINATED AT 41.5 FEET BGS.** GROUNDWATER ENCOUNTERED AT 16 FEET BGS.	

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-4

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-9
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	5

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	11.5	3414

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING ---

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
							4 Inches of grass (topsoil).	
							FILL (Af): SILTY SAND with GRAVEL (SM); medium dense, reddish brown, dry, fine to coarse grained, trace CLAY.	WA
			CAL	21			PID: 56.4 ppm	
3410	5							
			SPT	12			PID: 31.1 ppm	
							CLAYEY SAND (SC); medium dense, reddish brown, dry, fine to coarse grained	
			CAL	15			PID: 28.3 ppm	
3405	10						**QUATERNARY LAKE DEPOSITS (Ql):** SANDY SILT with GRAVEL (ML); loose, brown, moist, fine to coarse grained.	
			SPT	6			PID: 1.6 ppm	
							BORING TERMINATED AT 11.5 FEET BGS. NO GROUNDWATER ENCOUNTERED.	
3400	15							
3395	20							

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-5

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-10
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	6

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	11.5	3415

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING ---

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
							2 Inches of Aggregate Base Course (ABC).	
							FILL (Af): CLAYEY SAND with GRAVEL (SC); medium dense, dark gray, moist, fine to medium grained.	PD MAX
			CAL	26			PID: 5.4 ppm	
3410	5						**QUATERNARY LAKE DEPOSITS (Ql):** SANDY SILT (ML); loose, dark gray to black, moist, fine to medium grained.	
			SPT	5			PID: 13.5 ppm	COR
			CAL	8			Dark black to mottled grayish brown, fine to coarse grained, trace GRAVEL. PID: 9.7 ppm	
3405	10						Mottled grayish brown.	
			SPT	4			PID: 31.3 ppm	
							BORING TERMINATED AT 11.5 FEET BGS. NO GROUNDWATER ENCOUNTERED.	
3400	15							
3395	20							

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-6

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

BORING RECORD

ATLAS PROJECT NAME	ATLAS PROJECT NUMBER	B-11
Quincy Courthouse	91-65859-PW	

SITE	START	END	SHEET NO.
253, 287, and 295 Lawrence Street, Quincy, California	9/17/25	9/17/25	7

DRILLING COMPANY	DRILL METHOD	LOGGED BY	REVIEWED BY
West Coast Drilling	Solid Stem Auger	KH	JF/DS

DRILLING EQUIPMENT	BORING DIA. (in.)	TOTAL DEPTH (ft)	GROUND ELEV. (ft)
Truck-Mounted Modified B-24	4	11.5	3416

DEPTH/ELEV. GROUND WATER (ft)
- ▽ AT TIME OF DRILLING ---
- ▼ AT END OF DRILLING ---
- ▼ AFTER DRILLING ---

SAMPLING METHOD: Rope and Cathead, 30-in Drop

NOTES: Elevations approximated using Topographic Map (BKF, 2023)

ELEVATION (ft)	DEPTH (ft)	BULK SAMPLE	DRIVE SAMPLE	BLOWS PER FOOT	N_{60}	MOISTURE (%)	DRY DENSITY (pcf)	GRAPHIC LOG	DESCRIPTION AND CLASSIFICATION	LAB TESTS
3415	0								**2 Inches of Asphalt Concrete (AC).** PID: 5.6ppm	
									FILL (Af): CLAYEY SAND with GRAVEL (SC); light brown, moist, fine to coarse grained.	EL
			SPT	4					**QUATERNARY LAKE DEPOSITS (Qal):** SANDY SILT (ML); very loose, black, moist, fine to medium grained, trace GRAVEL. PID: 14.2 ppm	AL
	5									
3410			CAL	10		35.6	83.0		Loose. PID: 9.6 ppm	
			SPT	6					Brown. PID: 4.2 ppm	
	10									
3405			SPT	7					PID: 11.8 ppm	
									BORING TERMINATED AT 11.5 FEET BGS. NO GROUNDWATER ENCOUNTERED.	
	15									
3400										
	20									
3395										

ATLAS

THIS SUMMARY APPLIES ONLY AT THE LOCATION OF THIS BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THIS LOCATION WITH THE PASSAGE OF TIME. THE DATA PRESENTED IS A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

Figure

I-7

BRIGHTLINE WITH ROD AND REC - - 10/22/25 15:11 - \\SD.SCST.COM\DFS_ROOT\CLIENTS\GEOSPHERE CONSULTANTS, INC (ATLAS)\18077.000 - GEOSPHERE LEGACY MASTER AGREEMENT\18077.000 - QUINCY COURTHOUSE\REPORTS\-1, PHASE II G\APP I - LO

APPENDIX II
CPT LOGS

Atlas Technical Consultants

https://www.oneatlas.com/

CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

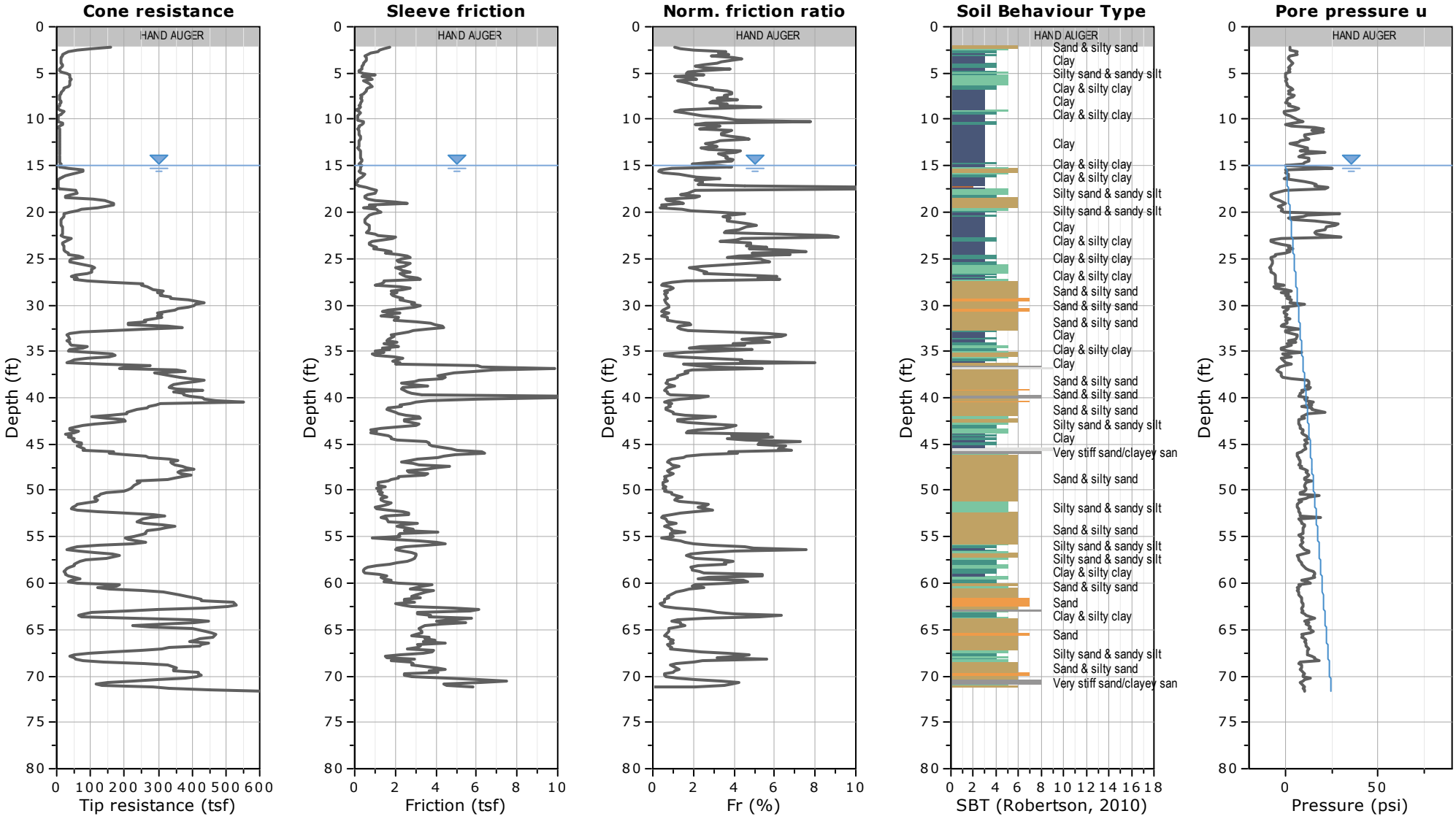
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

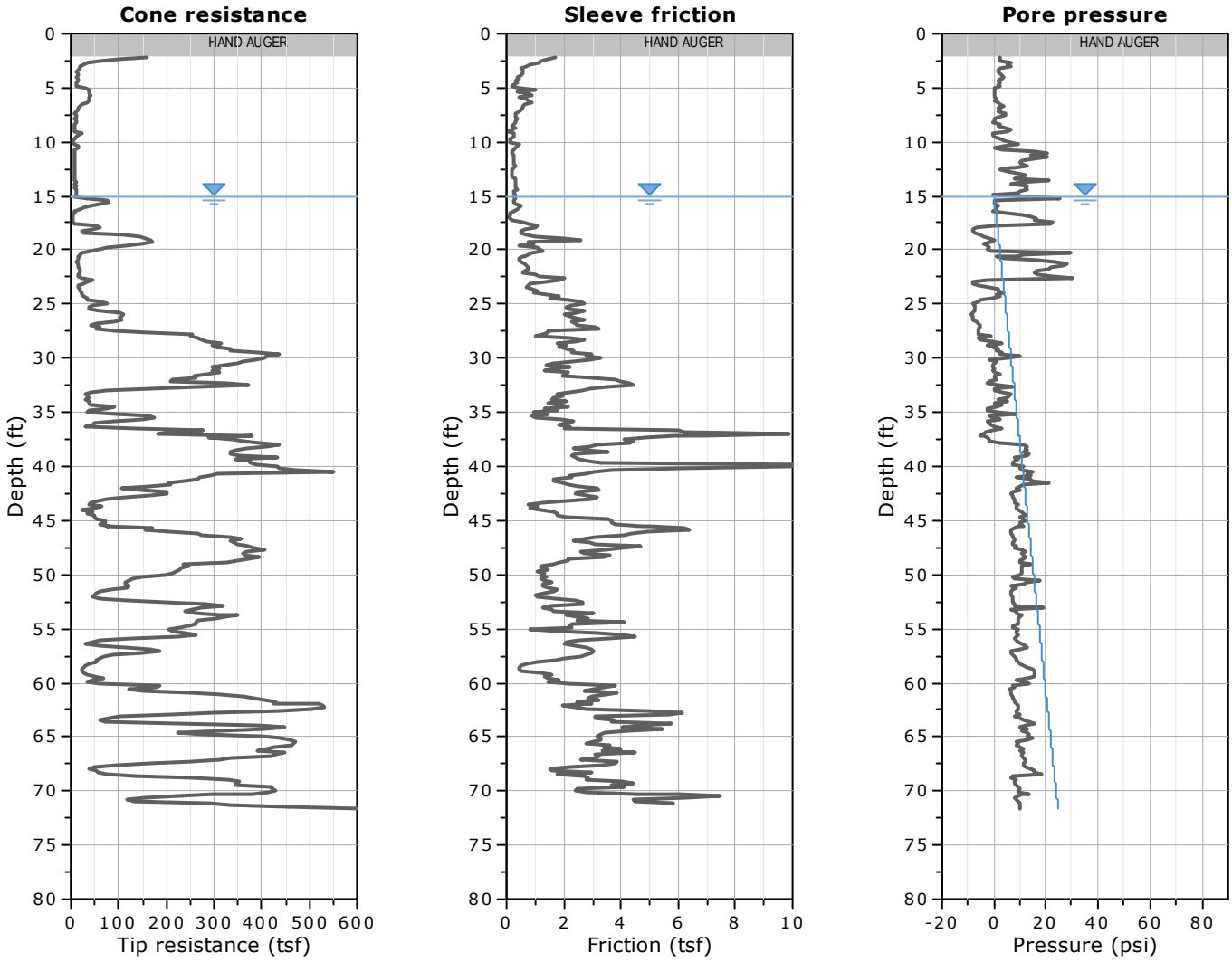
Est. GWL: 15.00 ft

Cone Type: 15cm²

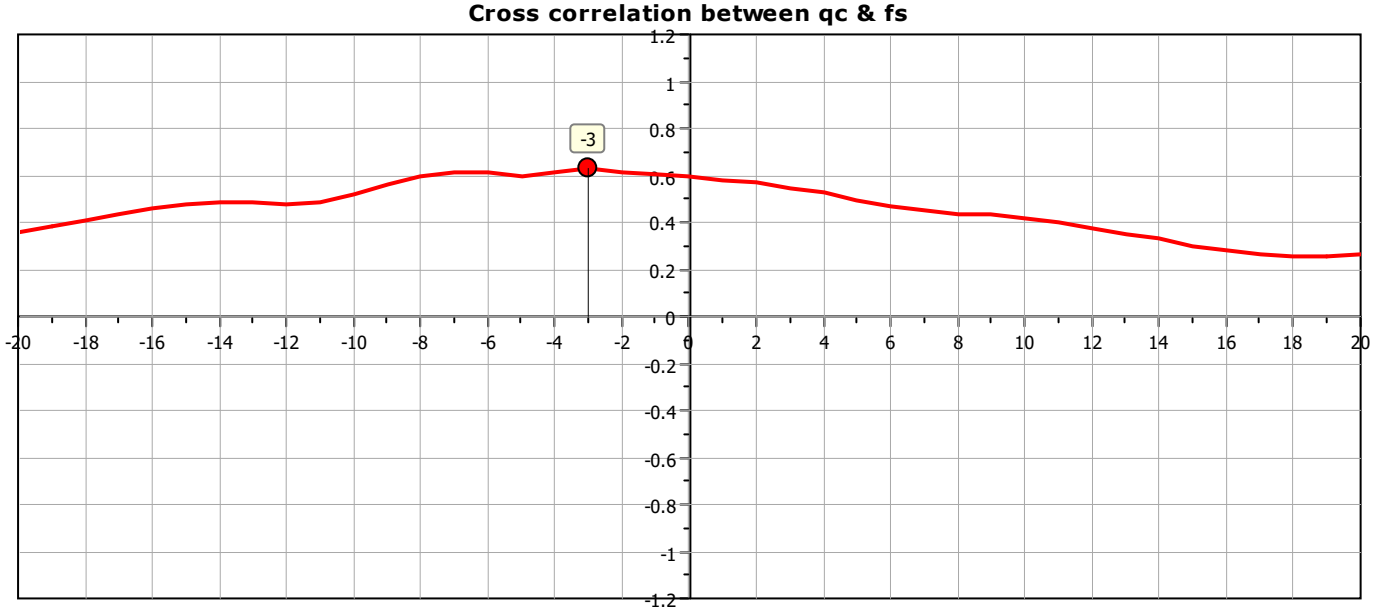
Cone Operator: JM-IY

Project: **Quincy Courthouse**

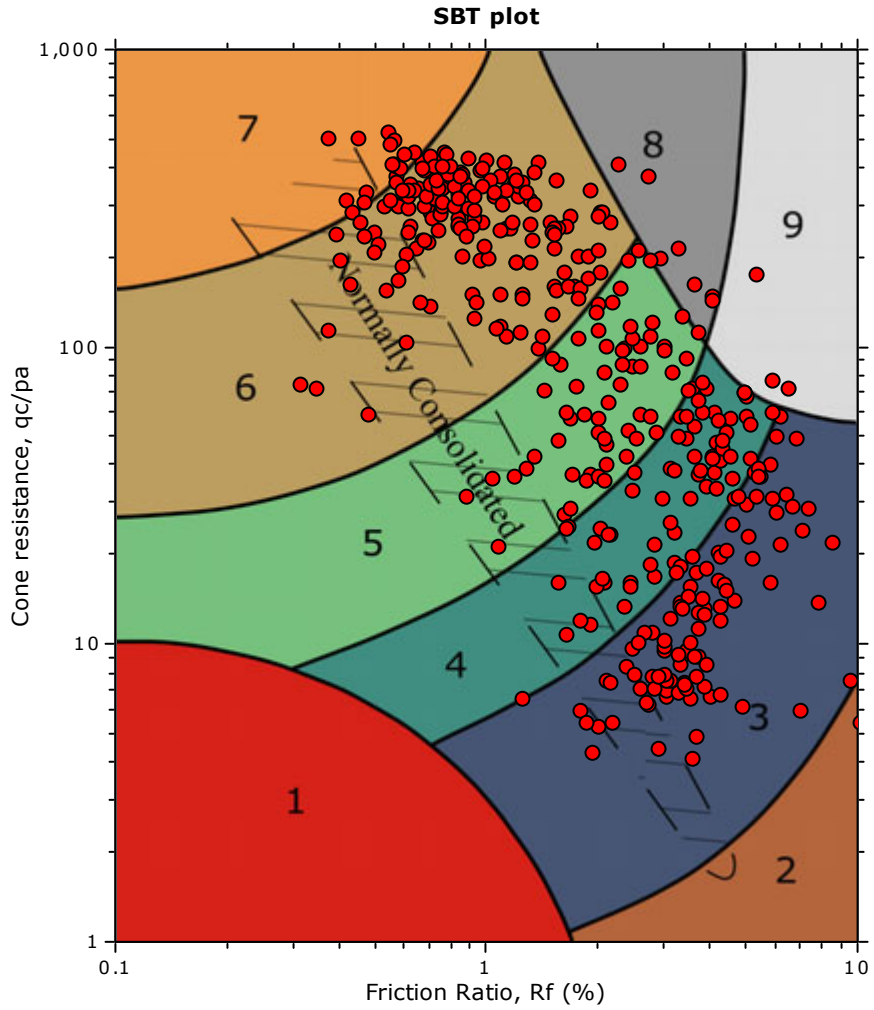
Location: **257 Lawrence Street, Quincy, CA 95971**

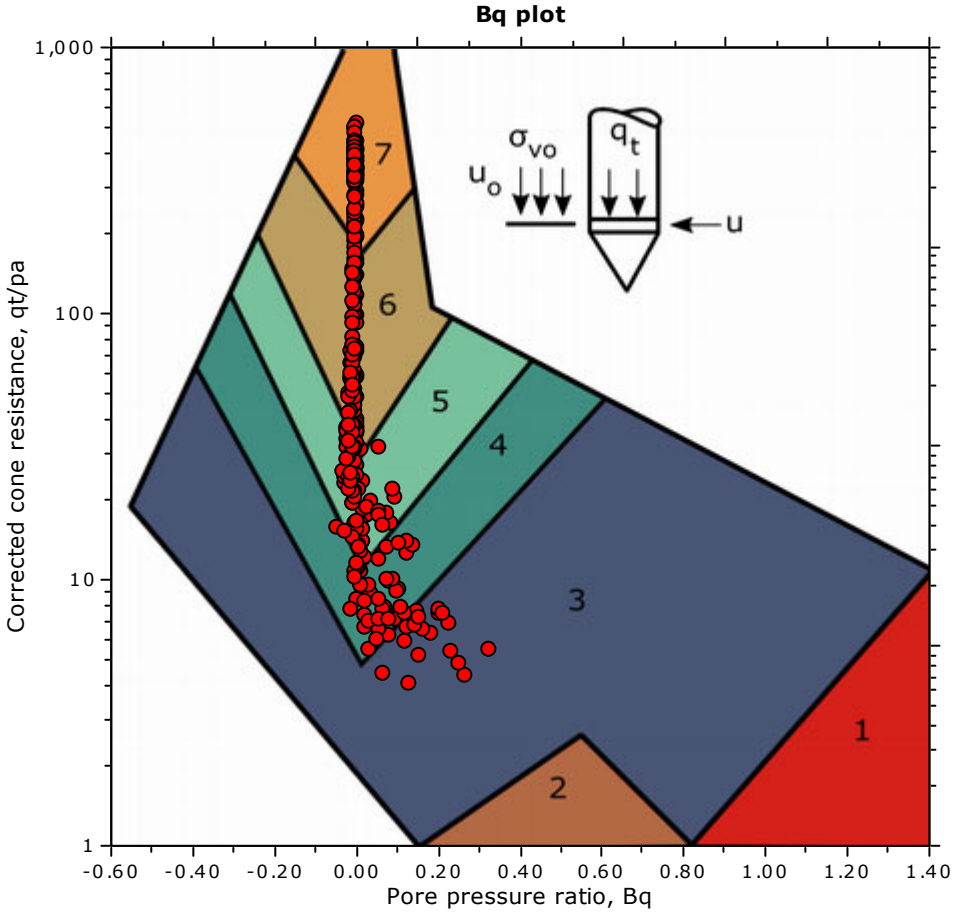


The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



SBT - Bq plots

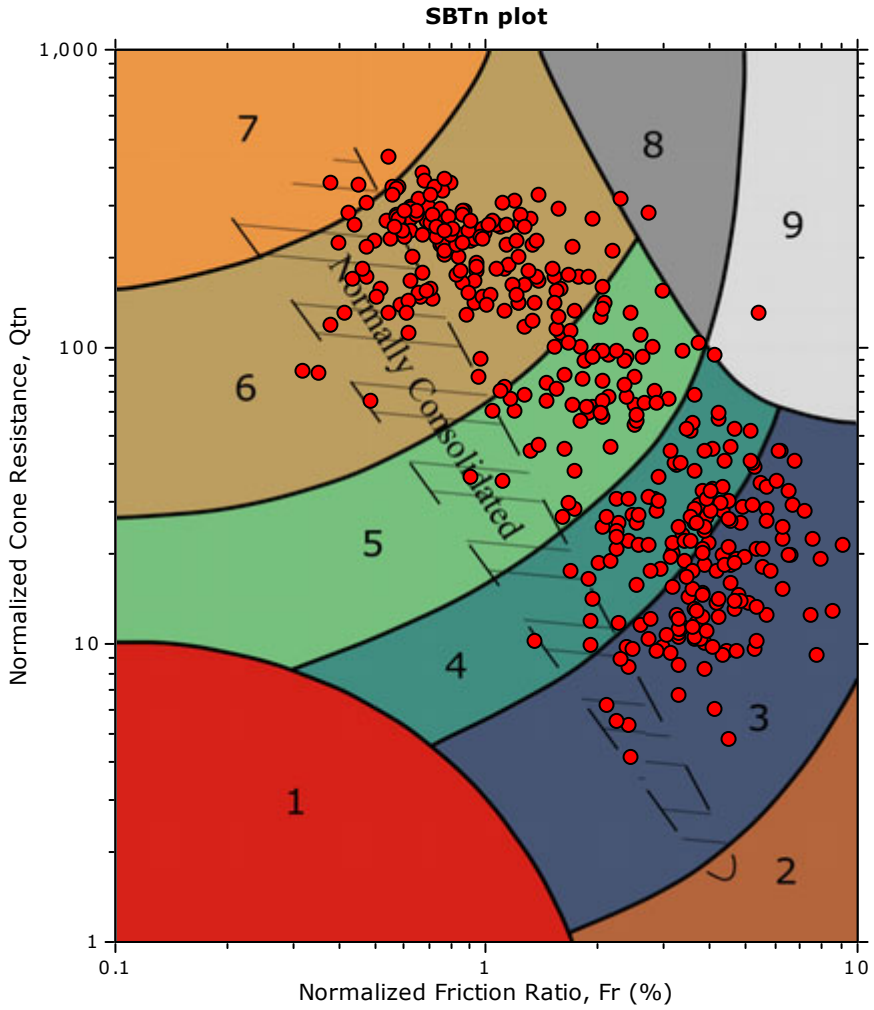


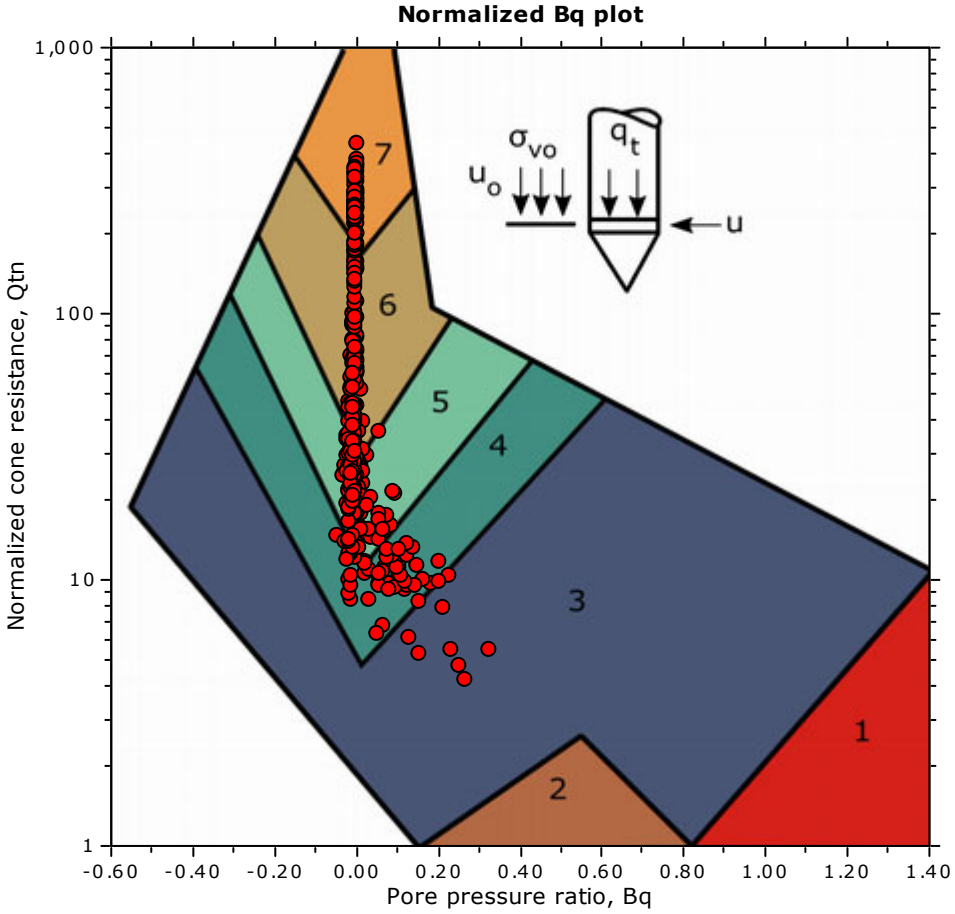


SBT legend

1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

SBT - Bq plots (normalized)

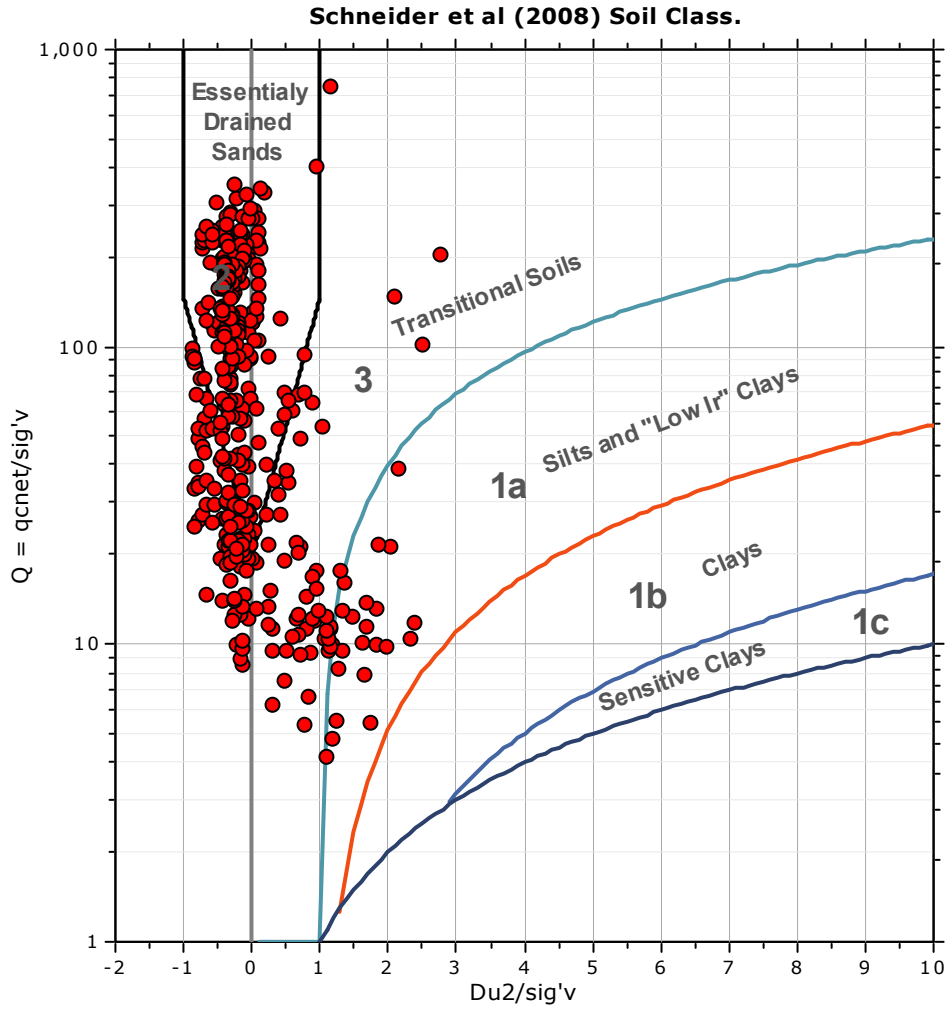


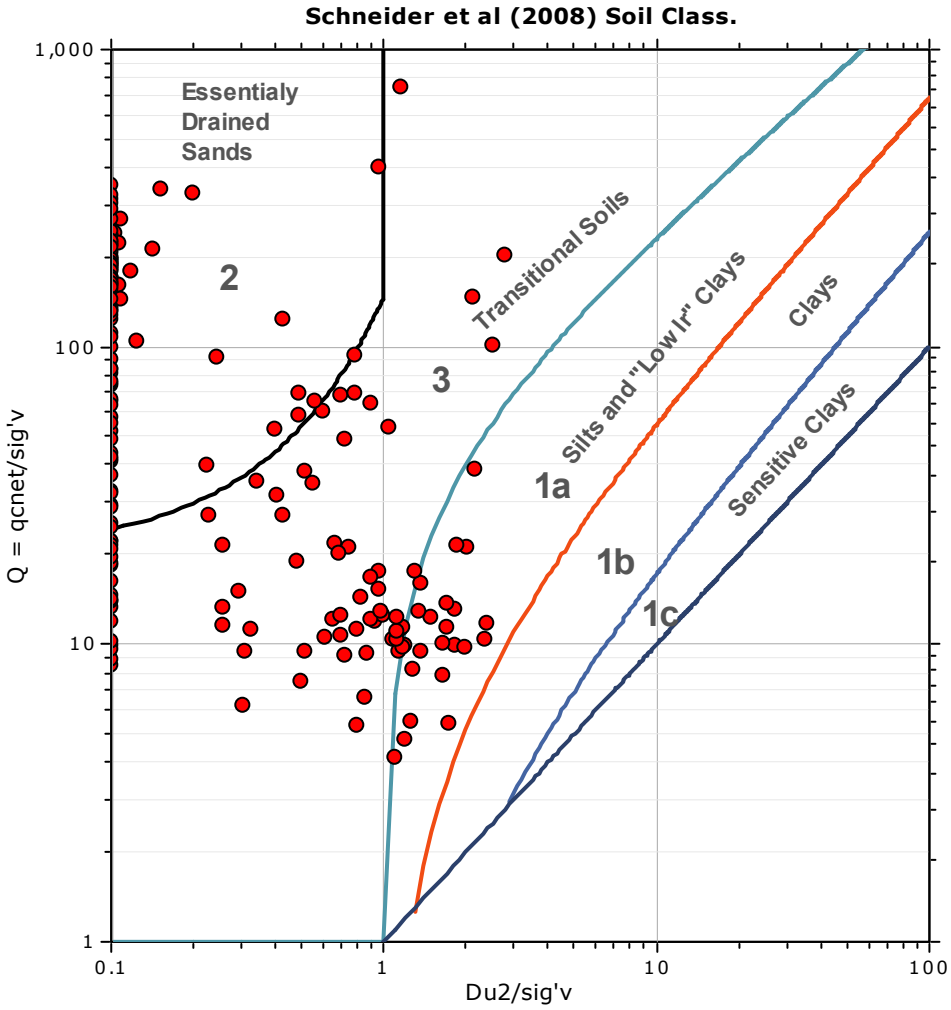


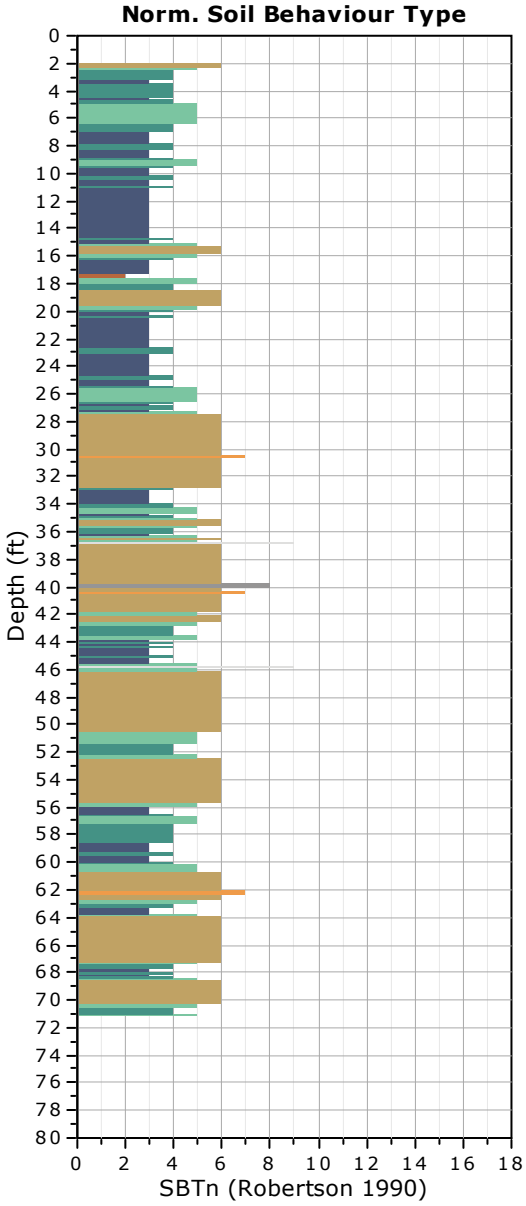
SBTn legend

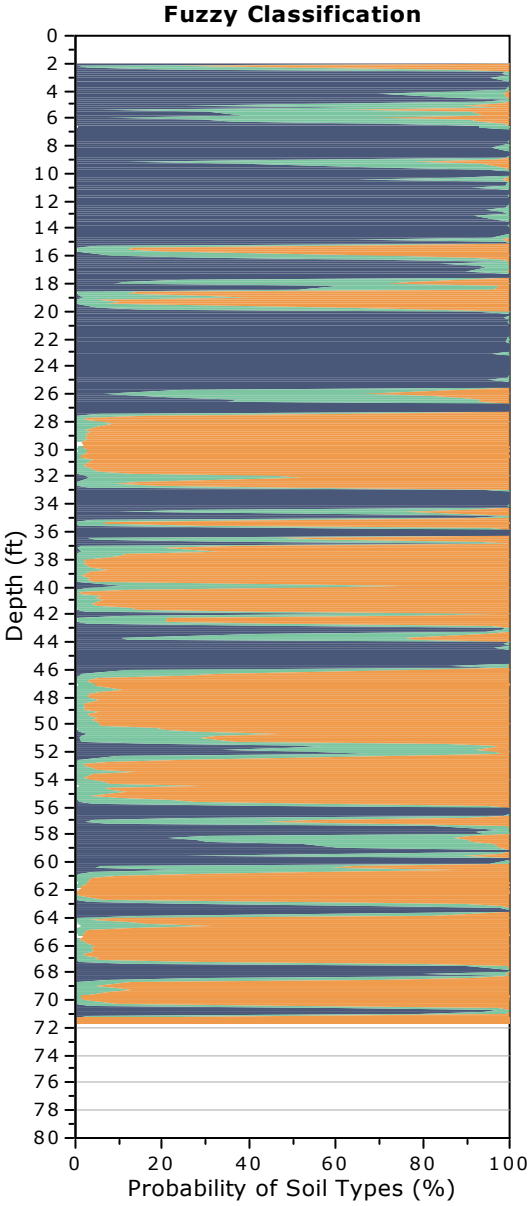
1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

Bq plots (Schneider)









Fuzzy classifiaction legend

- Highly probable clayey soil
- Highly probable mixture soil
- Highly probable sandy soil

CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

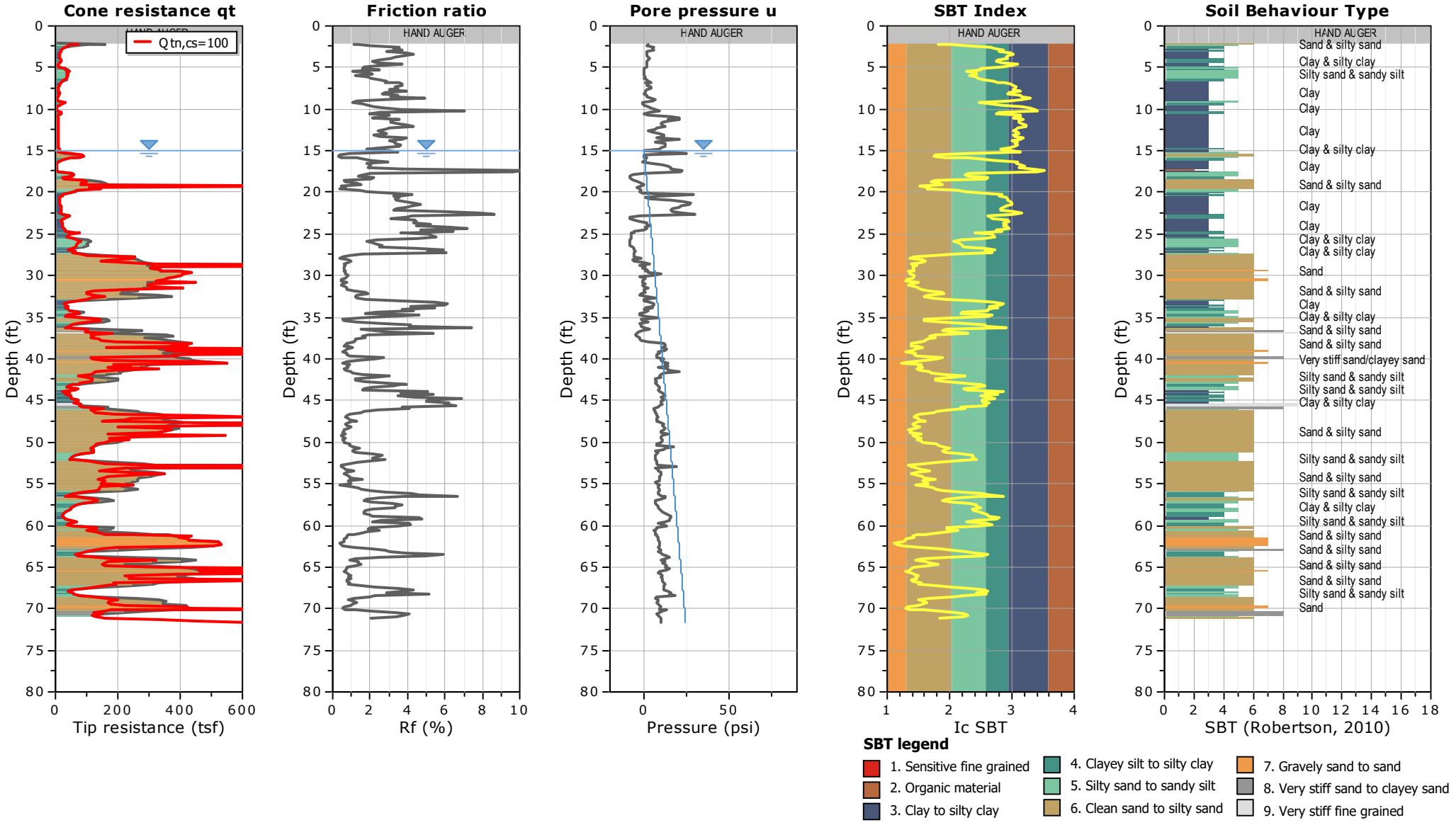
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

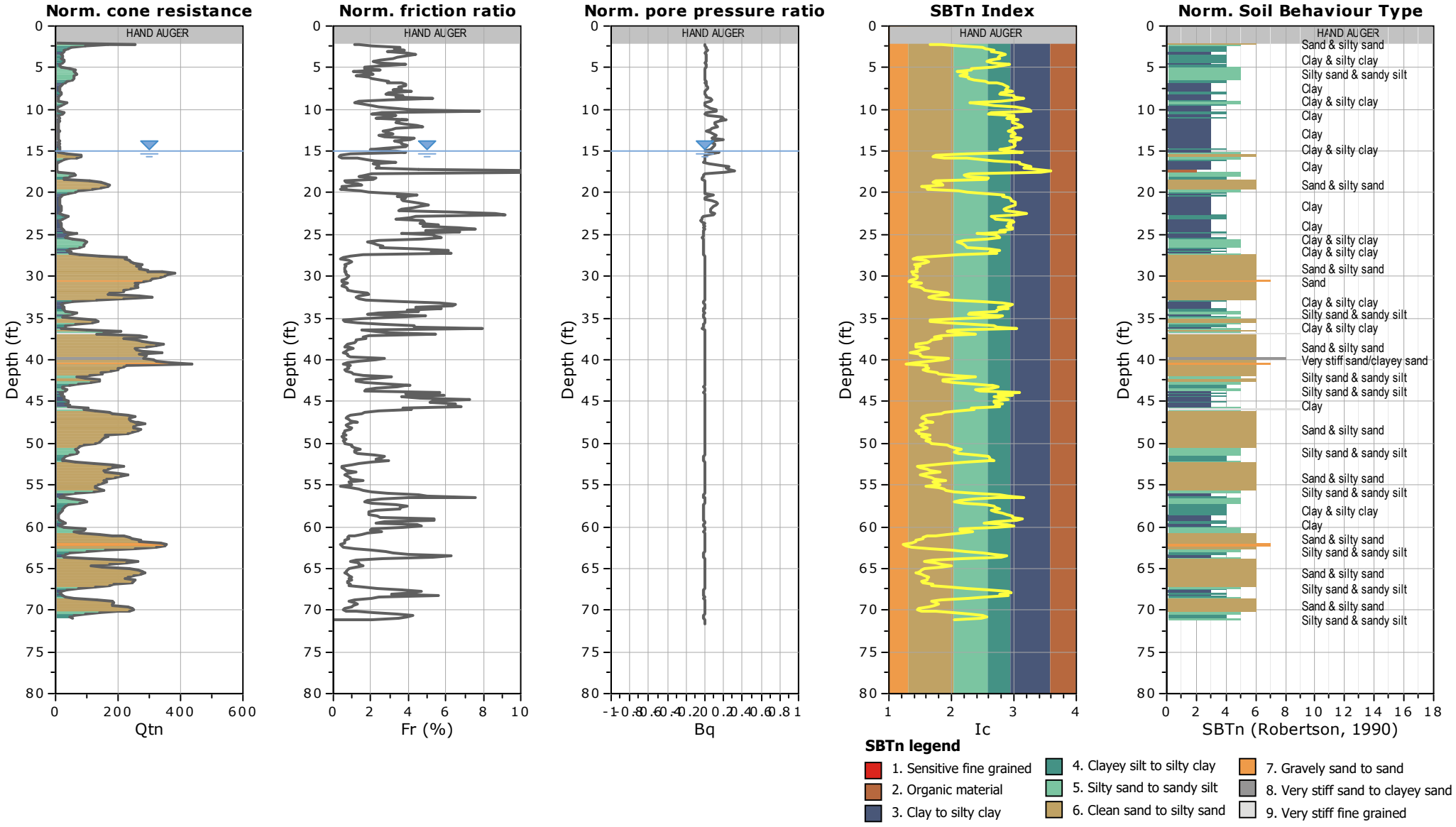
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

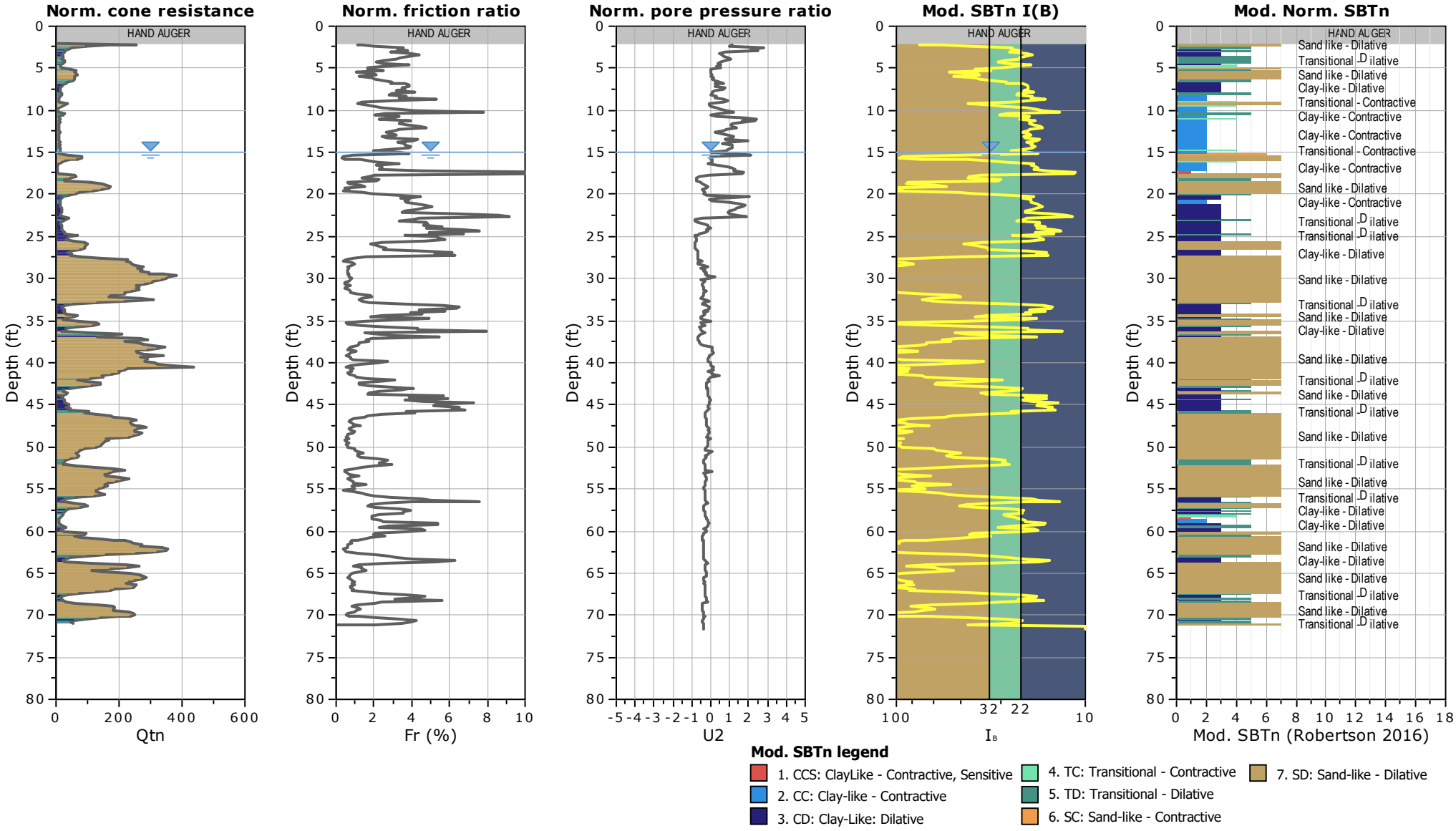
Est. GWL: 15.00 ft

Cone Type: 15cm²

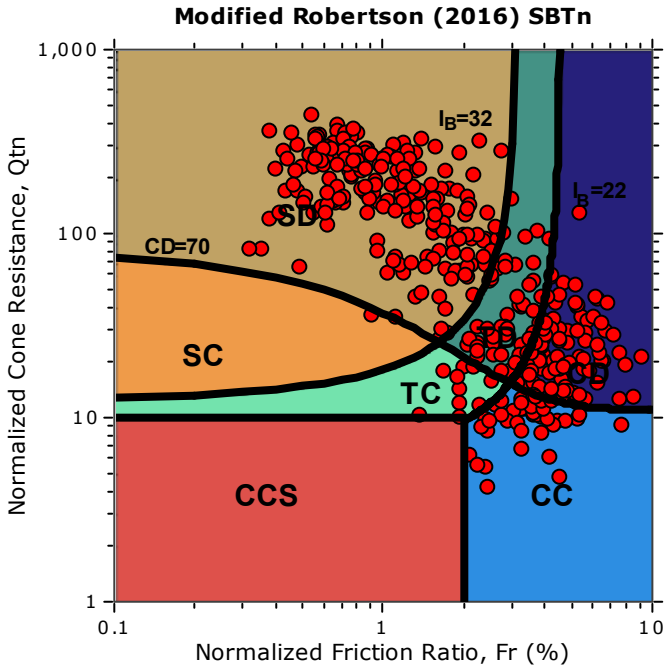
Cone Operator: JM-IY

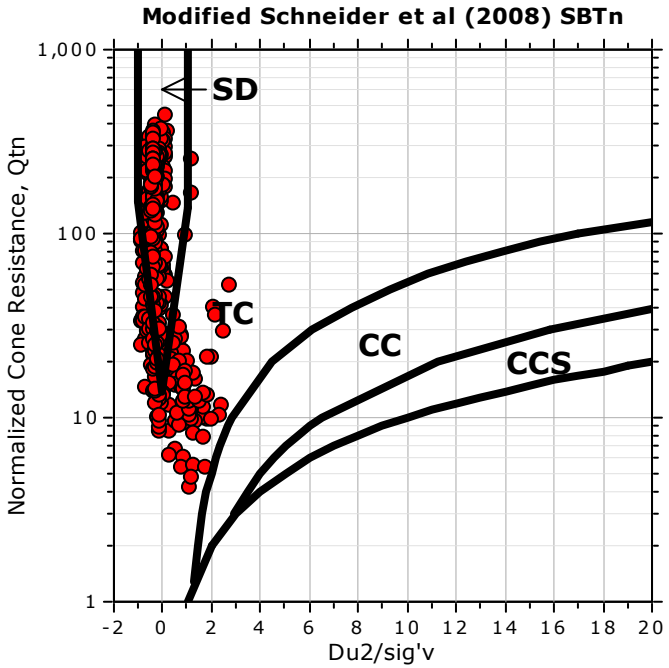
Project: Quincy Courthouse

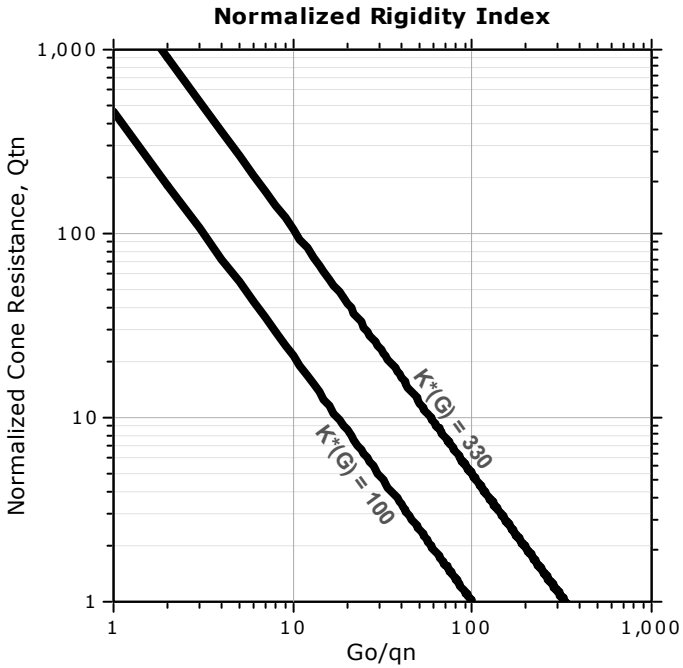
Location: 257 Lawrence Street, Quincy, CA 95971



Updated SBTn plots

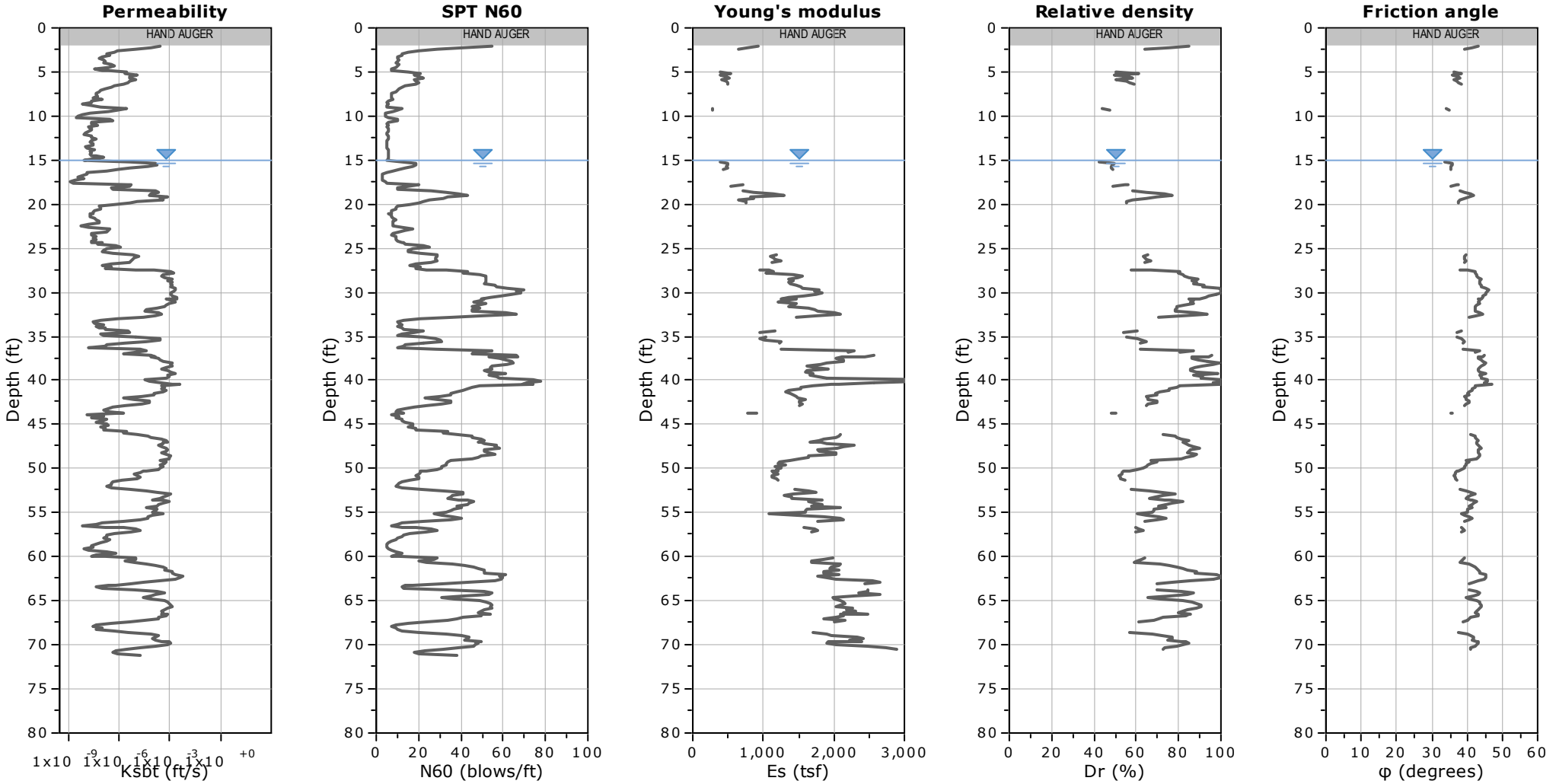






CCS: Clay-like - Contractive - Sensitive
CC: Clay-like - Contractive
CD: Clay-like - Dilative
TC: Transitional - Contractive
TD: Transitional - Dilative
SC: Sand-like - Contractive
SD: Sand-like - Dilative

K(G) > 330: Soils with significant microstructure (e.g. age/cementation)



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative density constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)

CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

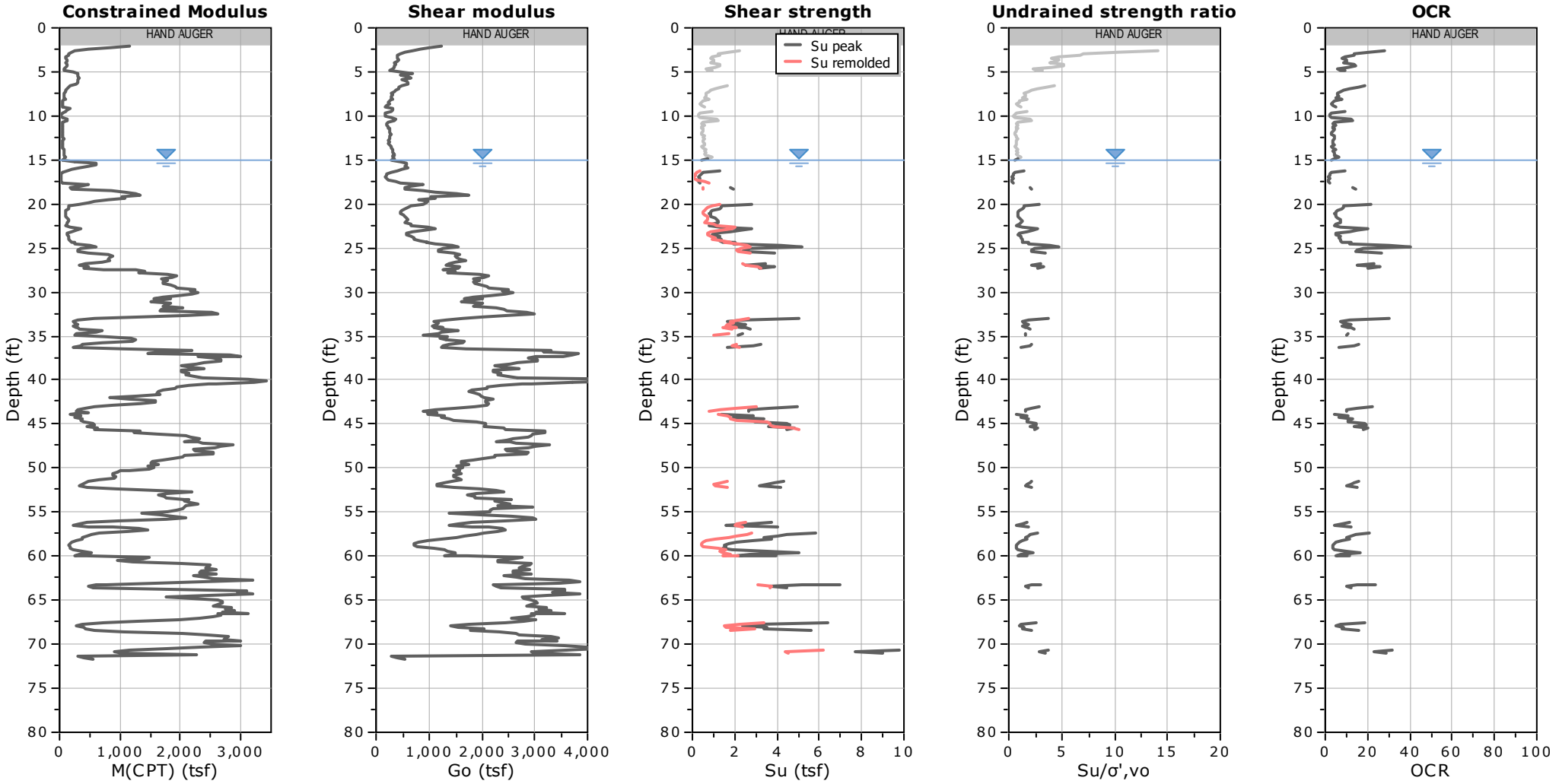
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)

Go: Based on variable *alpha* using I_c (Robertson, 2009)

Undrained shear strength cone factor for clays, N_{kt}: Auto

OCR factor for clays, N_{kt}: Auto

Flat Dilatometer Test data

CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

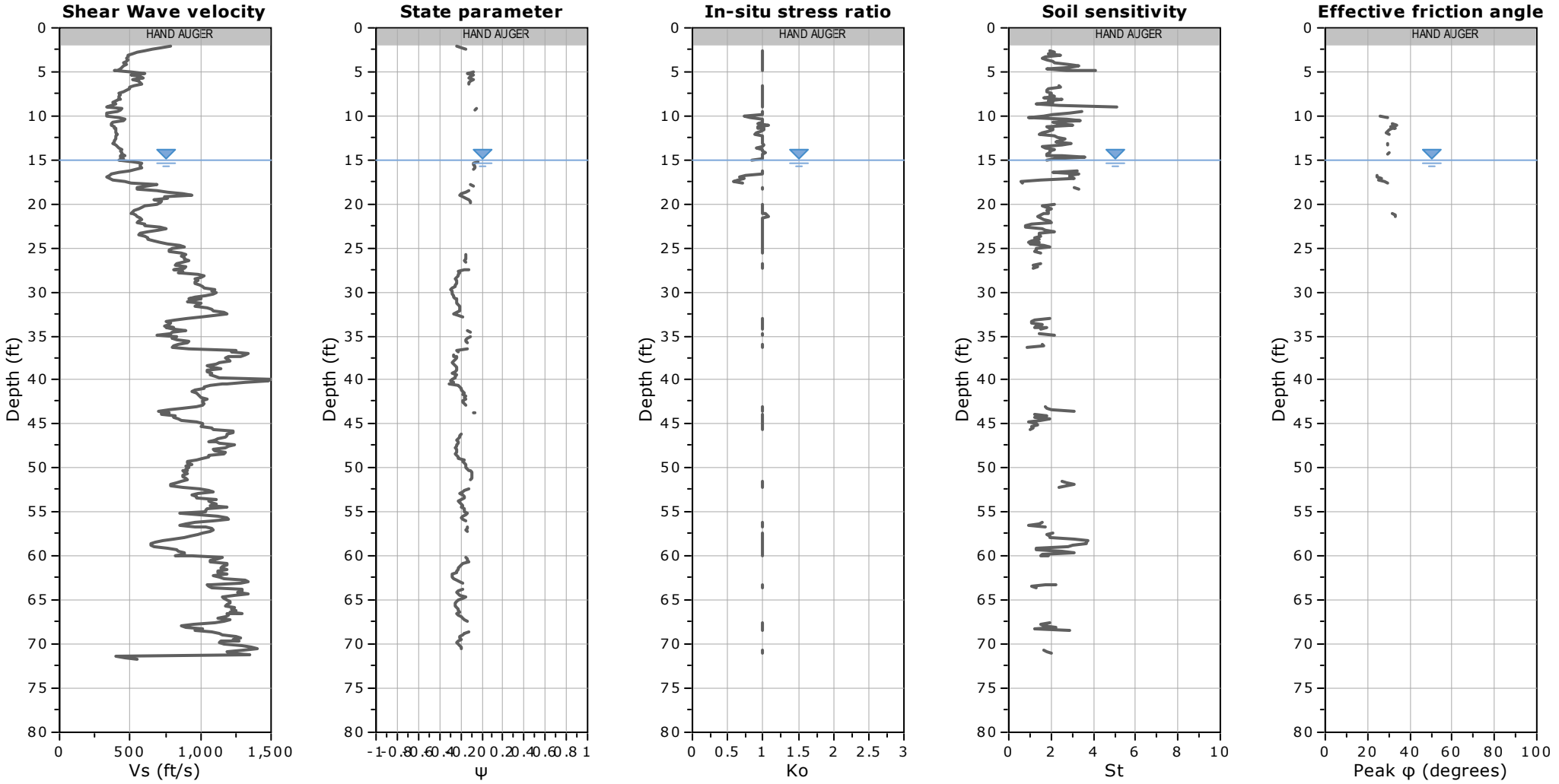
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

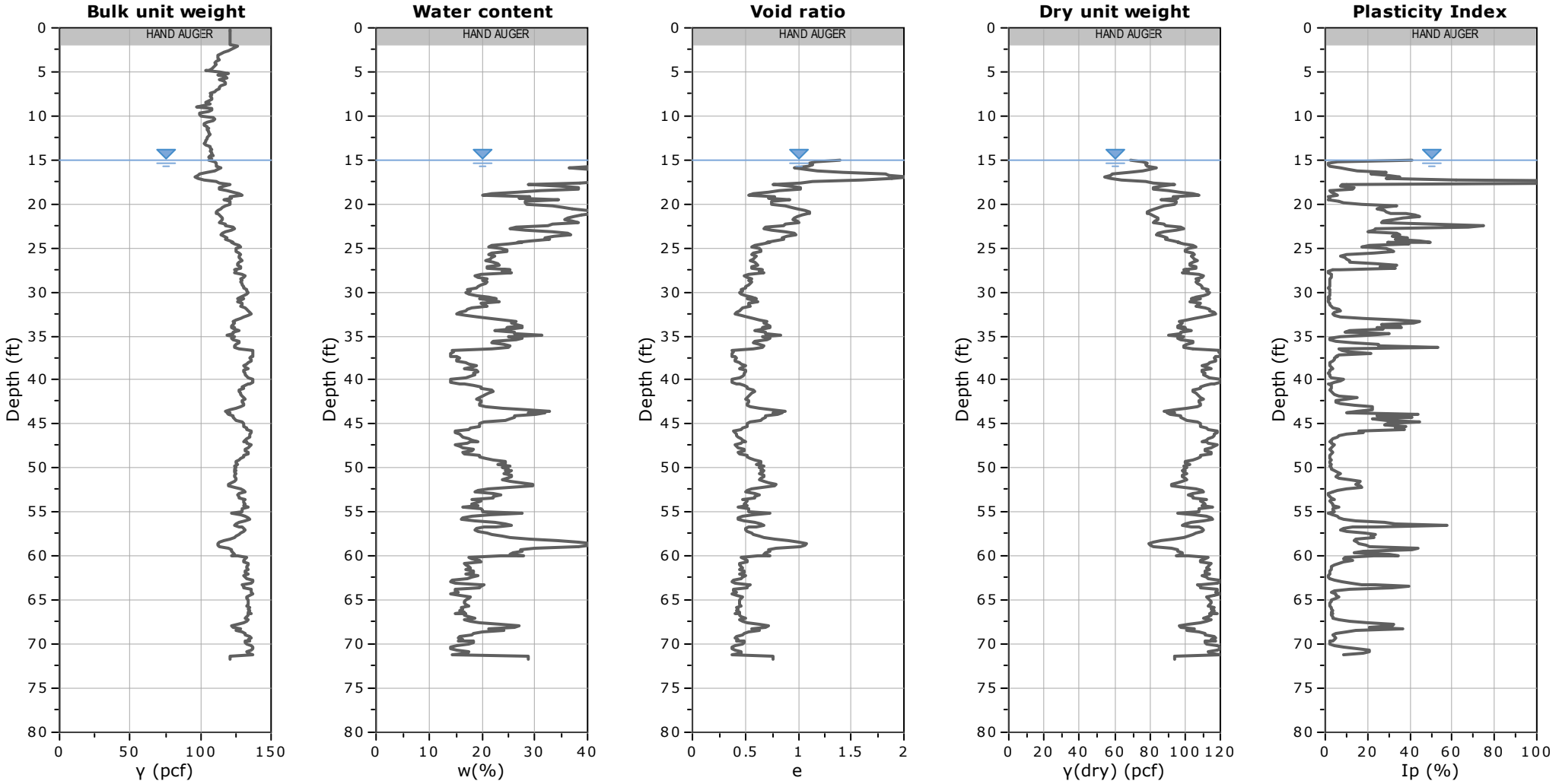
Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Soil Sensitivity factor, N_S: 7.00


Bulk unit weight
Water content
Void ratio
Dry unit weight
Plasticity Index
HAND AUGER
Depth (ft)
γ (pcf)
w(%)
e
γ(dry) (pcf)
Ip (%)

CPT: CPT-01

Total depth: 71.69 ft, Date: 9/16/2025

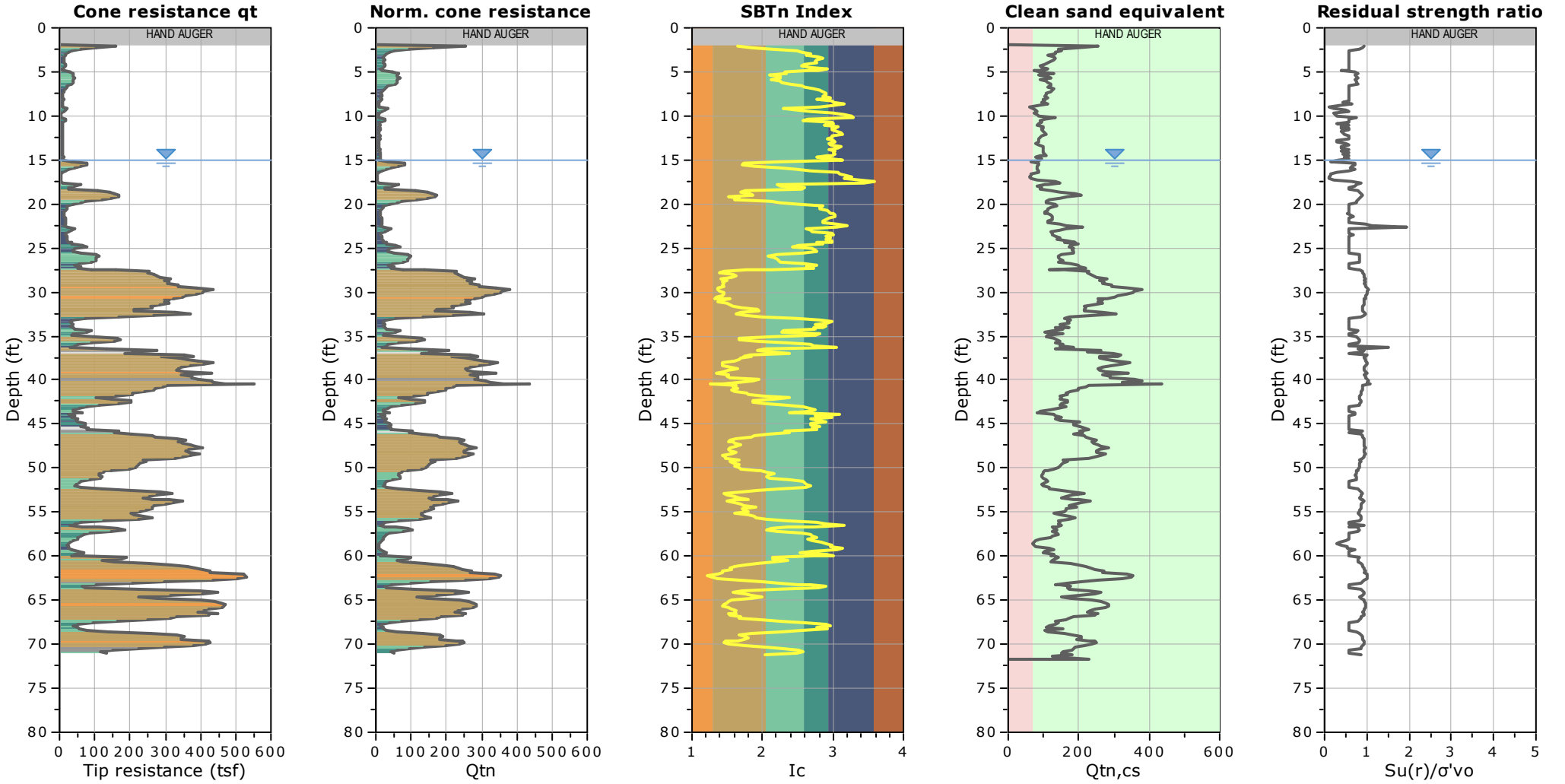
Est. GWL: 15.00 ft

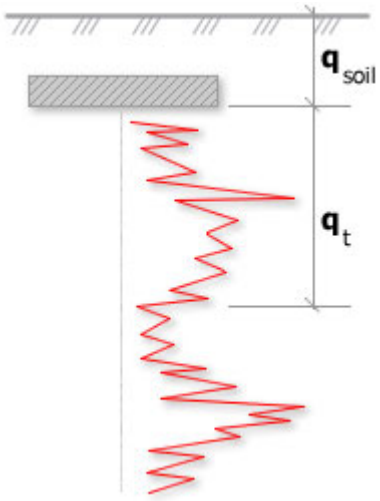
Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971

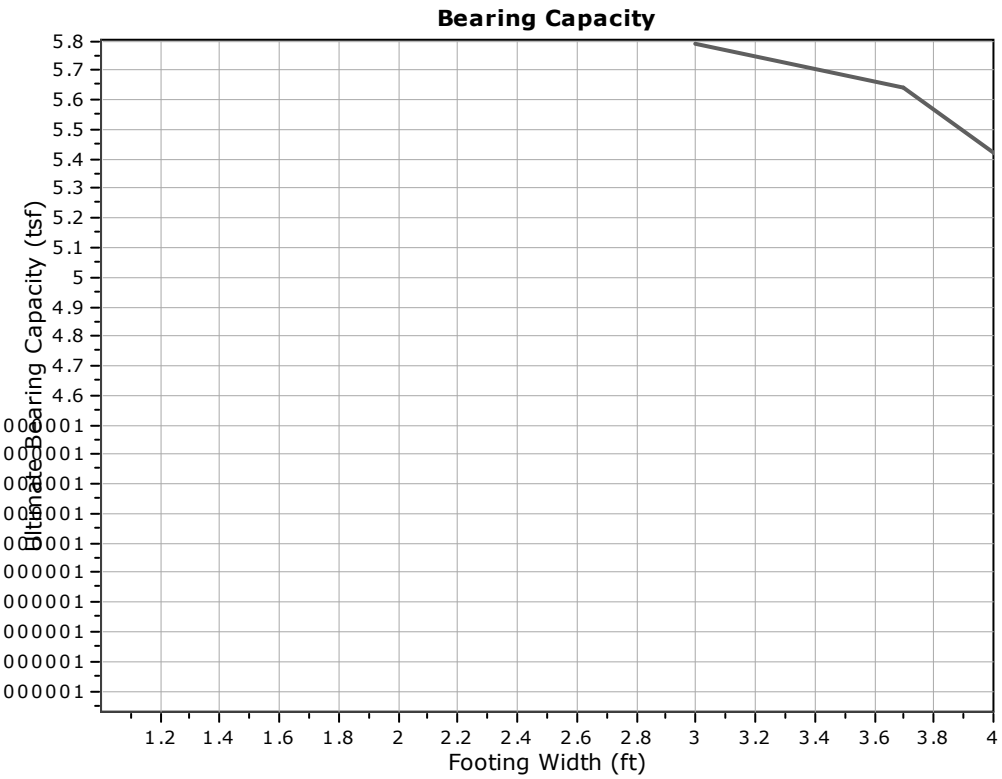




Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (ft)	Start Depth (ft)	End Depth (ft)	Ave. q_t (tsf)	R_k	Soil Press. (tsf)	Ult. bearing cap. (tsf)
1	3.00	1.60	6.10	28.47	0.20	0.10	5.79
2	3.70	1.60	7.15	27.73	0.20	0.10	5.64
3	4.40	1.60	8.20	25.17	0.20	0.10	5.13
4	5.10	1.60	9.25	22.93	0.20	0.10	4.68
5	5.80	1.60	10.30	21.32	0.20	0.10	4.36
6	6.50	1.60	11.35	20.00	0.20	0.10	4.10
7	7.20	1.60	12.40	18.89	0.20	0.10	3.87
8	7.90	1.60	13.45	18.00	0.20	0.10	3.70
9	8.60	1.60	14.50	17.23	0.20	0.10	3.54
10	9.30	1.60	15.55	17.79	0.20	0.10	3.65
11	10.00	1.60	16.60	19.02	0.20	0.10	3.90
12	10.70	1.60	17.65	18.21	0.20	0.10	3.74
13	11.40	1.60	18.70	20.21	0.20	0.10	4.14
14	12.10	1.60	19.75	27.69	0.20	0.10	5.63
15	12.80	1.60	20.80	27.80	0.20	0.10	5.66

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236 \right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a} \right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$

(applicable only to $I_c < I_{c_cutoff}$)

:: Relative Density, Dr (%) ::

$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$ (applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: State Parameter, ψ ::

$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$

:: Drained Friction Angle, φ (°) ::

$\varphi = \varphi'_{cv} + 15.94 \cdot \log(Q_{tn,cs}) - 26.88$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$
$\alpha = 14$ for $Q_{tn} > 14$
$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$
$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \geq 2.20$

$M_{CPT} = 0.03 \cdot (q_t - \sigma_v) \cdot 10^{0.55 \cdot I_c + 1.68}$

:: Small strain shear Modulus, Go (MPa) ::

$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho} \right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))} \right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: In situ Stress Ratio, Ko ::

$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Peak Friction Angle, φ' (°) ::

$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$

(applicable for $0.10 < B_q < 1.00$)

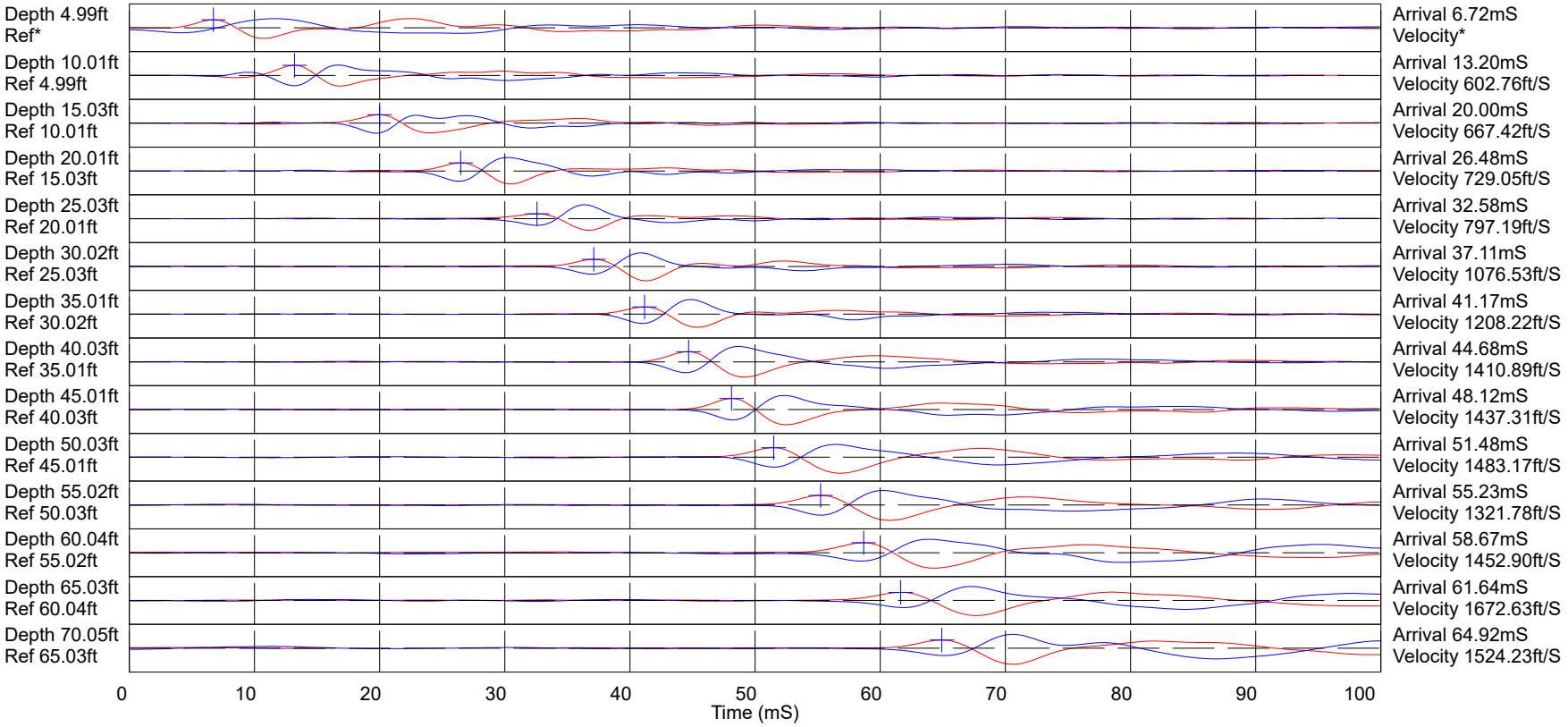
References

• Robertson, P.K., Cabal K.L., Guide to Cone Penetration Testing for Geotechnical Engineering, Gregg Drilling & Testing, Inc., 5th Edition, November 2012

• Robertson, P.K., Interpretation of Cone Penetration Tests - a unified approach., Can. Geotech. J. 46(11): 1337–1355 (2009)

• N Barounis, J Philpot, Estimation of in-situ water content, void ratio, dry unit weight and porosity using CPT for saturated sands, Proc. 20th NZGS Geotechnical Symposium

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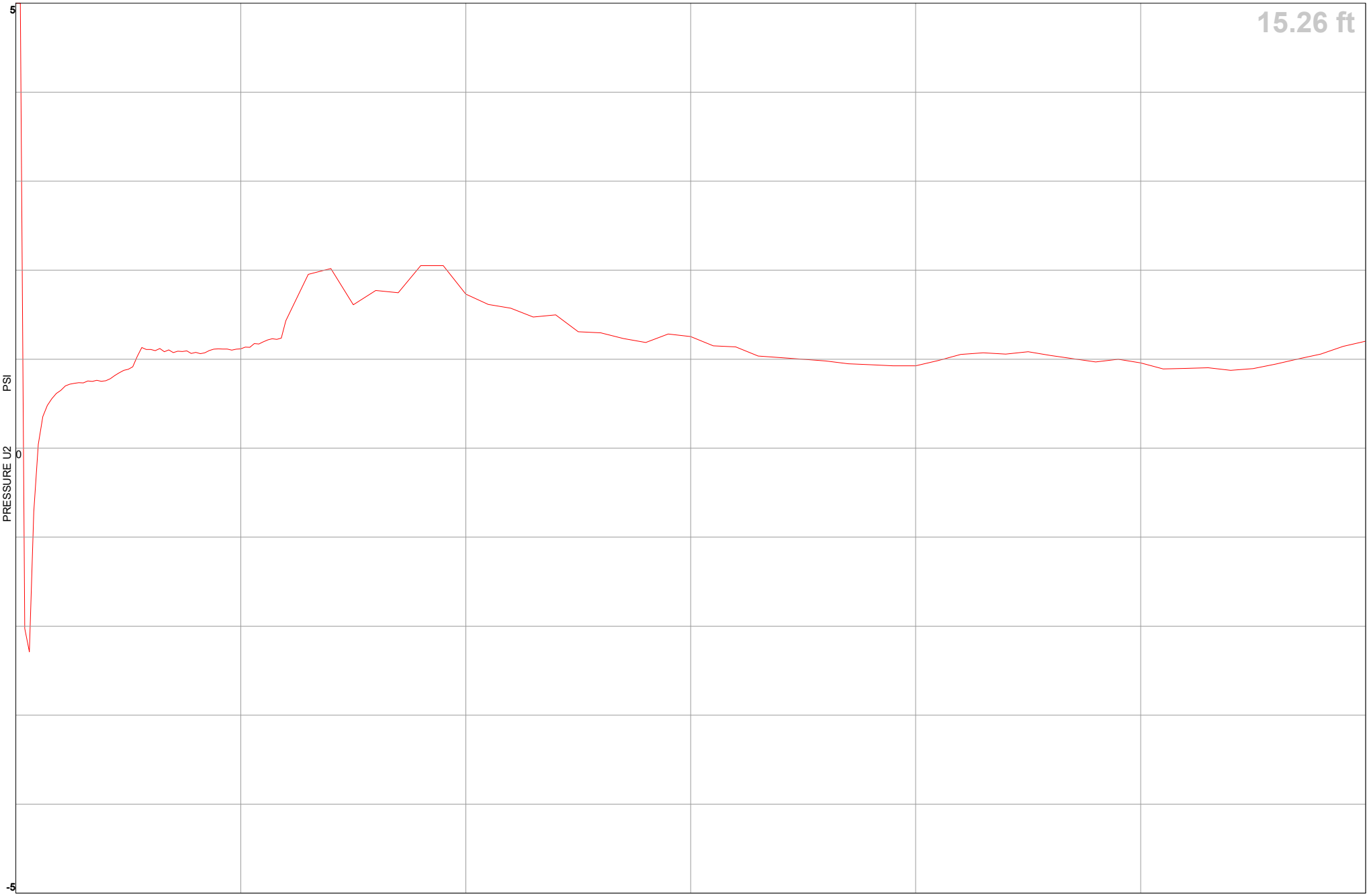
Hammer to Rod String Distance (ft): 5.83
* = Not Determined

COMMENT:

15.26-1.25psi*144/62.4=12.4ft

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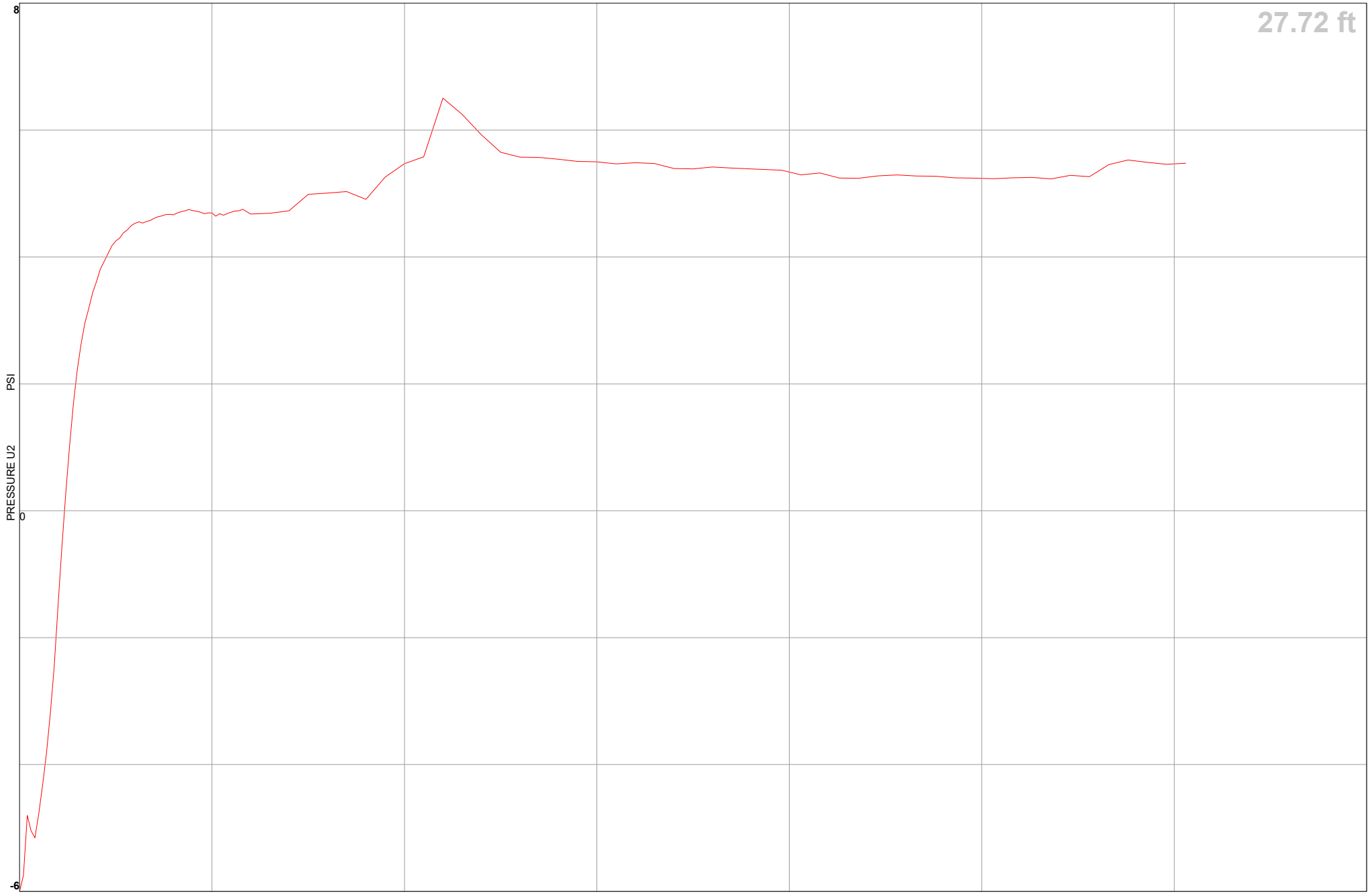
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Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-01	Date and Time	9/16/2025 8:45:26 AM	
Equilized Pressure	1.1	EST GW Depth During Test	12.5	



27.72-5.5psi*144/62.4=15.0 ft

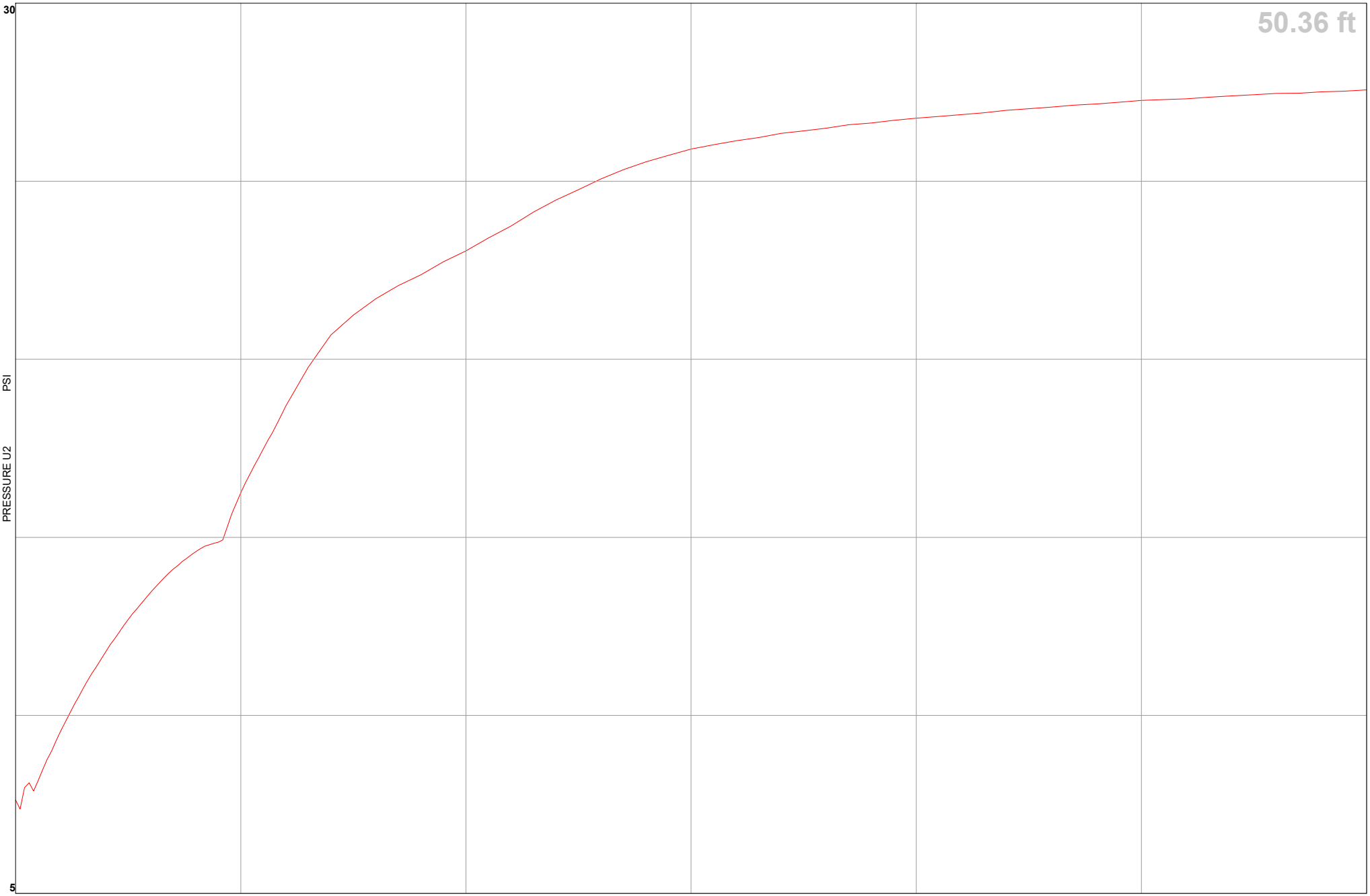
Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS	
Job Number	18077.000	Cone Number	DDG1627		
Hole Number	CPT-01	Date and Time	9/16/2025 8:45:26 AM		
Equilized Pressure	5.4	EST GW Depth During Test	15.0		



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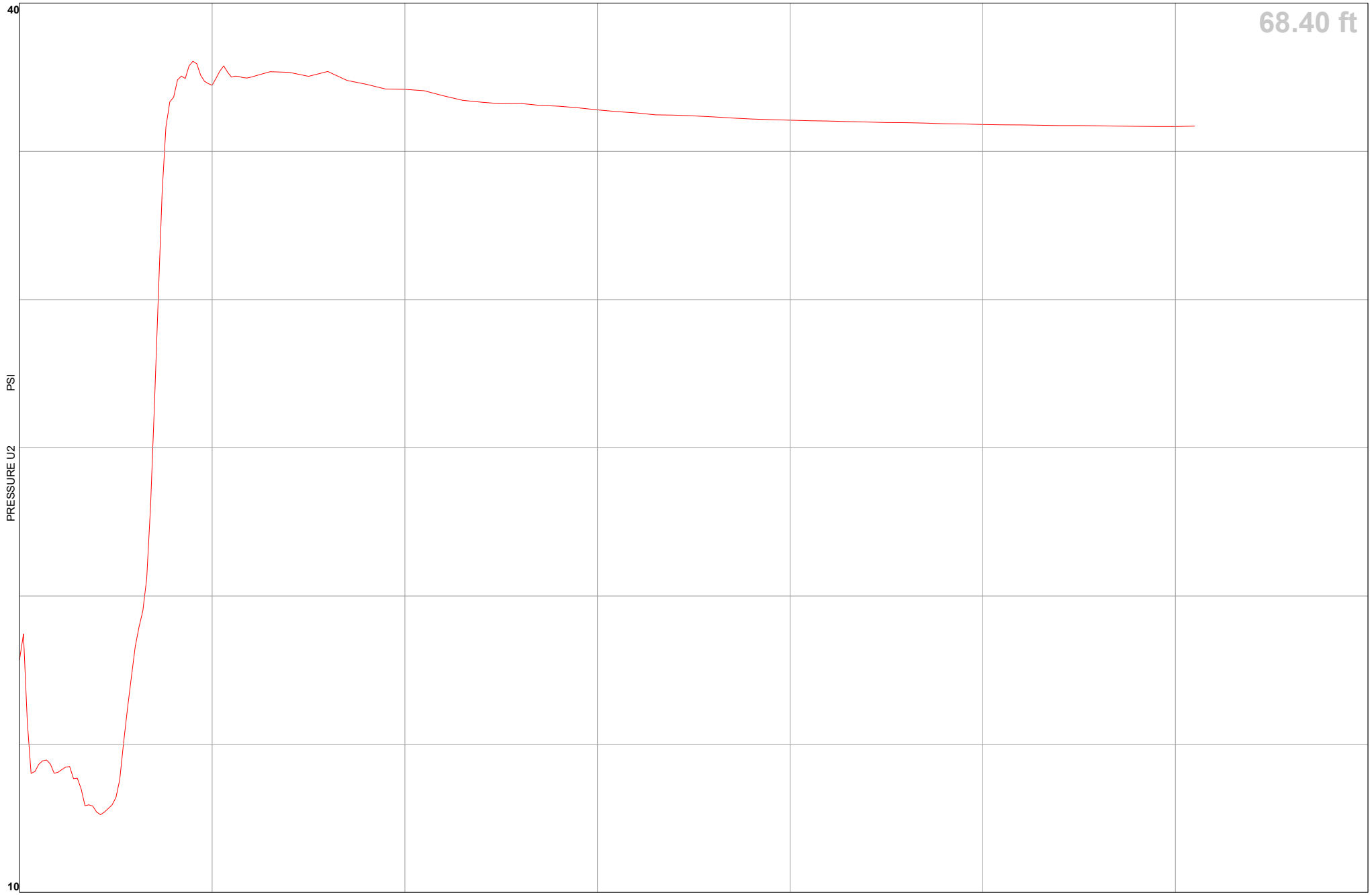
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Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-01	Date and Time	9/16/2025 8:45:26 AM	
Equilized Pressure	27.5	EST GW Depth During Test	+13.2	



50.36-27.5psi*144/62.4=13.1 ft

Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-01	Date and Time	9/16/2025 8:45:26 AM	
Equilized Pressure	35.7	EST GW Depth During Test	+14.2	



68.40-35.8psi*144/62.4= - 14.2 ft

CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

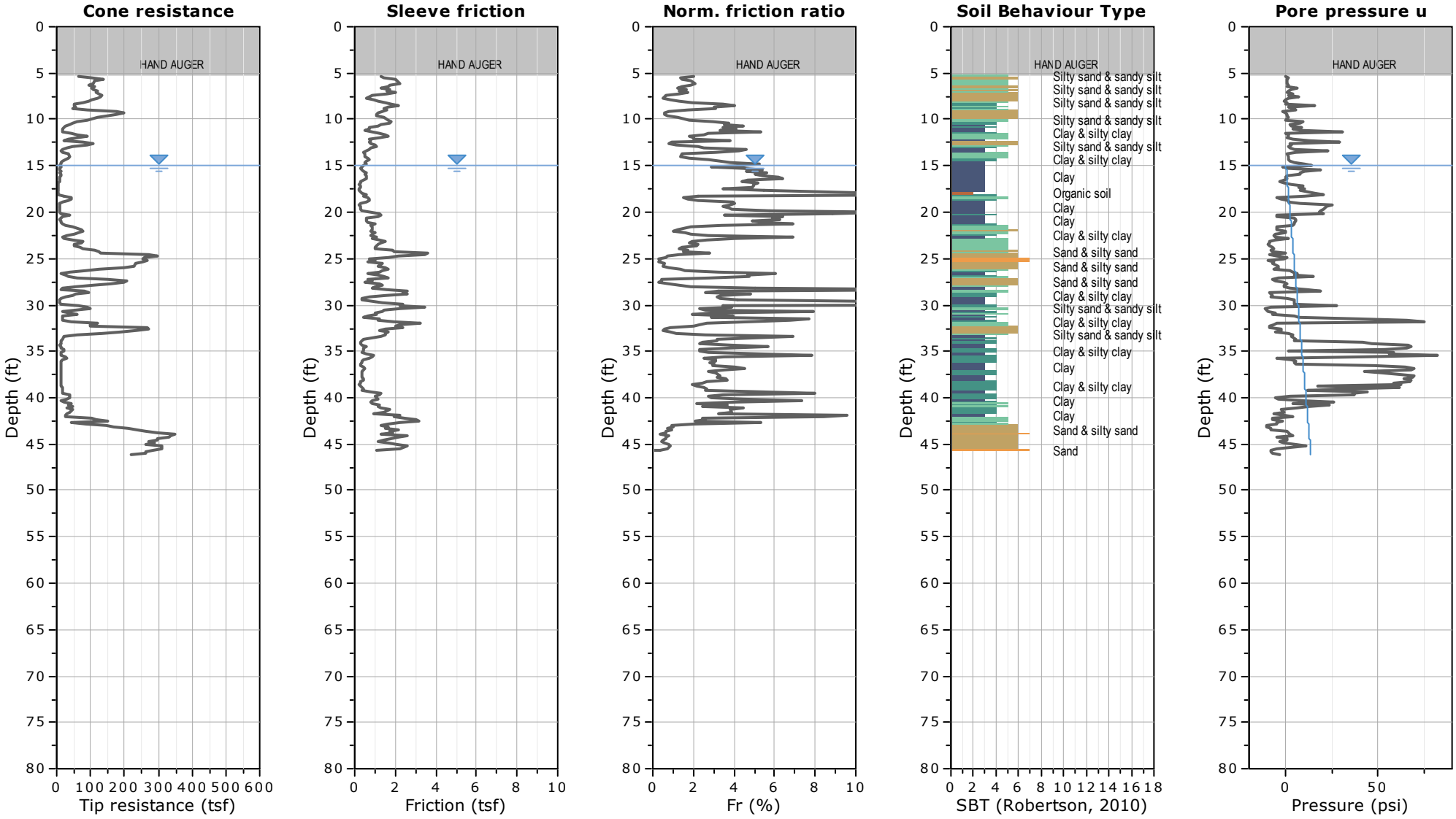
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

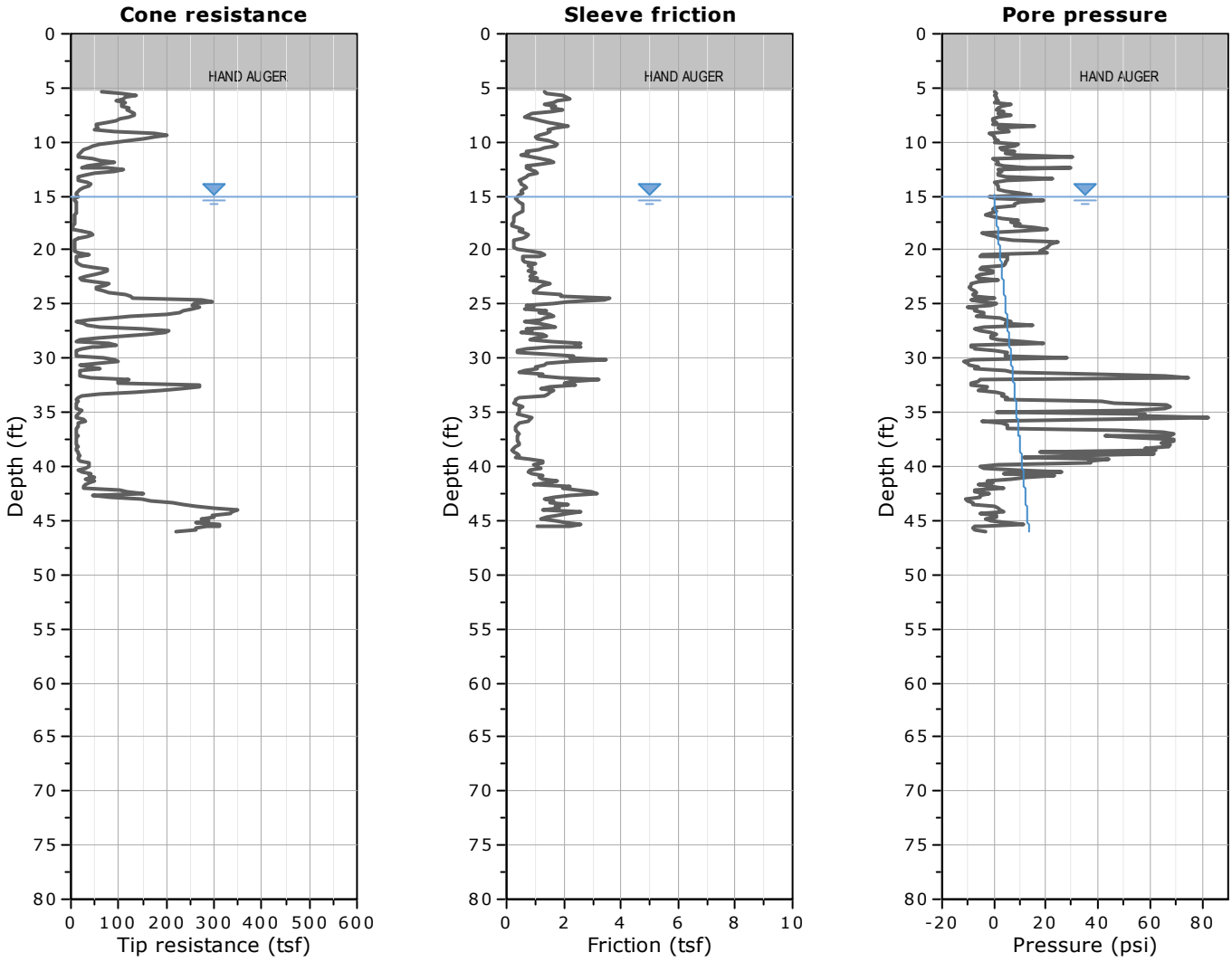
Est. GWL: 15.00 ft

Cone Type: 15cm²

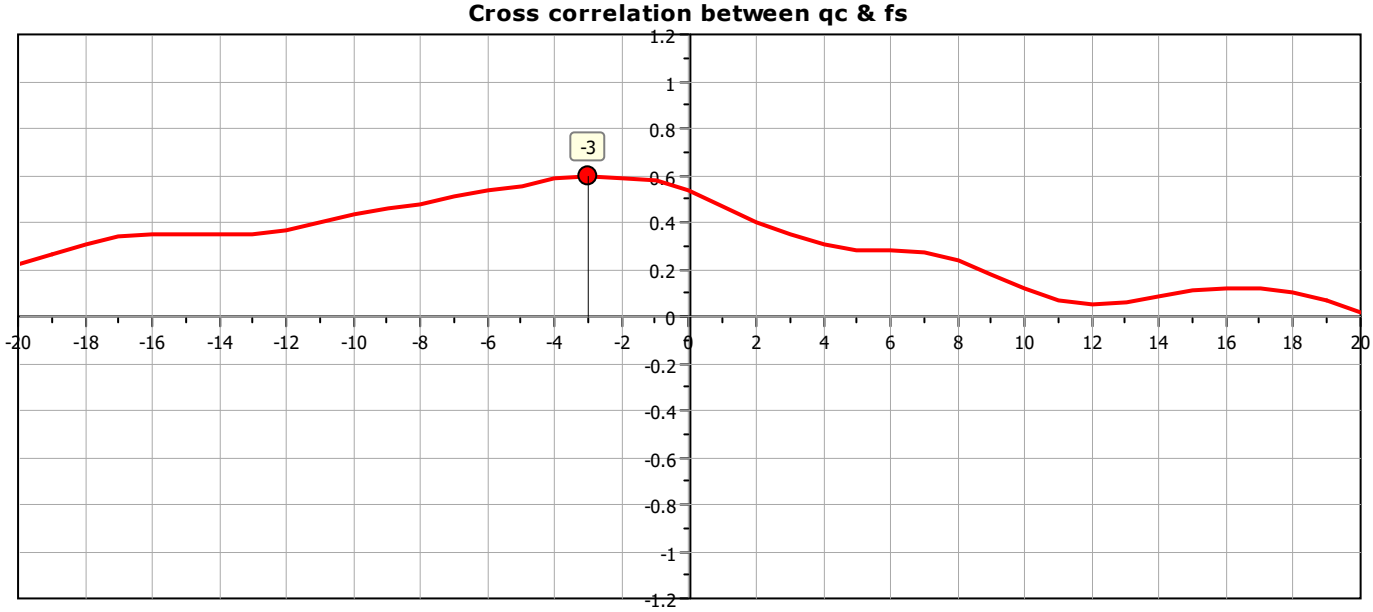
Cone Operator: JM-IY

Project: **Quincy Courthouse**

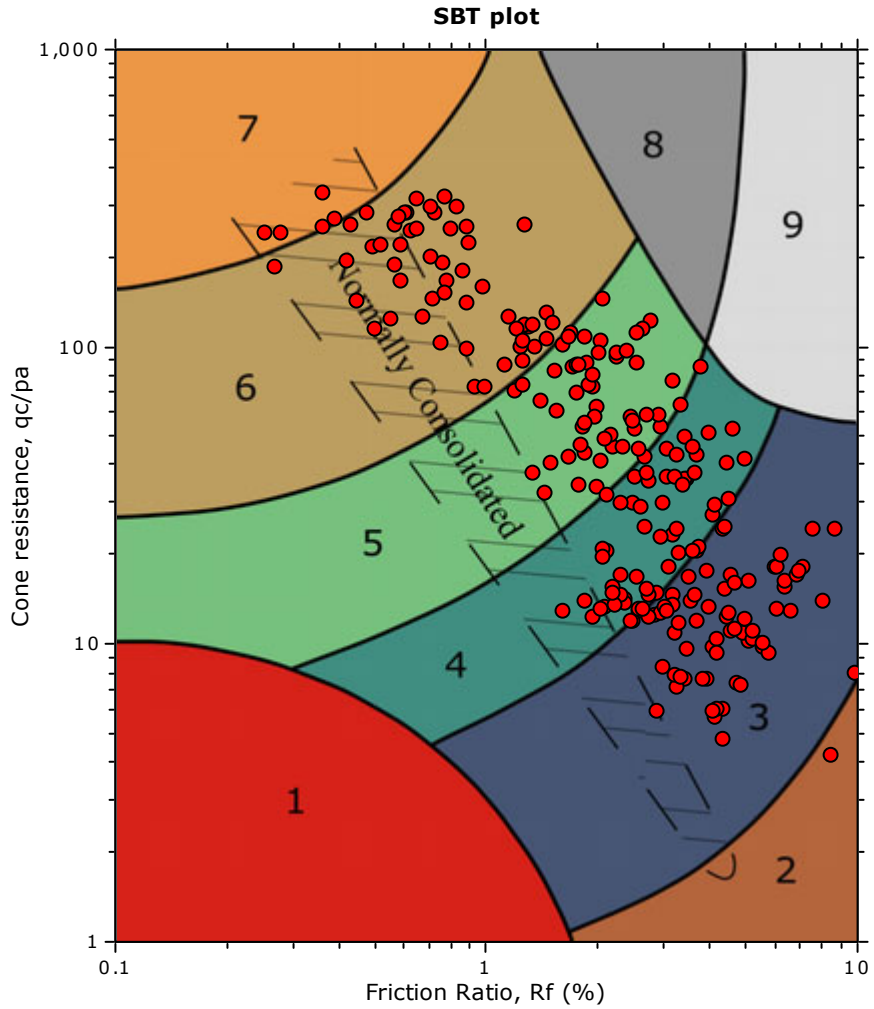
Location: **257 Lawrence Street, Quincy, CA 95971**

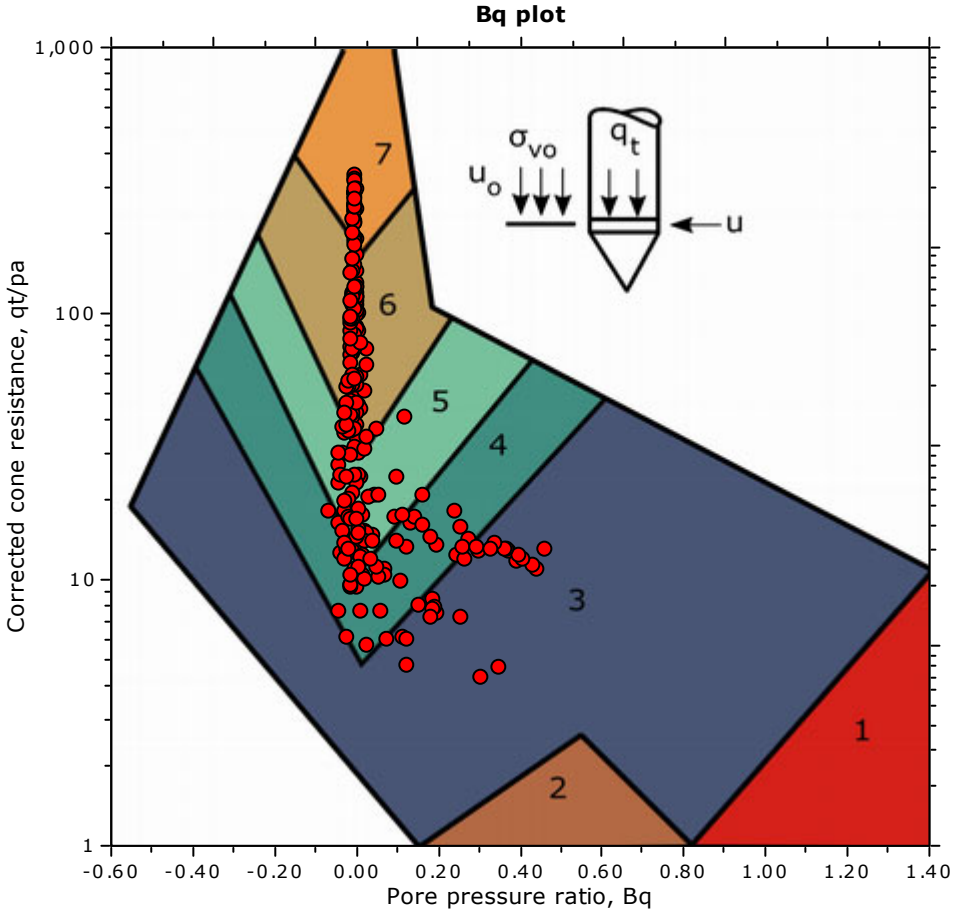


The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



SBT - Bq plots

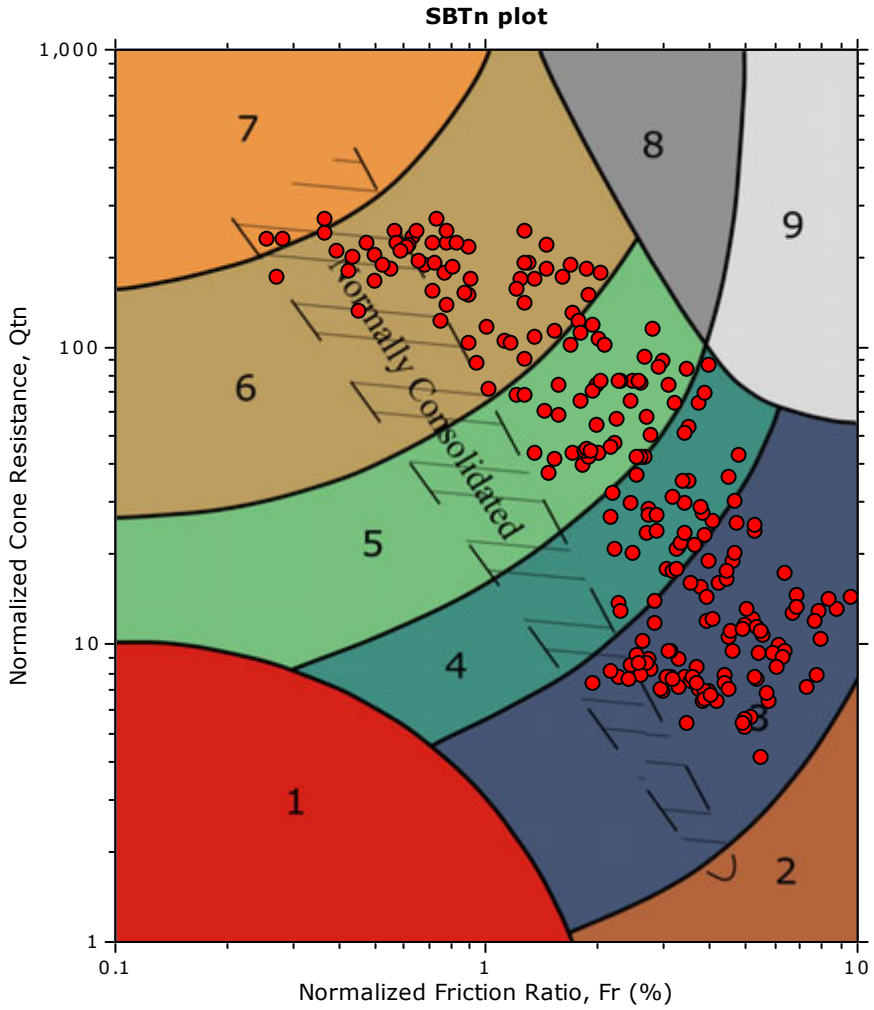


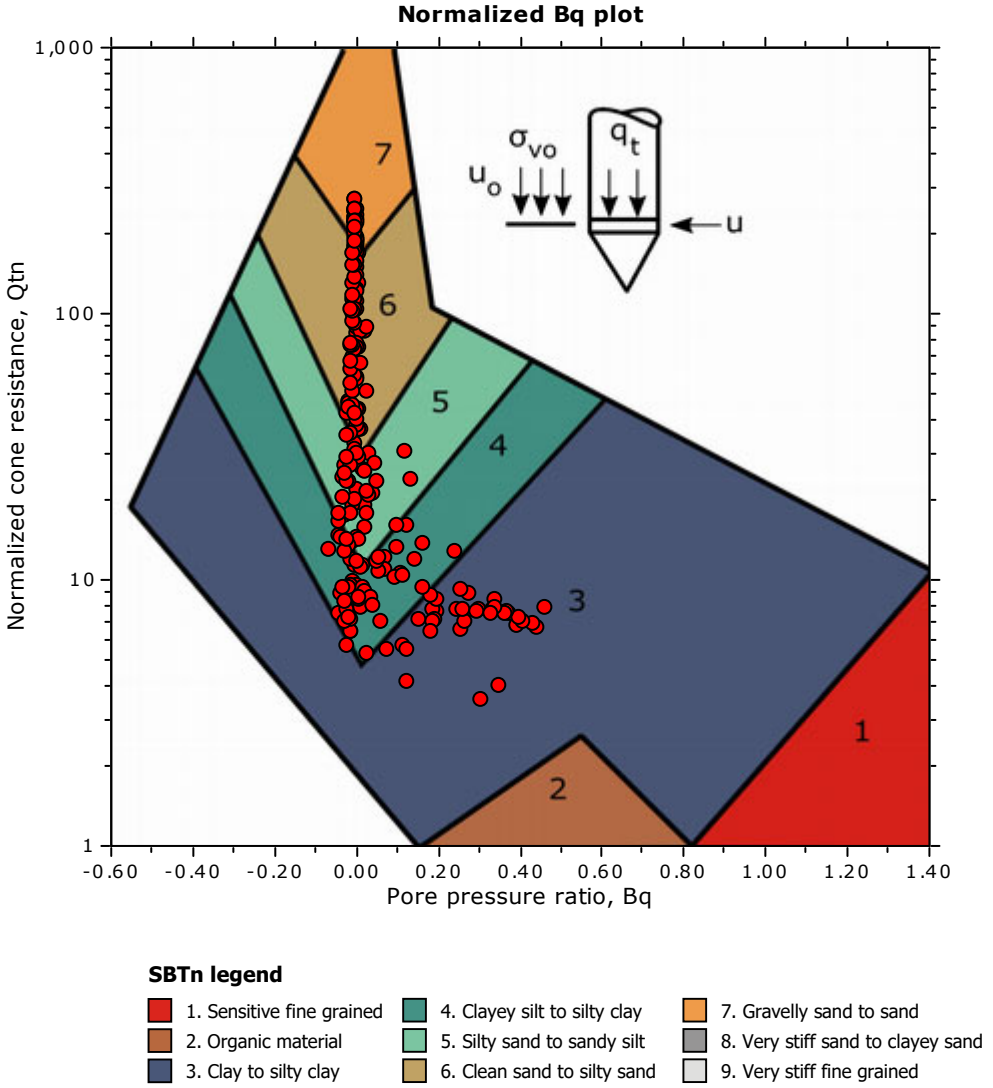


SBT legend

1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

SBT - Bq plots (normalized)

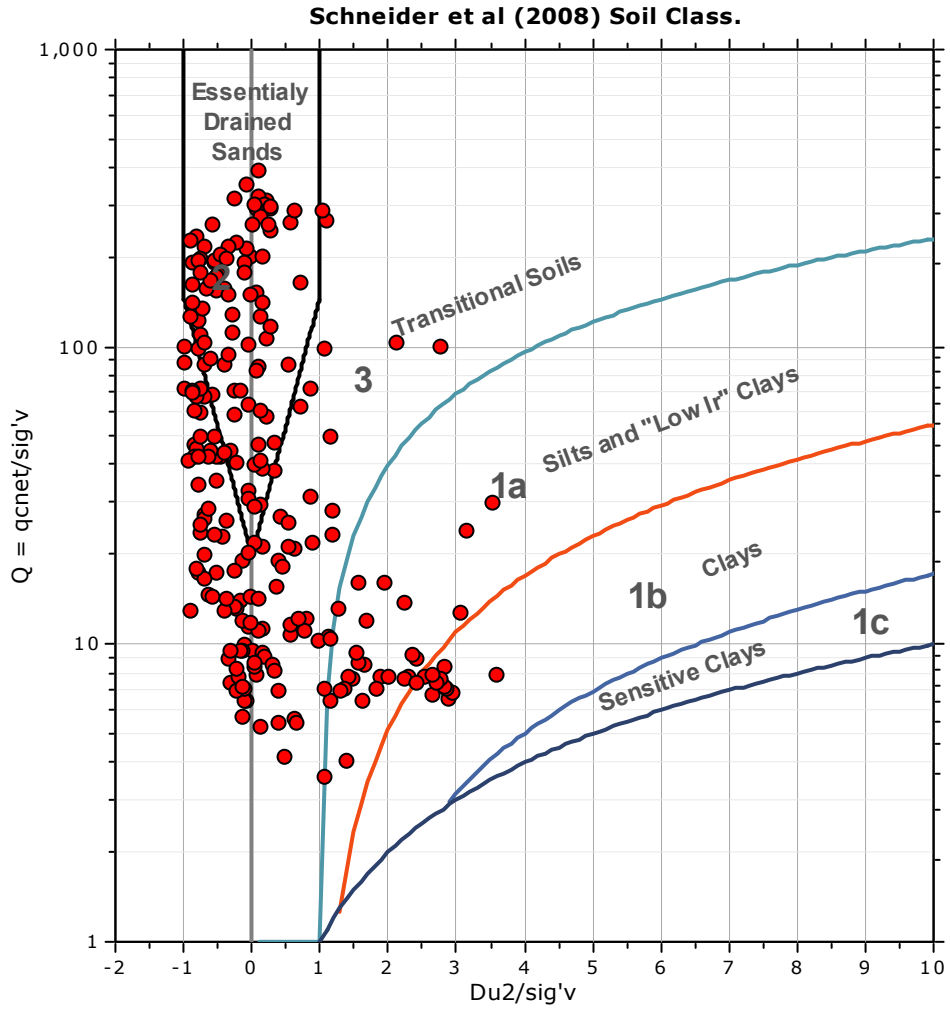


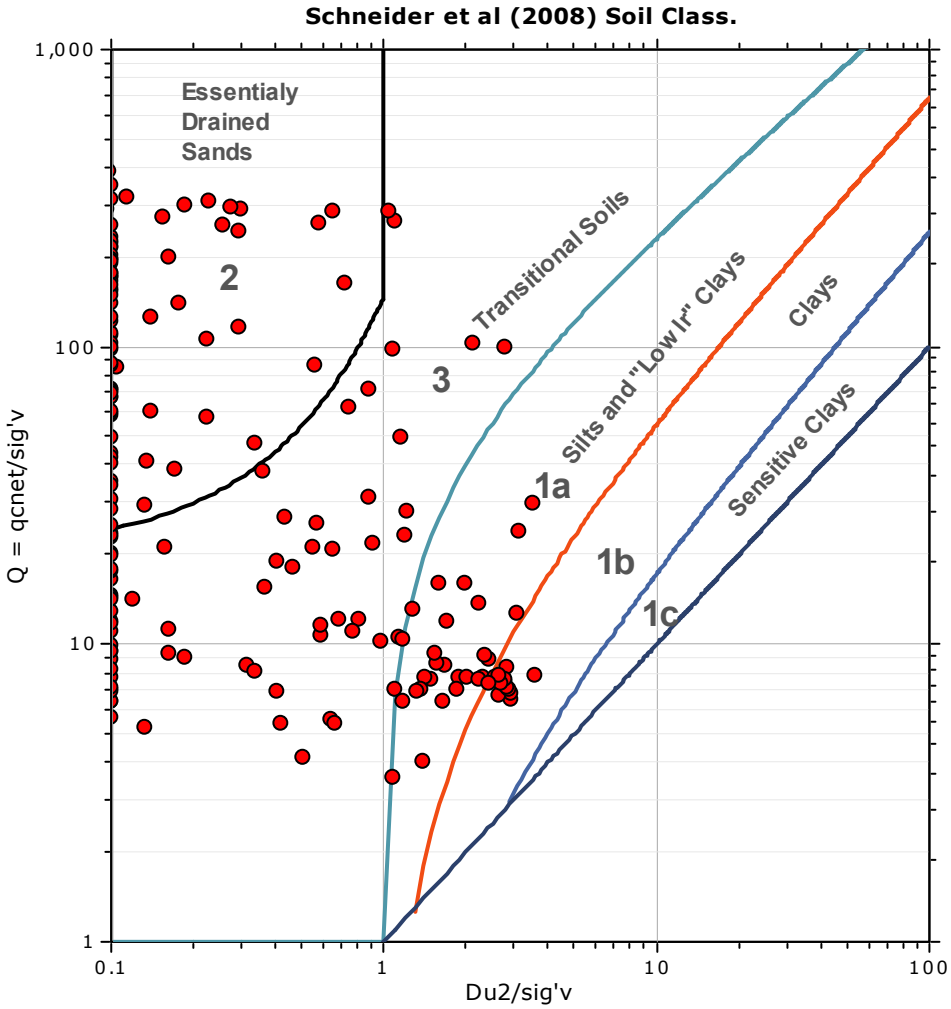


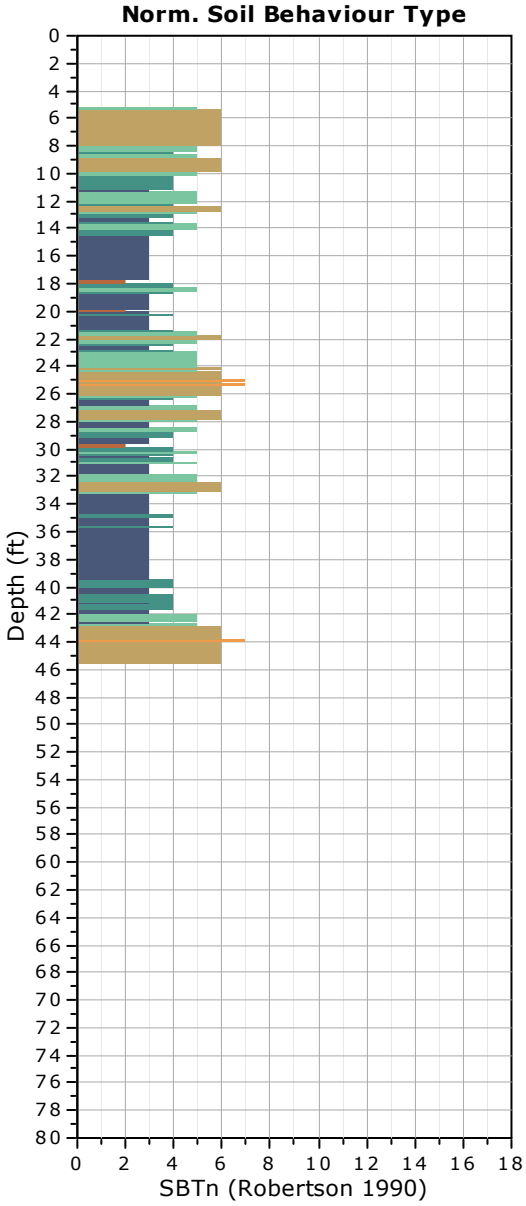
SBTn legend

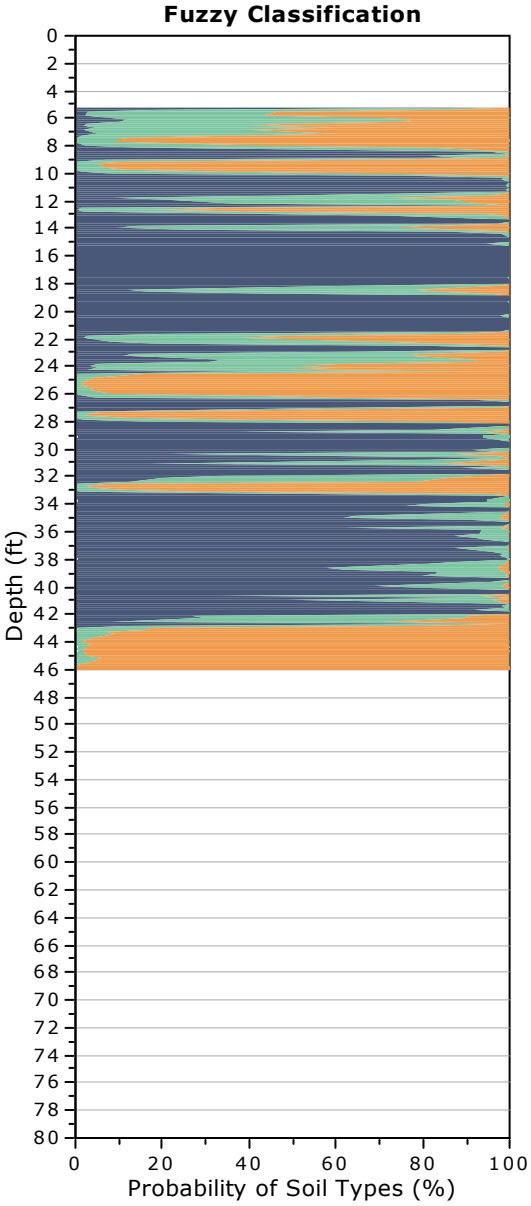
1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

Bq plots (Schneider)









Fuzzy classifiaction legend

- Highly probable clayey soil
- Highly probable mixture soil
- Highly probable sandy soil

CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

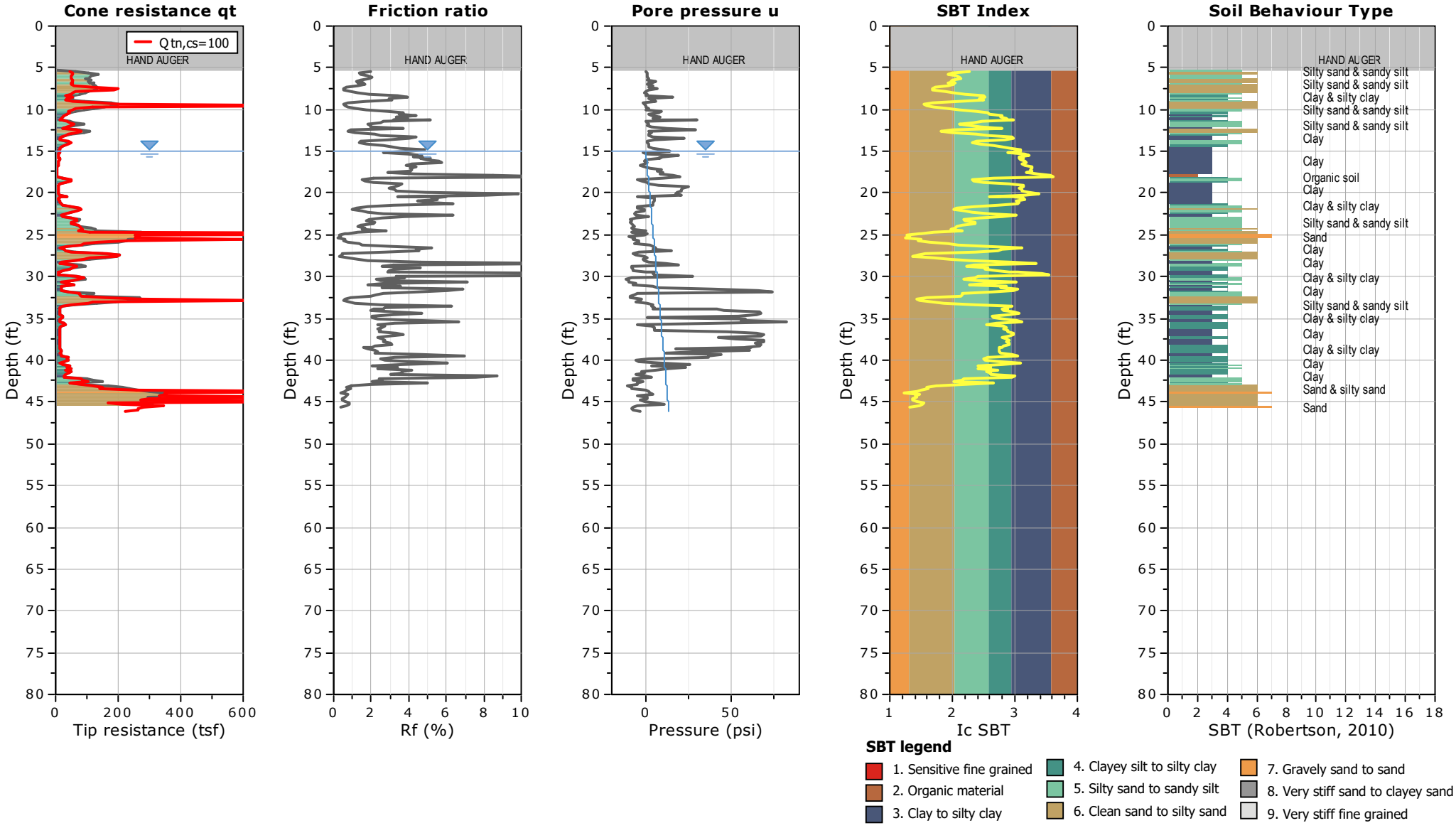
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

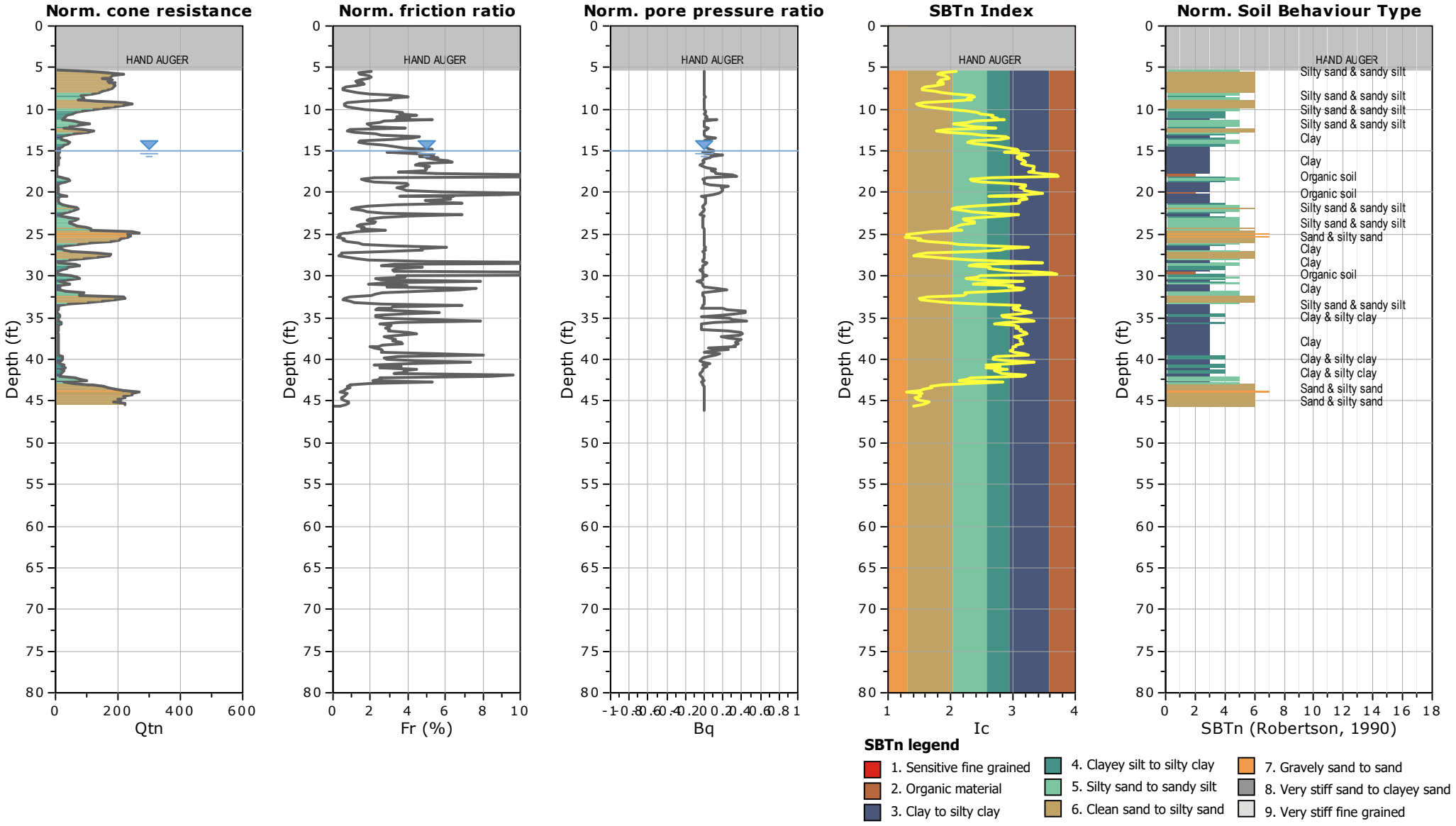
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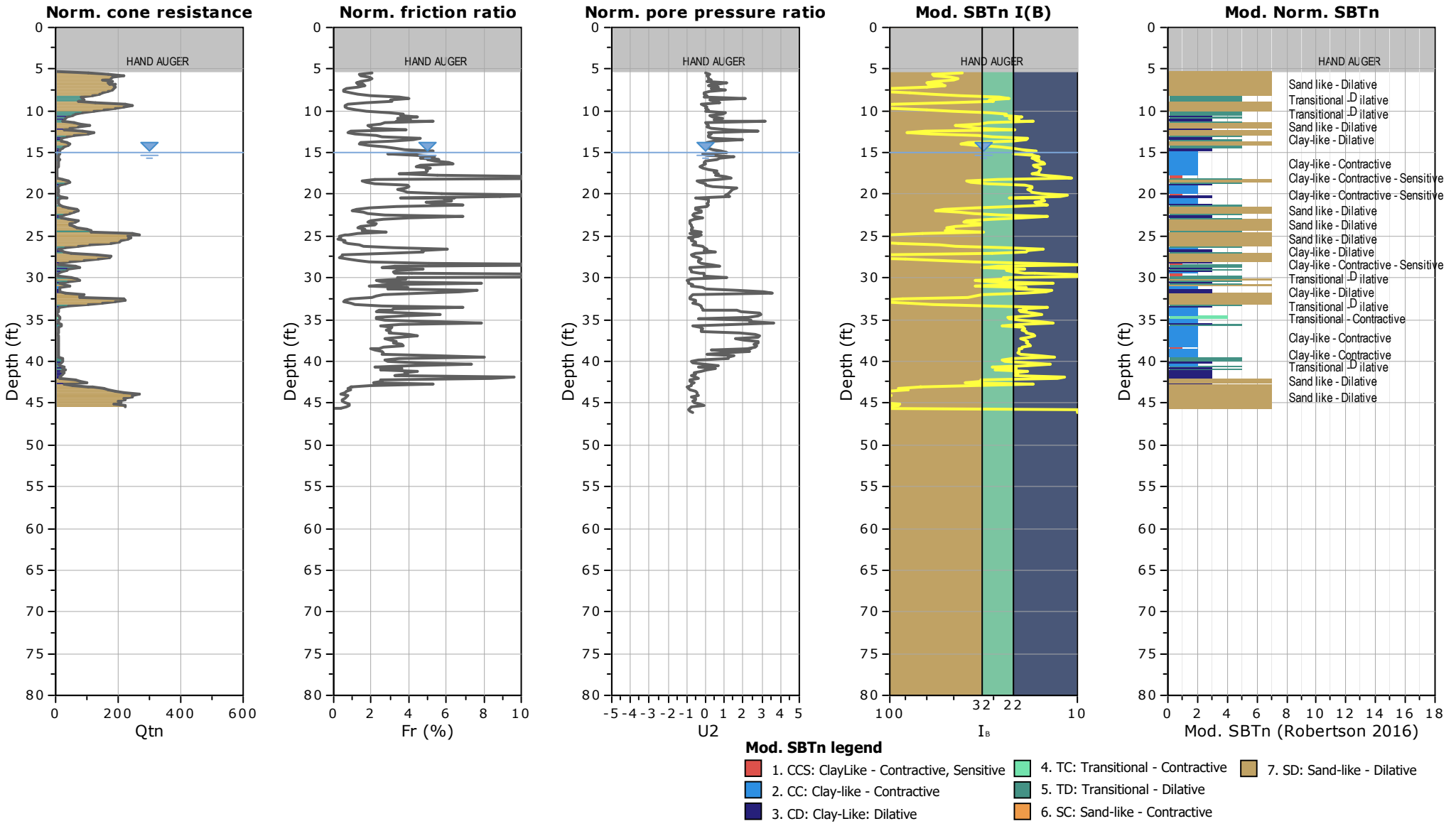
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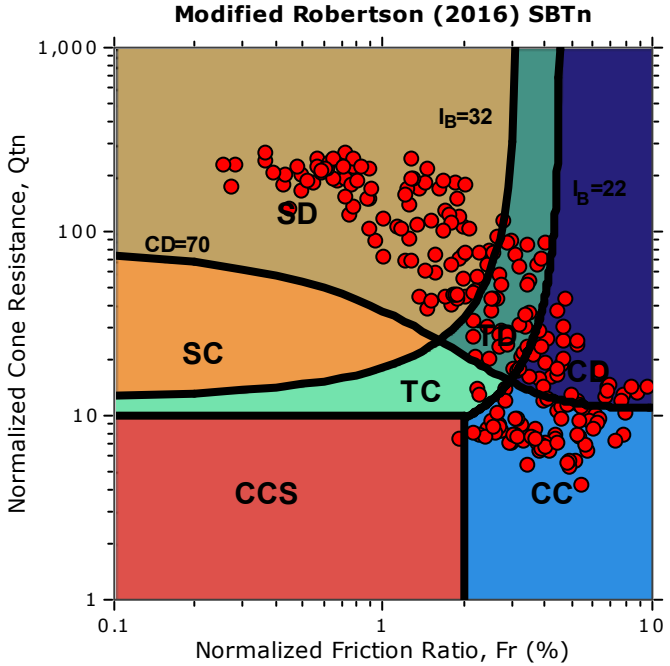
Cone Operator: JM-IY

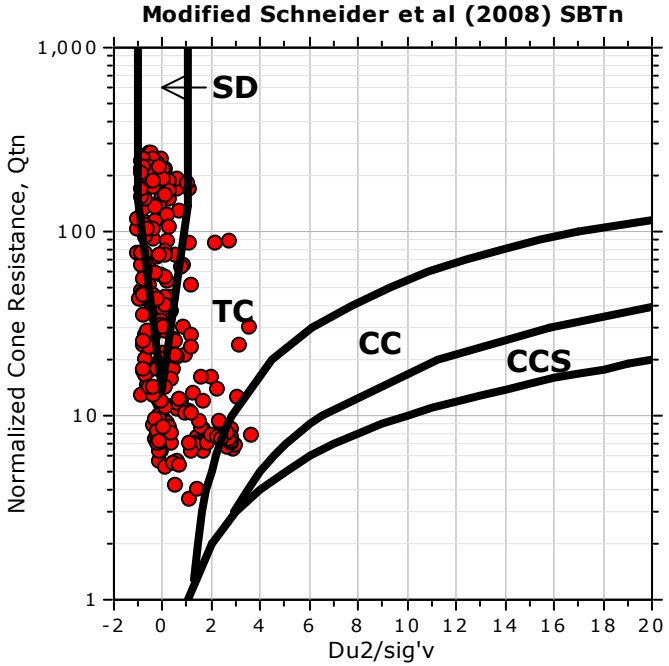
Project: Quincy Courthouse

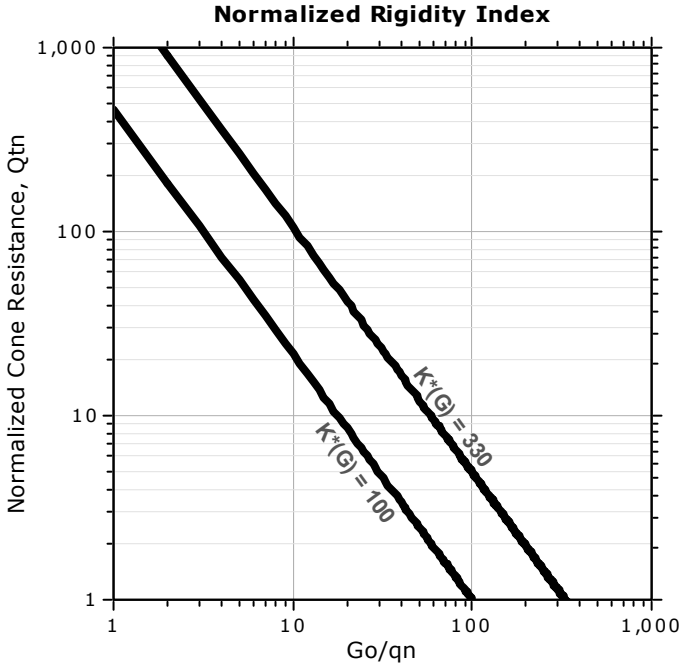
Location: 257 Lawrence Street, Quincy, CA 95971



Updated SBTn plots







CCS: Clay-like - Contractive - Sensitive
CC: Clay-like - Contractive
CD: Clay-like - Dilative
TC: Transitional - Contractive
TD: Transitional - Dilative
SC: Sand-like - Contractive
SD: Sand-like - Dilative

K(G) > 330: Soils with significant microstructure (e.g. age/cementation)

CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

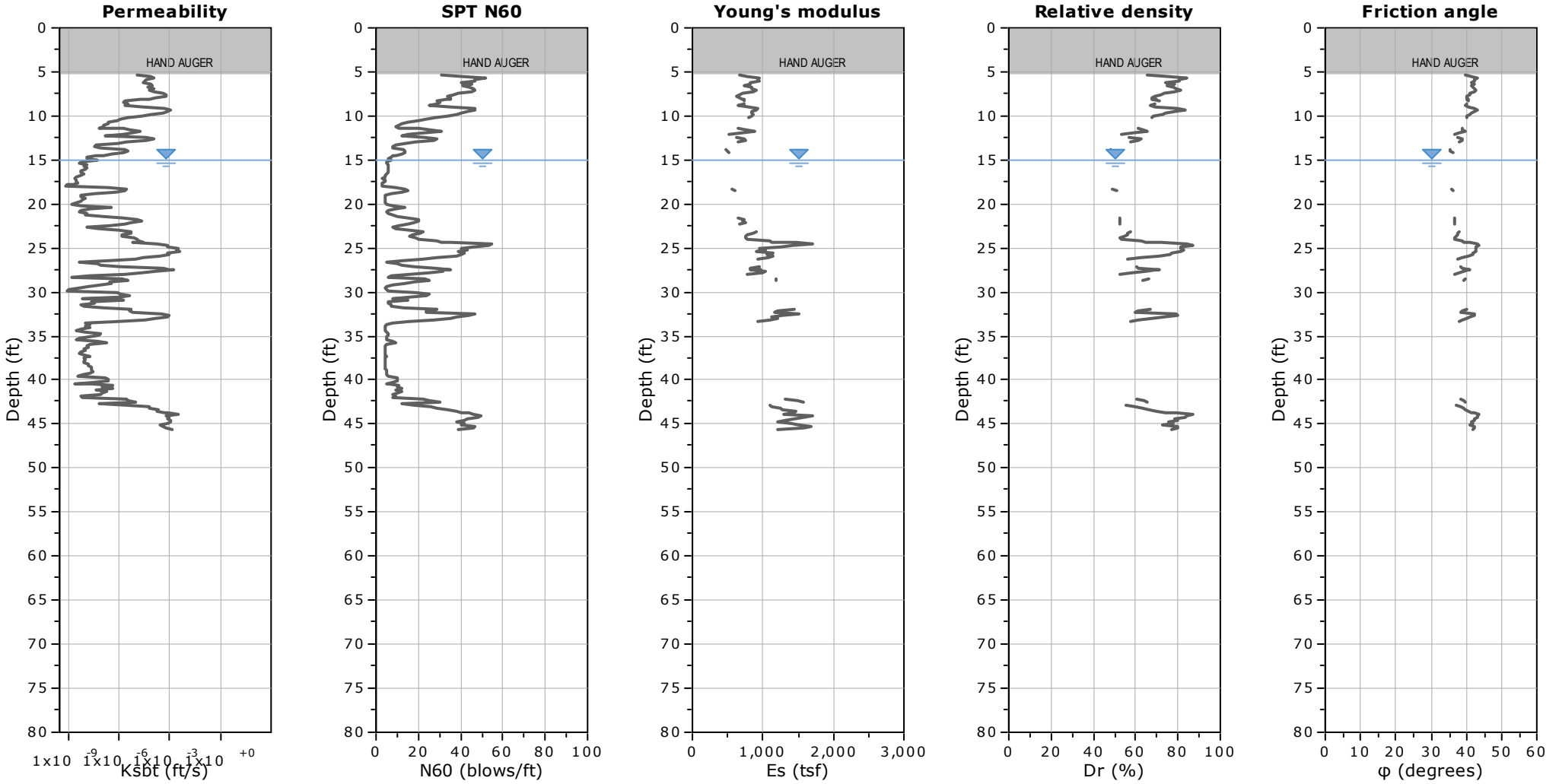
Est. GWL: 15.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

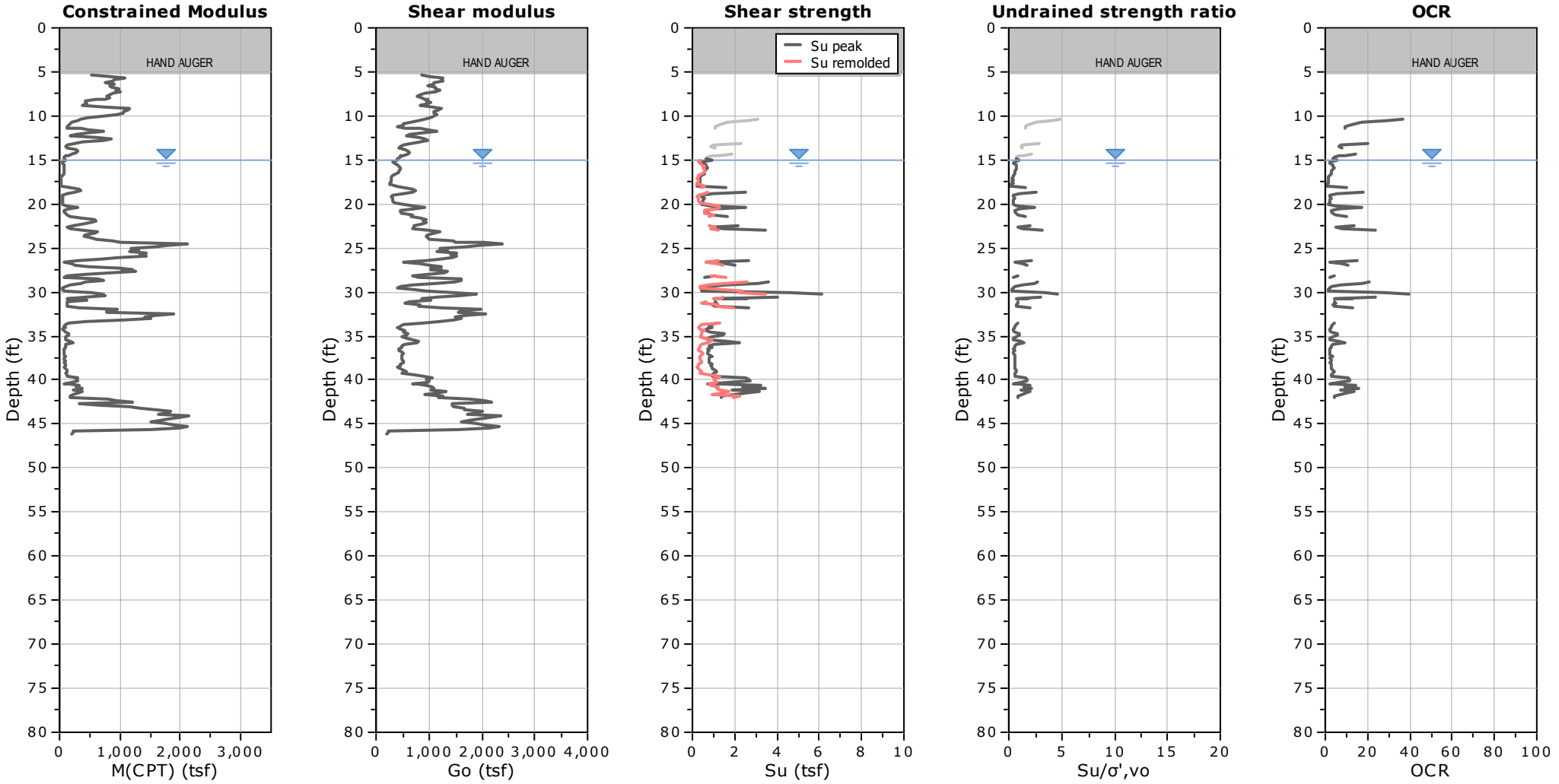
Permeability: Based on SBT_n

SPT N_{60}: Based on I_c and q_t

Young's modulus: Based on variable alpha using I_c (Robertson, 2009)

Relative density constant, C_{Dr}: 350.0

Phi: Based on Kulhawy & Mayne (1990)



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: Auto
OCR factor for clays, N_{kt}: Auto
Flat Dilatometer Test data

CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

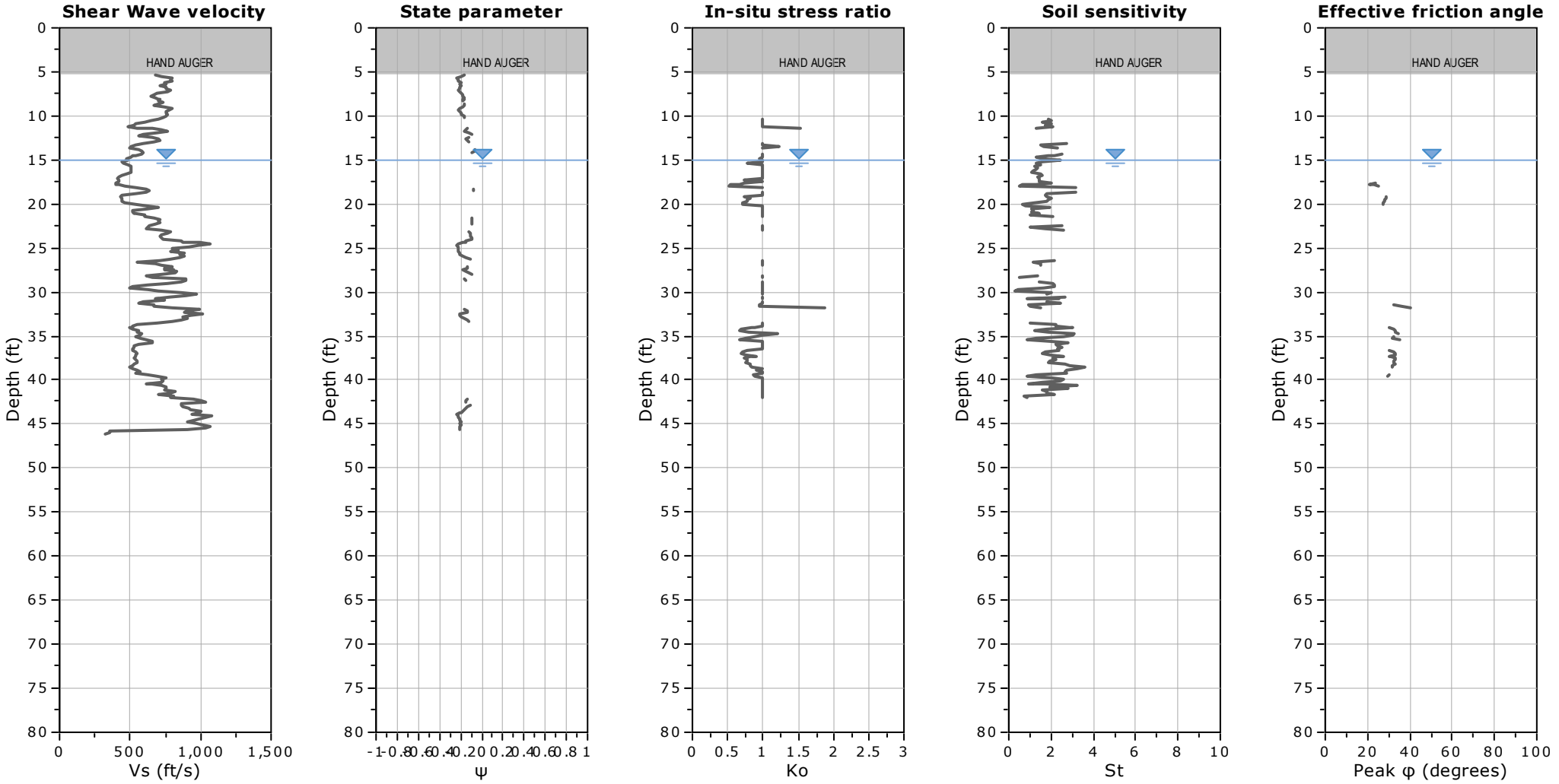
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Cone Operator: JM-IY

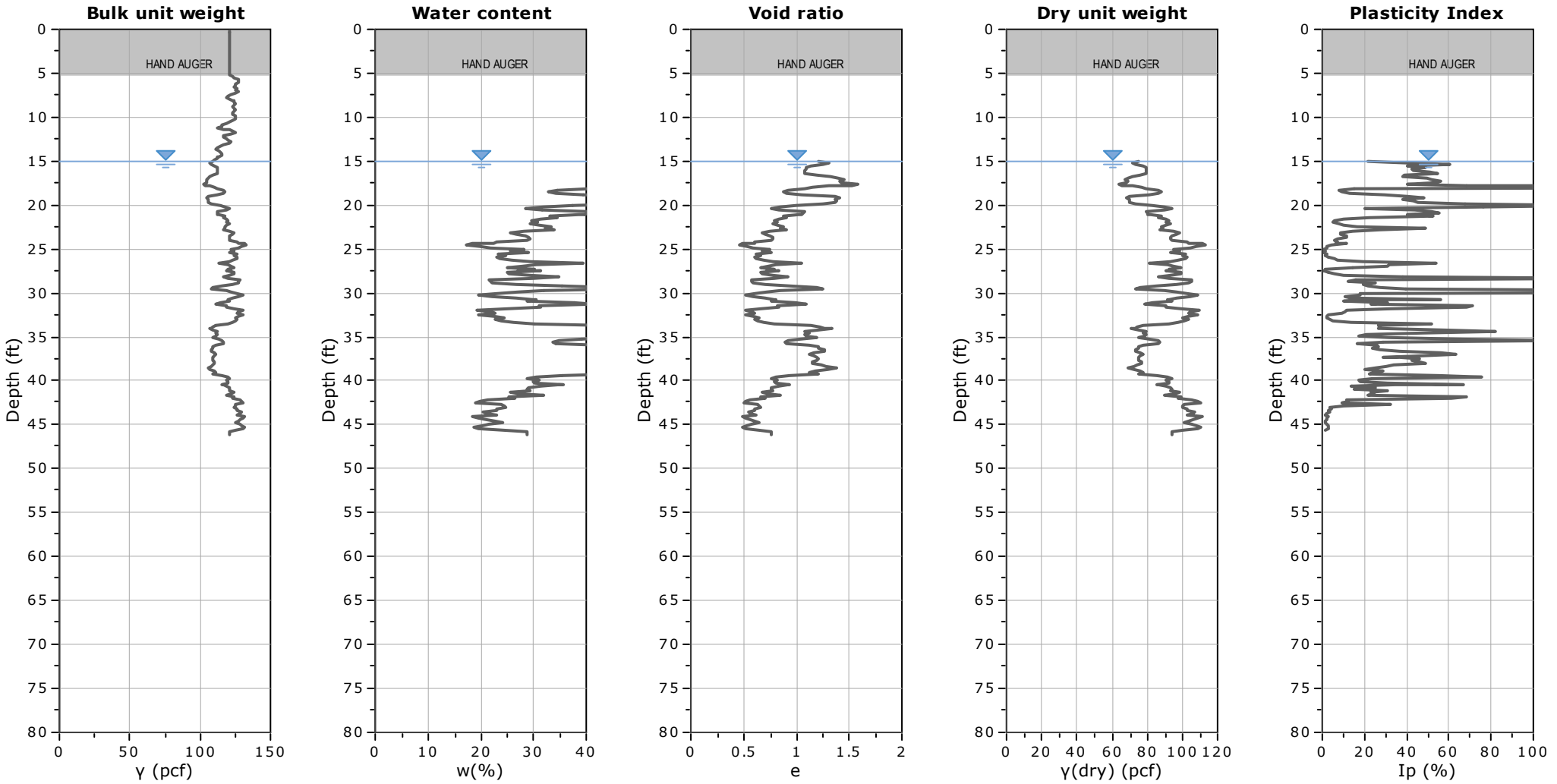
Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Soil Sensitivity factor, N_S: 7.00


Bulk unit weight
Water content
Void ratio
Dry unit weight
Plasticity Index
HAND AUGER
Depth (ft)
γ (pcf)
w(%)
e
γ(dry) (pcf)
Ip (%)

CPT: CPT-02

Total depth: 46.10 ft, Date: 9/16/2025

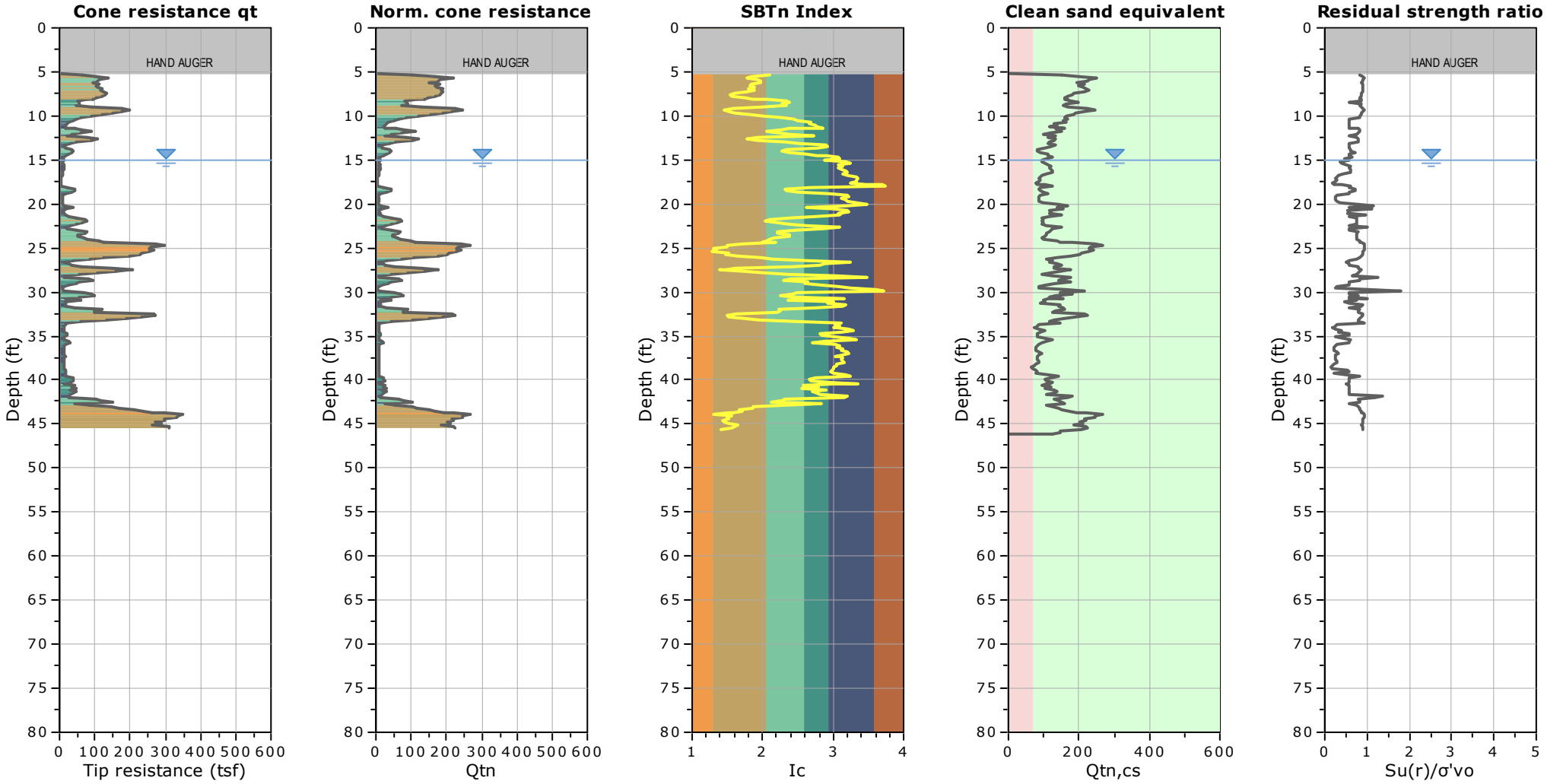
Est. GWL: 15.00 ft

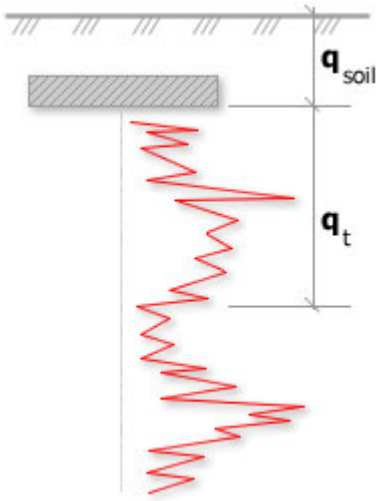
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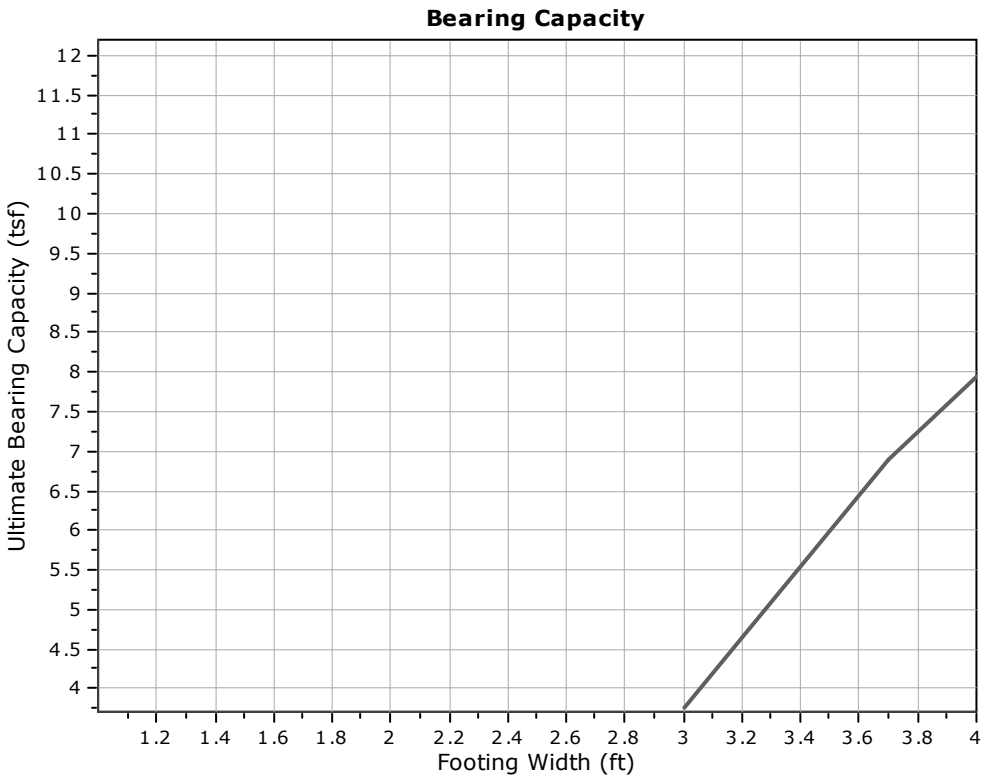




Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (ft)	Start Depth (ft)	End Depth (ft)	Ave. q_t (tsf)	R_k	Soil Press. (tsf)	Ult. bearing cap. (tsf)
1	3.00	1.60	6.10	18.32	0.20	0.10	3.76
2	3.70	1.60	7.15	33.97	0.20	0.10	6.89
3	4.40	1.60	8.20	46.28	0.20	0.10	9.35
4	5.10	1.60	9.25	51.07	0.20	0.10	10.31
5	5.80	1.60	10.30	60.25	0.20	0.10	12.15
6	6.50	1.60	11.35	56.32	0.20	0.10	11.36
7	7.20	1.60	12.40	56.00	0.20	0.10	11.30
8	7.90	1.60	13.45	56.52	0.20	0.10	11.40
9	8.60	1.60	14.50	53.89	0.20	0.10	10.87
10	9.30	1.60	15.55	50.89	0.20	0.10	10.27
11	10.00	1.60	16.60	47.87	0.20	0.10	9.67
12	10.70	1.60	17.65	45.37	0.20	0.10	9.17
13	11.40	1.60	18.70	43.95	0.20	0.10	8.89
14	12.10	1.60	19.75	42.01	0.20	0.10	8.50
15	12.80	1.60	20.80	40.71	0.20	0.10	8.24

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236 \right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a} \right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$$

(applicable only to $I_c < I_{c_cutoff}$)

:: Relative Density, Dr (%) ::

$$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$$ (applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: State Parameter, ψ ::

$$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$$

:: Drained Friction Angle, φ (°) ::

$$\varphi = \varphi'_{cv} + 15.94 \cdot \log(Q_{tn,cs}) - 26.88$$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$
$\alpha = 14$ for $Q_{tn} > 14$
$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$
$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \geq 2.20$

$$M_{CPT} = 0.03 \cdot (q_t - \sigma_v) \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Small strain shear Modulus, Go (MPa) ::

$$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho} \right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))} \right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: In situ Stress Ratio, Ko ::

$$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Peak Friction Angle, φ' (°) ::

$$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$$

(applicable for $0.10 < B_q < 1.00$)

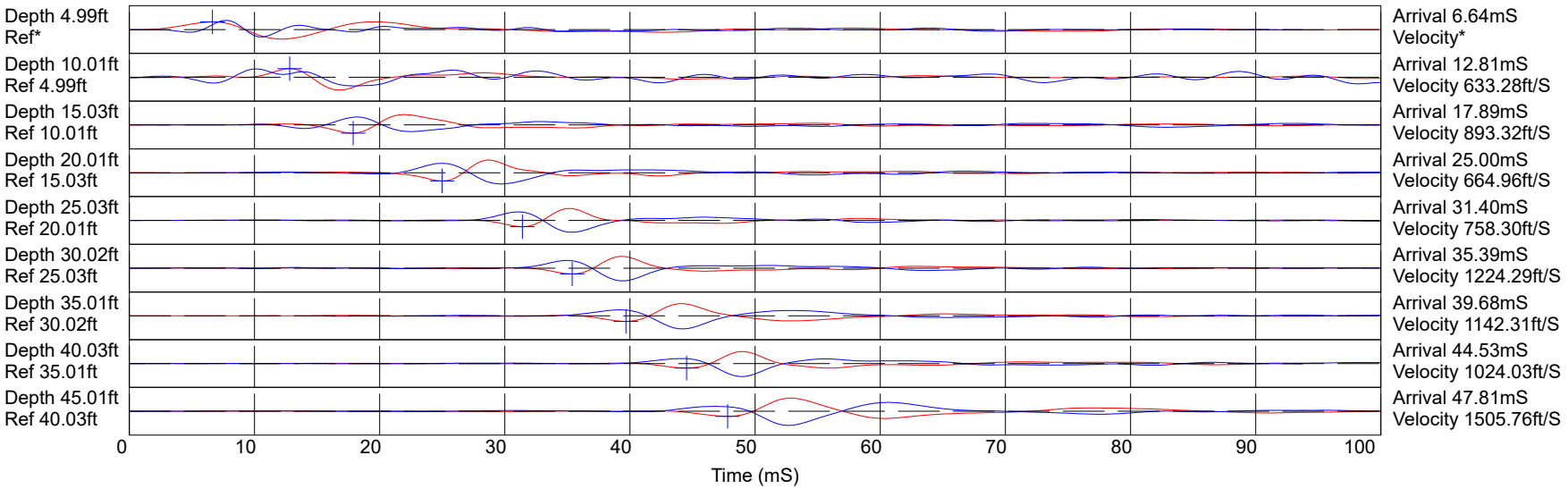
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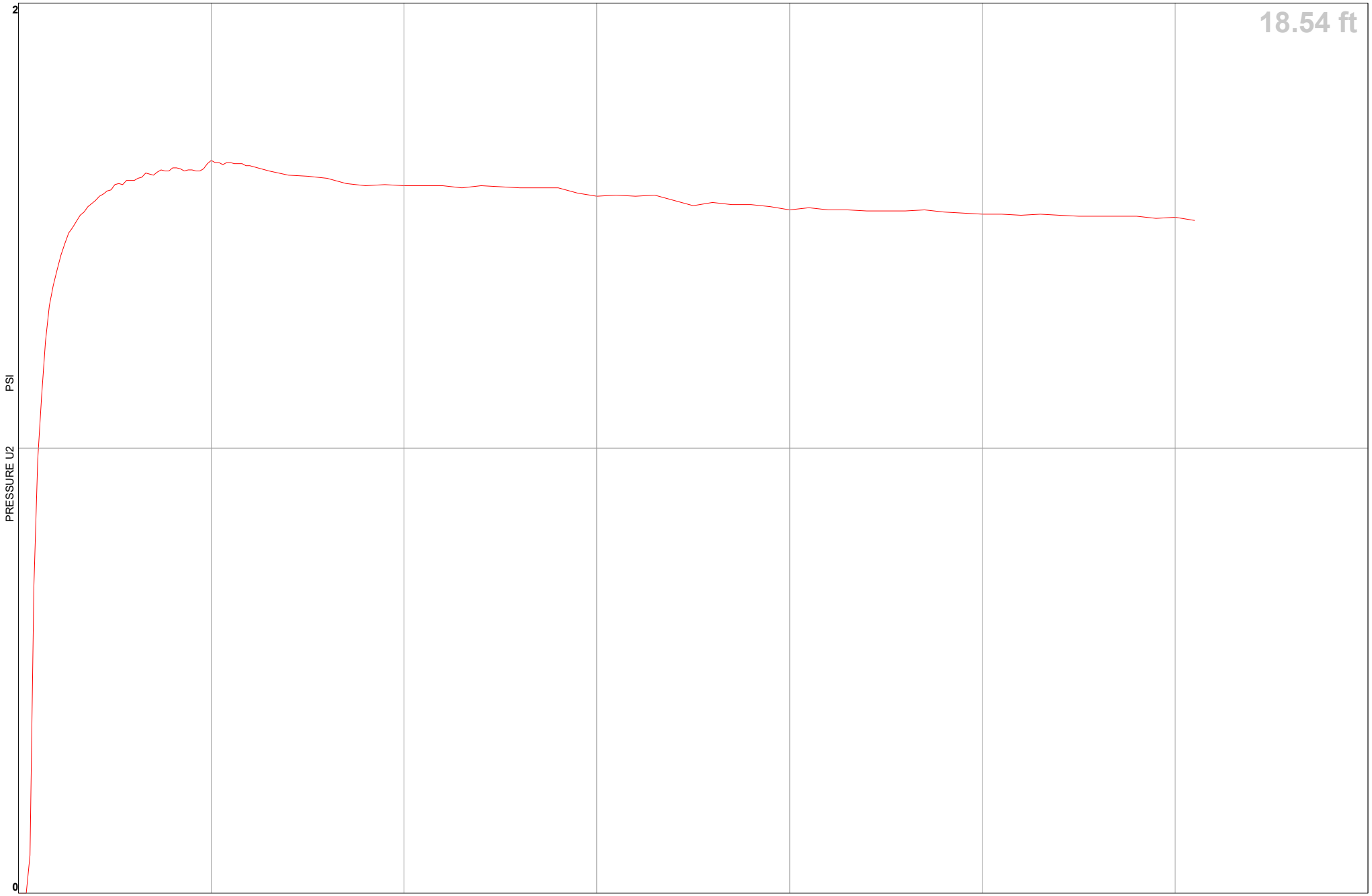


Hammer to Rod String Distance (ft): 5.83
* = Not Determined

COMMENT:

Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-02	Date and Time	9/16/2025 11:14:05 AM	
Equilized Pressure	1.5	EST GW Depth During Test	15.0	



18.54-1.5psi*144/62.4=15.1 ft

Atlas Technical Consultants

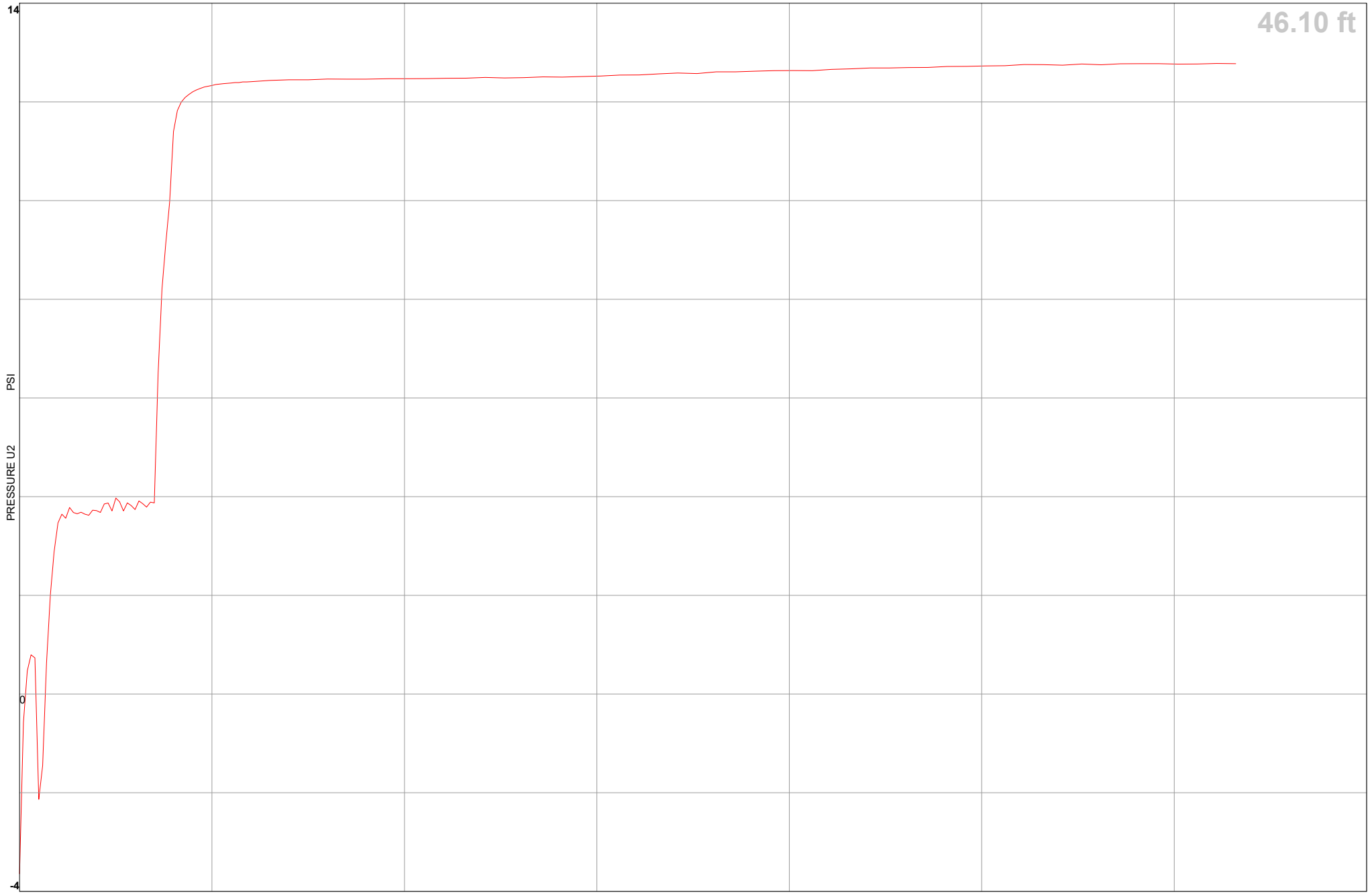
Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-02	Date and Time	9/16/2025 11:14:05 AM	
Equilized Pressure	11.4	EST GW Depth During Test	15.8	



42.32-11.5psi*144/62.4=15.8 ft

Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-02	Date and Time	9/16/2025 11:14:05 AM	
Equilized Pressure	12.7	EST GW Depth During Test	16.6	



46.10-12.75psi*144/62.4= 16.7 ft

Atlas Technical Consultants

https://www.oneatlas.com/

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

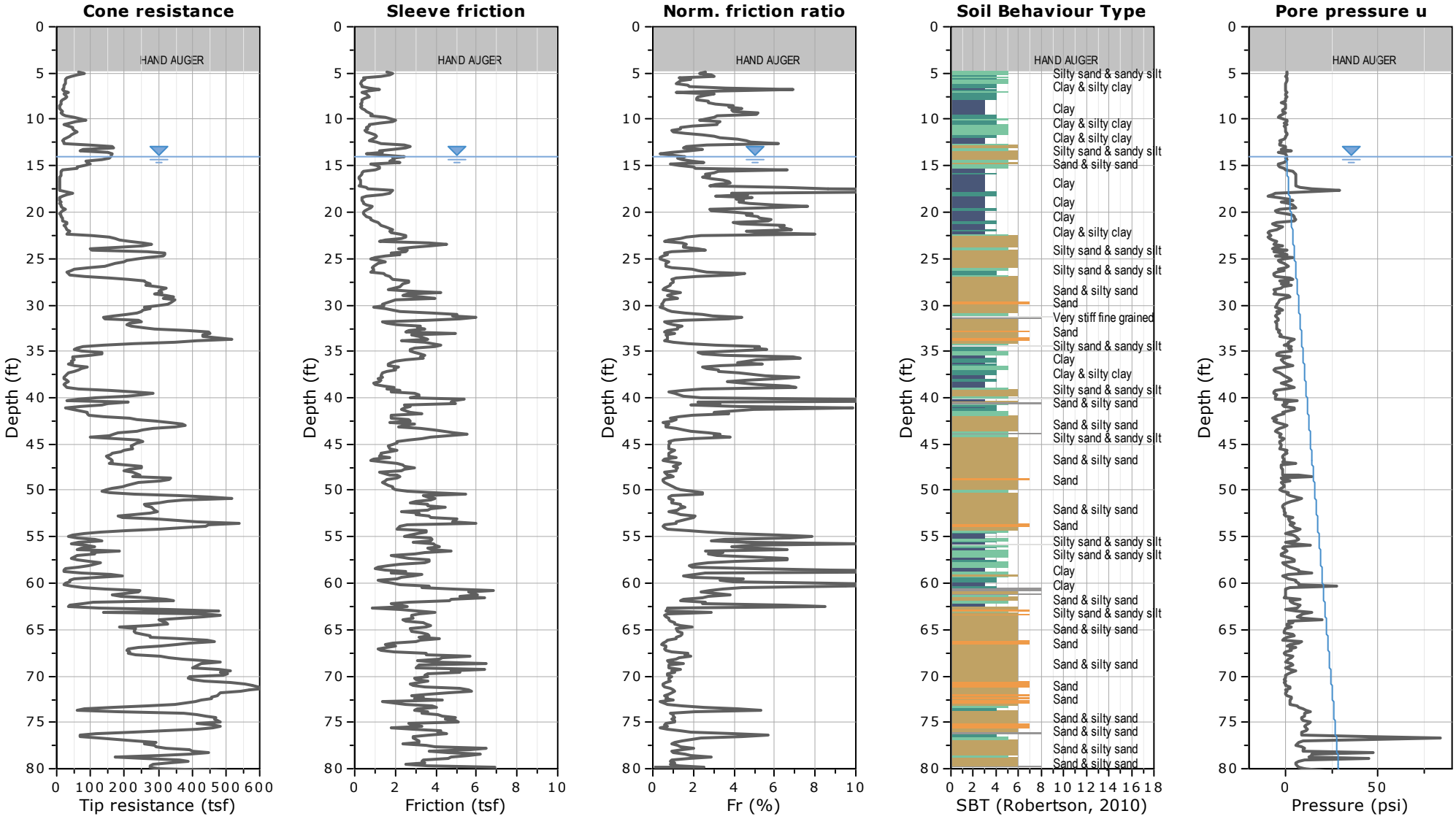
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Atlas Technical Consultants

https://www.oneatlas.com/

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

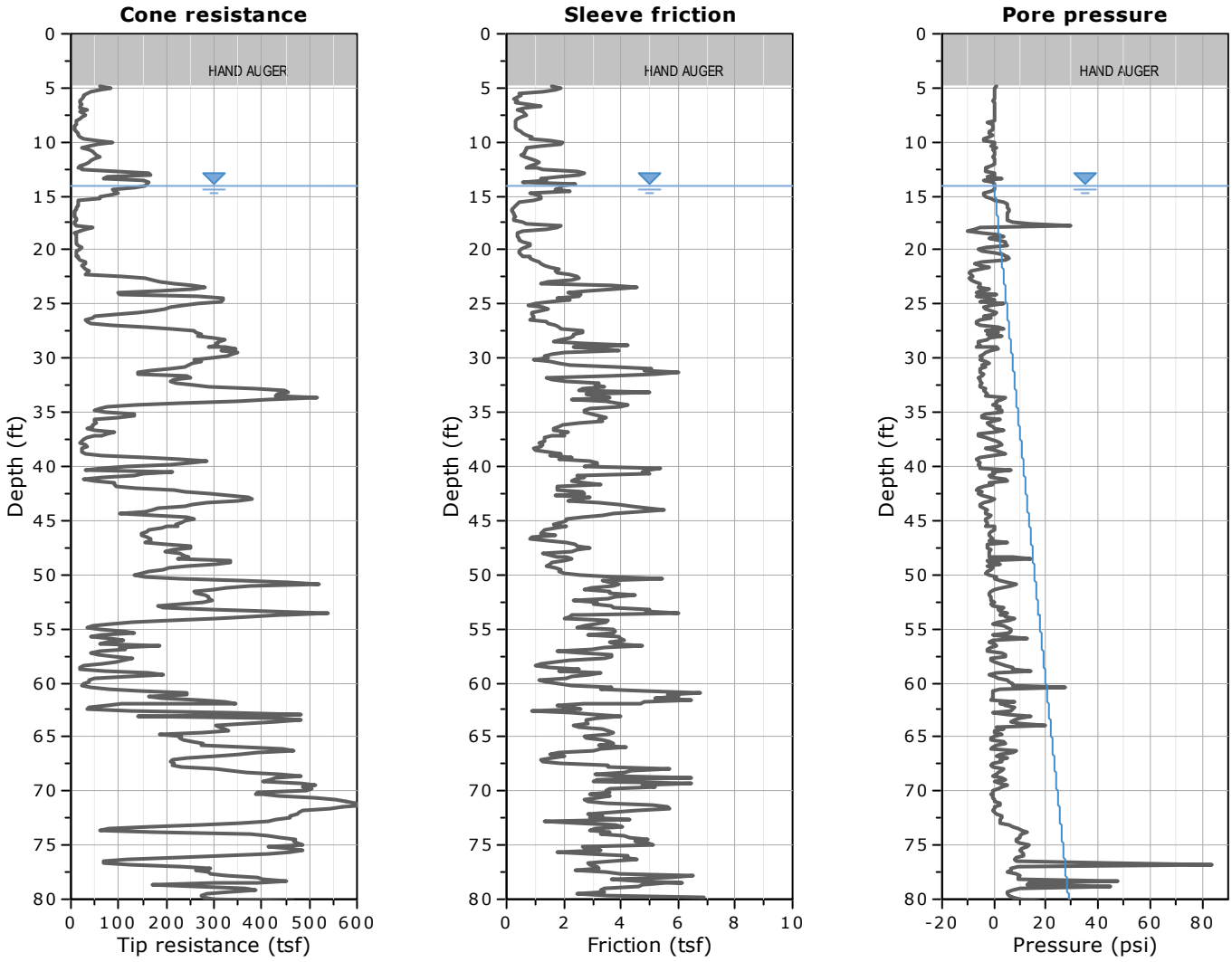
Est. GWL: 14.00 ft

Cone Type: 15cm²

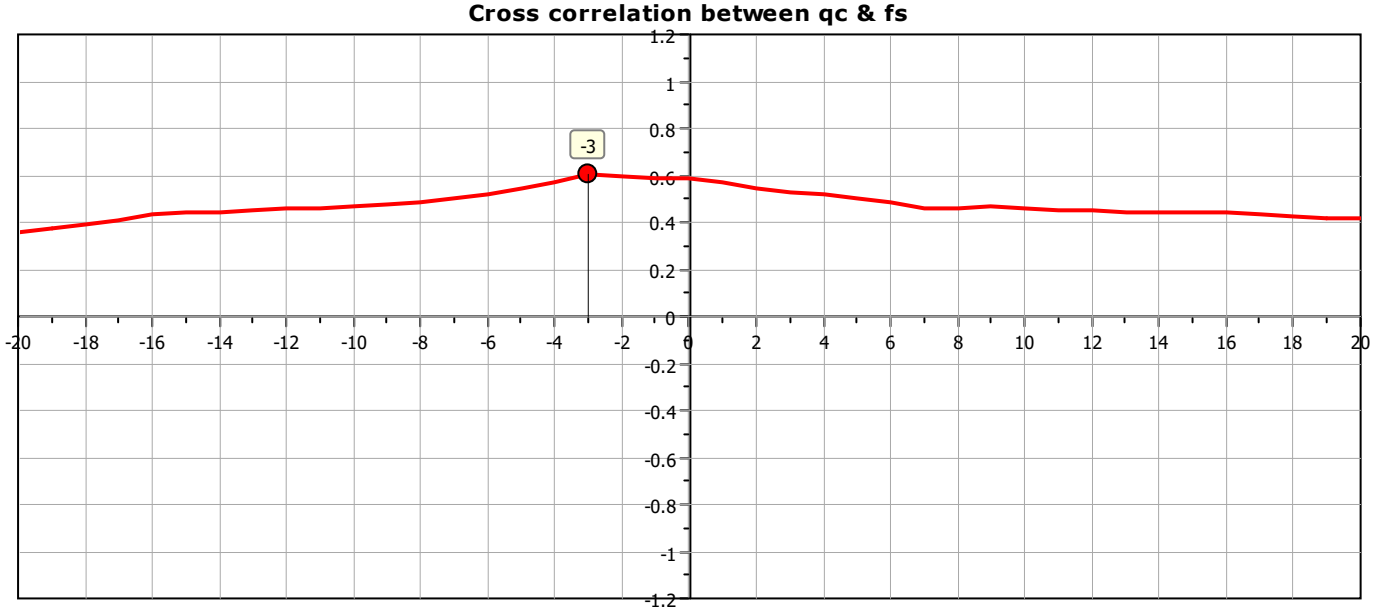
Cone Operator: JM-IY

Project: **Quincy Courthouse**

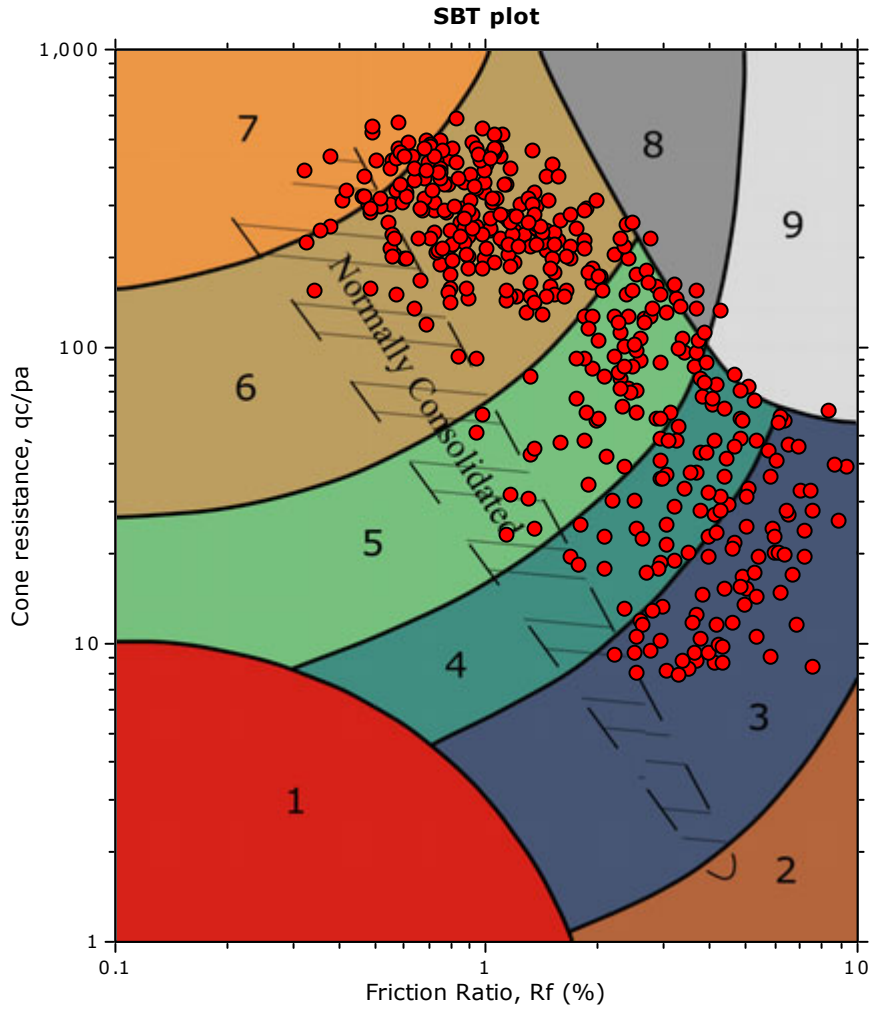
Location: **257 Lawrence Street, Quincy, CA 95971**

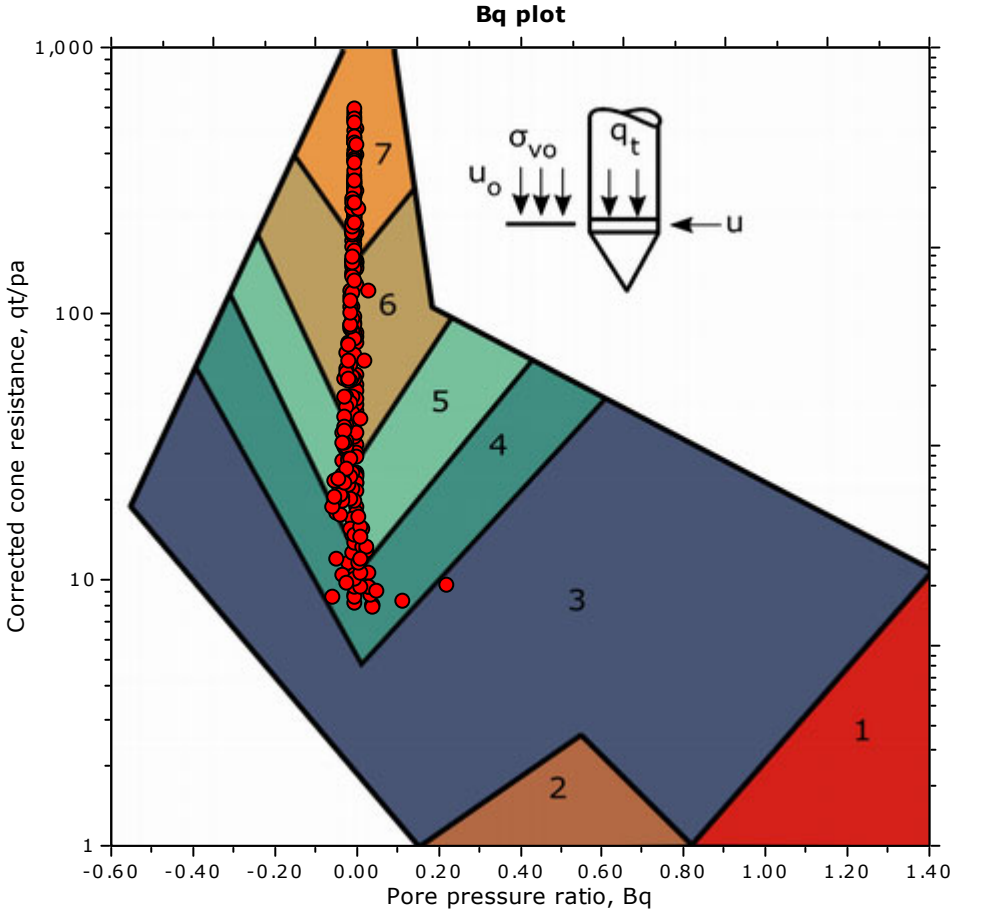


The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



SBT - Bq plots

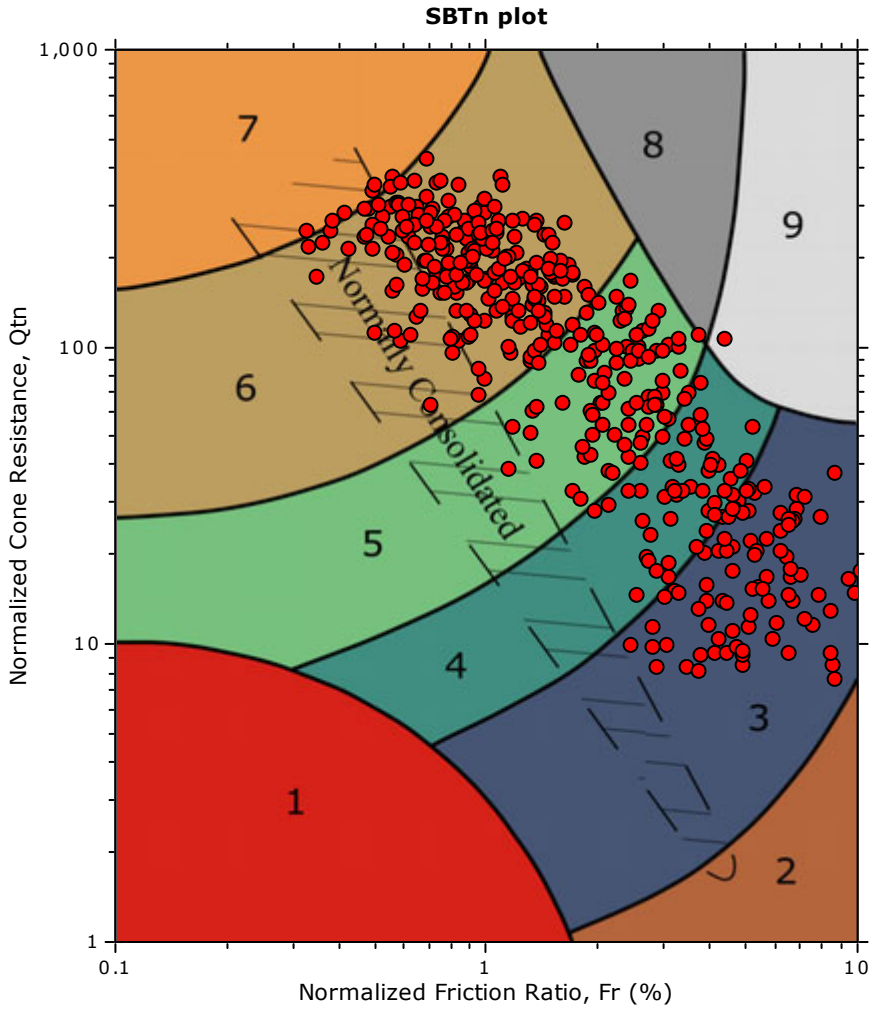


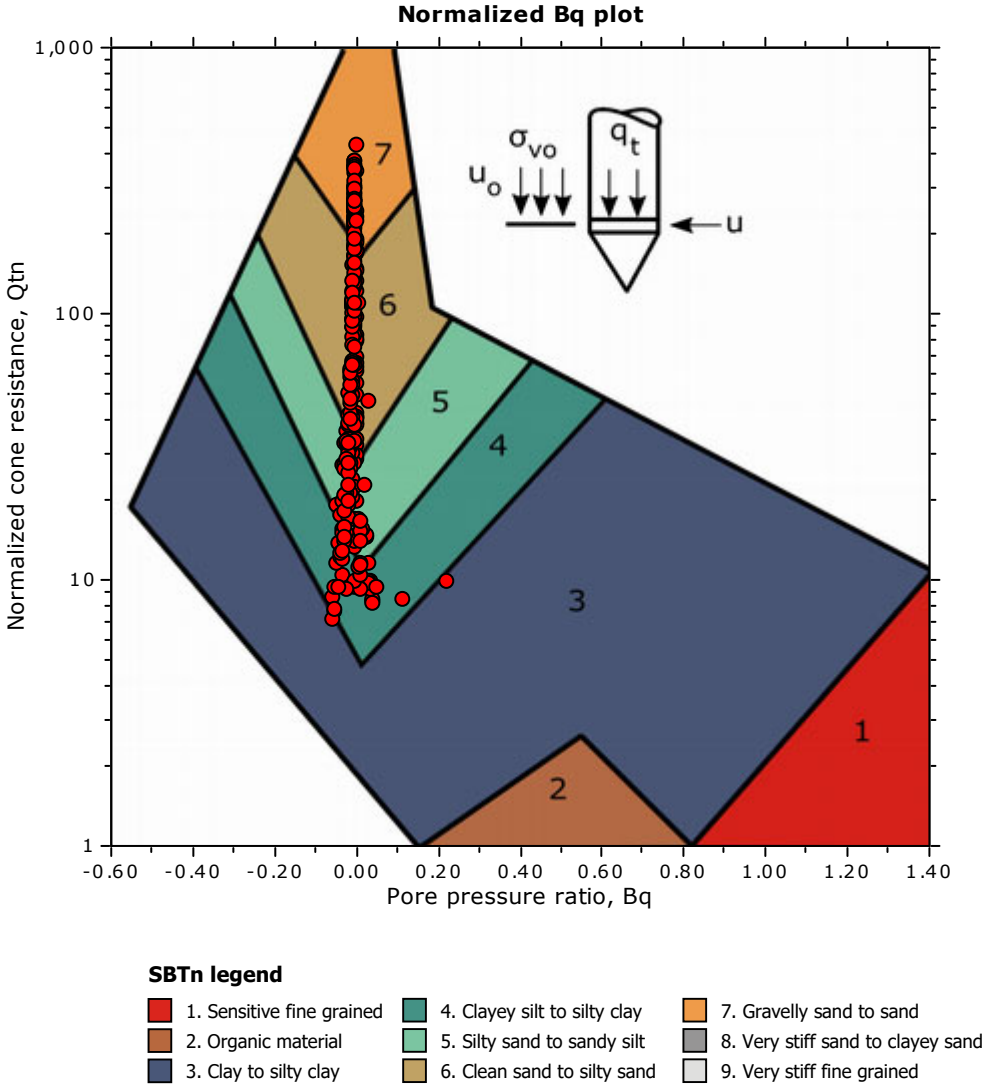


SBT legend

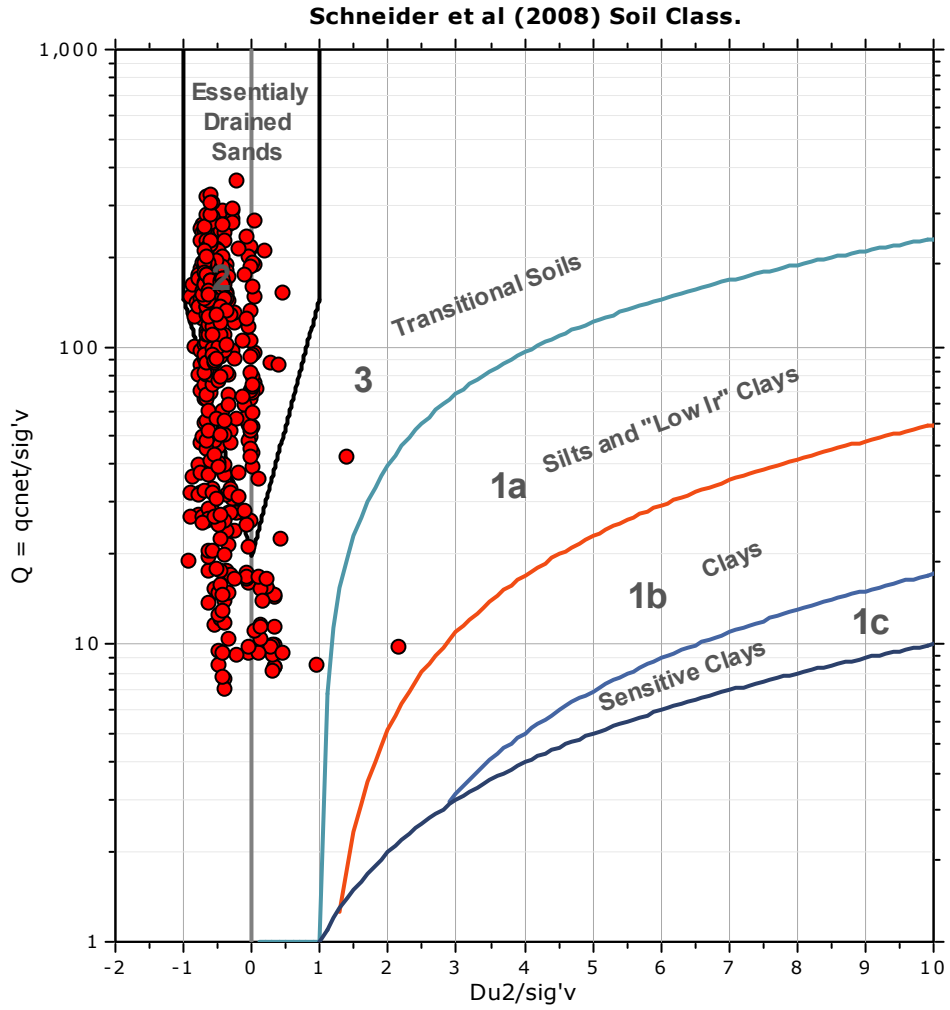
1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

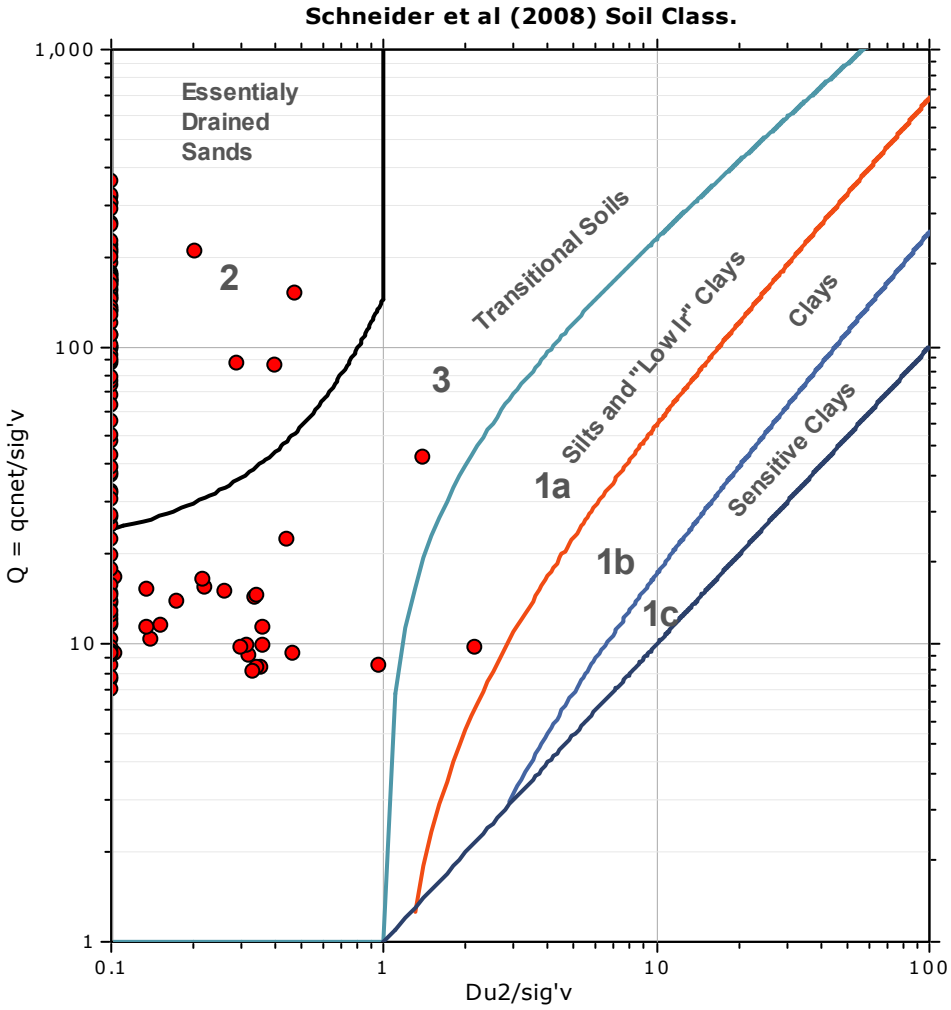
SBT - Bq plots (normalized)

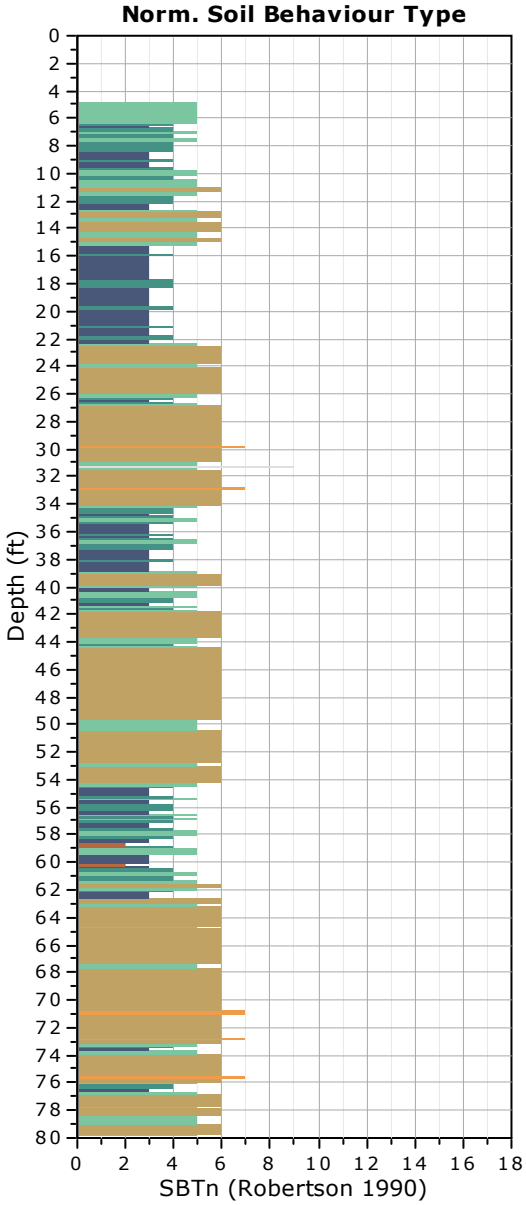


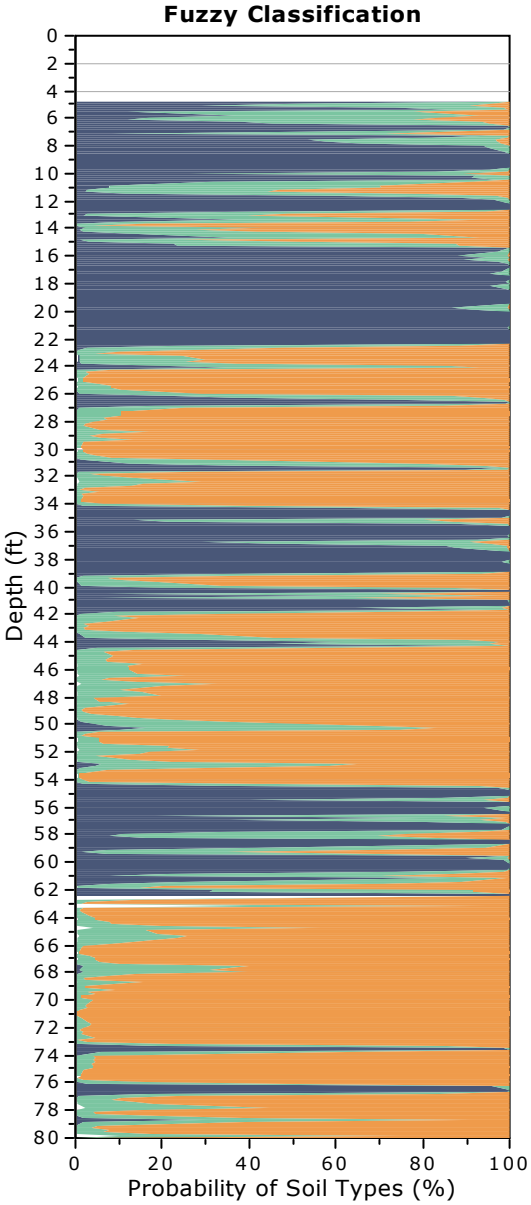


Bq plots (Schneider)









Fuzzy classifiaction legend

- Highly probable clayey soil
- Highly probable mixture soil
- Highly probable sandy soil

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

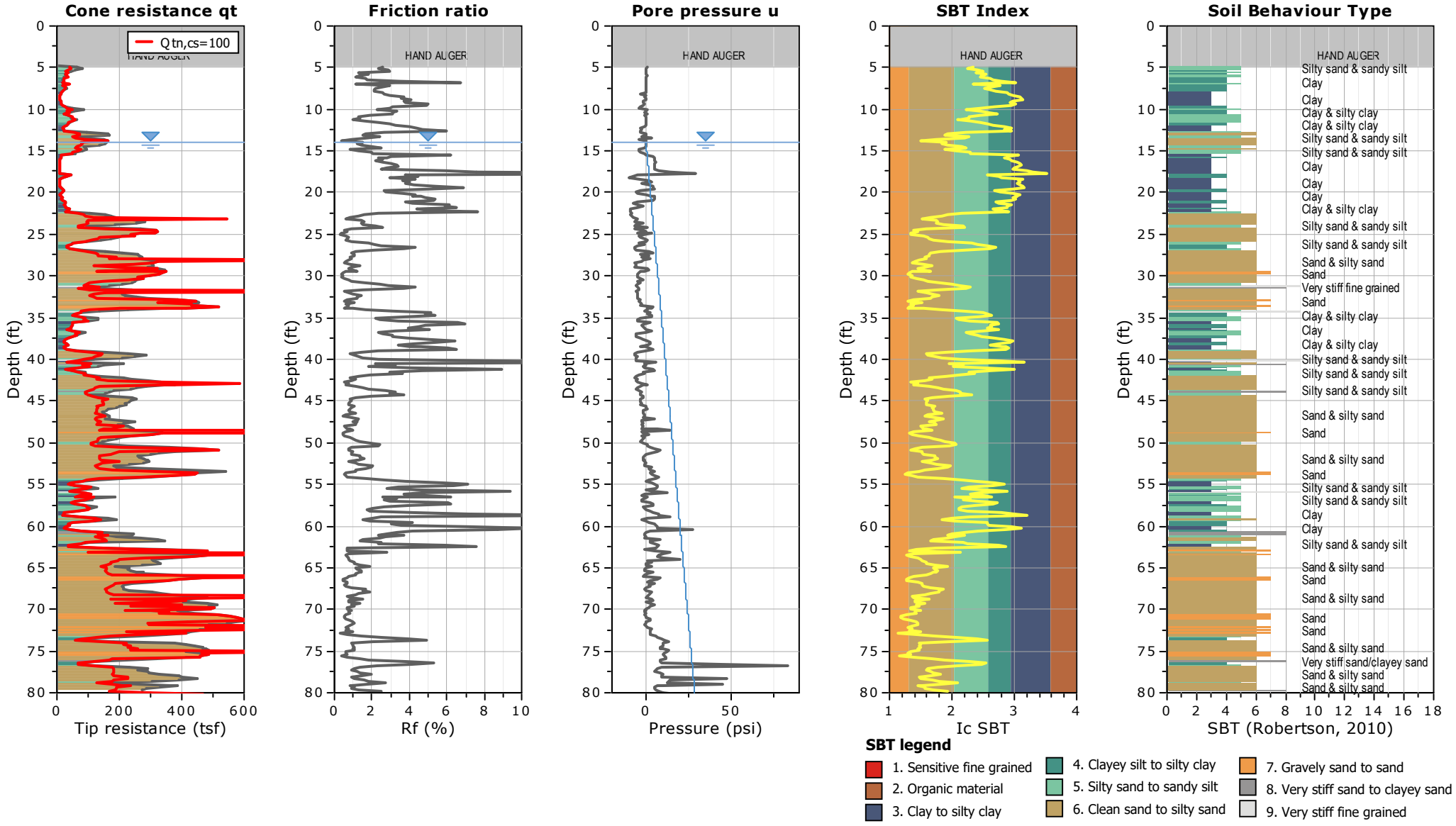
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

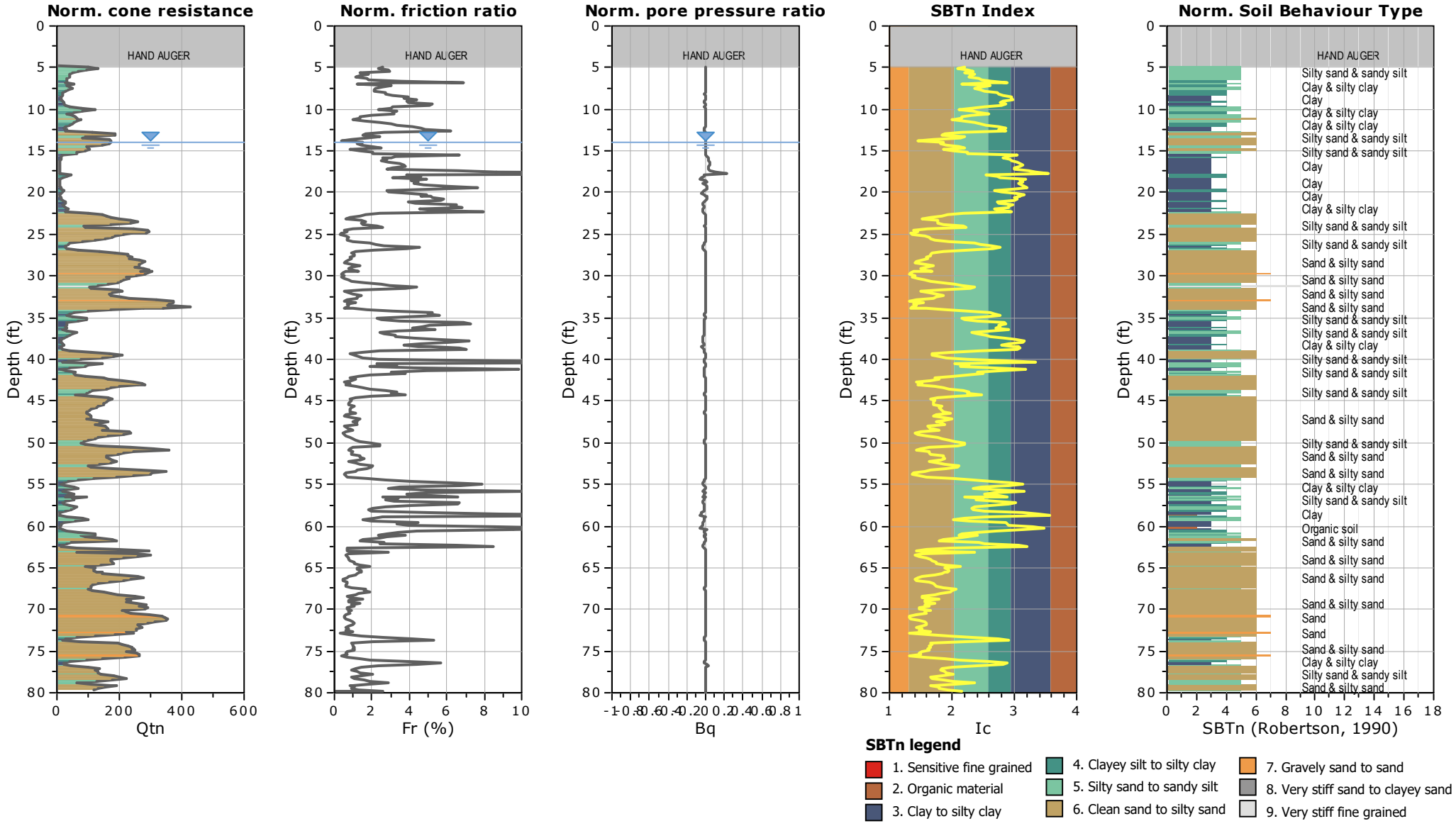
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

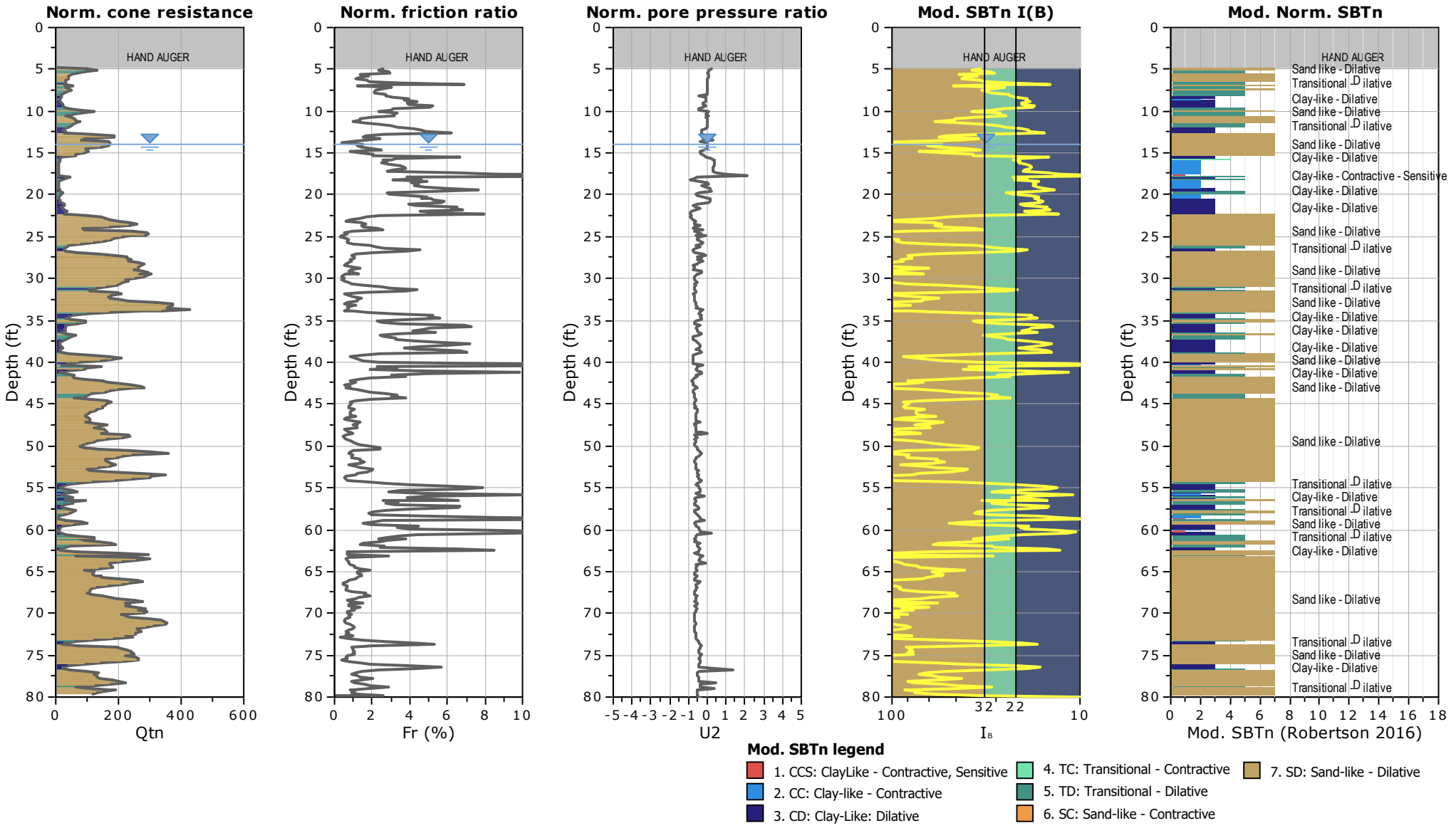
Est. GWL: 14.00 ft

Cone Type: 15cm²

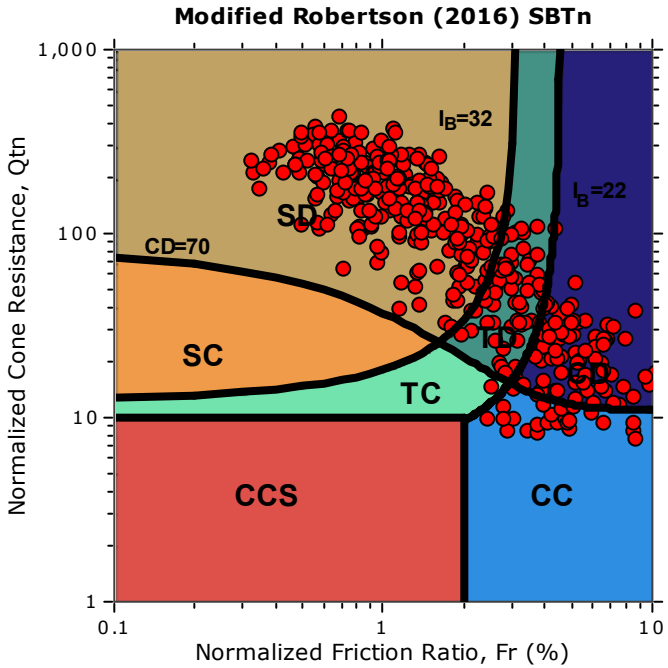
Cone Operator: JM-IY

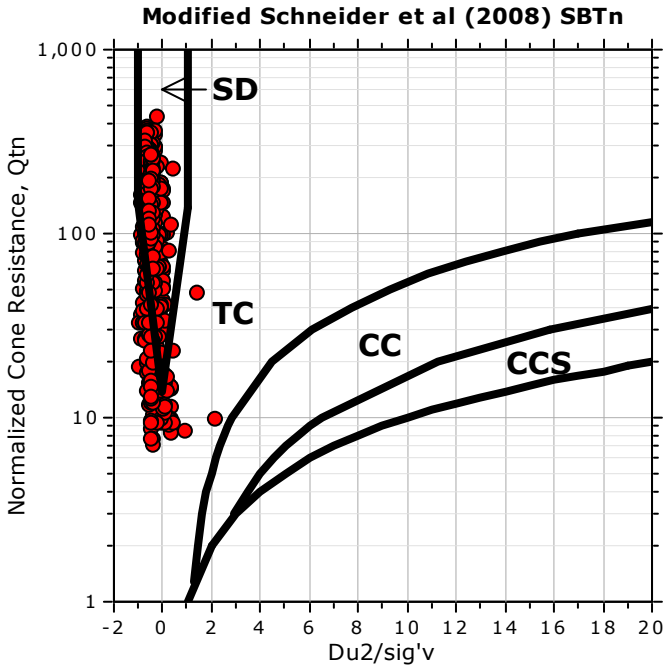
Project: Quincy Courthouse

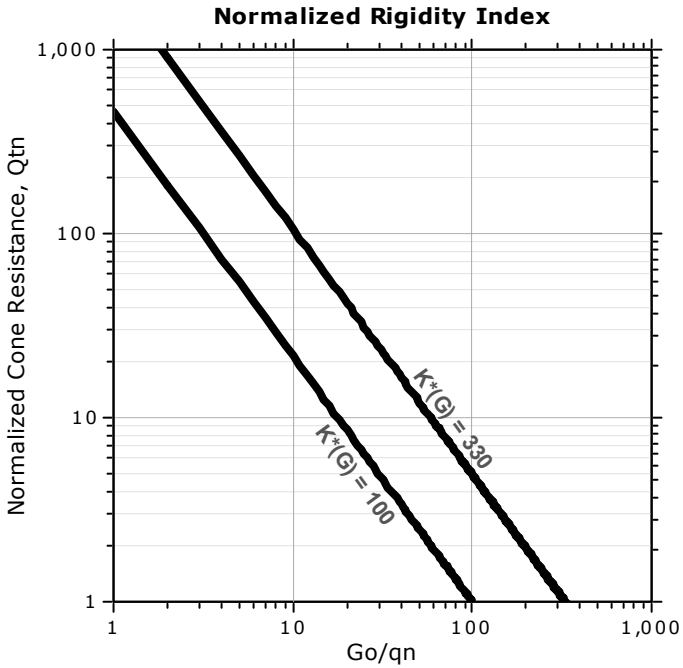
Location: 257 Lawrence Street, Quincy, CA 95971



Updated SBTn plots

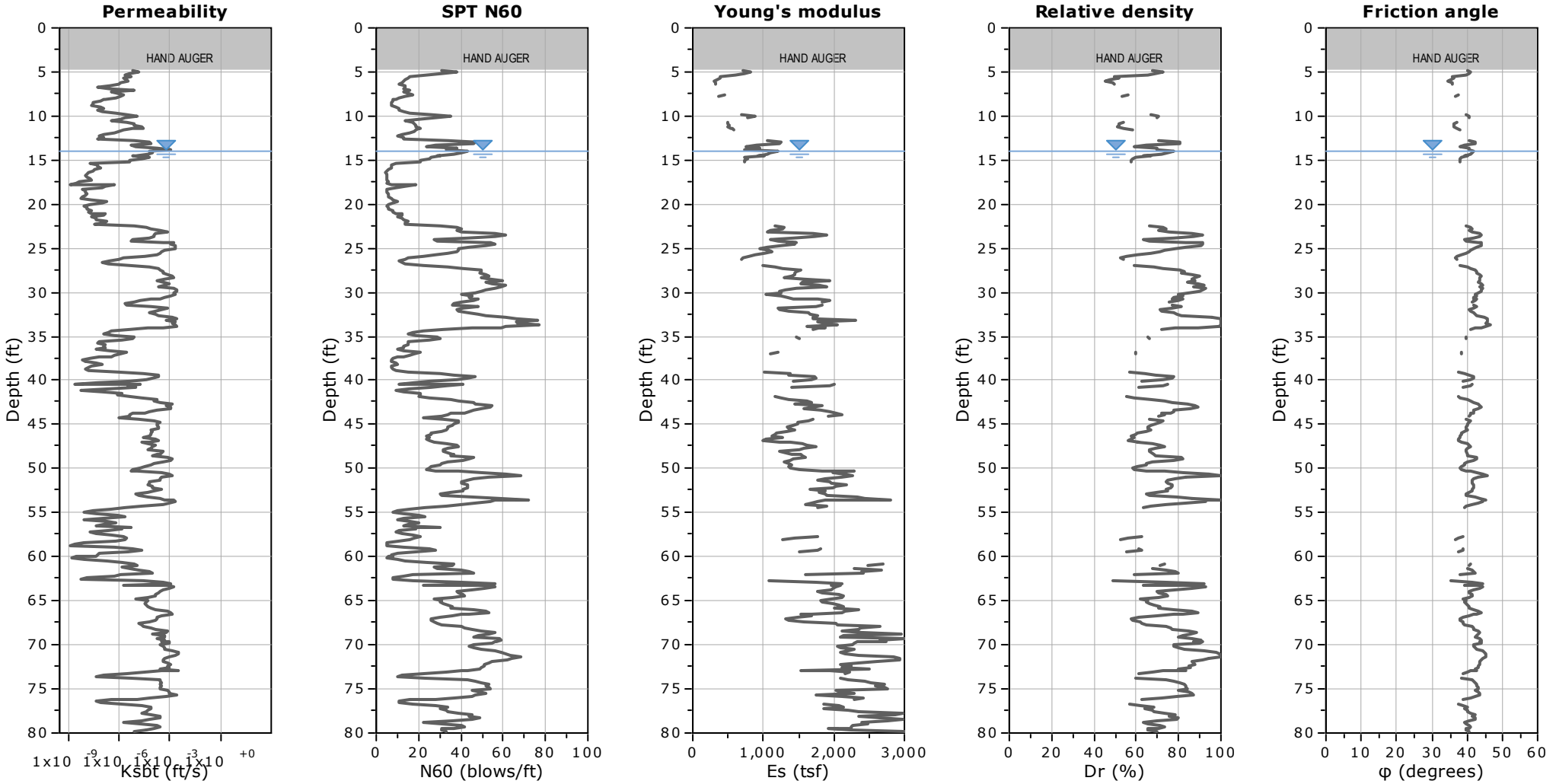






CCS: Clay-like - Contractive - Sensitive
CC: Clay-like - Contractive
CD: Clay-like - Dilative
TC: Transitional - Contractive
TD: Transitional - Dilative
SC: Sand-like - Contractive
SD: Sand-like - Dilative

K(G) > 330: Soils with significant microstructure (e.g. age/cementation)



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative density constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

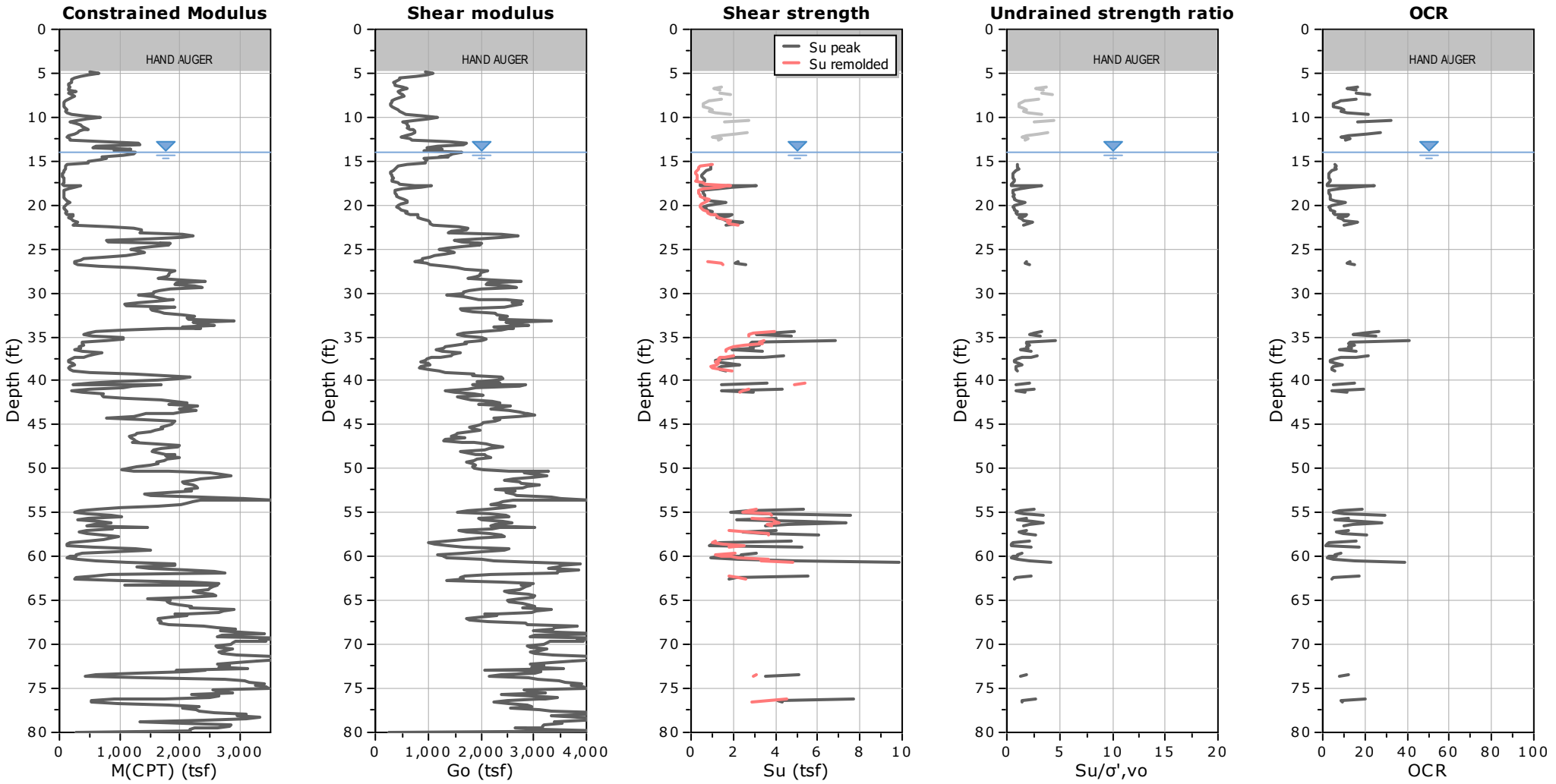
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)

Go: Based on variable *alpha* using I_c (Robertson, 2009)

Undrained shear strength cone factor for clays, N_{kt}: Auto

OCR factor for clays, N_{kt}: Auto

Flat Dilatometer Test data

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

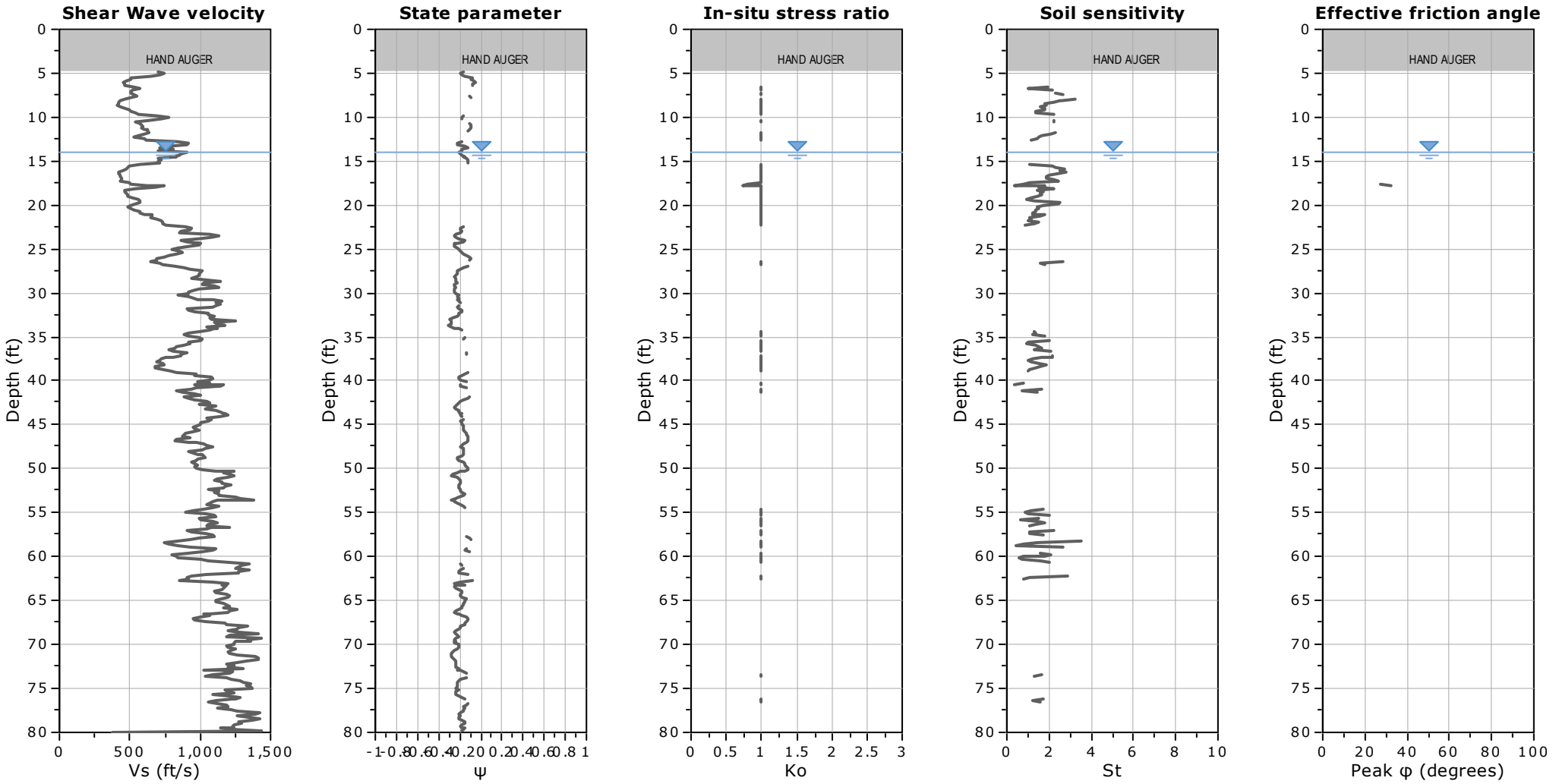
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

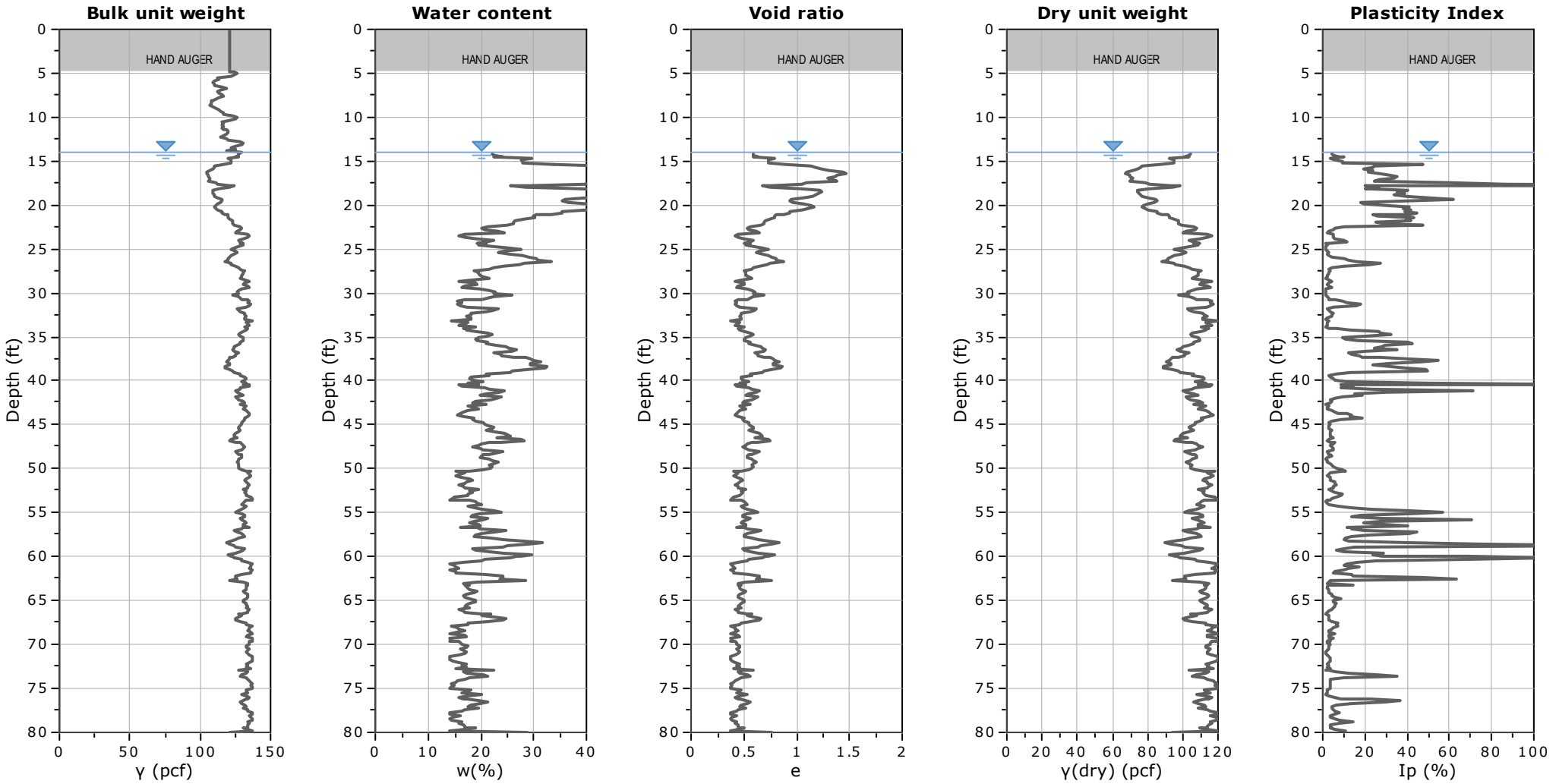
Est. GWL: 14.00 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-03

Total depth: 80.38 ft, Date: 9/16/2025

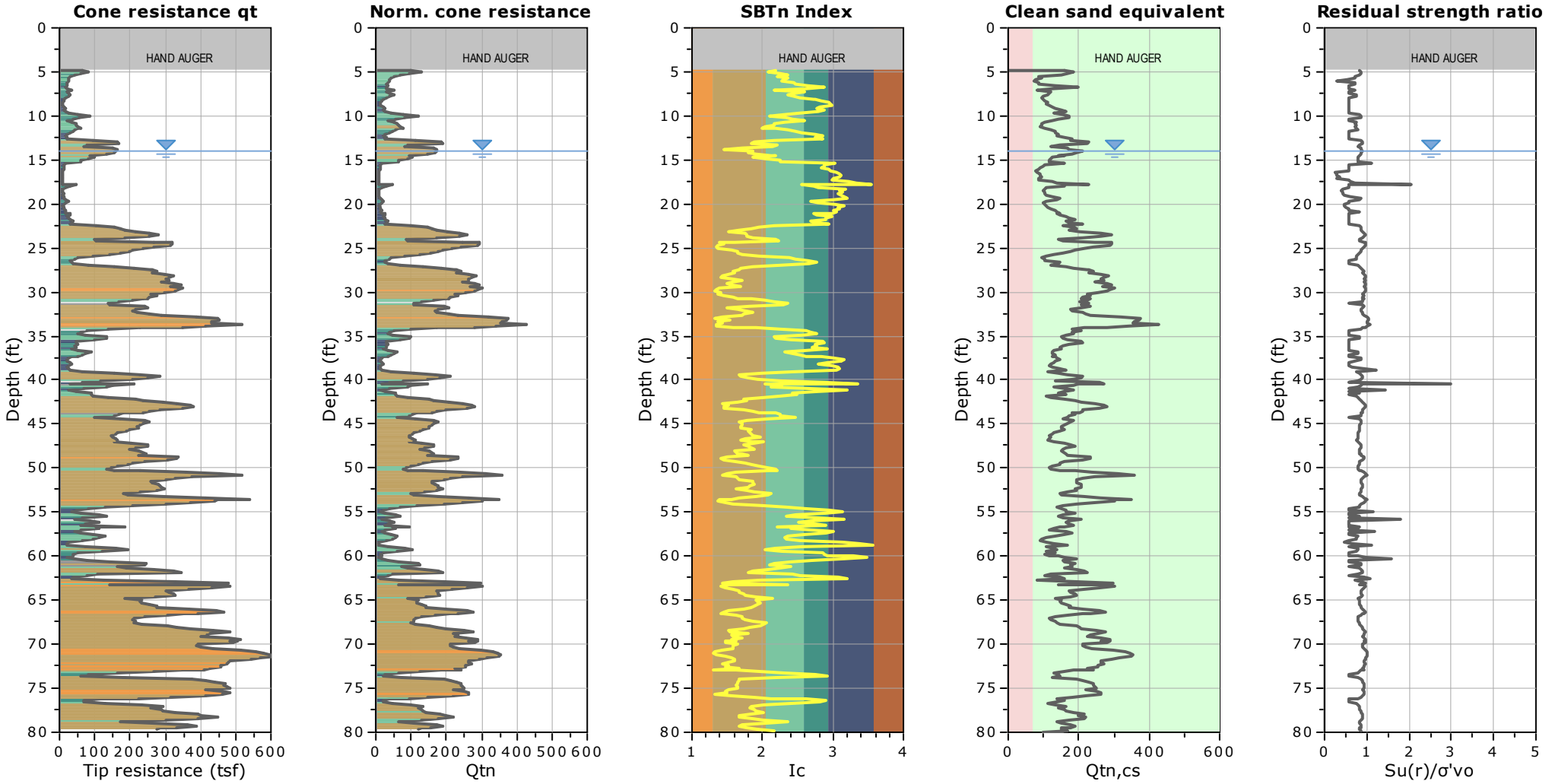
Est. GWL: 14.00 ft

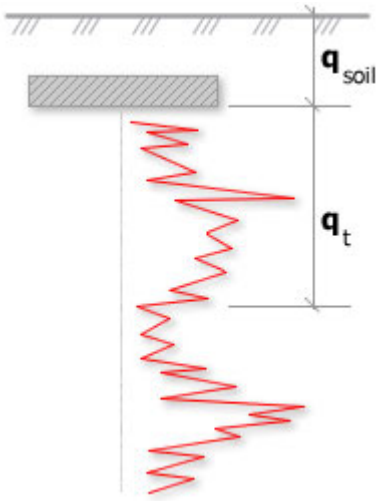
Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971

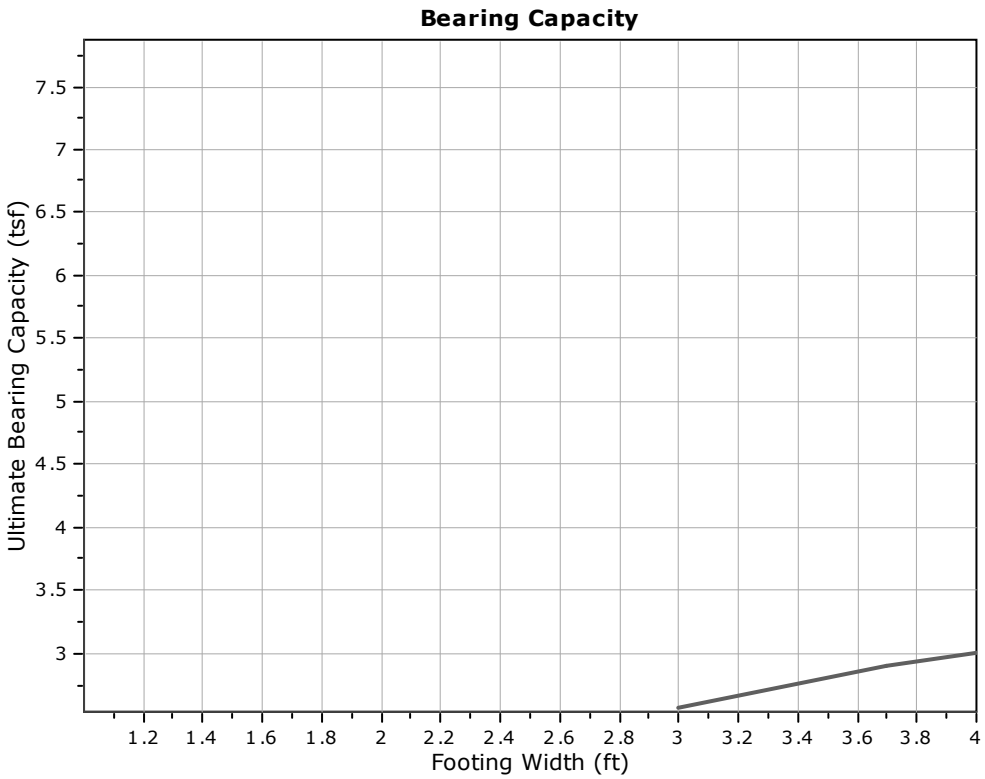




Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (ft)	Start Depth (ft)	End Depth (ft)	Ave. q_t (tsf)	R_k	Soil Press. (tsf)	Ult. bearing cap. (tsf)
1	3.00	1.60	6.10	12.34	0.20	0.10	2.56
2	3.70	1.60	7.15	14.03	0.20	0.10	2.90
3	4.40	1.60	8.20	15.22	0.20	0.10	3.14
4	5.10	1.60	9.25	14.64	0.20	0.10	3.02
5	5.80	1.60	10.30	17.71	0.20	0.10	3.64
6	6.50	1.60	11.35	20.71	0.20	0.10	4.24
7	7.20	1.60	12.40	21.79	0.20	0.10	4.45
8	7.90	1.60	13.45	27.47	0.20	0.10	5.59
9	8.60	1.60	14.50	36.58	0.20	0.10	7.41
10	9.30	1.60	15.55	38.74	0.20	0.10	7.84
11	10.00	1.60	16.60	36.67	0.20	0.10	7.43
12	10.70	1.60	17.65	35.01	0.20	0.10	7.10
13	11.40	1.60	18.70	34.20	0.20	0.10	6.94
14	12.10	1.60	19.75	32.91	0.20	0.10	6.68
15	12.80	1.60	20.80	31.94	0.20	0.10	6.48

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236 \right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a} \right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$$

(applicable only to $I_c < I_{c_cutoff}$)

:: Relative Density, Dr (%) ::

$$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$$ (applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: State Parameter, ψ ::

$$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$$

:: Drained Friction Angle, φ (°) ::

$$\varphi = \varphi'_{cv} + 15.94 \cdot \log(Q_{tn,cs}) - 26.88$$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$
$\alpha = 14$ for $Q_{tn} > 14$
$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$
$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \geq 2.20$

$$M_{CPT} = 0.03 \cdot (q_t - \sigma_v) \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Small strain shear Modulus, Go (MPa) ::

$$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho} \right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))} \right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: In situ Stress Ratio, Ko ::

$$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Peak Friction Angle, φ' (°) ::

$$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$$

(applicable for $0.10 < B_q < 1.00$)

References

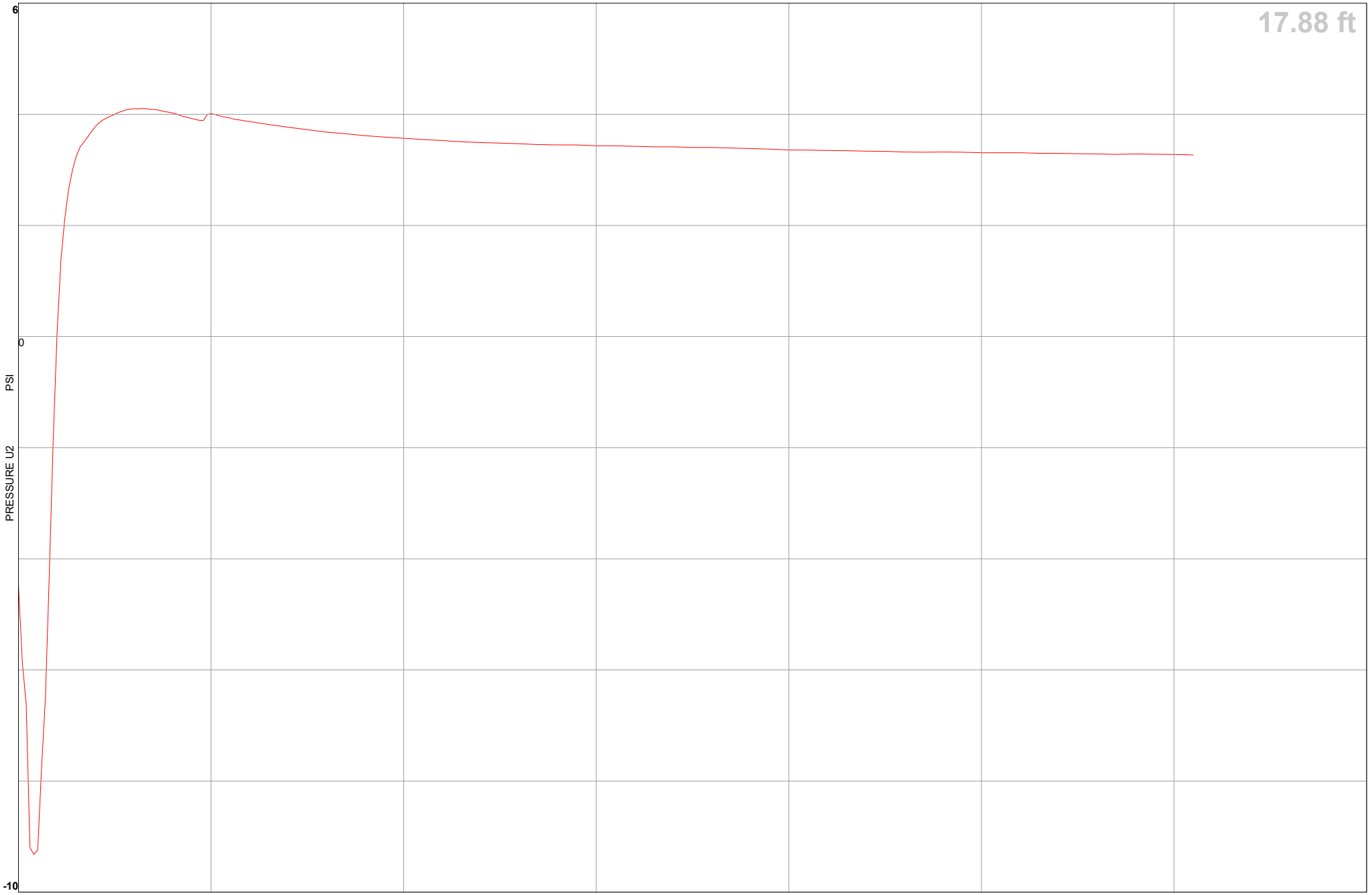
• Robertson, P.K., Cabal K.L., Guide to Cone Penetration Testing for Geotechnical Engineering, Gregg Drilling & Testing, Inc., 5th Edition, November 2012

• Robertson, P.K., Interpretation of Cone Penetration Tests - a unified approach., Can. Geotech. J. 46(11): 1337–1355 (2009)

• N Barounis, J Philpot, Estimation of in-situ water content, void ratio, dry unit weight and porosity using CPT for saturated sands, Proc. 20th NZGS Geotechnical Symposium

Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-03	Date and Time	9/16/2025 12:48:32 PM	
Equilized Pressure	3.2	EST GW Depth During Test	10.3	



Atlas Technical Consultants

https://www.oneatlas.com/

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

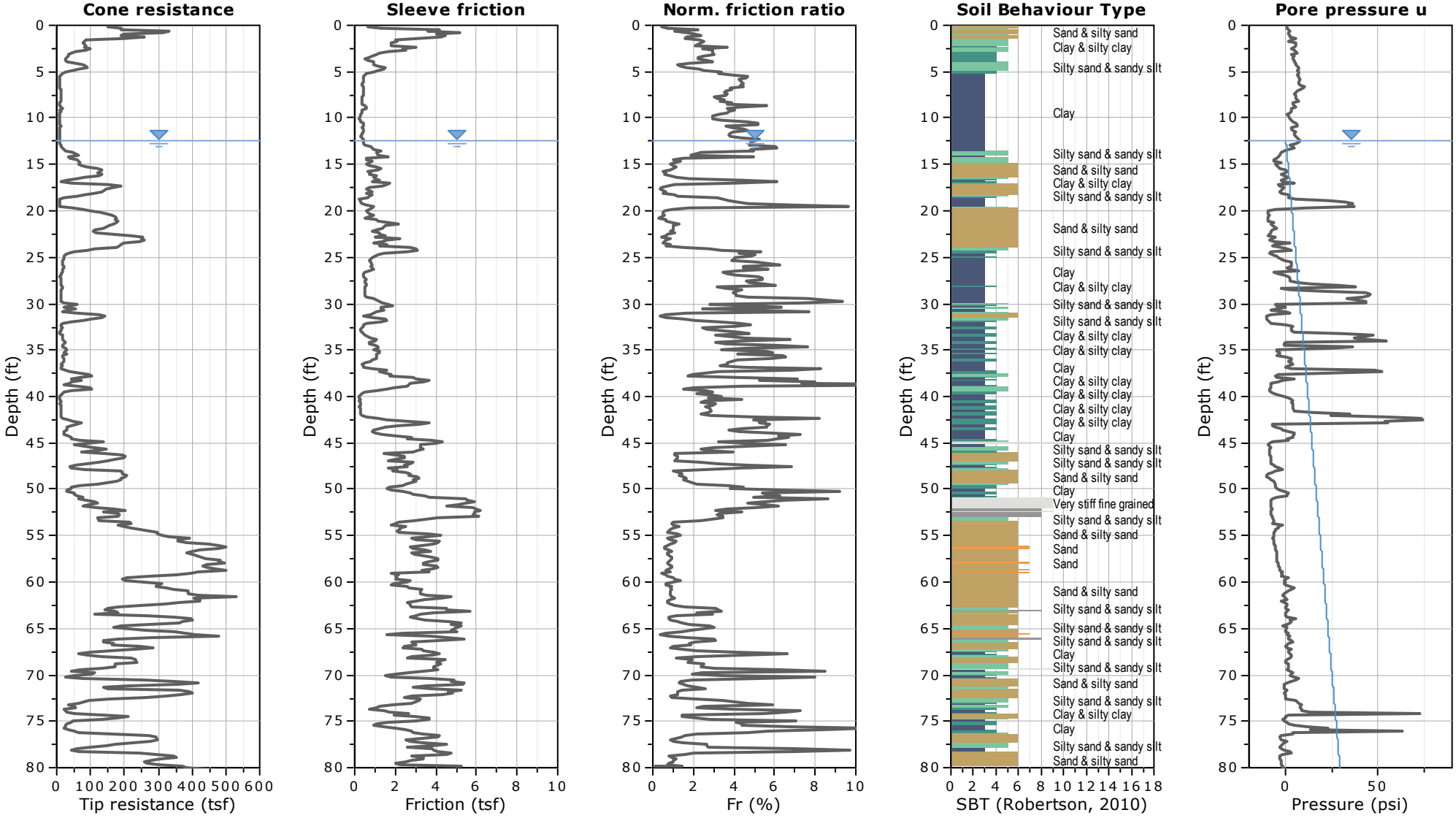
Est. GWL: 12.50 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Atlas Technical Consultants

https://www.oneatlas.com/

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

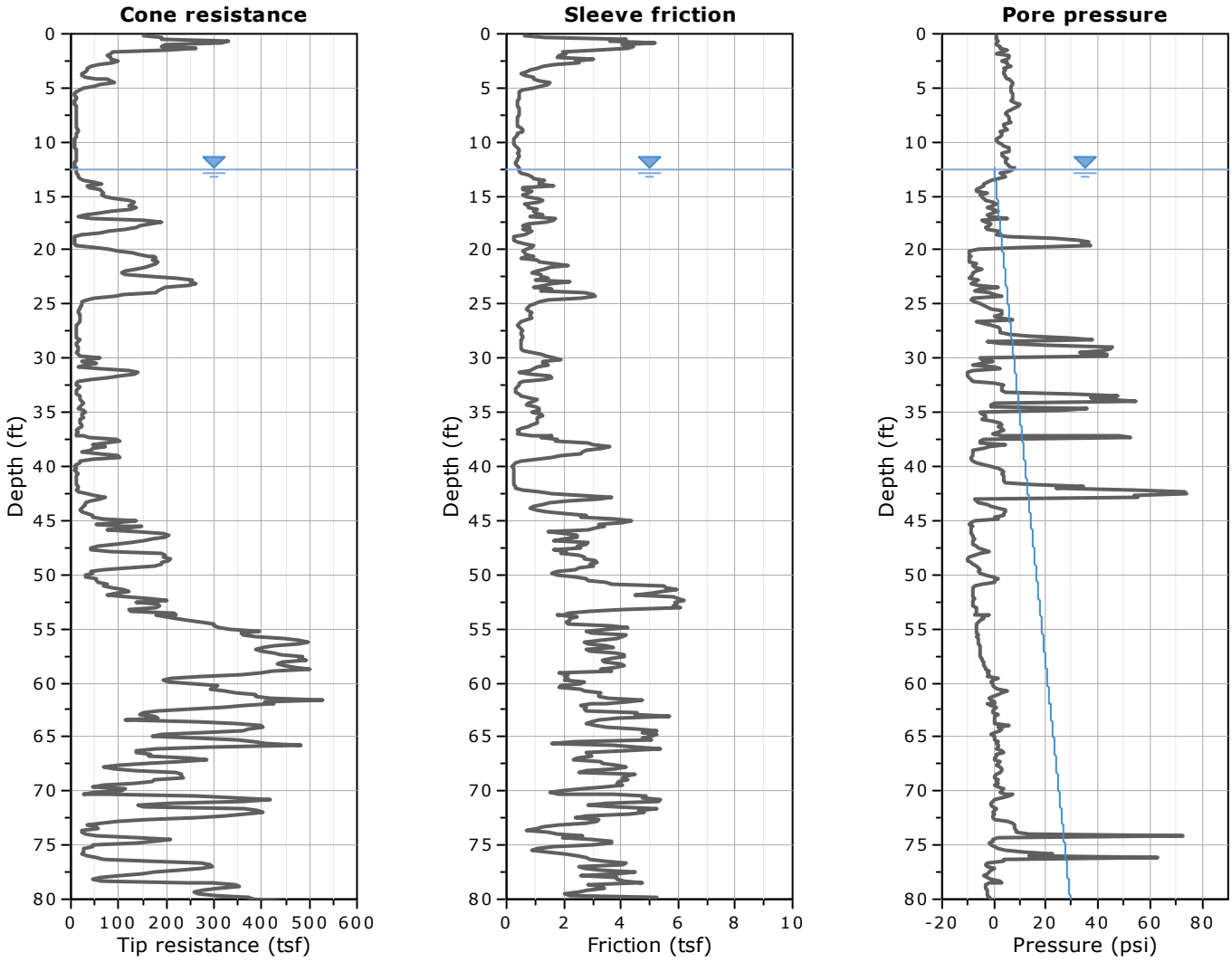
Est. GWL: 12.50 ft

Cone Type: 15cm²

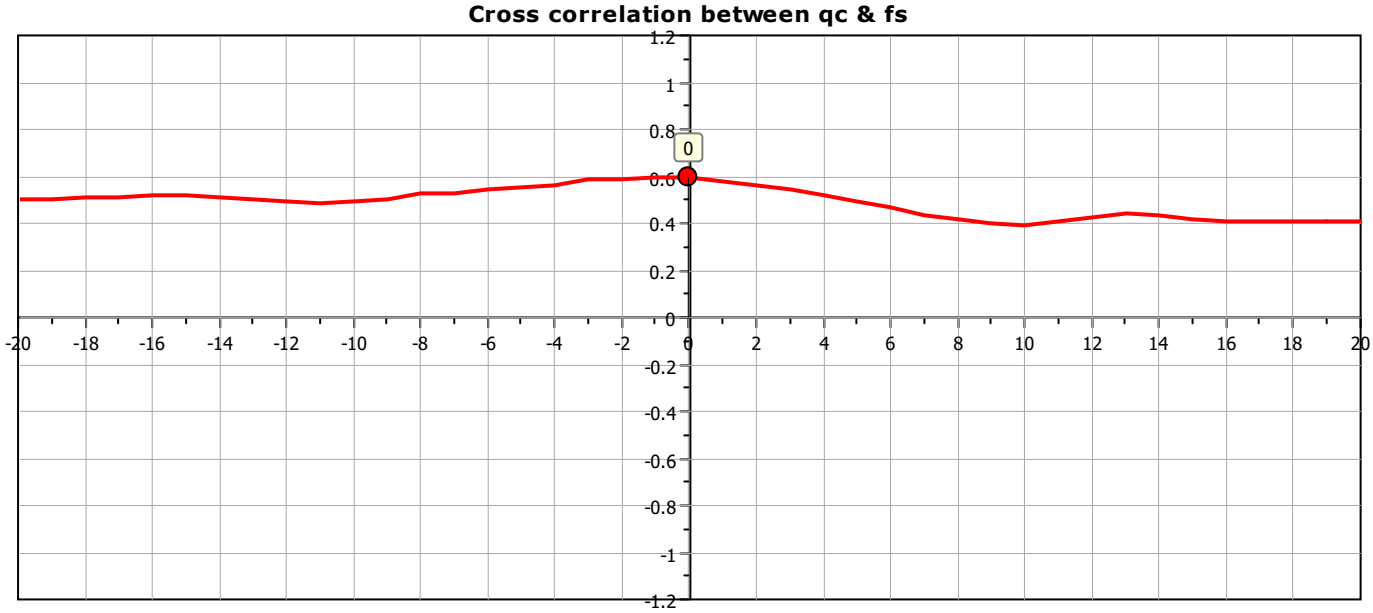
Cone Operator: JM-IY

Project: **Quincy Courthouse**

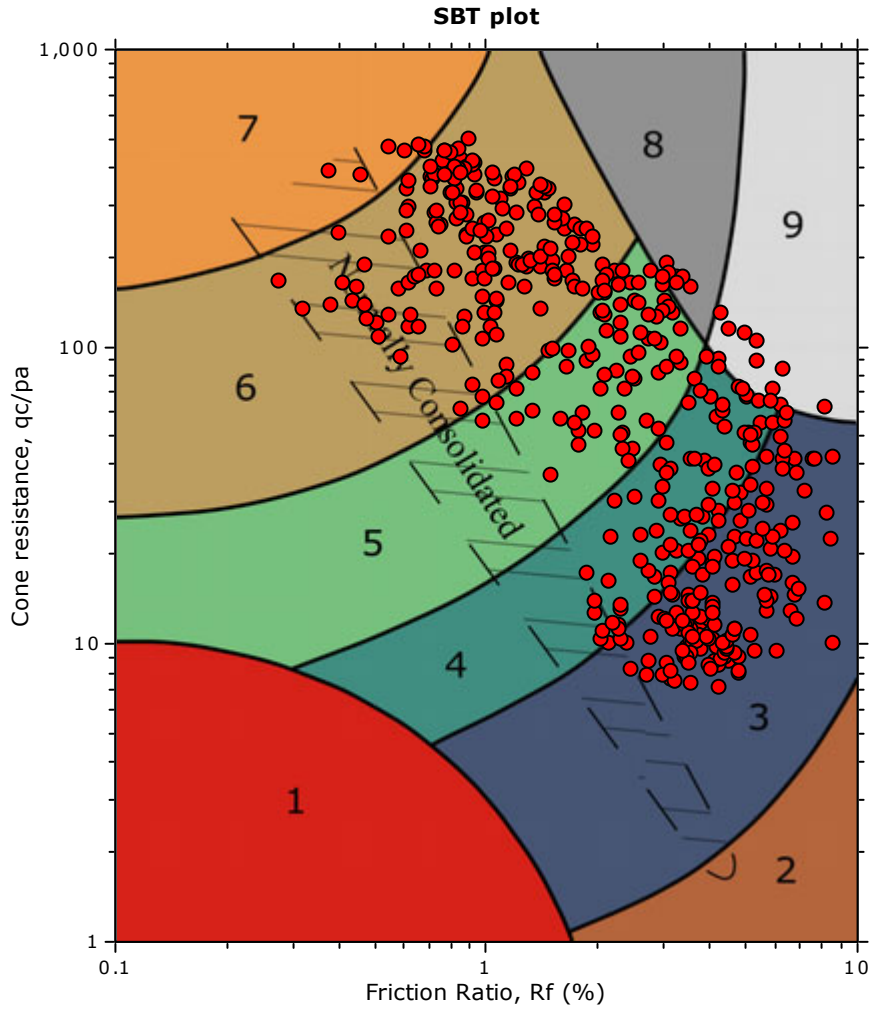
Location: **257 Lawrence Street, Quincy, CA 95971**

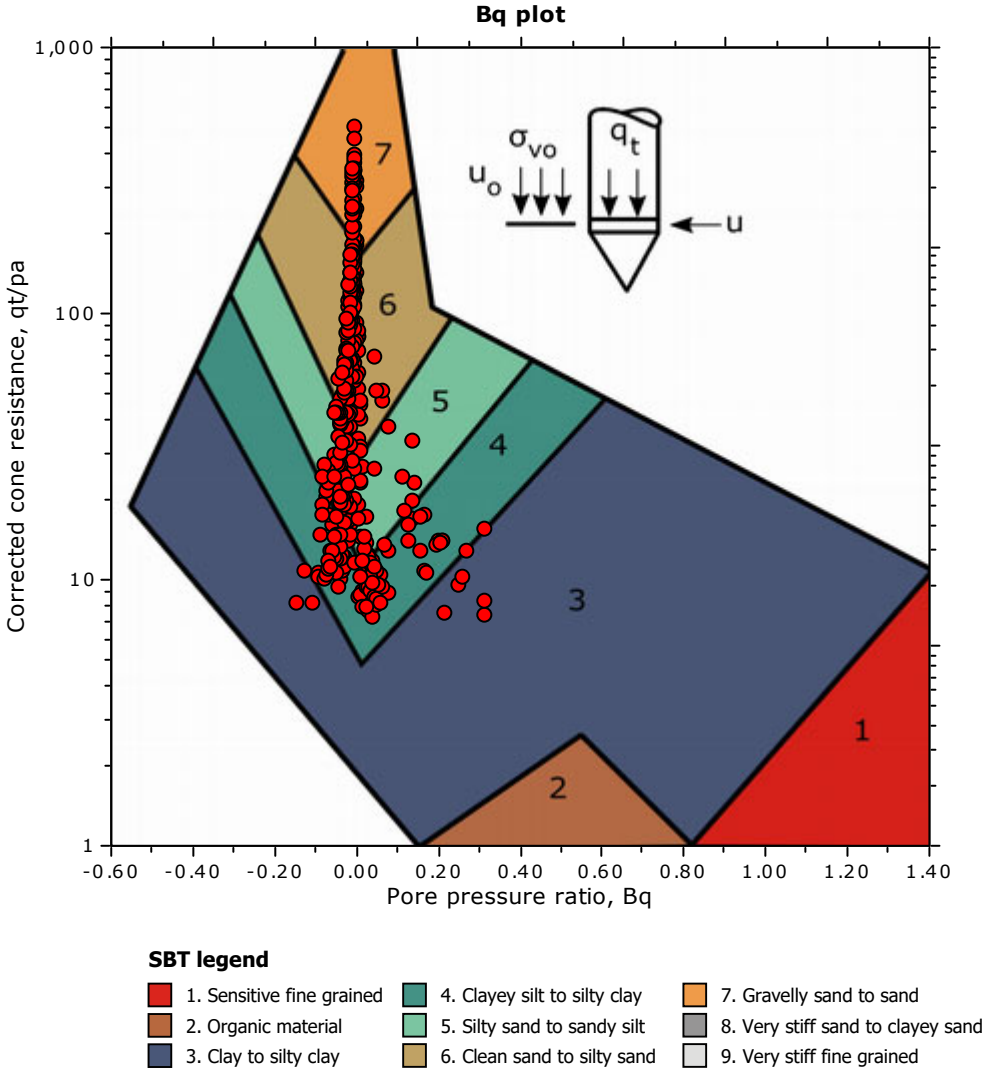


The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).

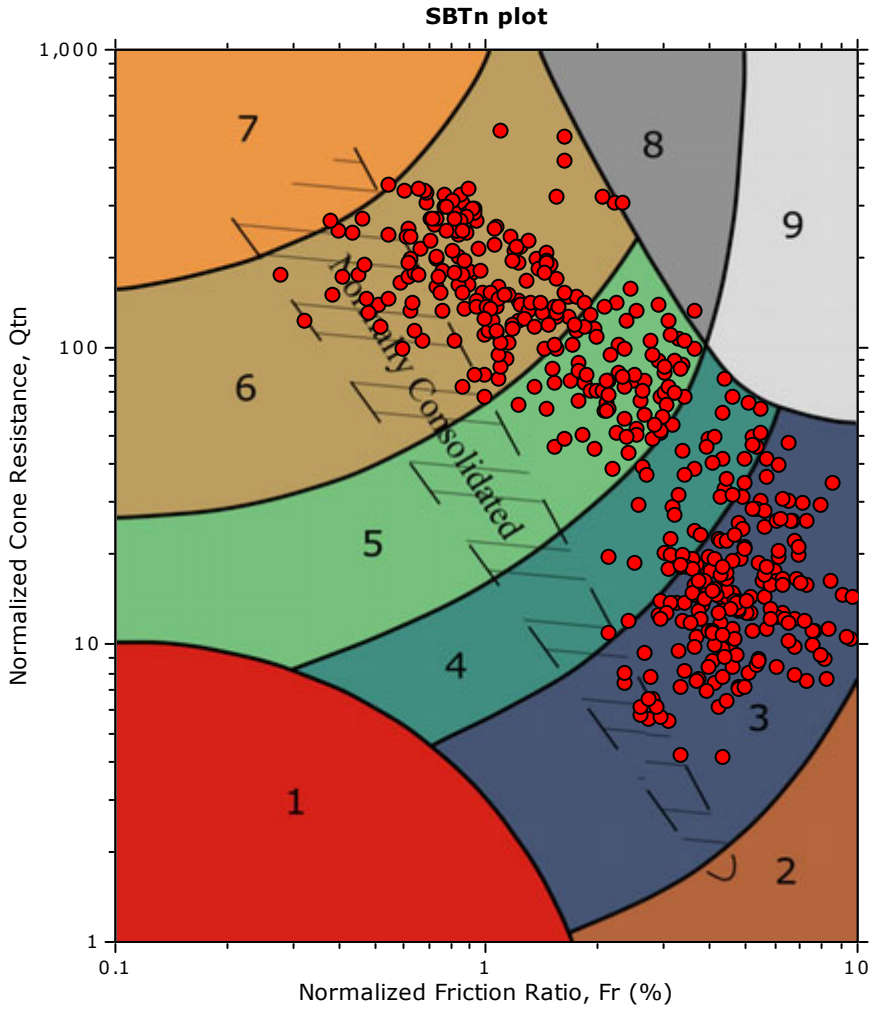


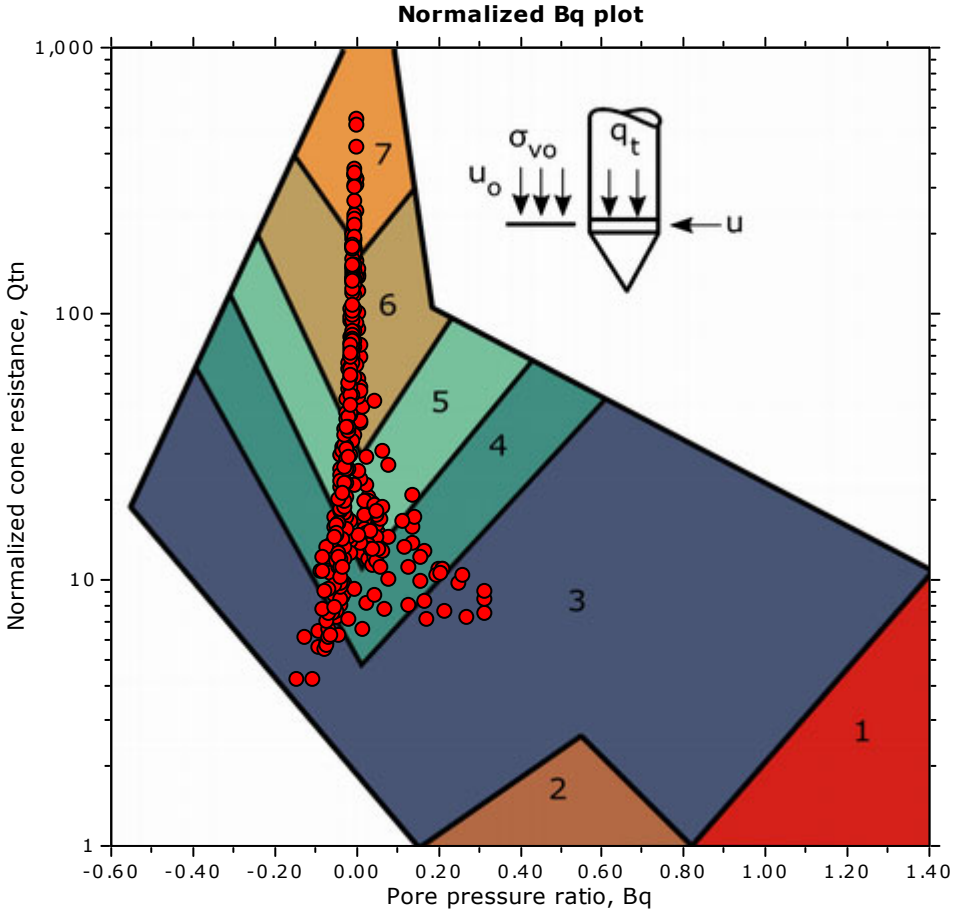
SBT - Bq plots


SBT plot
1,000
100
10
1
0.1
1
10
Cone resistance, qc/pa
Friction Ratio, Rf (%)
Normally Consolidated
1
2
3
4
5
6
7
8
9


Bq plot
1,000
100
10
1
-0.60
-0.40
-0.20
0.00
0.20
0.40
0.60
0.80
1.00
1.20
1.40
Corrected cone resistance, qt/pa
Pore pressure ratio, Bq
σvo
uo
qt
u
1
2
3
4
5
6
7
SBT legend
1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravelly sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

SBT - Bq plots (normalized)

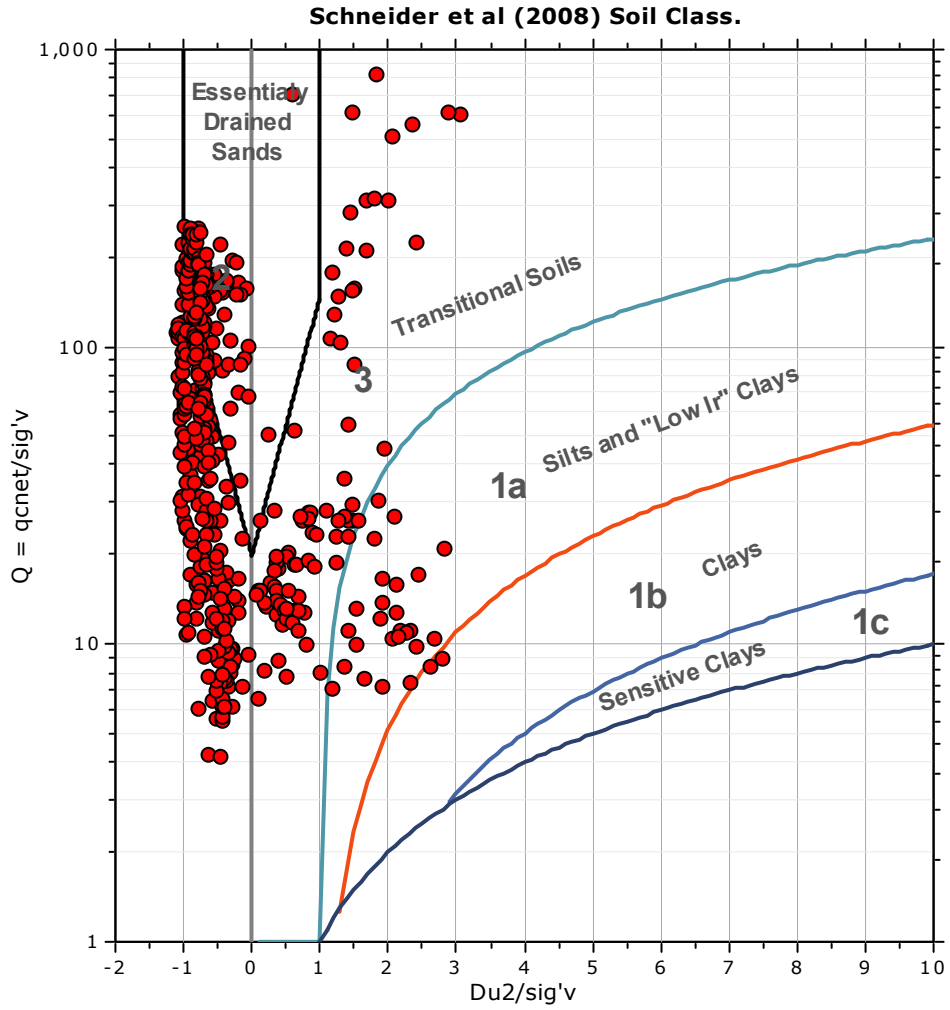


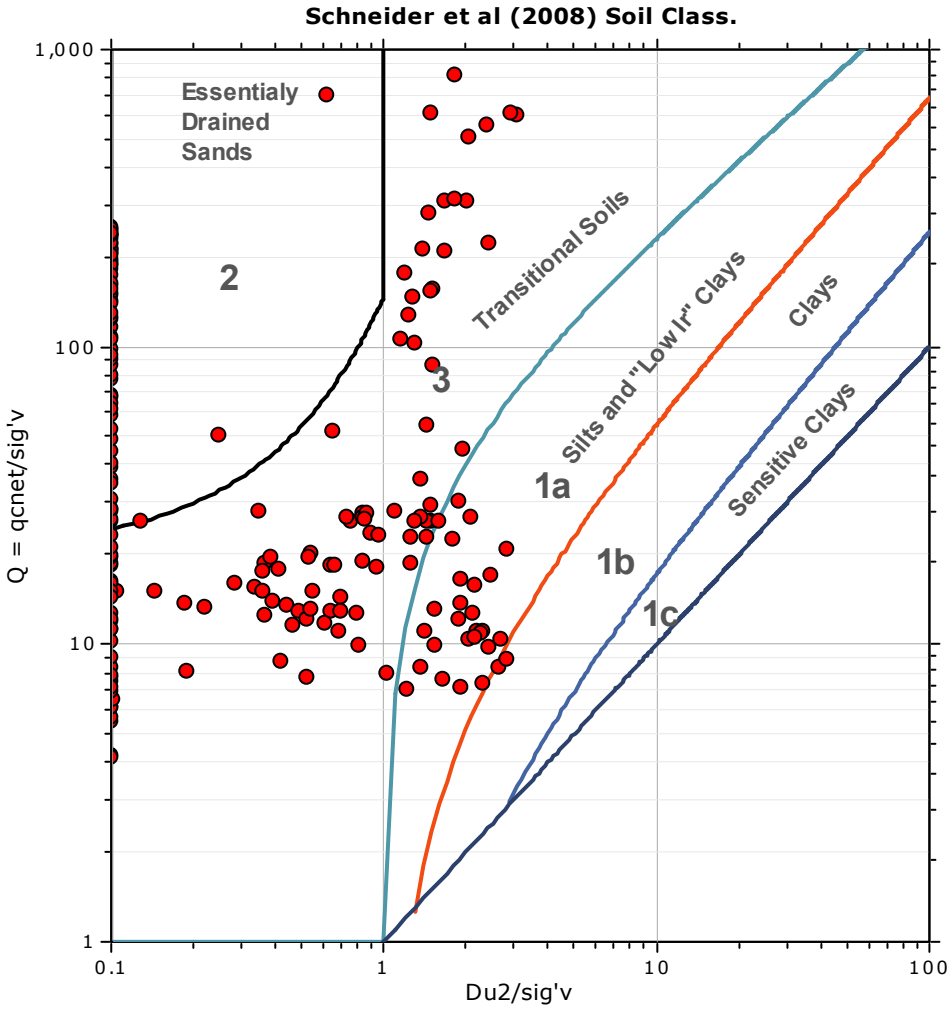


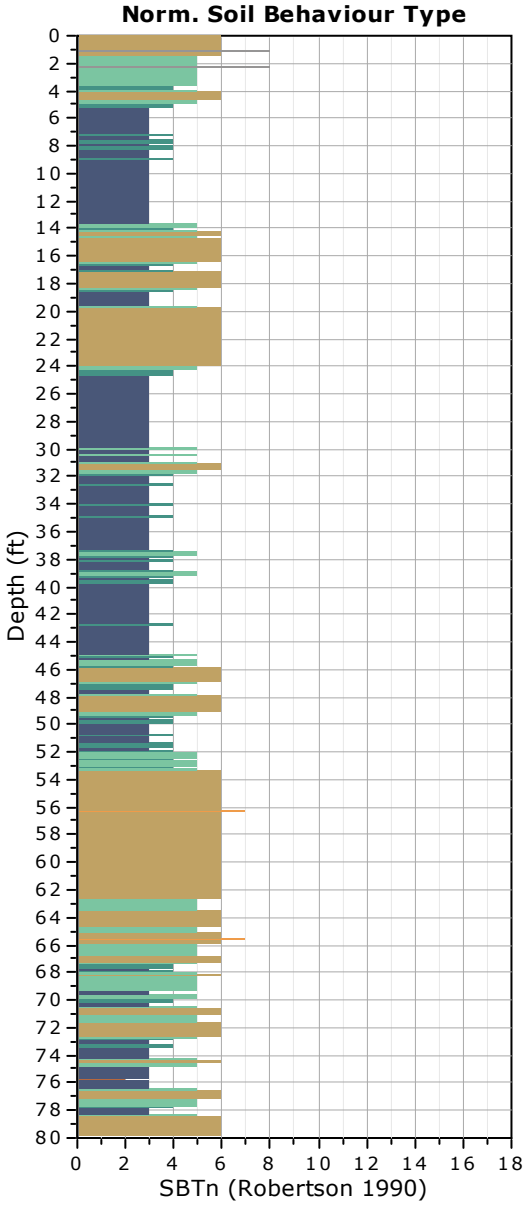
SBTn legend

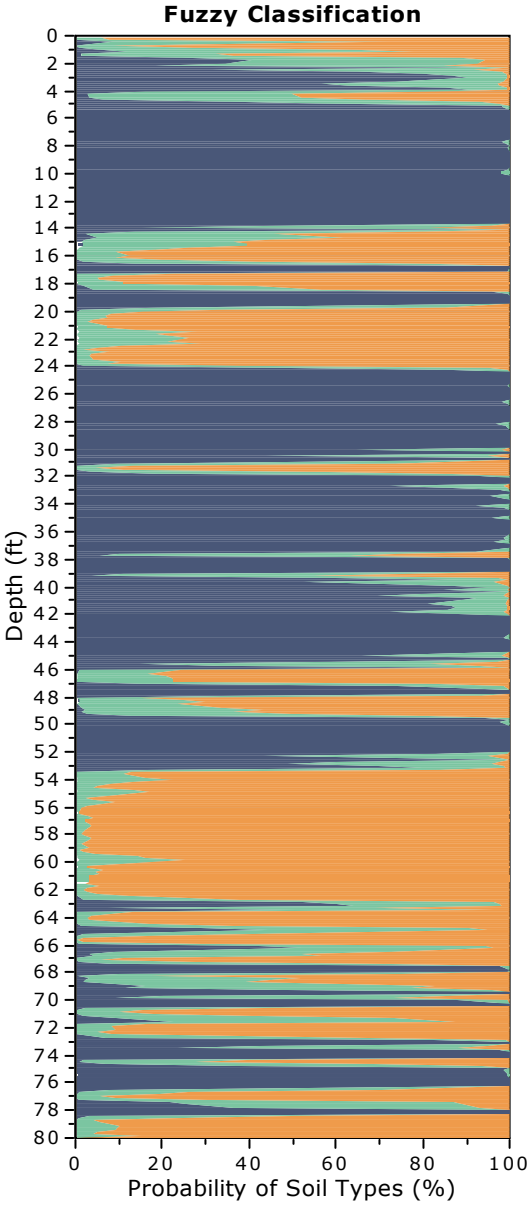
1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to clayey sand
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

Bq plots (Schneider)









Fuzzy classifiaction legend

- Highly probable clayey soil
- Highly probable mixture soil
- Highly probable sandy soil

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

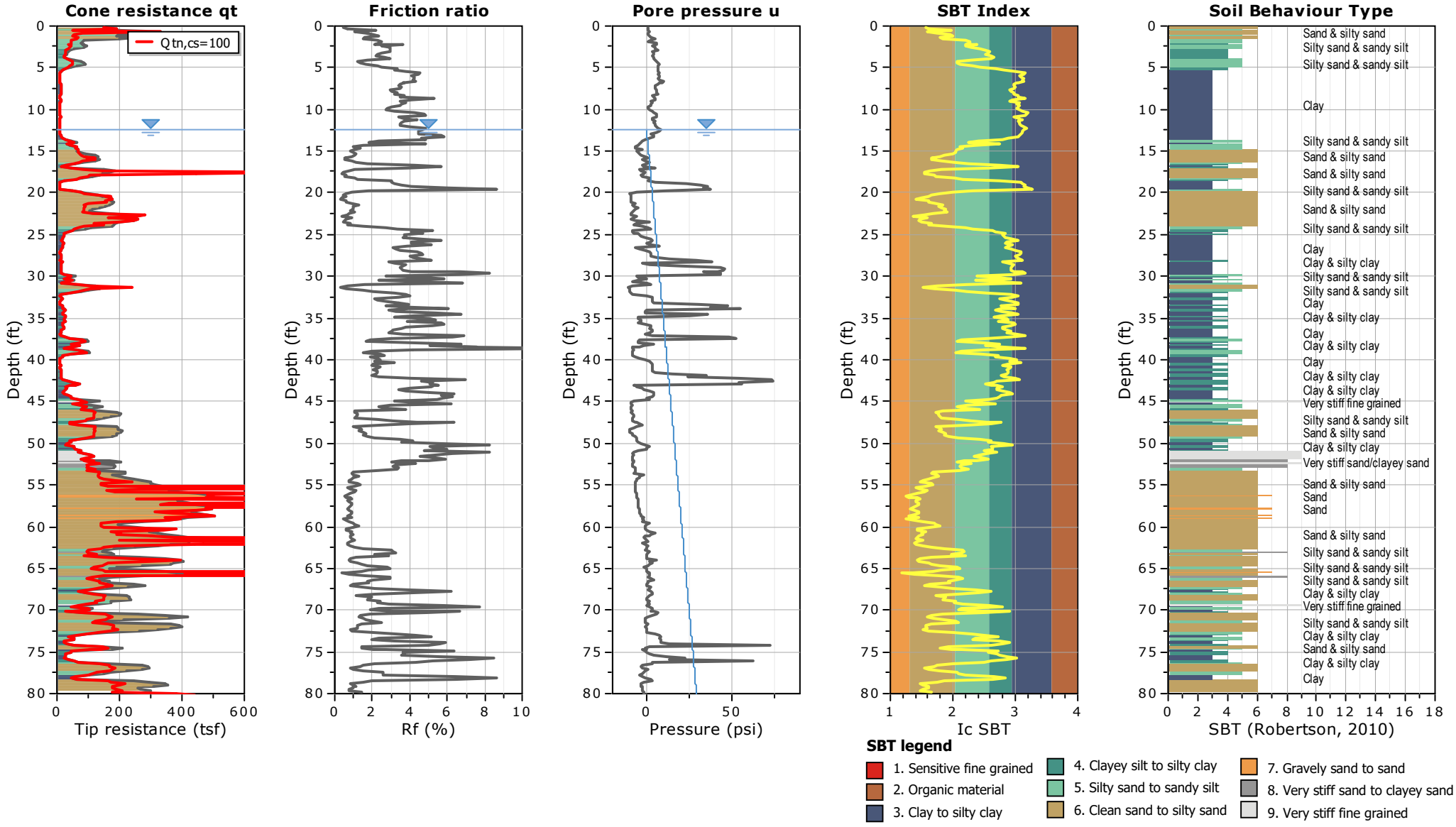
Est. GWL: 12.50 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

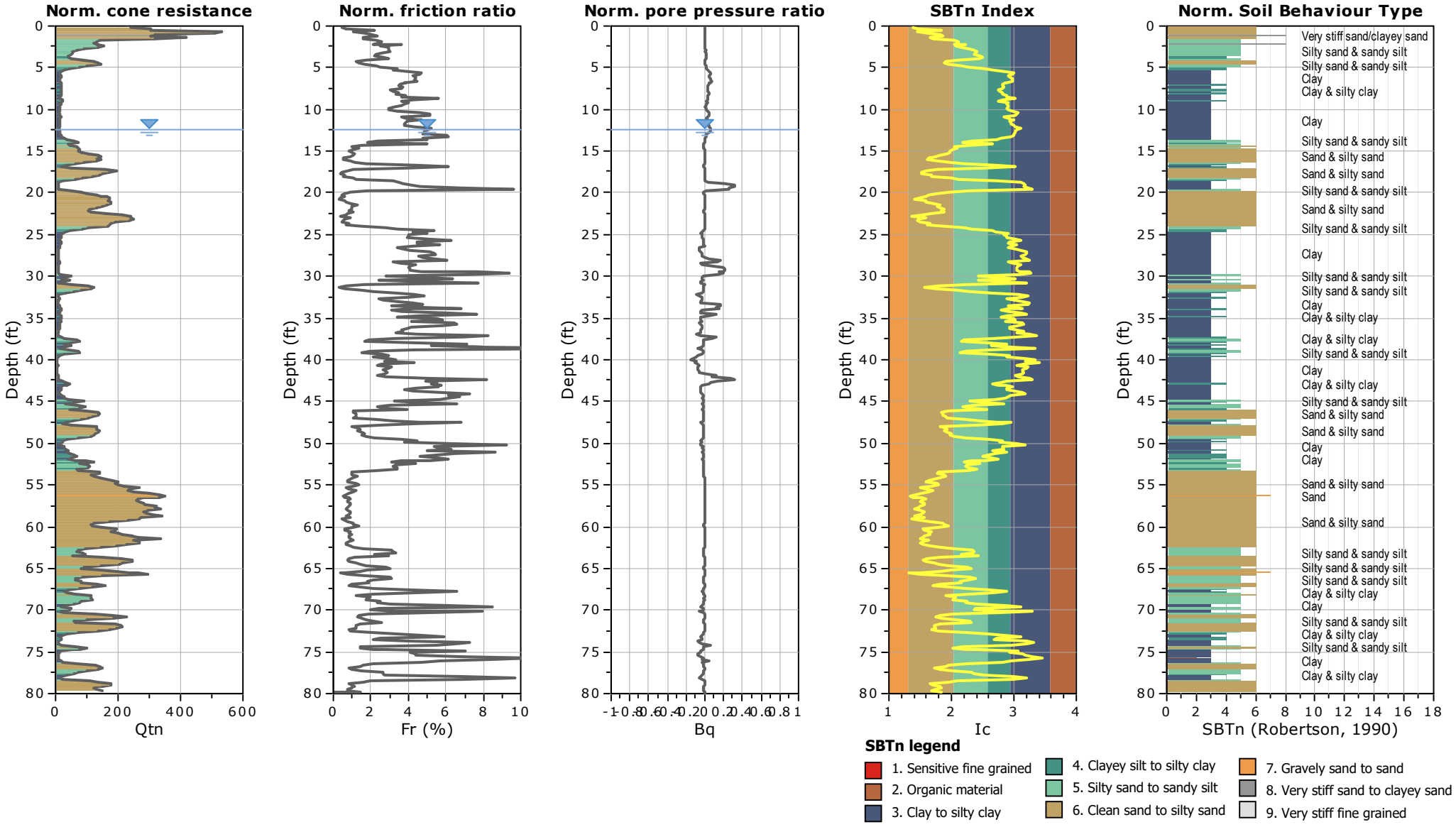
Est. GWL: 12.50 ft

Cone Type: 15cm²

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Project: Quincy Courthouse

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CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

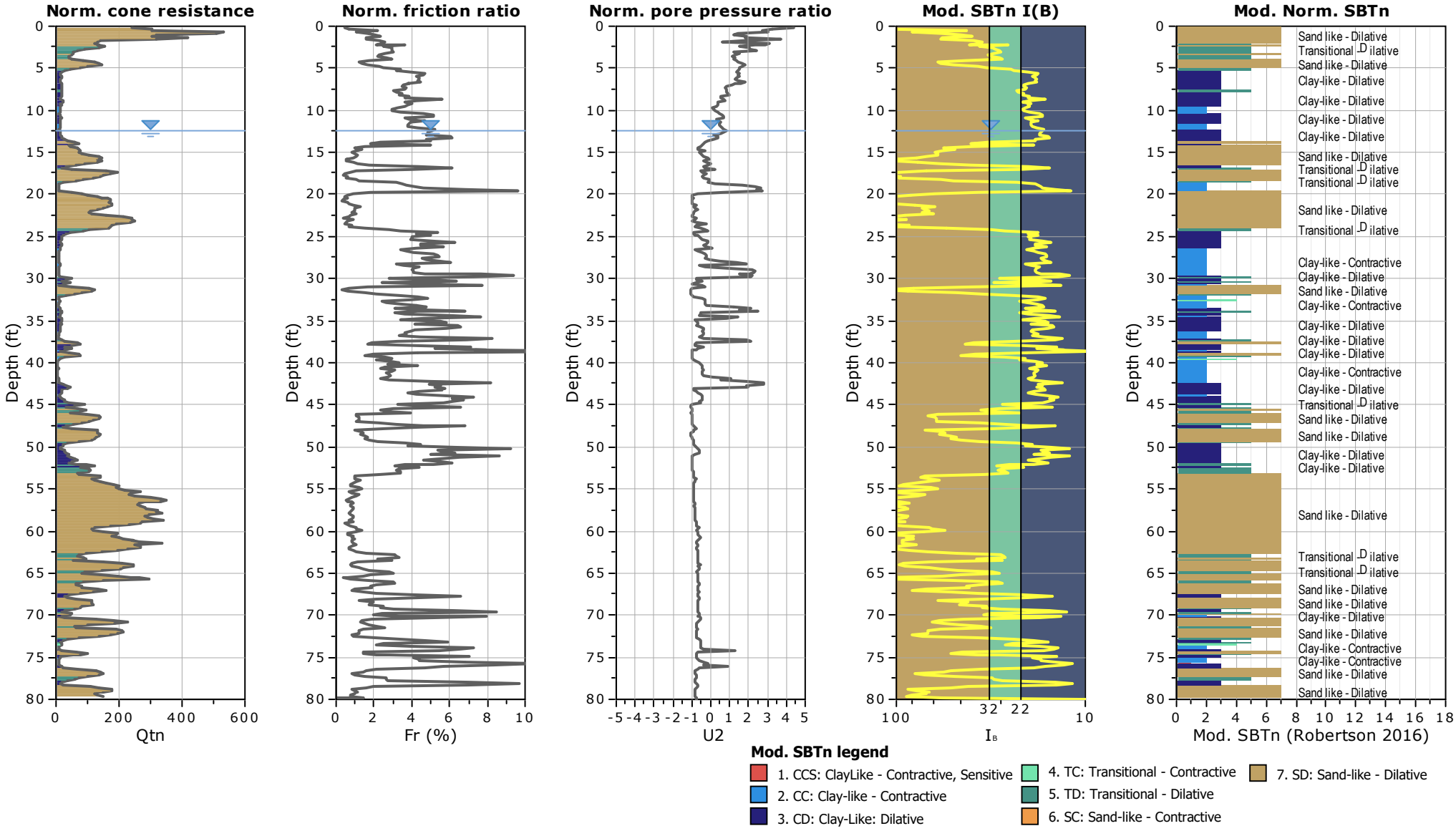
Est. GWL: 12.50 ft

Cone Type: 15cm²

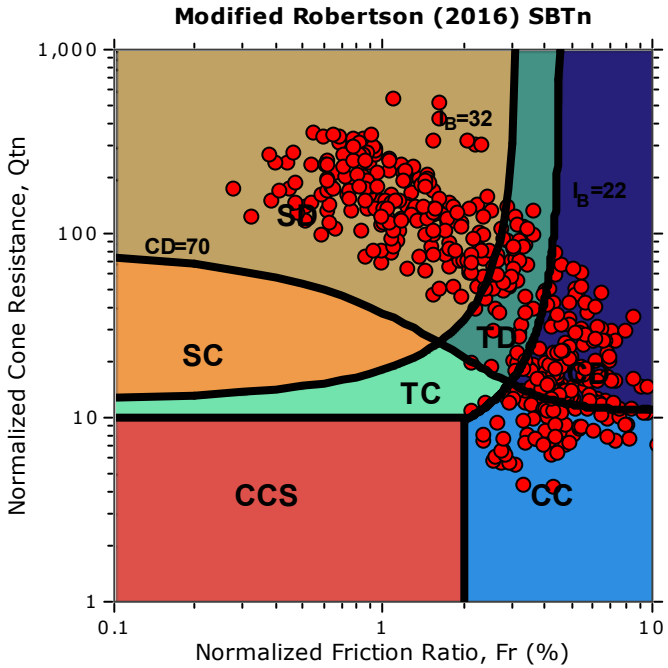
Cone Operator: JM-IY

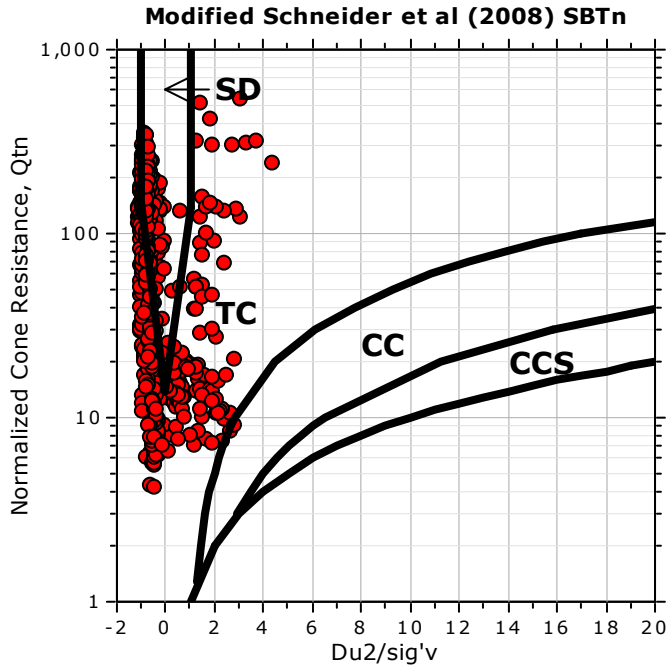
Project: Quincy Courthouse

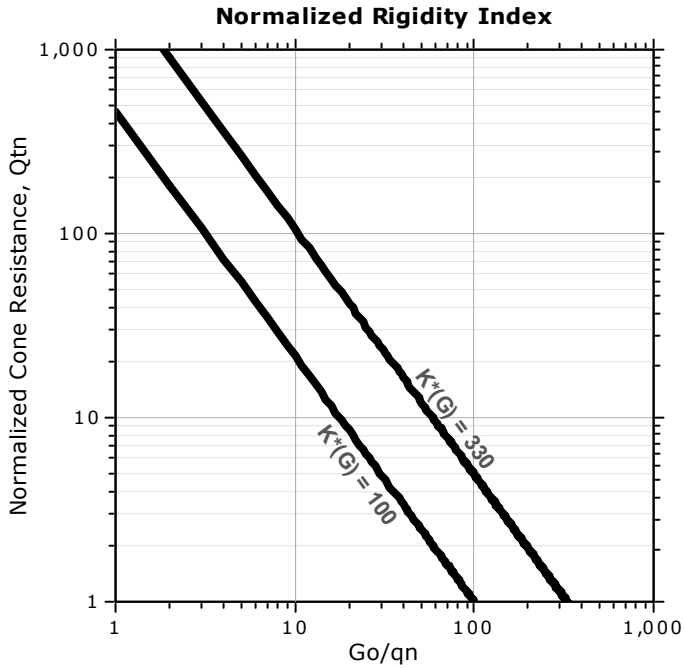
Location: 257 Lawrence Street, Quincy, CA 95971



Updated SBTn plots







CCS: Clay-like - Contractive - Sensitive
CC: Clay-like - Contractive
CD: Clay-like - Dilative
TC: Transitional - Contractive
TD: Transitional - Dilative
SC: Sand-like - Contractive
SD: Sand-like - Dilative

K(G) > 330: Soils with significant microstructure (e.g. age/cementation)

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

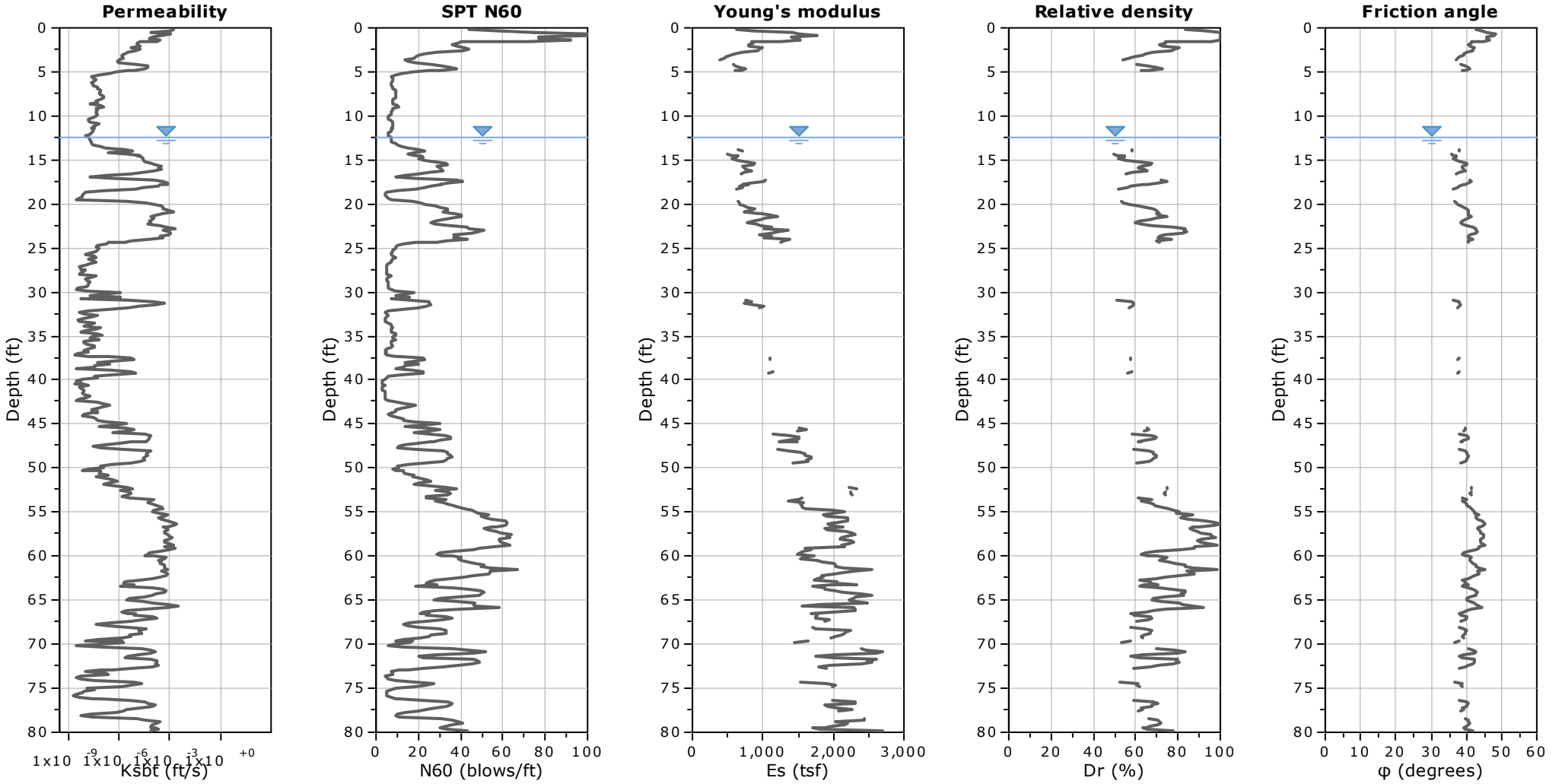
Est. GWL: 12.50 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

Permeability: Based on SBT_n

SPT N_{60}: Based on I_c and q_t

Young's modulus: Based on variable alpha using I_c (Robertson, 2009)

Relative density constant, C_{Dr}: 350.0

Phi: Based on Kulhawy & Mayne (1990)

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

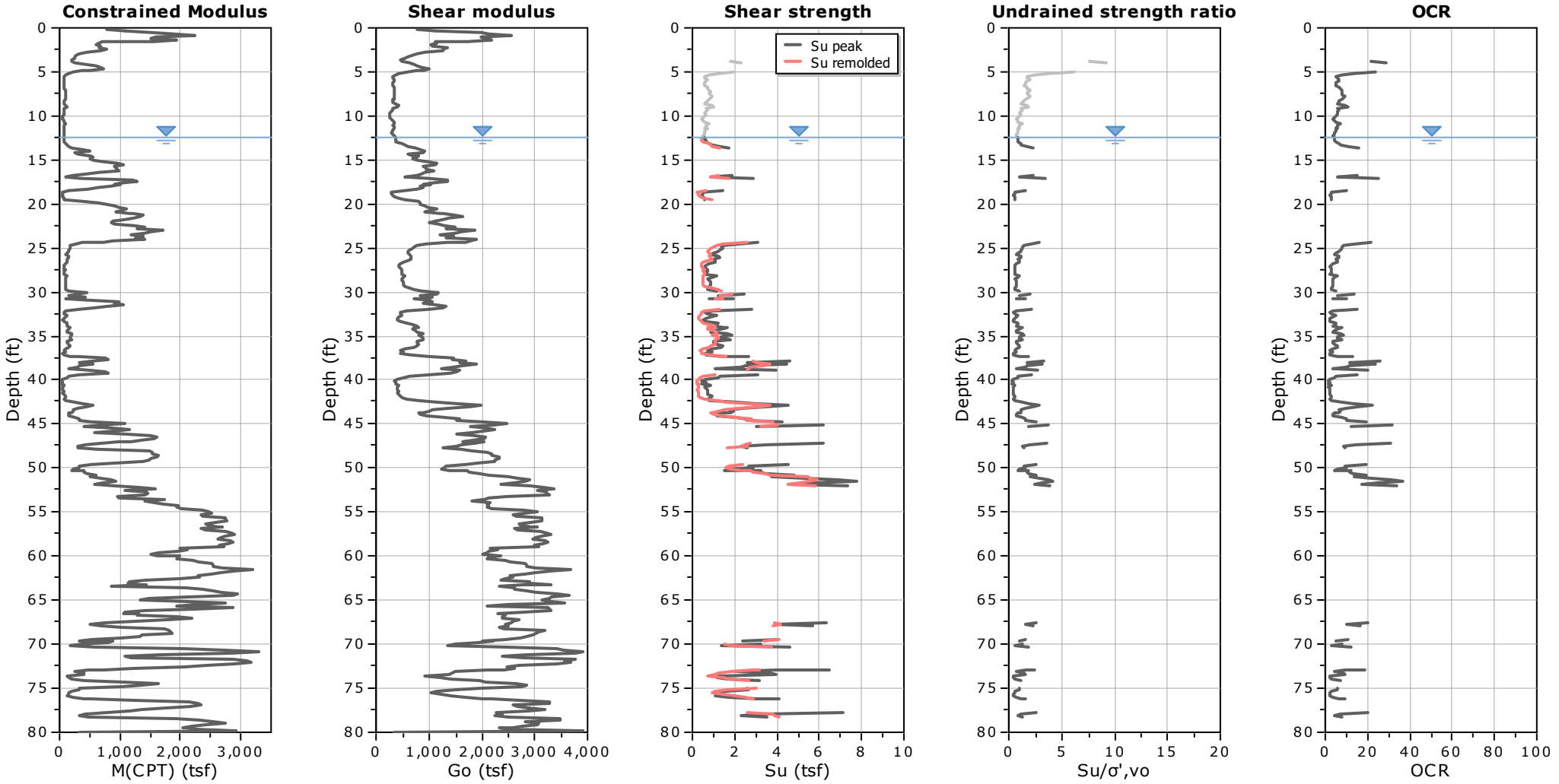
Est. GWL: 12.50 ft

Cone Type: 15cm²

Cone Operator: JM-IY

Project: Quincy Courthouse

Location: 257 Lawrence Street, Quincy, CA 95971



Calculation parameters

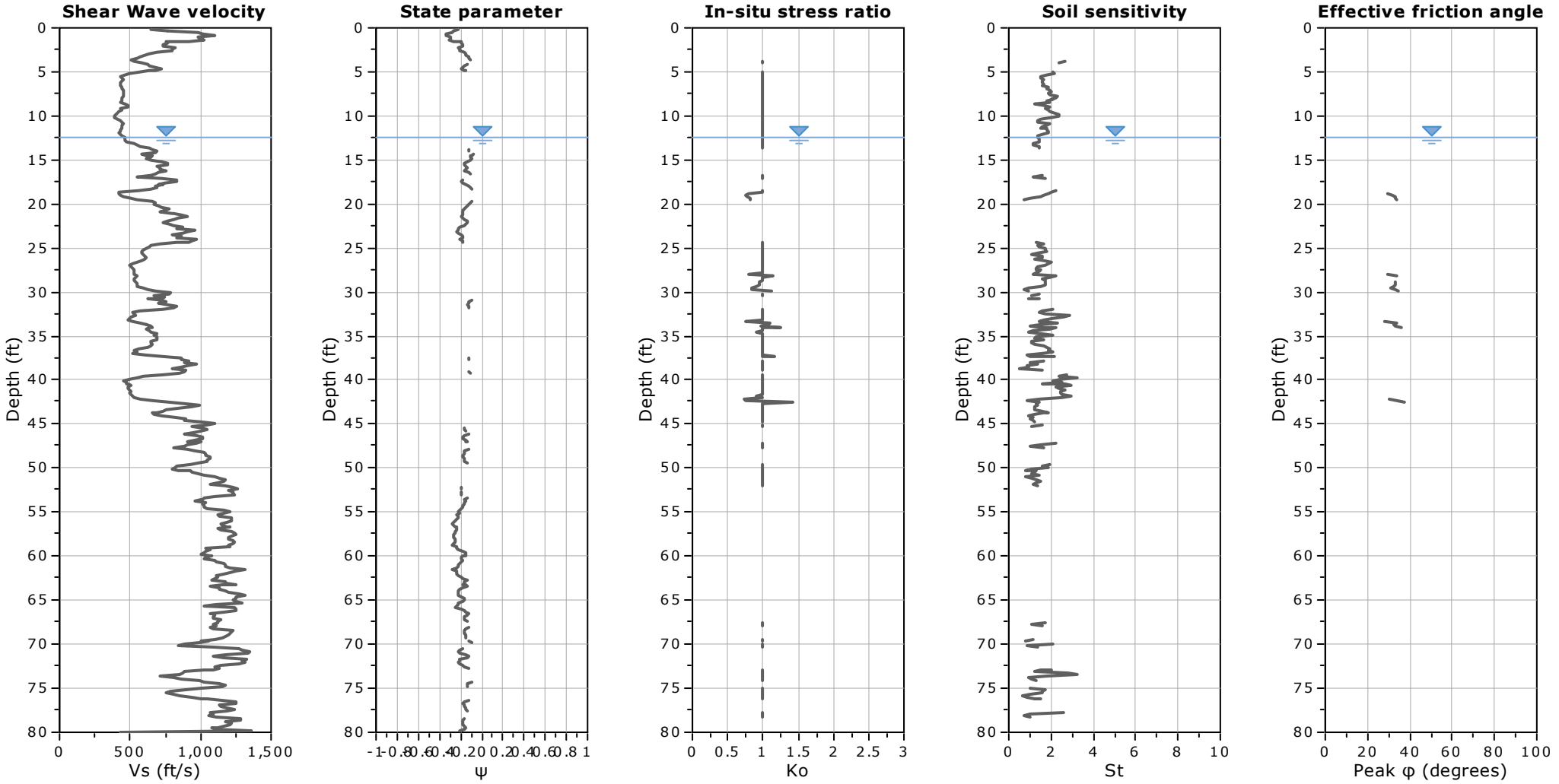
Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)

Go: Based on variable *alpha* using I_c (Robertson, 2009)

Undrained shear strength cone factor for clays, N_{kt}: Auto

OCR factor for clays, N_{kt}: Auto

Flat Dilatometer Test data



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

CPT: CPT-04

Total depth: 80.38 ft, Date: 9/16/2025

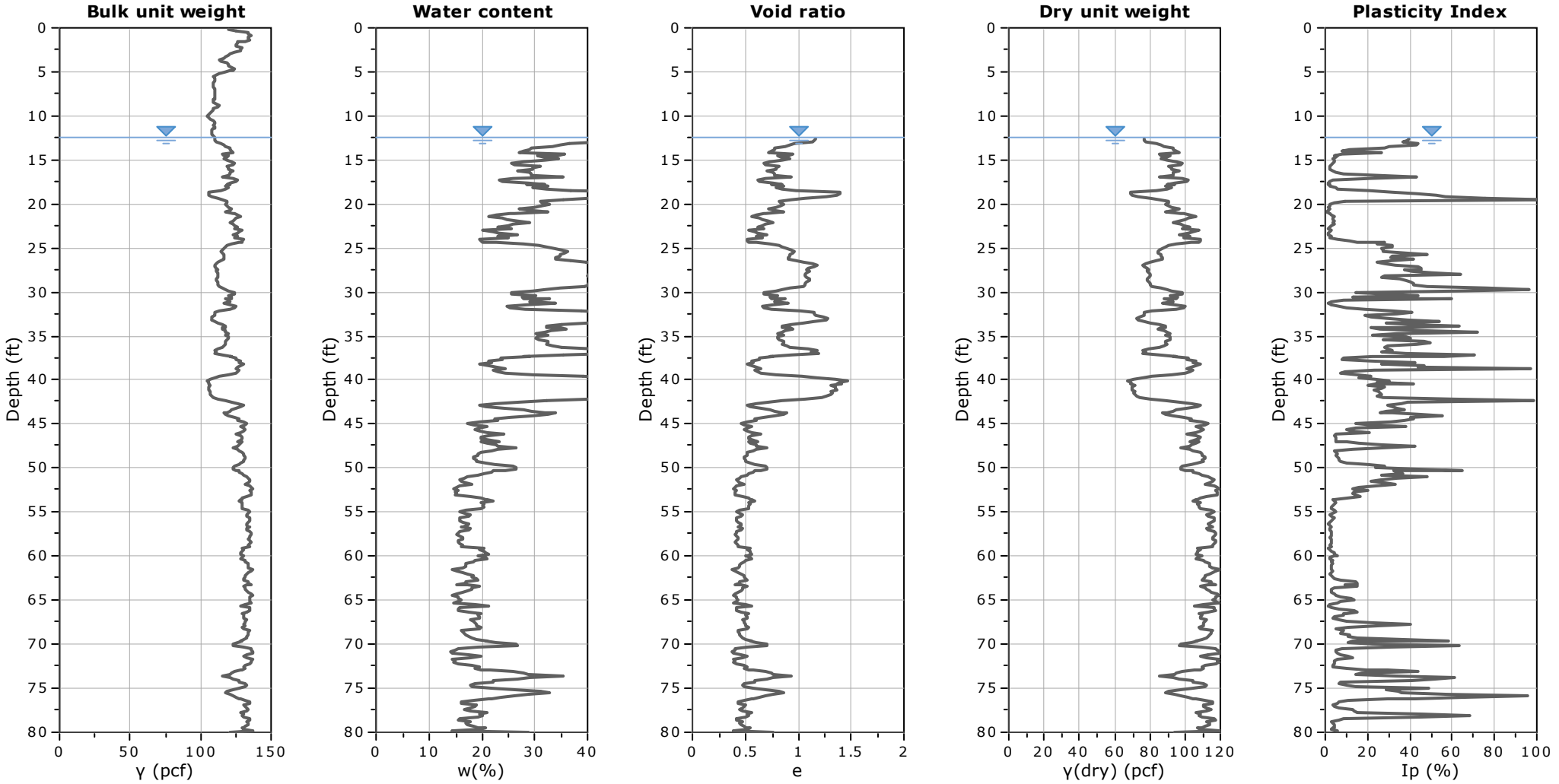
Est. GWL: 12.50 ft

Cone Type: 15cm²

Cone Operator: JM-IY

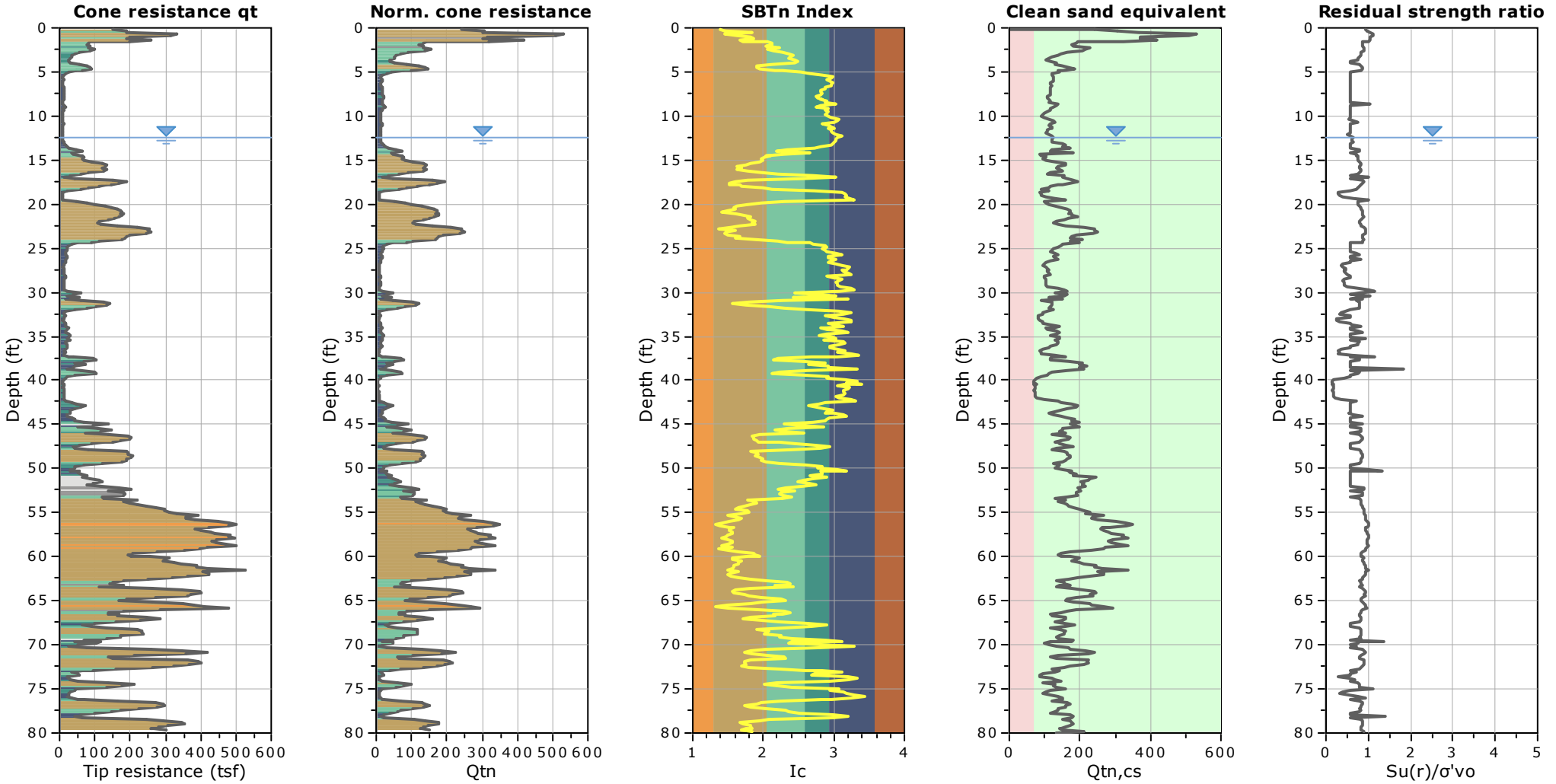
Project: Quincy Courthouse

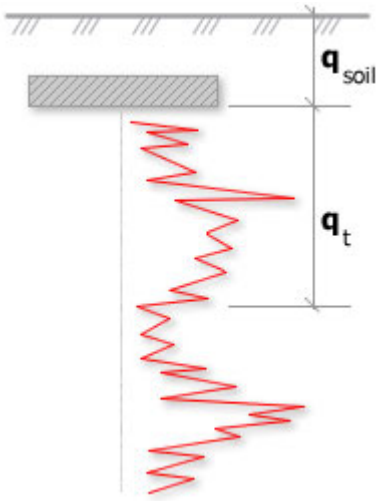
Location: 257 Lawrence Street, Quincy, CA 95971



Project: Quincy Courthouse
Location: 257 Lawrence Street, Quincy, CA 95971

CPT: CPT-04
Total depth: 80.38 ft, Date: 9/16/2025
Est. GWL: 12.50 ft
Cone Type: 15cm²
Cone Operator: JM-IY

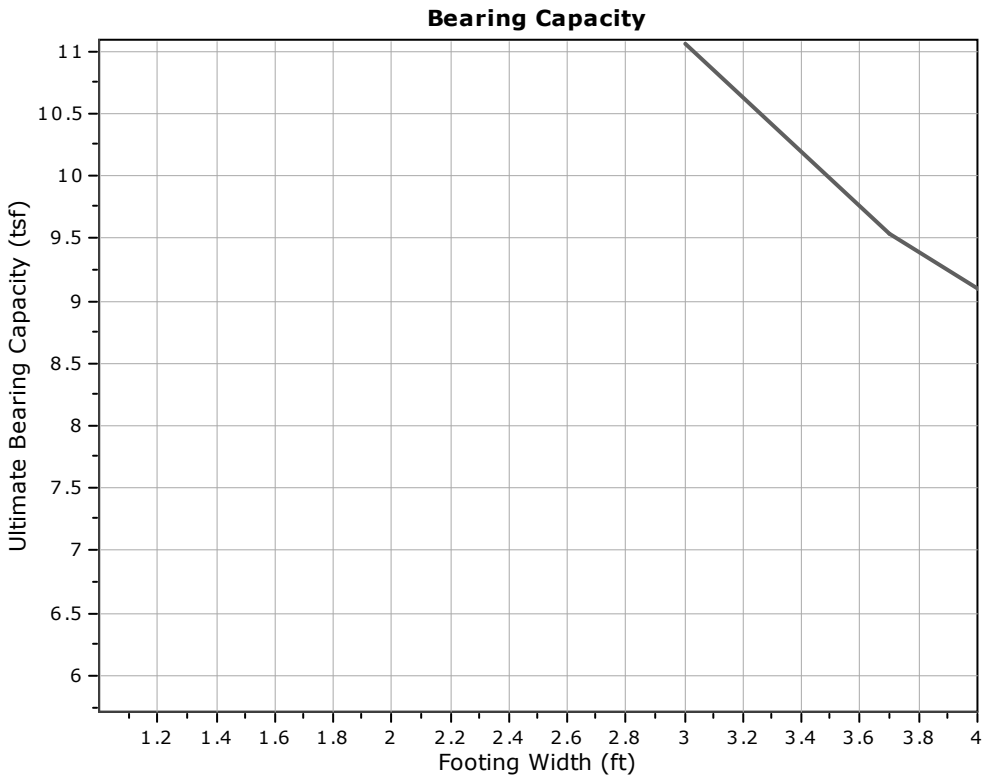




Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (ft)	Start Depth (ft)	End Depth (ft)	Ave. q_t (tsf)	R_k	Soil Press. (tsf)	Ult. bearing cap. (tsf)
1	3.00	1.60	6.10	54.83	0.20	0.10	11.06
2	3.70	1.60	7.15	47.21	0.20	0.10	9.54
3	4.40	1.60	8.20	42.11	0.20	0.10	8.52
4	5.10	1.60	9.25	37.70	0.20	0.10	7.64
5	5.80	1.60	10.30	34.53	0.20	0.10	7.00
6	6.50	1.60	11.35	31.69	0.20	0.10	6.43
7	7.20	1.60	12.40	29.70	0.20	0.10	6.04
8	7.90	1.60	13.45	28.22	0.20	0.10	5.74
9	8.60	1.60	14.50	29.38	0.20	0.10	5.97
10	9.30	1.60	15.55	32.94	0.20	0.10	6.68
11	10.00	1.60	16.60	38.90	0.20	0.10	7.88
12	10.70	1.60	17.65	42.54	0.20	0.10	8.60
13	11.40	1.60	18.70	45.41	0.20	0.10	9.18
14	12.10	1.60	19.75	43.49	0.20	0.10	8.79
15	12.80	1.60	20.80	47.96	0.20	0.10	9.69

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236 \right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a} \right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$$

(applicable only to $I_c < I_{c_cutoff}$)

:: Relative Density, Dr (%) ::

$$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$$ (applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: State Parameter, ψ ::

$$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$$

:: Drained Friction Angle, φ (°) ::

$$\varphi = \varphi'_{cv} + 15.94 \cdot \log(Q_{tn,cs}) - 26.88$$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c_cutoff}$)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$
$\alpha = 14$ for $Q_{tn} > 14$
$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$
$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \geq 2.20$

$$M_{CPT} = 0.03 \cdot (q_t - \sigma_v) \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Small strain shear Modulus, Go (MPa) ::

$$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho} \right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))} \right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: In situ Stress Ratio, Ko ::

$$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c_cutoff}$)

:: Peak Friction Angle, φ' (°) ::

$$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$$

(applicable for $0.10 < B_q < 1.00$)

References

• Robertson, P.K., Cabal K.L., Guide to Cone Penetration Testing for Geotechnical Engineering, Gregg Drilling & Testing, Inc., 5th Edition, November 2012

• Robertson, P.K., Interpretation of Cone Penetration Tests - a unified approach., Can. Geotech. J. 46(11): 1337–1355 (2009)

• N Barounis, J Philpot, Estimation of in-situ water content, void ratio, dry unit weight and porosity using CPT for saturated sands, Proc. 20th NZGS Geotechnical Symposium

Atlas Technical Consultants

Location	Quincy Courthouse	Operator	JM-IY	GPS
Job Number	18077.000	Cone Number	DDG1627	
Hole Number	CPT-04	Date and Time	9/16/2025 2:49:14 PM	
Equilized Pressure	15.3	EST GW Depth During Test	12.5	



APPENDIX III
GEOTECHNICAL LABORATORY TESTING

Laboratory tests were performed to provide geotechnical parameters for engineering analyses. The following tests were performed:

- **CLASSIFICATION:** Field classifications were verified in the laboratory by visual examination. The final soil classifications are in accordance with the Unified Soil Classification System.
- **PARTICLE-SIZE DISTRIBUTION:** Particle-size distribution testing was performed on selected soil samples in accordance with ASTM C136 or ASTM D6913.
- **MATERIALS FINER THAN NO. 200:** Percent passing the no. 200 sieve testing was performed on selected soil samples in accordance with ASTM D1140.
- **ATTERBERG LIMITS:** Atterberg limits testing was performed on selected soil samples in accordance with ASTM D4318.
- **UNIT WEIGHT / MOISTURE CONTENT:** Unit weight and moisture content testing was performed on selected soil samples in accordance with ASTMs D2937, D4643, D2216, and D464.
- **EXPANSION INDEX:** Expansion Index testing was performed on selected soil samples in accordance with ASTM D4829.
- **CORROSIVITY**: Corrosivity tests were performed on a select soil sample. The pH and minimum resistivity were determined in accordance with California Test 643 and ASTM G51. The soluble chloride content was determined in accordance with California Test 422. The soluble sulfate content was determined in accordance with California Test 417.
- **R-VALUE:** R-value tests were performed on selected soil samples in accordance with California Test Method 301.
- **MAXIMUM DENSITY AND OPTIMUM MOISTURE CONTENT:** Maximum density testing of soils was performed on a select soil sample in accordance with ASTM D1557.
- **DIRECT SHEAR:** Direct shear testing was performed on a selected soil sample in accordance with ASTM D3080.
- **UNCONSOLIDATED/UNDRAINED TRIAXIAL SHEAR TEST:** An unconsolidated-undrained triaxial shear test was performed on selected samples in accordance with ASTM D22850. Test results are presented in this appendix.
- **CONSOLIDATION:** A consolidation test was performed on a select soil sample in accordance with ASTM D2435.

Soil samples not tested are stored in our laboratory for future reference and analysis, if needed. Unless notified, all samples will be disposed of 30 days from the date of this report.

RESISTIVITY, pH, SOLUBLE CHLORIDE and SOLUBLE SULFATE

CALIFORNIA TESTS 417, 422, 643 / ASTM G51

SAMPLE	RESISTIVITY (Ω-cm)	pH	CHLORIDE (%)	SULFATE (%)
B-2 at 2 to 2.5 Feet	7015	7.2	0.0002	0.0004
B-7 at 1 to 5 Feet	1590	7.23	0.002	0.008
B-8 at 1 to 5 Feet	2890	7.04	0.002	0.003
B-10 at 5.5 to 6.5 Feet	2550	6.56	0.001	0.0108

Water-Soluble Sulfate Exposure [1]

Water-Soluble Sulfate (SO_4) in soil (percent by weight)	Exposure Severity	Exposure Class	Cement Type (ASTM C150)	Max. W/C	Min. f_c' (psi)
$SO_4 < 0.10$	N/A	S0	No type restriction	N/A	2500
$0.10 \le SO_4 < 0.20$	Moderate	S1	II	0.5	4000
$2{,}000 \le SO_4 \le 20{,}000$	Severe	S2	V	0.45	4500
$SO_4 > 20{,}000$	Very Severe	S3	V plus pozzolan or slag cement	0.45	4500

1 - Modified from ACI 318-14 Table 19.3.1.1 and Table 19.3.2.1

PERCENT FINER THAN NO. 200 SIEVE

ASTM D1140

SAMPLE	DESCRIPTION	PERCENT FINER THAN NO. 200
B-9 at 1 to 5 Feet	SILTY SAND with GRAVEL (SM)	27.6

ATTERBERG LIMITS

ASTM D4318

SAMPLE	FINES DESCRIPTION	LIQUID LIMIT	PLASTIC LIMIT	PLASTIC INDEX
B-4 at 4 to 4.5 Feet	ML	33	24	9
B-5 at 2 to 2.5 Feet	ML	36	26	10
B-6 at 2 to 4.5 Feet	ML	33	24	9
B-8 at 8 to 8.5 Feet	ML	30	25	5
B-11 at 3 to 4 Feet	ML	46	36	10

EXPANSION INDEX

ASTM D4829

SAMPLE	EXPANSION INDEX	EXPANSION POTENTIONAL
B-6 at 2 to 4.5 Feet	18	Very Low
B-11 at 1 to 5 Feet	4	Very Low

Expansion Index	Expansion Potential
1-20	Very Low
21-50	Low
51-90	Medium
91-130	High
Above 130	Very High

R-VALUE

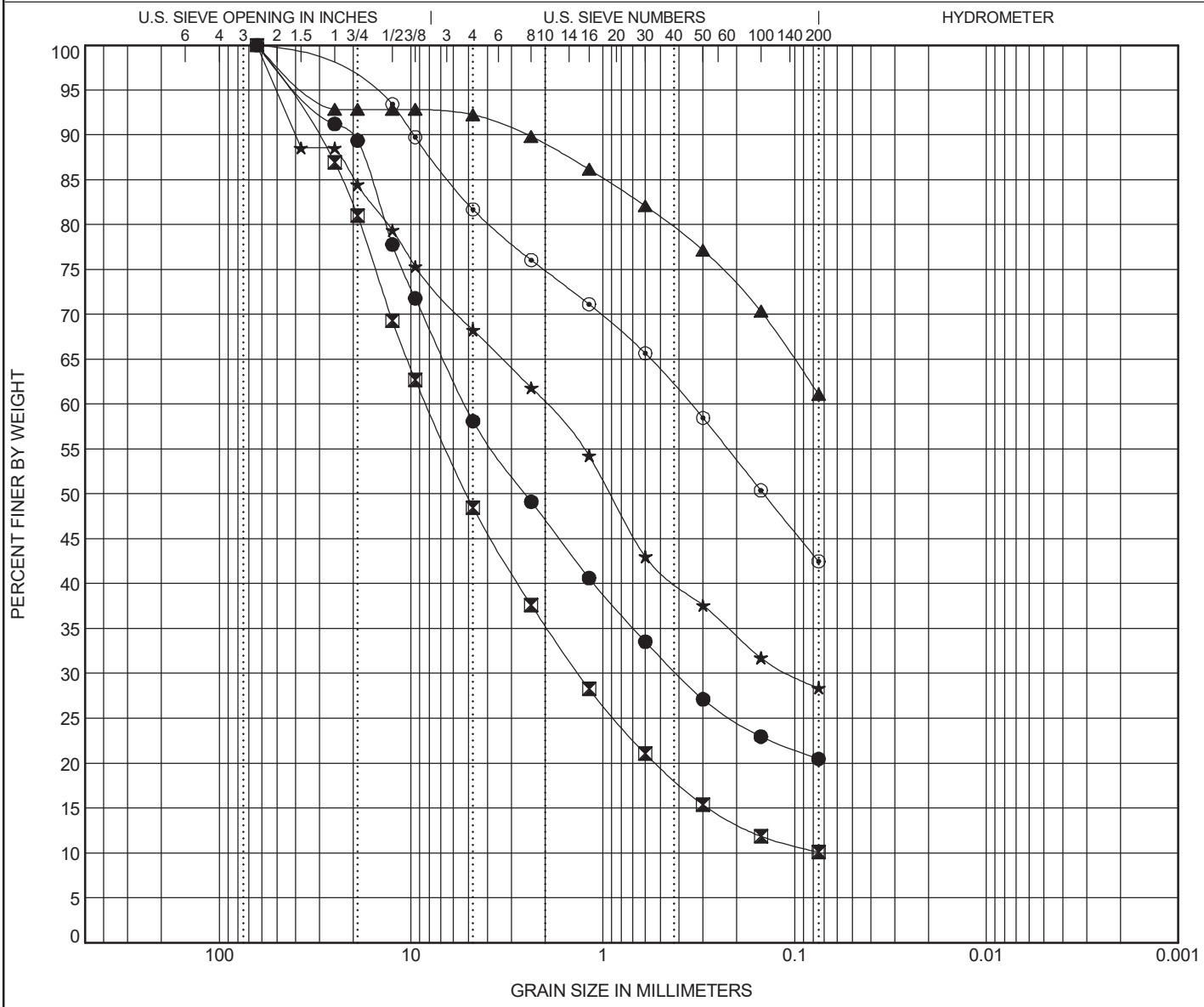
CALIFORNIA TEST 301

SAMPLE	DESCRIPTION	R-VALUE
B-2 and B-3 at 1 to 5 Feet	CLAYEY SAND with GRAVEL (SC)	56
B-8 at 1 to 5 Feet	CLAYEY SAND with GRAVEL (SC)	67

GRAIN SIZE DISTRIBUTION

CLIENT Judicial Council of California (JCC) **PROJECT NAME** New Quincy Courthouse - Potential Site 2

PROJECT NUMBER 91-65859-PW **PROJECT LOCATION** 570 Main St, Quincy, CA



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

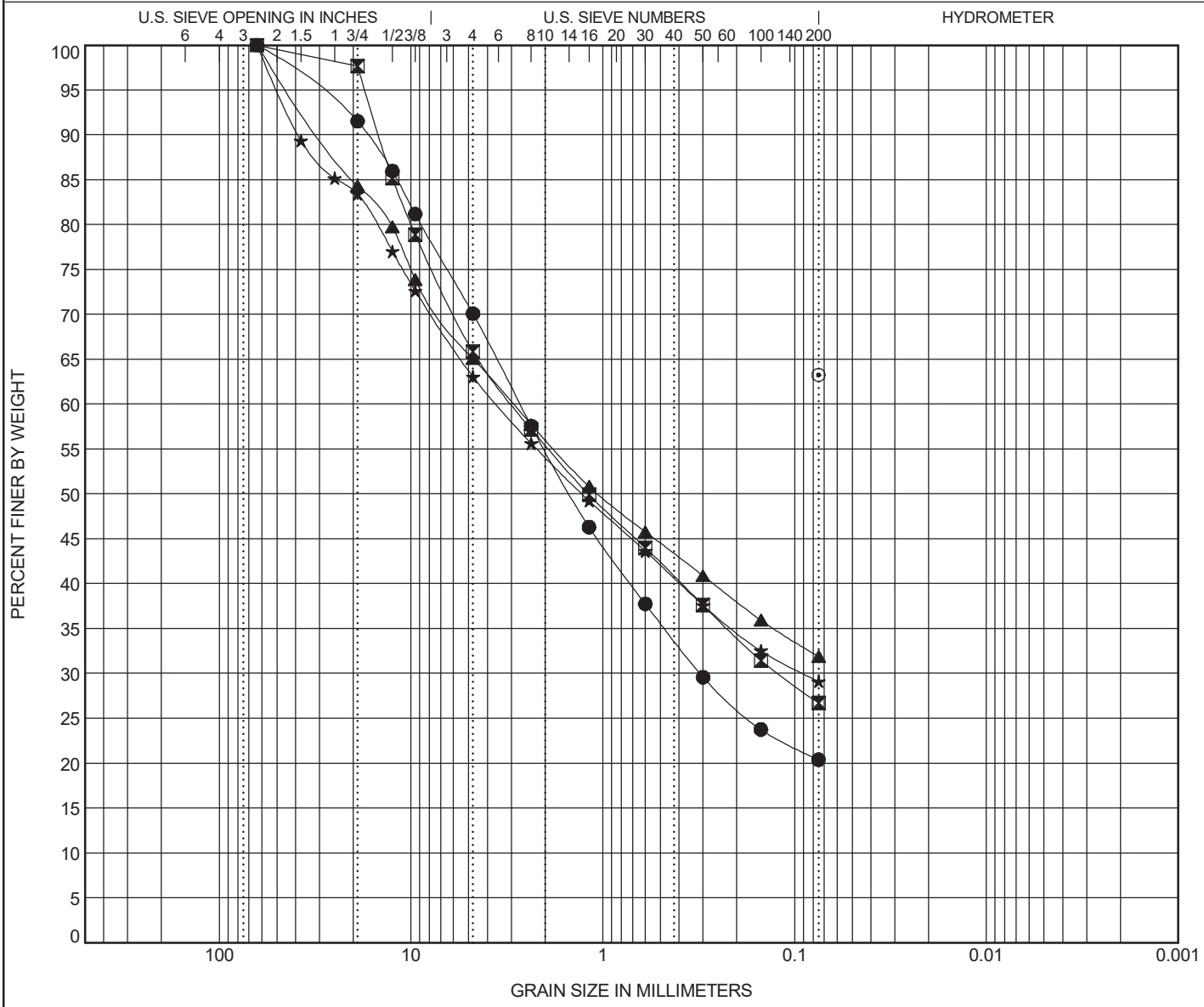
	Specimen Identification		Classification	LL	PL	PI	Cc	Cu
●	B-1	2.0	CLAYEY GRAVEL WITH SAND (GC)					
⊠	B-1	14.5	POORLY GRADED GRAVEL WITH SAND AND CLAY (GP-GC)				2.97	114.24
▲	B-1	24.5	SANDY LEAN CLAY (CL)					
★	B-2	4.5	CLAYEY SAND WITH GRAVEL (SC)					
⊙	B-3	14.5	CLAYEY SAND WITH GRAVEL (SC)					

	Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	B-1	2.0	63.5	5.232	0.41		41.9	37.6	20.5	
⊠	B-1	14.5	63.5	8.326	1.343		51.5	38.4	10.1	
▲	B-1	24.5	63.5				7.8	31.2	61.1	
★	B-2	4.5	63.5	1.997	0.105		31.7	39.9	28.4	
⊙	B-3	14.5	63.5	0.348			18.3	39.2	42.5	

GRAIN SIZE DISTRIBUTION

CLIENT Judicial Council of California (JCC) **PROJECT NAME** New Quincy Courthouse - Potential Site 2

PROJECT NUMBER 91-65859-PW **PROJECT LOCATION** 570 Main St, Quincy, CA



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

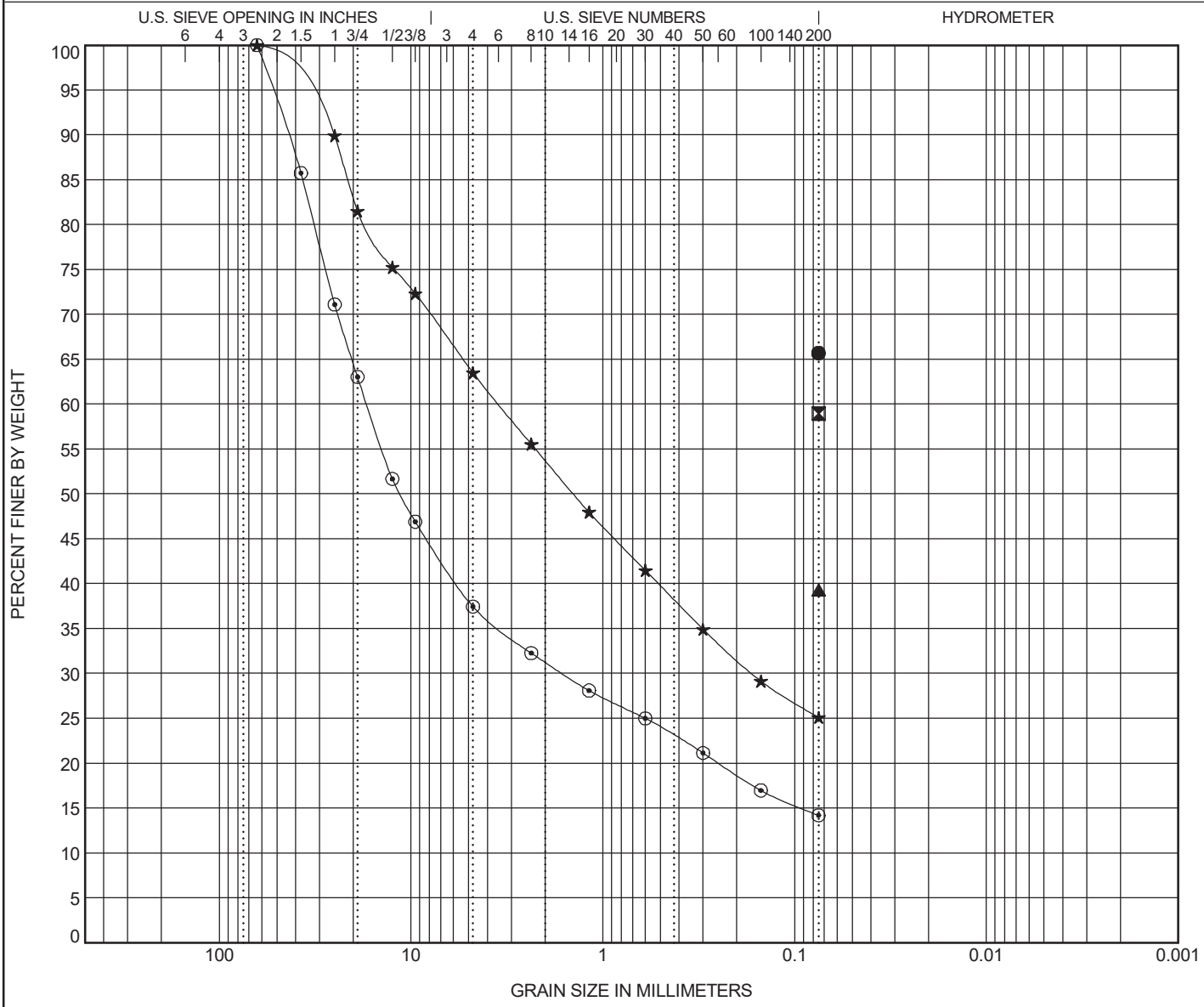
Specimen Identification			Classification	LL	PL	PI	Cc	Cu
●	B-3	24.5	CLAYEY SAND WITH GRAVEL(SC)					
⊠	B-3	29.5	CLAYEY SAND WITH GRAVEL (SC)					
▲	B-3	39.5	CLAYEY GRAVEL WITH SAND (GC)					
★	B-4	2.0	SILTY GRAVEL WITH SAND (GM)					
⊙	B-4	4.5	SANDY SILT WITH GRAVEL (ML)	33	24	9		

Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	B-3	24.5	63.5	2.705	0.311		29.9	49.7	20.4	
⊠	B-3	29.5	63.5	2.96	0.121		34.2	39.1	26.7	
▲	B-3	39.5	63.5	2.932			34.9	33.2	31.9	
★	B-4	2.0	63.5	3.565	0.09		37.0	33.9	29.1	
⊙	B-4	4.5							63.3	

GRAIN SIZE DISTRIBUTION

CLIENT Judicial Council of California (JCC) **PROJECT NAME** New Quincy Courthouse - Potential Site 2

PROJECT NUMBER 91-65859-PW **PROJECT LOCATION** 570 Main St, Quincy, CA



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

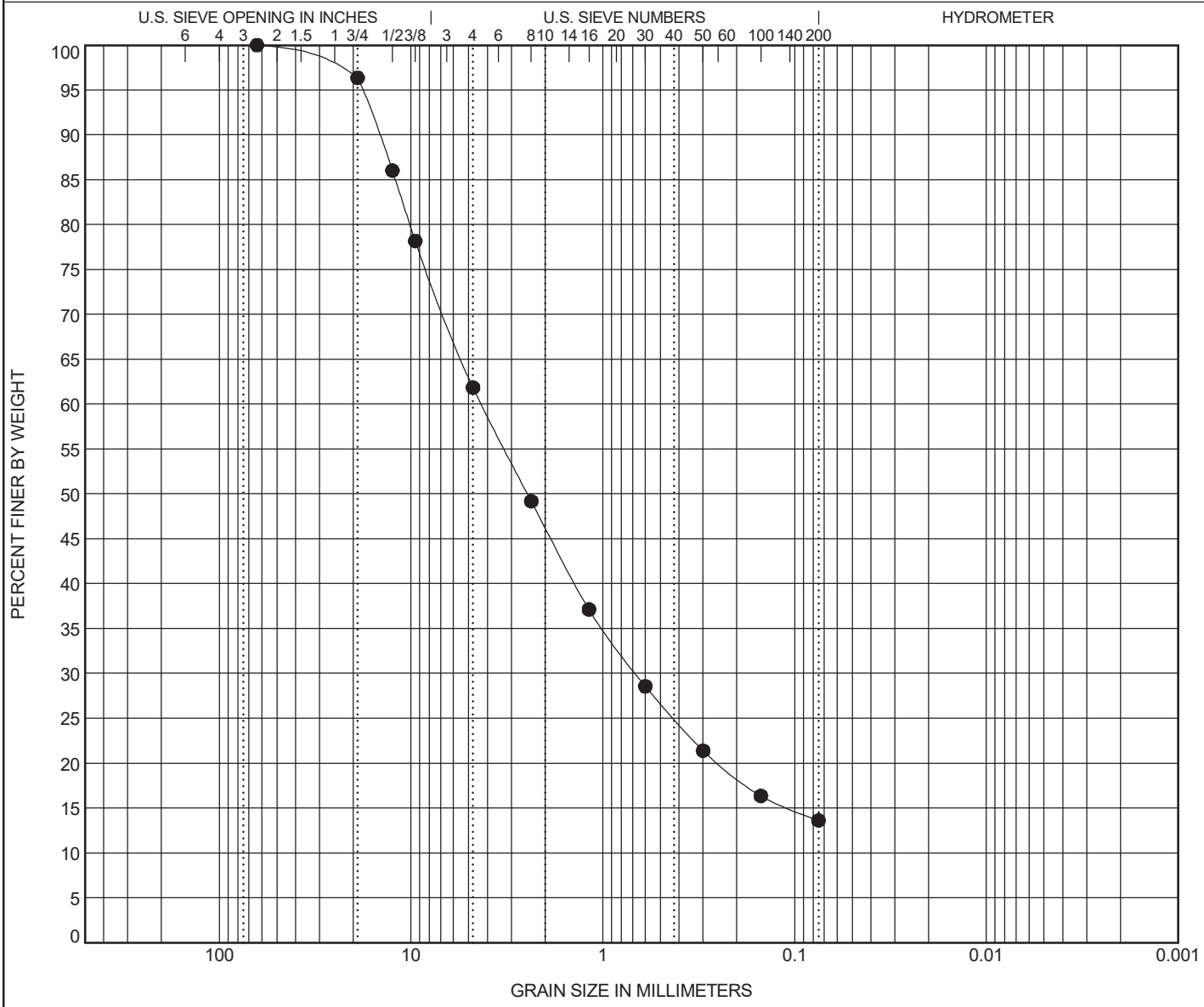
Specimen Identification			Classification	LL	PL	PI	Cc	Cu
●	B-4	19.5	SANDY CLAY WITH GRAVEL (CL)					
⊠	B-4	24.5	SANDY CLAY WITH GRAVEL (CL)					
▲	B-5	2.0	SILTY SAND WITH GRAVEL (ML)	36	26	10		
★	B-5	4.5	CLAYEY SAND WITH GRAVEL (SC)					
⊙	B-6	9.5	SILTY GRAVEL WITH SAND (GM)					

Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	B-4	19.5							65.7	
⊠	B-4	24.5							59.0	
▲	B-5	2.0							39.3	
★	B-5	4.5	63.5	3.495	0.166		36.5	38.4	25.1	
⊙	B-6	9.5	63.5	16.995	1.624		62.6	23.3	14.2	

GRAIN SIZE DISTRIBUTION

CLIENT Judicial Council of California (JCC) **PROJECT NAME** New Quincy Courthouse - Potential Site 2

PROJECT NUMBER 91-65859-PW **PROJECT LOCATION** 570 Main St, Quincy, CA



COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

	Specimen Identification		Classification	LL	PL	PI	Cc	Cu
●	**B-6**	**19.5**	**CLAYEY SAND WITH GRAVEL (SC)**					

	Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	**B-6**	**19.5**	**63.5**	**4.291**	**0.673**		**38.2**	**48.2**	**13.6**	

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Sieve Analysis Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B-7 @ 7.5'	

SIEVE ANALYSIS (ASTM C136)

Sieve Size	Percent Passing
1"	**100**
3/4"	**97**
1/2"	**94**
3/8"	**92**
No. 4	**88**
No. 8	**82**
No. 10	**80**
No. 16	**73**
No. 30	**63**
No. 40	**58**
No. 50	**52**
No. 100	**40**
No. 200	**32.0**

Reviewed by: _____
Guang H. Zhu
Staff Engineer

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Sieve Analysis Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B-7 15'	

SIEVE ANALYSIS (ASTM C136)

Sieve Size	Percent Passing
1"	**100**
3/4"	**91**
1/2"	**69**
3/8"	**61**
No. 4	**44**
No. 8	**32**
No. 10	**29**
No. 16	**24**
No. 30	**19**
No. 40	**16**
No. 50	**14**
No. 100	**11**
No. 200	**9.7**

Reviewed by: _____
Guang H. Zhu
Staff Engineer

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Sieve Analysis Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B-7 @ 30'	

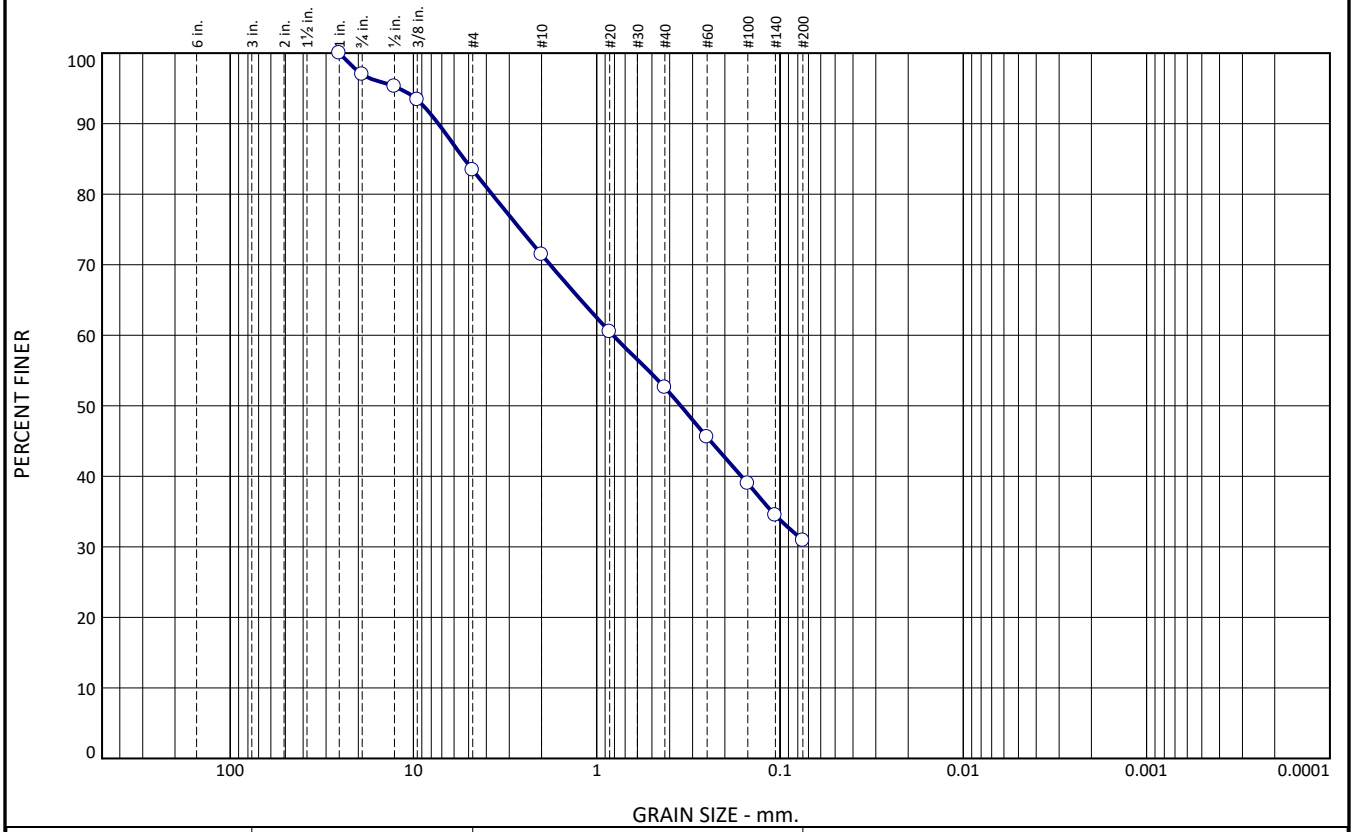
SIEVE ANALYSIS (ASTM C136)

Sieve Size	Percent Passing
1"	**100**
3/4"	**93**
1/2"	**85**
3/8"	**79**
No. 4	**67**
No. 8	**55**
No. 10	**52**
No. 16	**46**
No. 30	**39**
No. 40	**35**
No. 50	**31**
No. 100	**25**
No. 200	**20.3**

Reviewed by: _____
Guang H. Zhu
Staff Engineer

Particle Size Distribution Report

ASTM D6913



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	3.0	13.6	12.0	18.8	21.7	30.9	

Test Results (ASTM D6913)

Sieve Size or Diam. (mm.)	Finer (%)	Spec.* (%)	Out of Spec. (%)	Pct. of Fines
1"	100.0			
3/4"	97.0			
1/2"	95.3			
3/8"	93.4			
#4	83.4			
#10	71.4			85.6
#20	60.5			72.5
#40	52.6			63.0
#60	45.6			54.6
#100	39.0			46.7
#140	34.5			41.3
#200	30.9			37.0

* (no specification provided)

Material Description

SILTY SAND with GRAVEL, yellowish brown

Atterberg Limits

PL= LL= PI=

Coefficients

D_{90}= 7.3238 D_{85}= 5.2914 D_{60}= 0.8149
D_{50}= 0.3480 D_{30}= D_{15}=
D_{10}= C_u= C_c=

Classification

USCS= AASHTO=

Test Remarks

Source of Sample: 6056-003.00 - New Quincy Courthouse - 91-65859-PW **Depth:** 10'
Sample Number: B-8 **Sample Date:**

Blackburn Consulting

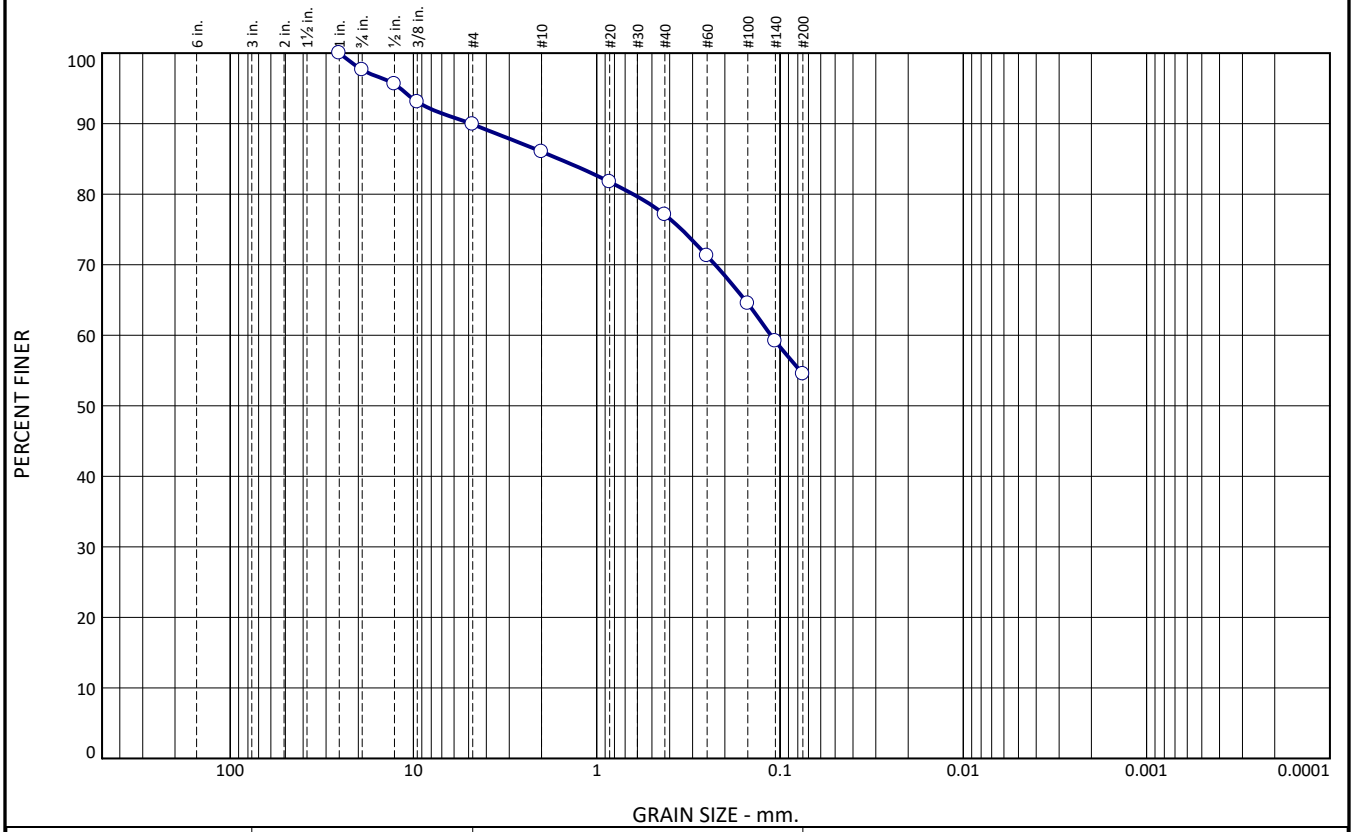
W. Sacramento, CA

Client: Raney Geotechnical, Inc.
Project: Raney Geotechnical, Inc. Lab Testing

Project No: 4563.X **Figure**

Particle Size Distribution Report

ASTM D6913



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	2.4	7.7	3.9	8.9	22.6	54.5	

Test Results (ASTM D6913)

Sieve Size or Diam. (mm.)	Finer (%)	Spec.* (%)	Out of Spec. (%)	Pct. of Fines
1"	100.0			
3/4"	97.6			
1/2"	95.6			
3/8"	93.1			
#4	89.9			
#10	86.0			95.7
#20	81.7			90.9
#40	77.1			85.7
#60	71.2			79.3
#100	64.5			71.7
#140	59.2			65.8
#200	54.5			60.6

* (no specification provided)

Material Description

SANDY SILT, yellowish brown

Atterberg Limits

PL= LL= PI=

Coefficients

D_{90}= 4.8610 D_{85}= 1.6120 D_{60}= 0.1121
D_{50}= D_{30}= D_{15}=
D_{10}= C_u= C_c=

Classification

USCS= AASHTO=

Test Remarks

Source of Sample: 6056-003.00 - New Quincy Courthouse - 91-65859-PW **Depth:** 20'
Sample Number: B-8 **Sample Date:**

Blackburn Consulting

W. Sacramento, CA

Client: Raney Geotechnical, Inc.
Project: Raney Geotechnical, Inc. Lab Testing

Project No: 4563.X **Figure**

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Sieve Analysis Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B-10 (1-5')	

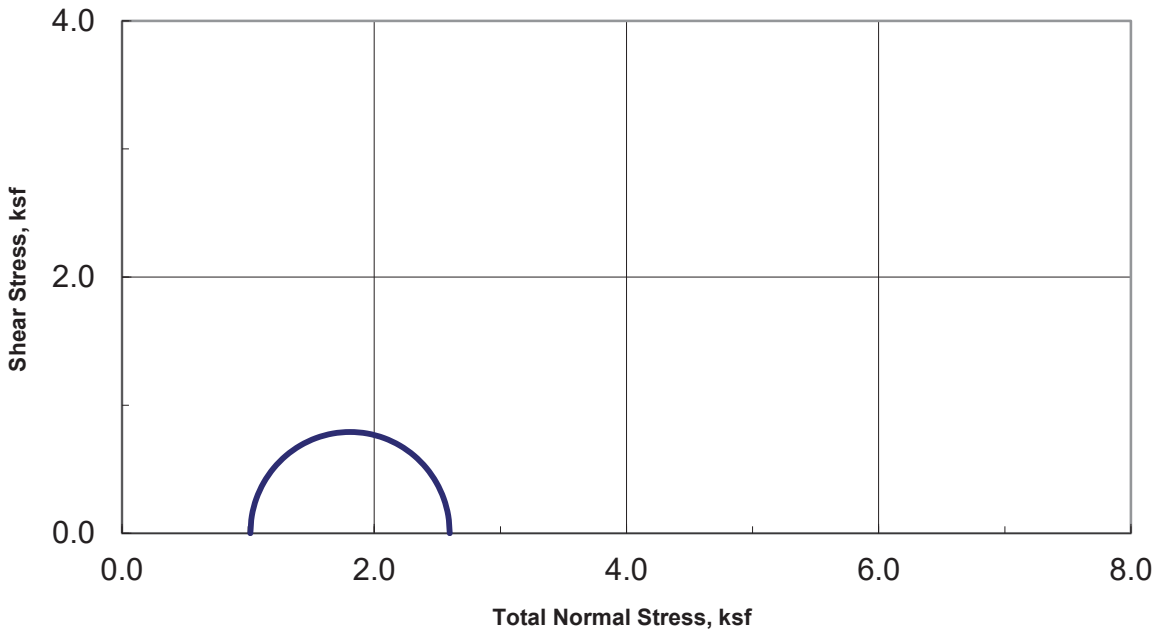
SIEVE ANALYSIS (ASTM C136)

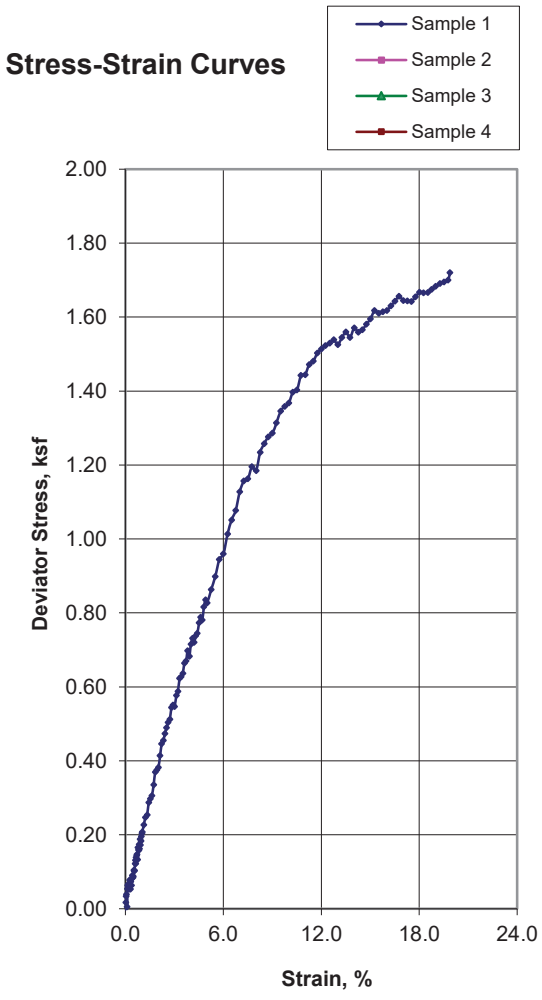
Sieve Size	Percent Passing
1"	**100**
3/4"	**99**
1/2"	**93**
3/8"	**88**
No. 4	**77**
No. 8	**68**
No. 10	**66**
No. 16	**62**
No. 30	**56**
No. 40	**52**
No. 50	**49**
No. 100	**42**
No. 200	**37.6**

Reviewed by: _____
Guang H. Zhu
Staff Engineer

Cooper Testing Labs, Inc.
937 Commercial Street
Palo Alto, CA 94303

Unconsolidated-Undrained Triaxial Test
ASTM D2850



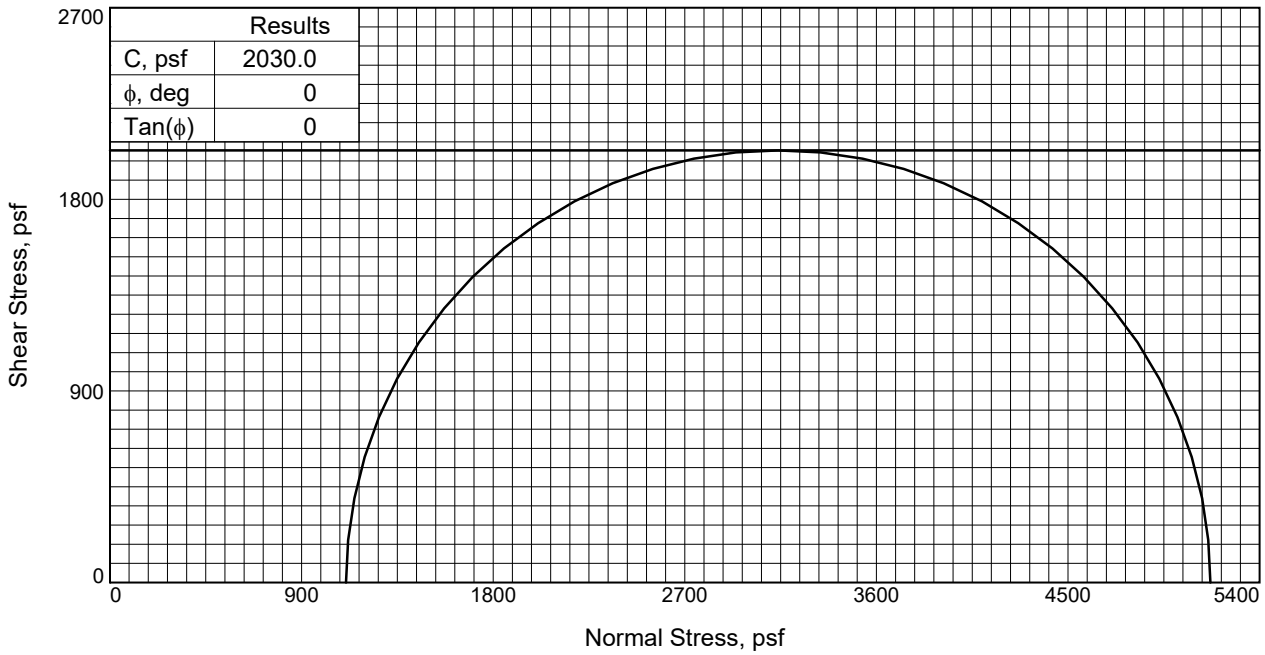


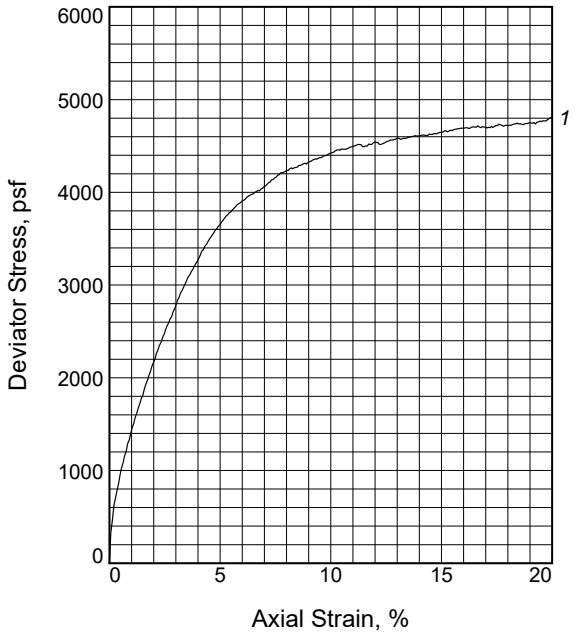
Sample Data	1	2	3	4
Moisture %	34.8			
Dry Den,pcf	87.5			
Void Ratio	0.962			
Saturation %	99.5			
Height in	4.99			
Diameter in	2.42			
Cell psi	7.1			
Strain %	15.00			
Deviator, ksf	1.581			
Rate %/min	0.99			
in/min	0.049			
Job No.:	1108-098			
Client:	Atlas			
Project:	New Quincy Courthouse (Site 2)			
Boring:	B-1			
Sample:	1-5			
Depth ft:	19.5			

Visual Soil Description	
Sample #	
1	Yellowish Brown CLAY w/ Sand
2	
3	
4	

Remarks:

Note: Strengths are picked at the peak deviator stress or 15% strain which ever occurs first per ASTM D2850.





Sample No.		1
Initial	Water Content, %	15.0
	Dry Density, pcf	113.2
	Saturation, %	82.7
	Void Ratio	0.4888
	Diameter, in.	2.438
	Height, in.	5.012
At Test	Water Content, %	15.0
	Dry Density, pcf	113.2
	Saturation, %	82.9
	Void Ratio	0.4888
	Diameter, in.	2.438
	Height, in.	5.012
Strain rate, in./min.		0.030
Back Pressure, psf		0.0
Cell Pressure, psf		1108.8
Fail. Stress, psf		4060.0
Strain, %		7.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		5168.8
σ_3 Failure, psf		1108.8

Type of Test:
Unconsolidated Undrained

Sample Type: CalMod

Description: SILTY SAND with GRAVEL, yellowish brown

Specific Gravity= 2.7

Remarks:

Figure _____

Client: Raney Geotechnical, Inc.

Project: Raney Geotechnical, Inc. Lab Testing

Source of Sample: 6056-003.00-New Quincy Courthouse-91-65859-PW

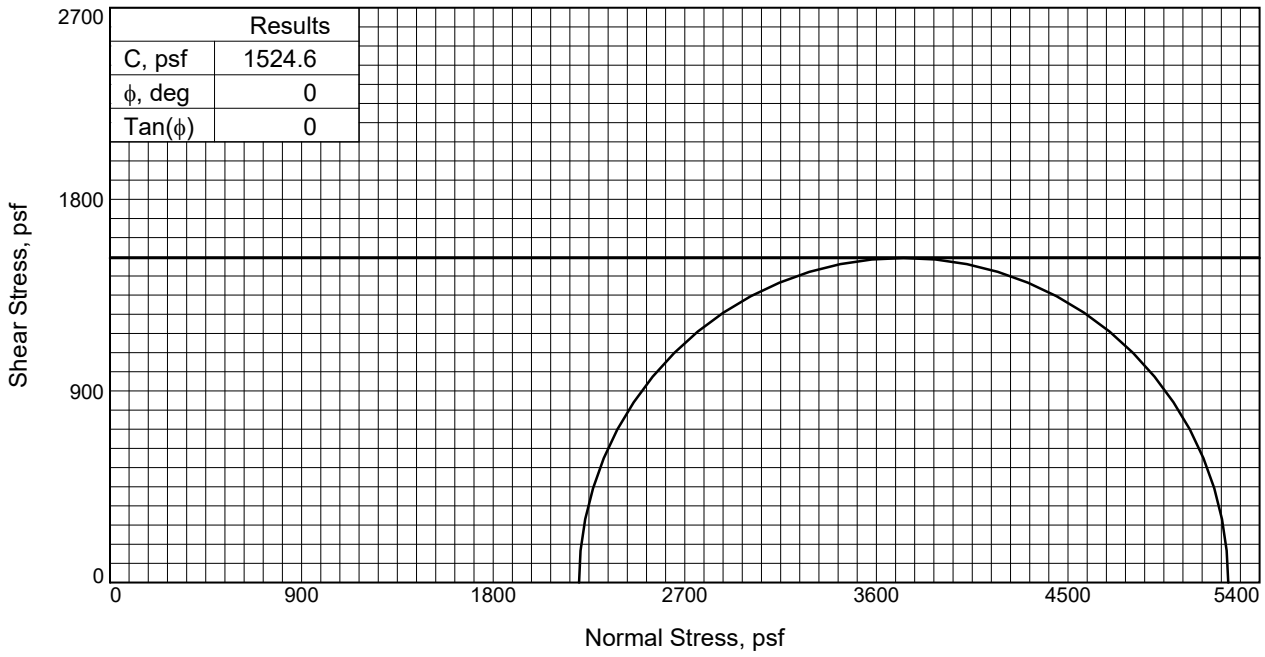
Sample Number: B-8 **Depth:** 10'

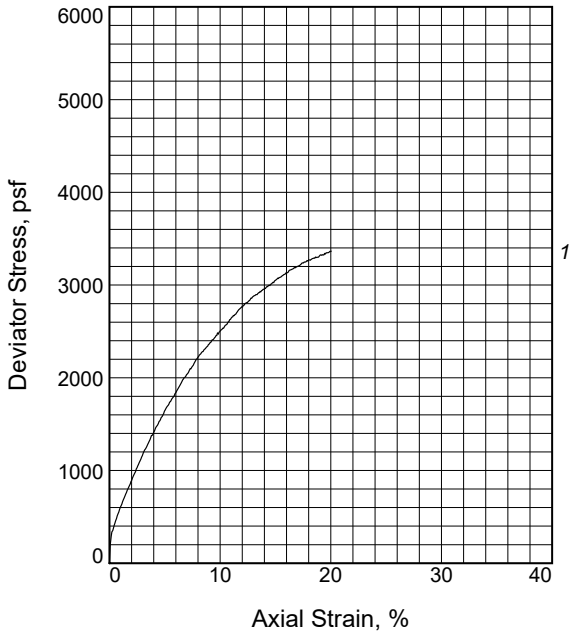
Proj. No.: 4563.X **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

Blackburn Consulting

W. Sacramento, CA





Sample No.		1
Initial	Water Content, %	22.6
	Dry Density, pcf	106.6
	Saturation, %	104.9
	Void Ratio	0.5813
	Diameter, in.	2.396
	Height, in.	5.000
At Test	Water Content, %	22.6
	Dry Density, pcf	106.6
	Saturation, %	105.0
	Void Ratio	0.5813
	Diameter, in.	2.396
	Height, in.	5.000
Strain rate, in./min.		0.030
Back Pressure, psf		0.0
Cell Pressure, psf		2203.2
Fail. Stress, psf		3049.3
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		5252.5
σ_3 Failure, psf		2203.2

Type of Test:
Unconsolidated Undrained

Sample Type: CalMod

Description: SANDY SILT, yellowish brown

Specific Gravity= 2.7

Remarks:

Figure _____

Client: Raney Geotechnical, Inc.

Project: Raney Geotechnical, Inc. Lab Testing

Source of Sample: 6056-003.00-New Quincy Courthouse-91-65859-PW

Sample Number: B-8 **Depth:** 20'

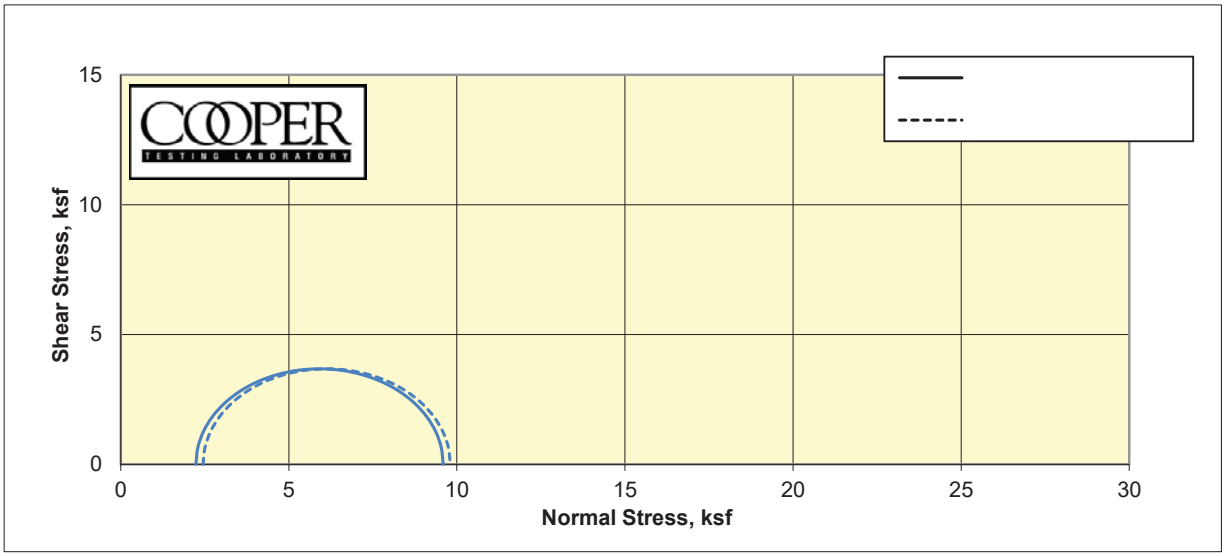
Proj. No.: 4563.X **Date Sampled:**

TRIAXIAL SHEAR TEST REPORT

Blackburn Consulting

W. Sacramento, CA

Consolidated Undrained Triaxial Compression with Pore Pressure
ASTM D4767



Specimen	1	2	3	4
Boring	B-6			
Sample	6-4			
Depth	14.5			
Visual Description	Yellow Sandy CLAY			
MC %	29.0			
Dry Density pcf	96.2			
Saturation %	99.3			
Void Ratio	0.817			
Diameter (in	2.41			
Height (in)	4.99			
	Final			
MC %	26.8			
Dry Density pcf	99.8			
Saturation %	100.0			
Void Ratio	0.751			
Diameter (in	2.37			
Height (in)	4.96			
Cell Pressure psi)	114.8			
Back Pressure (psi)	99.3			
	Effective Stresses At:			
Strain (%)	15.0			
Deviator ksf)	7.356			
Excess PP (psi)	-1.5			
Sigma 1 (ksf	9.804			
Sigma 3 (ksf	2.448			
P (ksf	6.126			
Q (ksf	3.678			
Stress Ratio	4.005			
Rate (in/min)	0.0004			

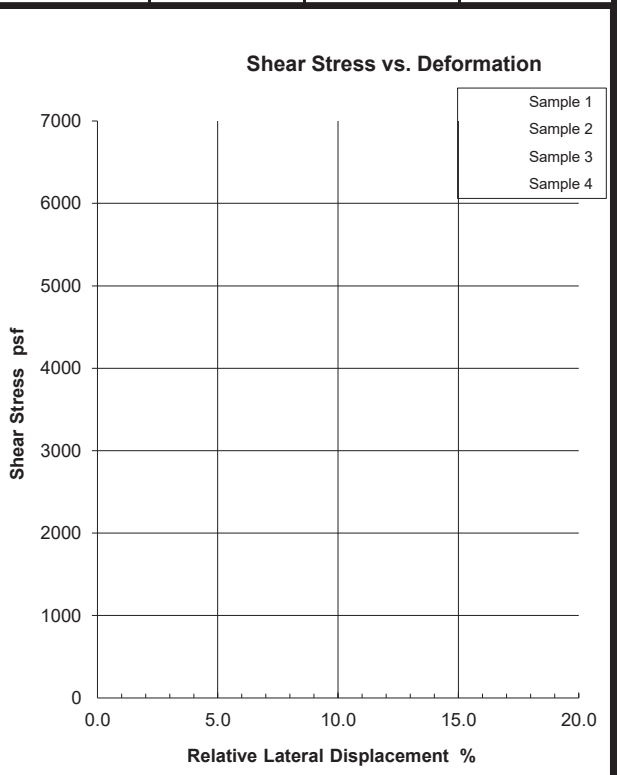
CTL Number:	1108-098		
Client Name:	Atlas		
Project Name:	New Quincy Courthouse (Site 2		
Project Number:			
Date:	7/21/2023	By:	MD/DC
Total C	#DIV/0!	ksf	
Total phi	#DIV/0!	degrees	
Eff. C	#DIV/0!	ksf	
Eff. Phi	#DIV/0!	degrees	©

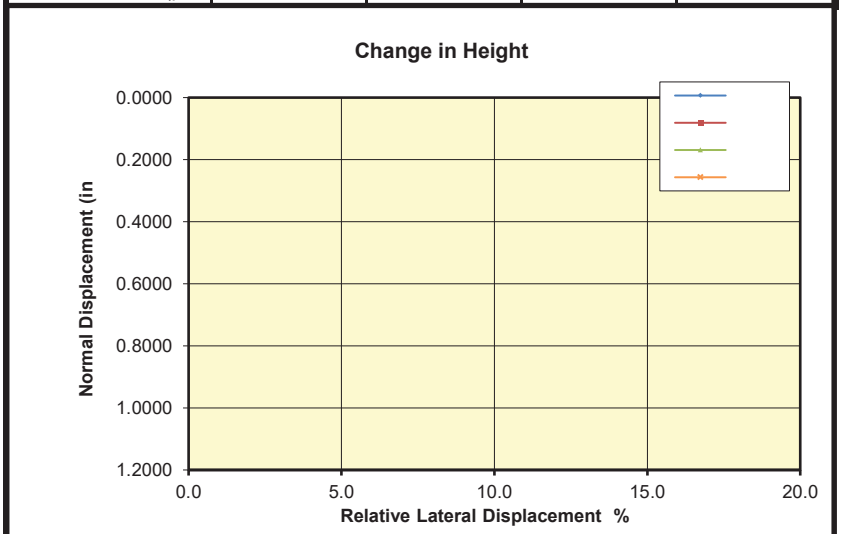
Consolidated Undrained Direct Shear (ASTM D3080M)

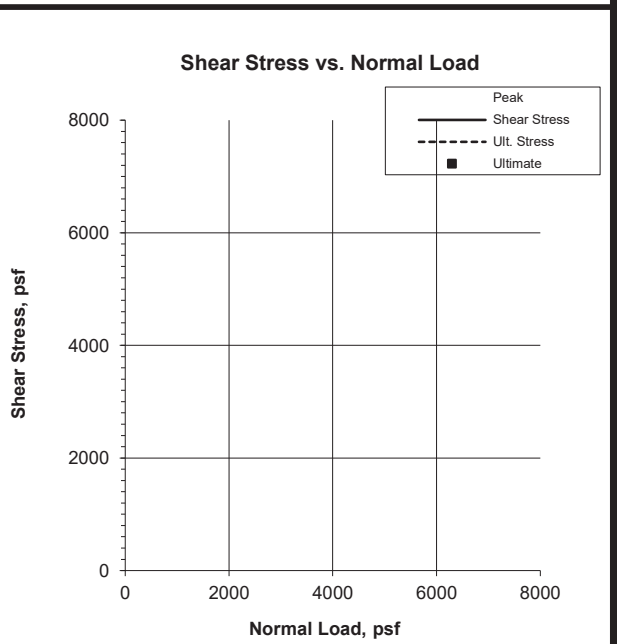
CTL Job #:	1108-098	Project #:		By:	MD
Client:	Atlas	Date:	7/18/2023	Checked:	PJ
Project Name:	New Quincy Courthouse (Site 2)	Remolding Info:			

Specimen Data				
	1	2	3	4
Boring:	B-3	B-3	B-3	
Sample:	3-1	3-1	3-1	
Depth (ft):	2	2	2	
Visual Description:	Dark Brown Sandy CLAY w/ Gravel	Dark Brown Sandy CLAY w/ Gravel	Dark Brown Sandy CLAY w/ Gravel	
Normal Load (psf)	1000	3000	5000	
Dry Mass of Specimen g	130.8	130.3	127.1	
Initial Height (in)	1.00	1.00	1.00	
Initial Diameter (in)	2.42	2.42	2.42	
Initial Void Ratio	0.556	0.562	0.602	
Initial Moisture (%)	7.7	11.7	17.2	
Initial Wet Density (pcf)	116.6	120.6	123.3	
Initial Dry Density pcf	108.3	107.9	105.2	
Initial Saturation (%	37.2	56.2	77.1	
ΔHeight Consol in	0.0242	0.0297	0.0457	
At Test Void Ratio	0.519	0.515	0.528	
At Test Moisture (%	16.3	17.6	18.5	
At Test Wet Density (pcf)	129.1	130.8	130.6	
At Test Dry Density (pcf)	111.0	111.2	110.3	
At Test Saturation (%)	84.8	92.0	94.3	
Strain Rate %/min)	1.1	1.1	1.1	
Strengths Picked at	Peak	Peak	Peak	
Shear Stress (psf)	1130	3234	6211	
ΔHeight (in) at Peak				
Ultimate Stress (psf				

Phi (deg)		Ult. Phi (deg	
Cohesion (psf)		Ult. Cohesion psf)	







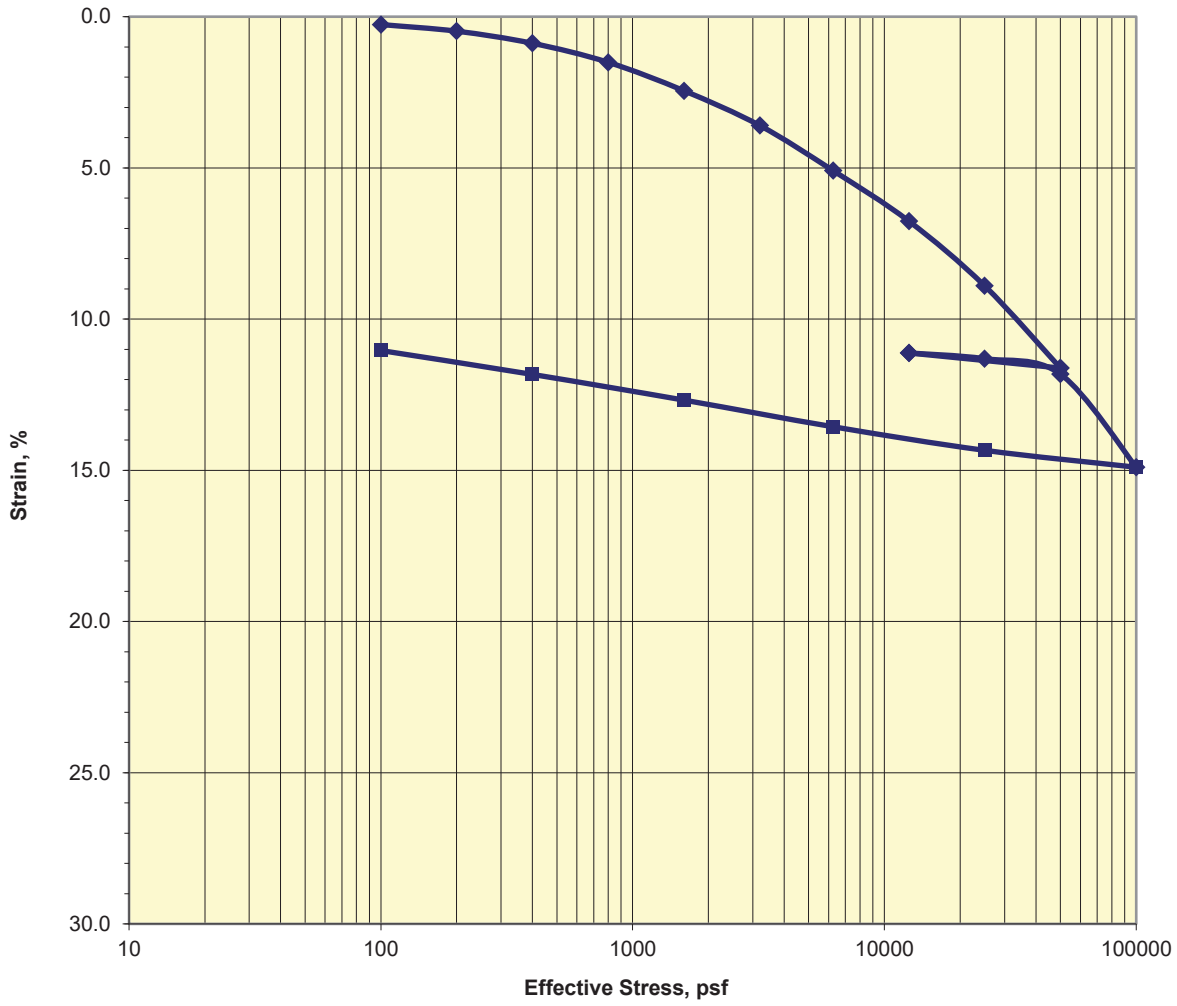
Remarks: DS-CU A fully undrained condition may not be attained in this test. ΔH is not measured during undrained direct shear tests. Engineering judgement is required to determine phi and cohesion, no phi or cohesion is reported. To add phi and cohesion to the report go to the "phi" tab and in cells G30, G31, H30, and H31 enter end points for a line through the 3 data points. The points plotted can be changed on the "Eng Values" tab using cells L6, A2, C2, and E2.

©

Consolidation Test
ASTM D2435

Job No.:	1108-098	**Boring:**	B-4	**Run By:**	HM
Client:	Atlas	**Sample:**	4-4	**Reduced:**	RU
Project:	New Quincy Courthouse (Site 2)	**Depth, ft.:**	14.5	**Checked:**	PJ
Soil Type:	Yellowish Brown Sandy CLAY Silty)			**Date:**	8/1/2023

Strain-Log-P Curve



Assumed Gs 2.75	Initial	Final
Moisture %:	27.4	20.1
Dry Density, pcf:	97.6	110.6
Void Ratio:	0.759	0.552
% Saturation:	99.3	100.0

Remarks:

RANEY GEOTECHNICAL INC

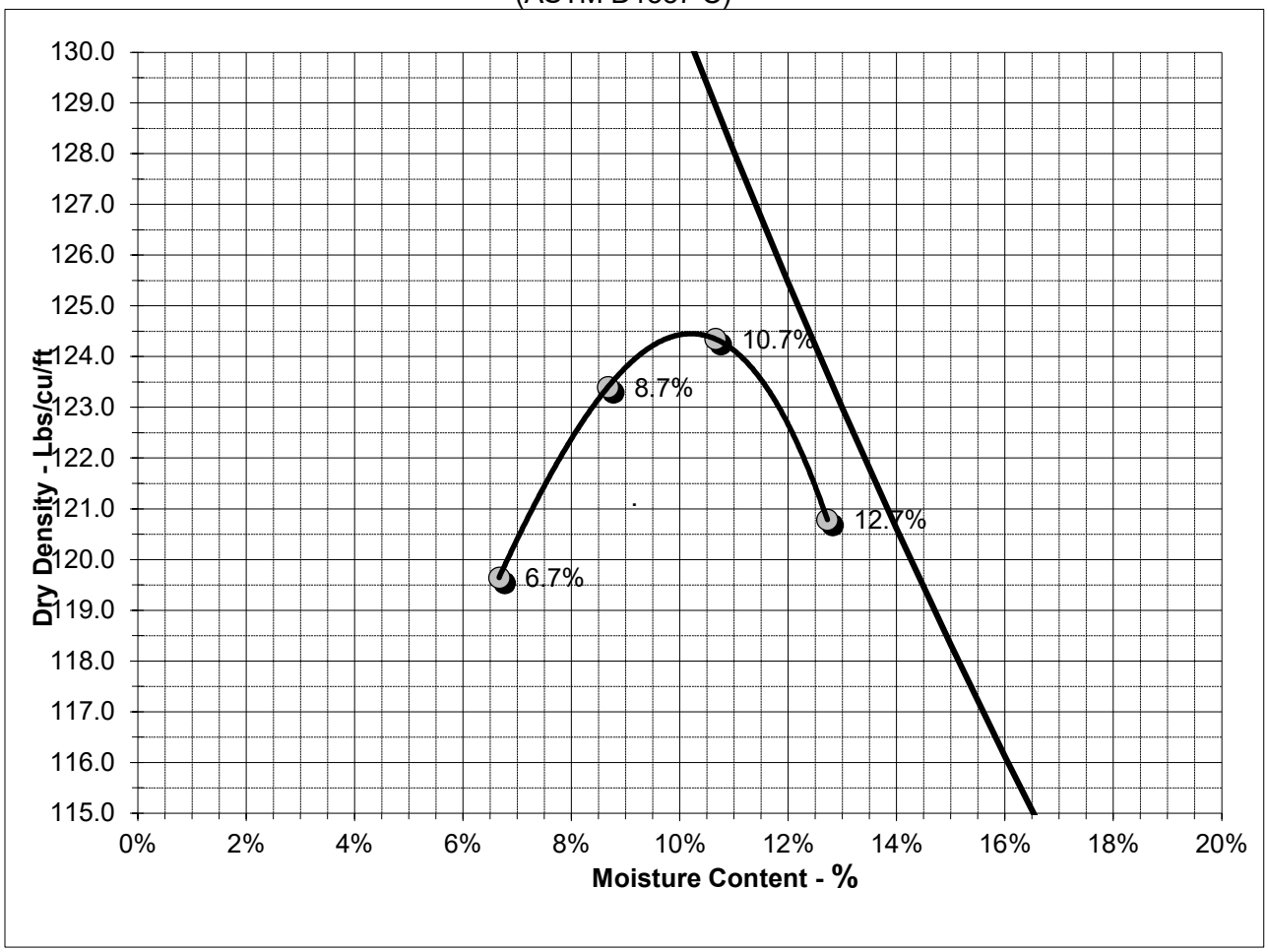
October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Compaction Characteristics
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B-10 @ 1' to 5'	

LABORATORY COMPACTION CHARACTERISTICS
(ASTM D1557 C)



Maximum Dry Unit Weight: 124.5 pcf
Optimum Moisture Content: 10.3 percent

Reviewed by: _____
Guang H. Zhu
Staff Engineer

Corrosivity Tests Summary

CTL # 1108-098 **Date:** 7/19/2023 **Tested By:** PJ **Checked:** PJ

Client: Atlas **Project:** New Quincy Courthouse (Site-2) **Proj. No:**

Remarks:

Sample Location or ID			Resistivity @ 15.5 °C (Ohm-cm			Chloride	Sulfate		pH	ORP		Sulfide	Moisture	Soil Visual Description
			As Rec.	Min	Sat.	mg/kg	mg/kg	%		Redox		Qualitative	At Test	
						Dry Wt.	Dry Wt.	Dry Wt.		E_H (mv	At Test	by Lead	%	
Boring	Sample, No.	Depth, ft.	ASTM G57	Cal 643	ASTM G57	ASTM D4327	ASTM D4327	ASTM D4327	ASTM G51	ASTM G200	Temp °C	Acetate Paper	ASTM D2216	
B-2	2-1	2	-	-	7,015	2	4	0.0004	7.2	489	22	Negative	35.1	Very Dark Brown CLAY w/ Sand, trace Gravel

COOPER TESTING LABORATORY

CTL Job No.:	1108-098	**Boring:**	B-6	**Date:**	7/26/2023
Client:	Atlas	**Sample:**	6-1 & 6-2	**By:**	PJ
Project Name:	New Quincy Courthouse (Site-2)	**Depth:**	2 & 4.5'		
Project No:					

Visual Description: Reddish Brown Sandy Lean CLAY w/ Gravel

Processing:

Percent Passing #4 Sieve

Total Air Dry Weight:	N/A
Wt. Retained on #4 Sieve:	N/A
% Retained	N/A
% Passing #4 Sieve:	N/A

Sample Dimensions

Height (in.) 1.002 **Diameter (in. =** 4.017

Moisture Calcs

	Initial	Final
Tare #		
Wet Wt. + Tare, (gm	689.5	736.8
Dry Wt. + Tare, (gm	647.3	647.3
Tare Wt., (gm	114.6	114.6
Wt. Of Water, (gm	42.1	89.5
% Water	12.5	26.6

Remolding:

Tamp two lifts, 15 blows/lift @ slightly below optimum moisture content

	Initial	Final	
Ring & Sample:	574.9	622.3	grams
Ring:	196.4	196.4	grams
Remolded Wet Wt.:	378.5	425.8	grams
Wet Density	113.5	125.5	pcf
Dry Density	100.9	99.1	pcf
% Sat. (2.7)(dry dens.)(m/c) / 168.48 - (dry dens.	50.5	102.7	UBC Saturation range 49-51% ASTM Saturation range 48-52%

Expansion Test:

Date	Time	Dial	Delta h, %
7/24/2023	11:14	0.0000	0.000
7/24/2023	11:35	-0.0056	0.559
7/25/2023	10:31	-0.0177	1.766
7/25/2023	11:43	-0.0177	1.766
		Total Dial	1.8

Tested with 1 psi Surcharge

Remarks:

Expansion Index

initial dial - final dial / initial sample height x 1000

Results

EI = 18

This test is a simplified index test and may not show the full potential for expansion and/or shrinkage. Use result with caution! See ASTM D 3877 or D4546

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory Expansion Index Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

EXPANSION INDEX (ASTM D4829)

Sampled By: Others	**Date Received:** 9/25/25
Client Project: Quincy Courthouse	**Client Job No.:** 91-65859-PW
Sample ID: B11 (1-5')	

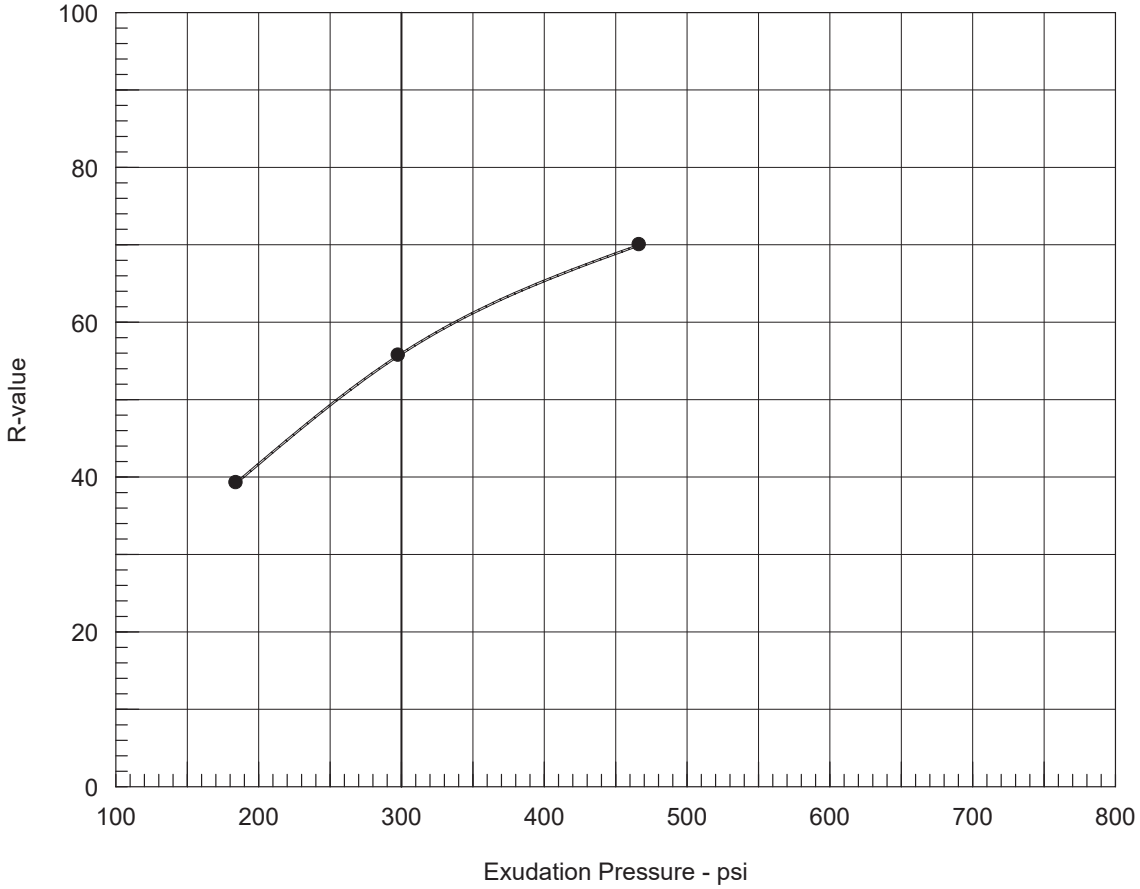
Depth (ft)	Initial Moisture Content (%)	Final Moisture Content (%)	Dry Density (pcf)	Expansion Index
1 – 5	10.8	20.5	106.8	**4**

Classification of Expansive Soil

Expansion Index	Expansion Potential
0-20	Very Low
21-50	Low
51-90	Moderate
91-130	High
Above 130	Very High

Reviewed by: _____
Hao Zhu, Staff Engineer

R-VALUE TEST REPORT



Resistance R-Value and Expansion Pressure - ASTM D2844

No.	Compact. Pressure psi	Density pcf	Moist. %	Expansion Pressure psi	Horizontal Press. psi @ 160 psi	Sample Height in.	Exud. Pressure psi	R Value	R Value Corr.
1	180	122.8	9.9	0.76	35	2.50	467	70	70
2	180	121.4	11.1	2.85	51	2.50	298	56	56
3	180	118.7	11.8	0.06	79	2.60	184	37	39

Test Results	Material Description
R-value at 300 psi exudation pressure = 56	Light Brown Clayey Sand w/ Gravel Sampled by J. Li on 06/05/2023

Project No.: 9165859PW
Project: New Quincy Courthouse (Site 2)
Location: Onsite / B2 & B3
Sample Number: 10S230711-4
Date: 7/13/2023

Tested by: EC
Checked by: GL
Remarks:

R-VALUE TEST REPORT

CONSOLIDATED ENGINEERING LABORATORIES

Figure 10S230711-4

RANEY GEOTECHNICAL INC

October 3, 2025

Kyle Hahn
Atlas Technical Consultants
Kyle.hahn@oneatlas.com

Laboratory R-Value Test Results
ATLAS LABORATORY TESTING SERVICES
Project No. 6056-003.00

RESISTANCE (R) VALUE (CTM 301)

Sample ID:	B8 (1-5')
Sampled By:	Others
Date Received:	9/25/25

Specimen Number	Dry Unit Weight	Moisture @ Compaction	Expansion Pressure		Exudation Pressure	R - Value
	(pcf)	(percent)	(dial)	(psf)	(psi)	
1	130.6	7.6	7	30	709	75
2	130.2	8.1	5	22	292	66
3	128.9	8.6	1	4	128	41
R-VALUE @ 300 PSI EXUDATION PRESSURE = 67						

Sample ID:	B11 (1-5')
Sampled By:	Others
Date Received:	9/25/25

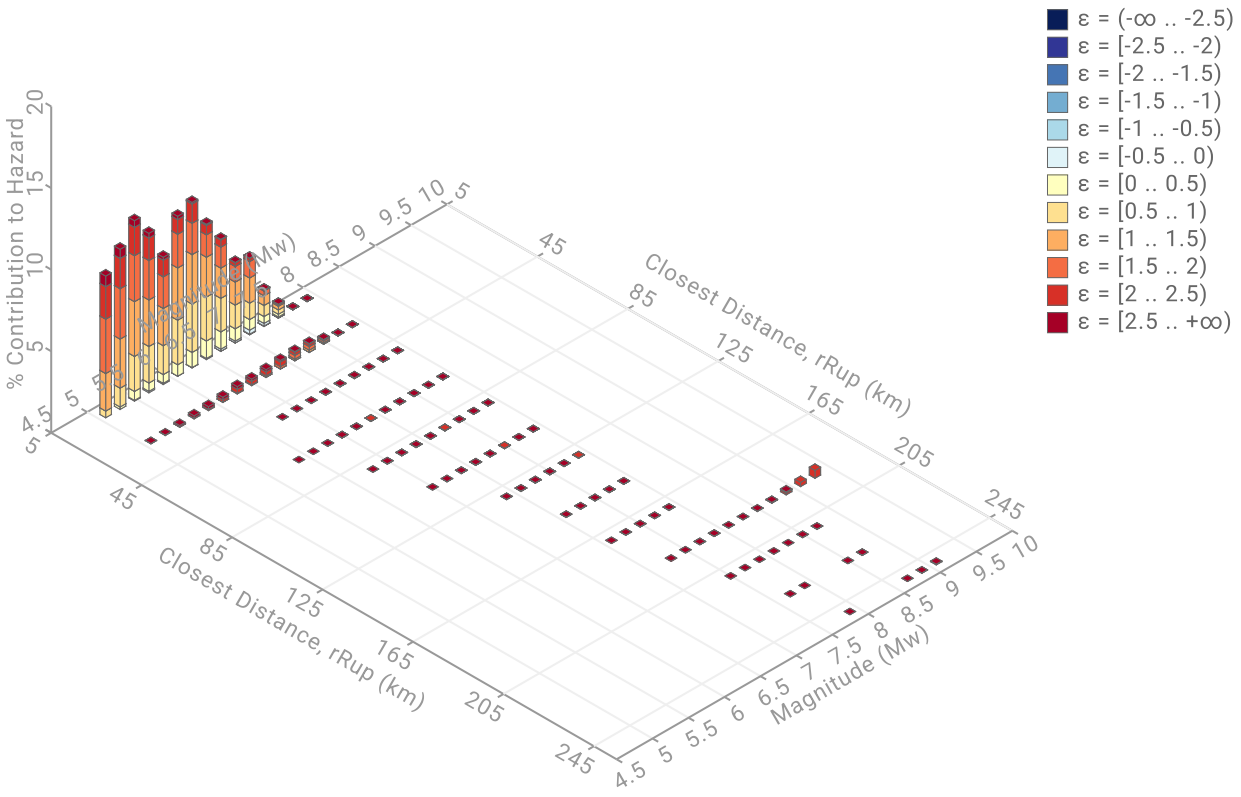
Specimen Number	Dry Unit Weight	Moisture @ Compaction	Expansion Pressure		Exudation Pressure	R - Value
	(pcf)	(percent)	(dial)	(psf)	(psi)	
1	120.9	11.8	33	143	339	69
2	120.6	12.3	30	130	251	64
3	119.3	12.8	23	100	209	60
R-VALUE @ 300 PSI EXUDATION PRESSURE = 67						

Reviewed by: _____
Hao Zhu, Staff Engineer

APPENDIX IV
SITE-SPECIFIC GROUND MOTION HAZARD ANALYSIS

Disaggregation Report

Disaggregation



2475 Years (2% in 50 Yeras) PGA Disaggregation

Geographical Disaggregation



Parameter Summary

Model: NSHM Conterminous U.S. 2018

Latitude: 39.938239 °

Longitude: -120.943783 °

Vs30: 335 m/s

Intensity Measure Type: PGA

Return Period: 2475 (2% in 50)

Component: Total

Disaggregation Summary: Total

Disaggregation targets

Return period : 2475 yrs

Exceedance rate : 4.040e-4 yr^{-1}

PGA ground motion : 6.575e-1 g

Recovered targets

Return period : 2452.0794 yrs

Exceedance rate : 4.078e-4 yr^{-1}

Totals

Binned : 100 %

Residual : 0 %

Trace : 0.19 %

Mean (over all sources)

m : 6.09

r : 11.76 km

ε_0 : 1.37 σ

Mode (largest m-r bin)

m : 5.5

r : 8.87 km

ε_0 : 1.43 σ

Contribution : 11.05 %

Mode (largest m-r-ε_0 bin)

m : 5.5

r : 7.74 km

ε_0 : 1.26 σ

Contribution : 3.36 %

Discretization

r : min = 0.0, max = 1000.0, Δ = 20.0 km

m : min = 4.4, max = 9.4, Δ = 0.2

ε : min = -3.0, max = 3.0, Δ = 0.5 σ

Epsilon keys

ε0 : [-∞ .. -2.5)

ε1 : [-2.5 .. -2.0)

ε2 : [-2.0 .. -1.5)

ε3 : [-1.5 .. -1.0)

ε4 : [-1.0 .. -0.5)

ε5 : [-0.5 .. 0.0)

ε6 : [0.0 .. 0.5)

ε7 : [0.5 .. 1.0)

ε8 : [1.0 .. 1.5)

ε9 : [1.5 .. 2.0)

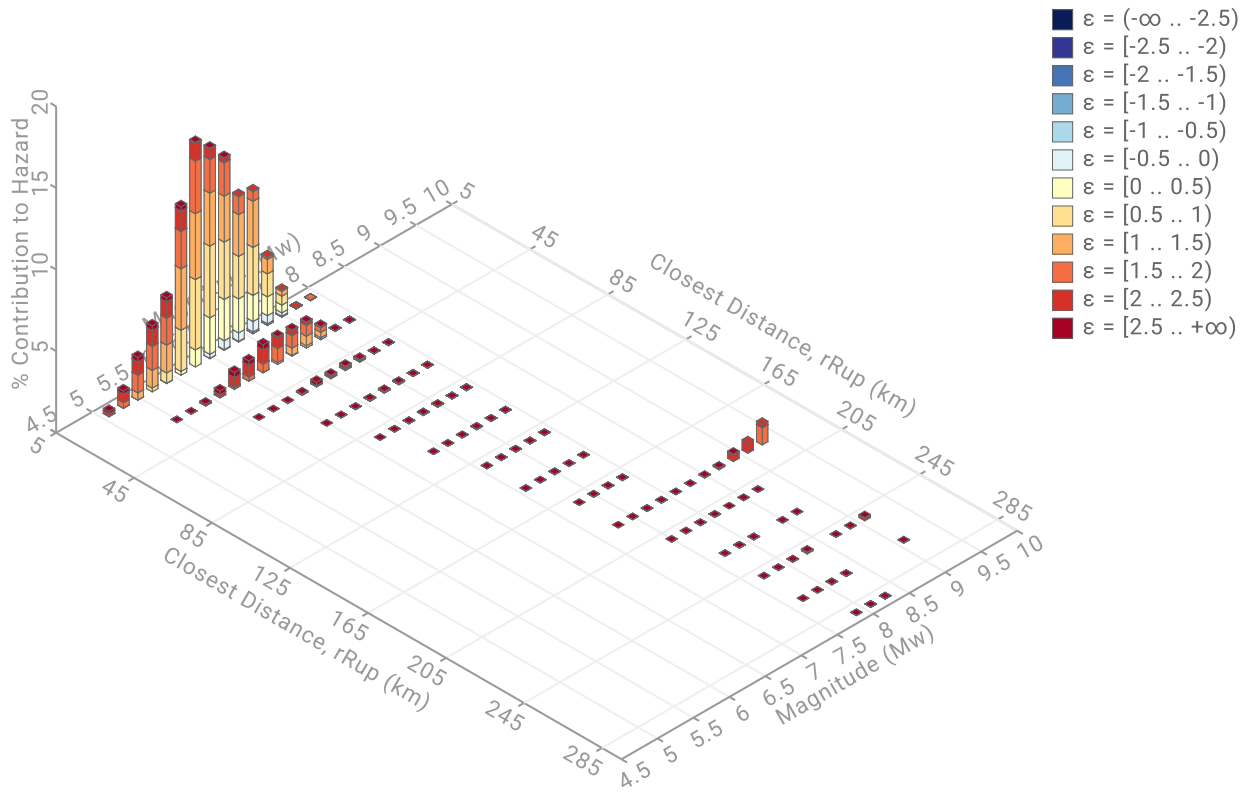
ε10 : [2.0 .. 2.5)

ε11 : [2.5 .. +∞]

2475 Years (2% in 50 Yeras) T=1.0s Disaggregation

Disaggregation Report

Disaggregation



Application Metadata

Application: Disaggregation
URL: https://earthquake.usgs.gov/nshmp/hazard/disagg

Repository: nshmp-apps
Version: 20.8.0
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-apps

Repository : nshmp-haz
Version: 2.6.18
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-haz

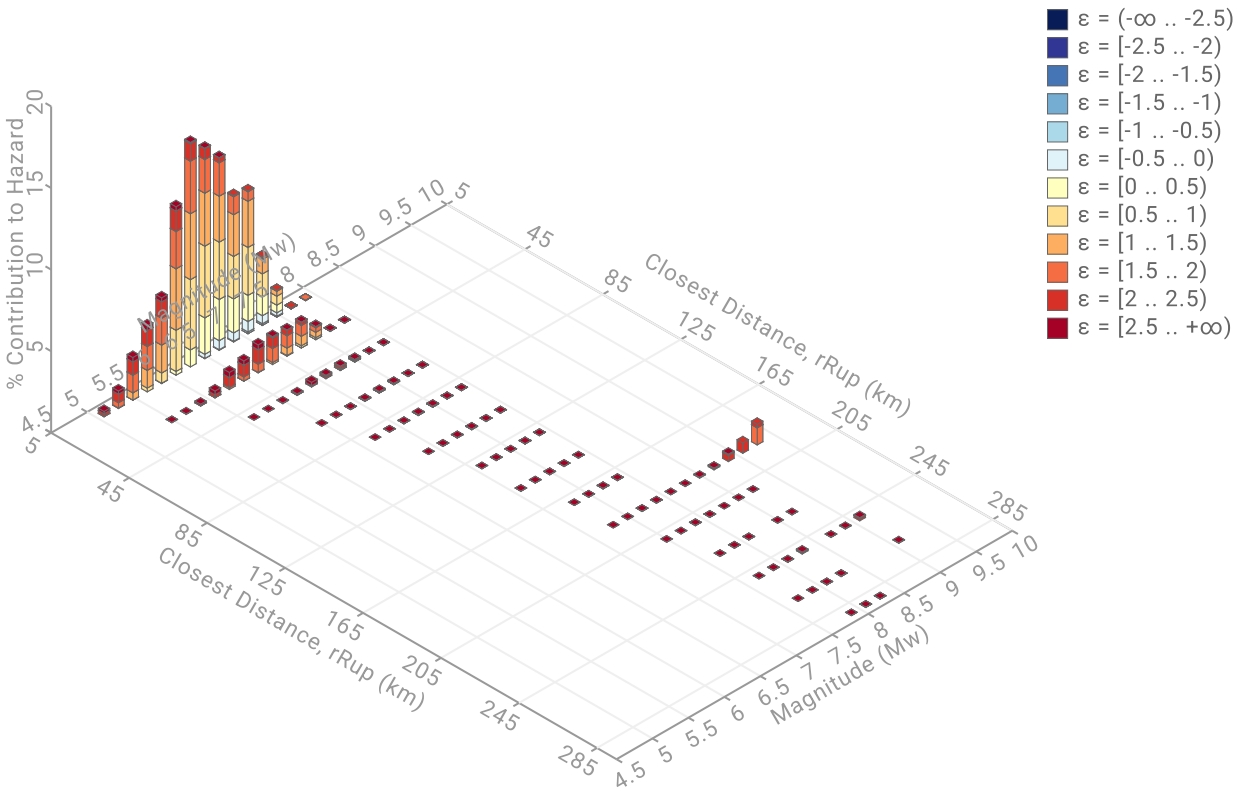
Repository : nshmp-lib
Version: 1.7.14
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-lib

Repository : nshm-conus
Version: 5.2.4
URL: https://code.usgs.gov/ghsc/nshmp/nshms/nshm-conus.git

October 08, 2025, 02:47 PM

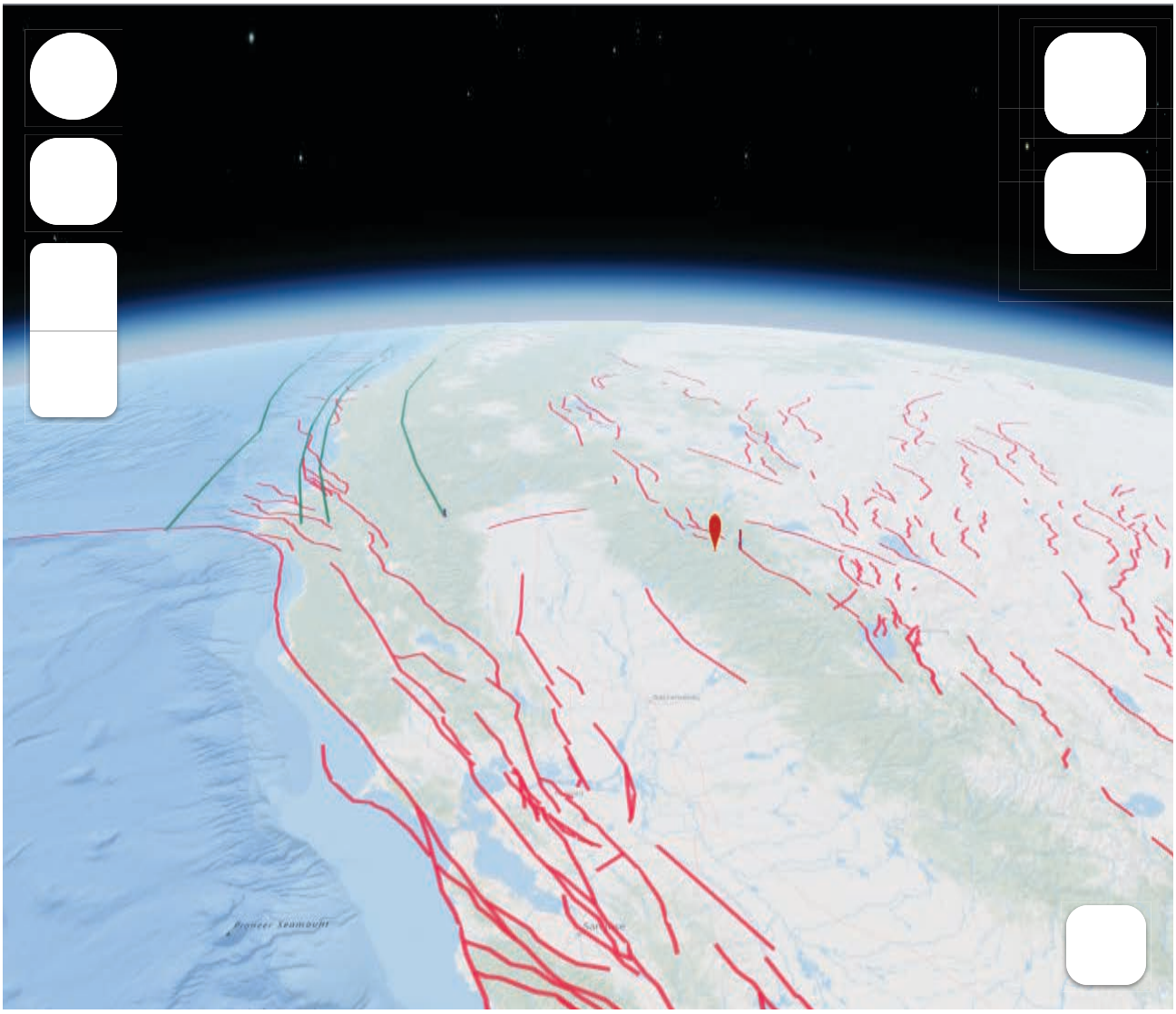
Disaggregation Report

Disaggregation



2475 Years (2% in 50 Yeras) T=1.0s Disaggregation

Geographical Disaggregation



Parameter Summary

Model: NSHM Conterminous U.S. 2018

Latitude: 39.938239 °

Longitude: -120.943783 °

Vs30: 335 m/s

Intensity Measure Type: 1.0 s

Return Period: 2475 (2% in 50)

Component: Total

Disaggregation Summary: Total

Disaggregation targets

Return period : 2475 yrs

Exceedance rate : 4.040e-4 yr^{-1}

1.0 s SA ground motion : 7.010e-1 g

Recovered targets

Return period : 2460.2924 yrs

Exceedance rate : 4.065e-4 yr^{-1}

Totals

Binned : 100 %

Residual : 0 %

Trace : 0.27 %

Mean (over all sources)

m : 6.61

r : 17.76 km

ε_0 : 1.26 σ

Mode (largest m-r bin)

m : 6.3

r : 10.58 km

ε_0 : 1.22 σ

Contribution : 13.75 %

Mode (largest m-r-ε_0 bin)

m : 6.5

r : 7.49 km

ε_0 : 0.74 σ

Contribution : 4.39 %

Discretization

r : min = 0.0, max = 1000.0, Δ = 20.0 km

m : min = 4.4, max = 9.4, Δ = 0.2

ε : min = -3.0, max = 3.0, Δ = 0.5 σ

Epsilon keys

ε0 : [-∞ .. -2.5)

ε1 : [-2.5 .. -2.0)

ε2 : [-2.0 .. -1.5)

ε3 : [-1.5 .. -1.0)

ε4 : [-1.0 .. -0.5)

ε5 : [-0.5 .. 0.0)

ε6 : [0.0 .. 0.5)

ε7 : [0.5 .. 1.0)

ε8 : [1.0 .. 1.5)

ε9 : [1.5 .. 2.0)

ε10 : [2.0 .. 2.5)

ε11 : [2.5 .. +∞]

Disaggregation Contributions: Total

Source Set ↳ Source	Type	r	m	ε_0	lon	lat	az	%
UCERF3 Fault Model 3.1 (opt)	Grid							24.29
UCERF3 Fault Model 3.2 (opt)	Grid							24.23
Extensional (fixed) (opt)	Grid							15.74
Extensional (adaptive) (opt)	Grid							15.02
UCERF3 Fault Model 3.1	FaultSystem							5.33
Mohawk Valley (8)		16.59	6.78	1.49	120.755°W	39.974°N	76.20	3.3
UCERF3 Fault Model 3.2	FaultSystem							5.24
Mohawk Valley (8)		16.59	6.77	1.50	120.755°W	39.974°N	76.20	3.2
Cascadia (full, bottom)	Interface							2.23
Cascadia (full, bottom)		181.51	9.17	2.03	122.945°W	40.376°N	286.62	2.23
Compressional - WA,OR (adaptive) (opt)	Grid							1.88
Compressional - No Puget (adaptive) (opt)	Grid							1.88
Compressional - No Puget (fixed) (opt)	Grid							1.78
Compressional - WA,OR (fixed) (opt)	Grid							1.78

Application Metadata

Application: Disaggregation
URL: https://earthquake.usgs.gov/nshmp/hazard/disagg

Repository: nshmp-apps
Version: 20.8.0
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-apps

Repository : nshmp-haz
Version: 2.6.18
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-haz

Repository : nshmp-lib
Version: 1.7.14
URL: https://code.usgs.gov/ghsc/nshmp/nshmp-lib

Repository : nshm-conus
Version: 5.2.4
URL: https://code.usgs.gov/ghsc/nshmp/nshms/nshm-conus.git

October 22, 2025, 05:48 PM

SITE-SPECIFIC GROUND MOTION ANALYSIS (ASCE 7-22)

Project:	Quincy Courthouse	**Latitude:**	39.938239 deg	**Calculated By:**	SD
Client:	BKF Engineers	**Longitude:**	-120.94378 deg	**Checked By:**	JF
Job No:	18077.000	**Vs_{30}:**	335 m/s	**Date:**	10/15/25

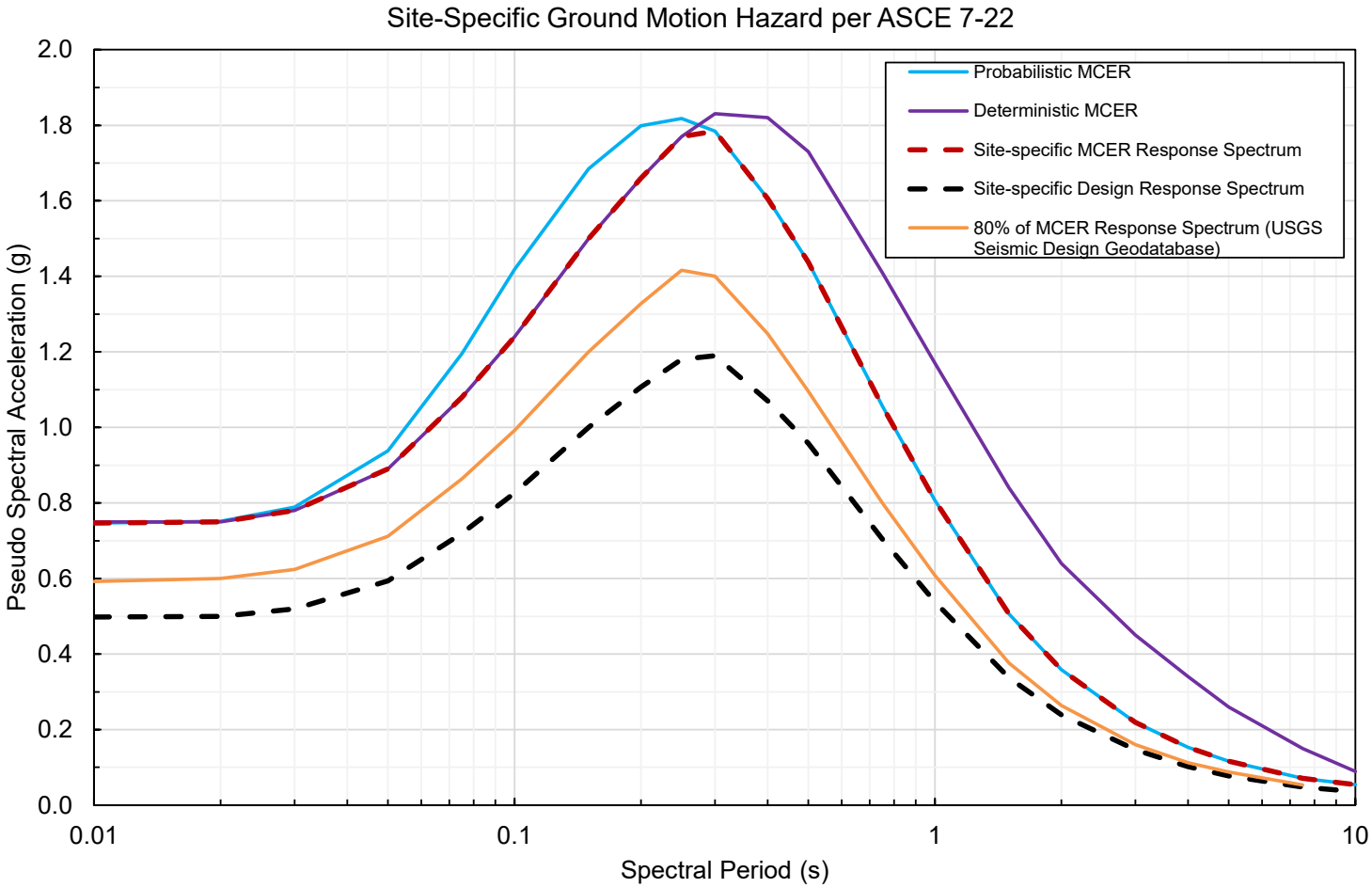
Site Class	Mapped Spectral Response Acceleration Parameters		Spectral Response Acceleration Parameters Adjusted for		Design Spectral Response Acceleration Parameters		Period			Vs30 (m/sec)	PGA
	Ss (g)	S1 (g)	S_{MS} (g)	S_{M1} (g)	S_{DS} (g)	S_{D1} (g)	To (sec)	Ts (sec)	T_L (sec)		PGA_M (g)
CD	1.43	0.38	1.59	0.76	1.06	0.51	0.096	0.478	16.0	335	0.56

Mapped Design Response Spectrum (USGS Seismic Design Geodatabase)							**Probabilistic MCE_R**				**Deterministic MCE_R**					80% of MCE_R Response Spectrum (USGS Seismic Design Geodatabase)	**Site-Specific MCE_R Response Spectrum**	**Site-Specific Design Response Spectrum**
Period (sec)	Mapped **Design Two-Period** Response Spectrum	Mapped **MCE_R Two-Period** Response Spectrum	Period (sec)	Mapped **Design Multi-Period** Response Spectrum	Mapped **MCE_R Multi-Period** Response Spectrum	Period (sec)	UHGM from USGS Geomean 2% in 50 Years	RTGM 1% Probability of Collapse in 50 Years	Max Horiz Direction Response to Geomean	1% Chance of Collapse in 50 Years (Rotated)	84th Percentile of Geomean	Max Horiz Direction Response to Geomean	84th Percentile of Geomean Rotated	Deterministic Lower Limit on Response Spectrum (Table 21.2-1)	Deterministic MCE_R Response Spectrum			
	Sa (g)	Sa (g)		Sa (g)	Sa (g)		Sa (g)	Sa (g)	Max/Mean	Sa (g)	Sa (g)	Max/Mean	Sa (g)	Sa (g)	Sa (g)	Sa (g)	Sa (g)	Sa (g)
0.00	0.42	0.636	0.00	0.490	0.740	0.00	0.657	0.619	1.200	0.743	0.437	1.200	0.524	0.740	0.740	0.592	0.740	0.493
0.01	0.49	0.736	0.01	0.500	0.740	0.01	0.662	0.623	1.200	0.747	0.437	1.200	0.524	0.750	0.750	0.592	0.747	0.498
0.02	0.557	0.836	0.02	0.500	0.750	0.02	0.661	0.626	1.200	0.752	0.438	1.200	0.526	0.750	0.750	0.600	0.750	0.500
0.03	0.624	0.935	0.03	0.520	0.780	0.03	0.696	0.657	1.200	0.789	0.456	1.200	0.547	0.780	0.780	0.624	0.780	0.520
0.05	0.757	1.135	0.05	0.590	0.890	0.05	0.823	0.781	1.200	0.938	0.529	1.200	0.635	0.890	0.890	0.712	0.890	0.593
0.075	0.923	1.384	0.08	0.720	1.080	0.08	1.048	0.996	1.200	1.195	0.654	1.200	0.785	1.080	1.080	0.864	1.080	0.720
0.096	1.060	1.590	0.10	0.830	1.240	0.10	1.235	1.183	1.200	1.419	0.768	1.200	0.921	1.240	1.240	0.992	1.240	0.827
0.10	1.060	1.590	0.15	1.000	1.500	0.15	1.475	1.404	1.200	1.685	0.938	1.200	1.126	1.500	1.500	1.200	1.500	1.000
0.15	1.060	1.590	0.20	1.110	1.660	0.20	1.575	1.499	1.200	1.799	1.032	1.200	1.239	1.660	1.660	1.328	1.660	1.107
0.20	1.060	1.590	0.25	1.180	1.770	0.25	1.597	1.511	1.203	1.818	1.071	1.203	1.288	1.770	1.770	1.416	1.770	1.180
0.25	1.060	1.590	0.30	1.170	1.750	0.30	1.573	1.479	1.206	1.784	1.076	1.206	1.298	1.830	1.830	1.400	1.784	1.189
0.30	1.060	1.590	0.40	1.040	1.560	0.40	1.424	1.324	1.213	1.606	1.024	1.213	1.242	1.820	1.820	1.248	1.606	1.070
0.40	1.060	1.590	0.50	0.910	1.370	0.50	1.266	1.179	1.219	1.437	0.947	1.219	1.154	1.730	1.730	1.096	1.437	0.958
0.478	1.060	1.590	0.75	0.670	1.000	0.75	0.923	0.856	1.234	1.057	0.720	1.234	0.889	1.410	1.410	0.800	1.057	0.704
0.50	1.013	1.520	1.00	0.510	0.760	1.00	0.701	0.645	1.250	0.807	0.566	1.250	0.708	1.170	1.170	0.608	0.807	0.538
0.75	0.676	1.013	1.50	0.310	0.470	1.50	0.438	0.404	1.253	0.506	0.377	1.253	0.472	0.840	0.840	0.376	0.506	0.337
1.00	0.507	0.760	2.00	0.220	0.330	2.00	0.311	0.286	1.256	0.359	0.274	1.256	0.344	0.640	0.640	0.264	0.359	0.239
1.50	0.338	0.507	3.00	0.140	0.200	3.00	0.190	0.174	1.261	0.219	0.172	1.261	0.217	0.450	0.450	0.160	0.219	0.146
2.00	0.253	0.380	4.00	0.095	0.140	4.00	0.132	0.121	1.267	0.153	0.119	1.267	0.150	0.340	0.340	0.112	0.153	0.102
3.00	0.169	0.253	5.00	0.072	0.110	5.00	0.101	0.091	1.272	0.116	0.086	1.272	0.109	0.260	0.260	0.088	0.116	0.077
4.00	0.127	0.190	7.50	0.045	0.067	7.50	0.061	0.055	1.286	0.071	0.043	1.286	0.055	0.150	0.150	0.054	0.071	0.047
5.00	0.101	0.152	10.00	0.034	0.051	10.00	0.045	0.042	1.300	0.054	0.024	1.300	0.031	0.089	0.089	0.041	0.054	0.036
7.50	0.068	0.101																
10.00	0.051	0.076																

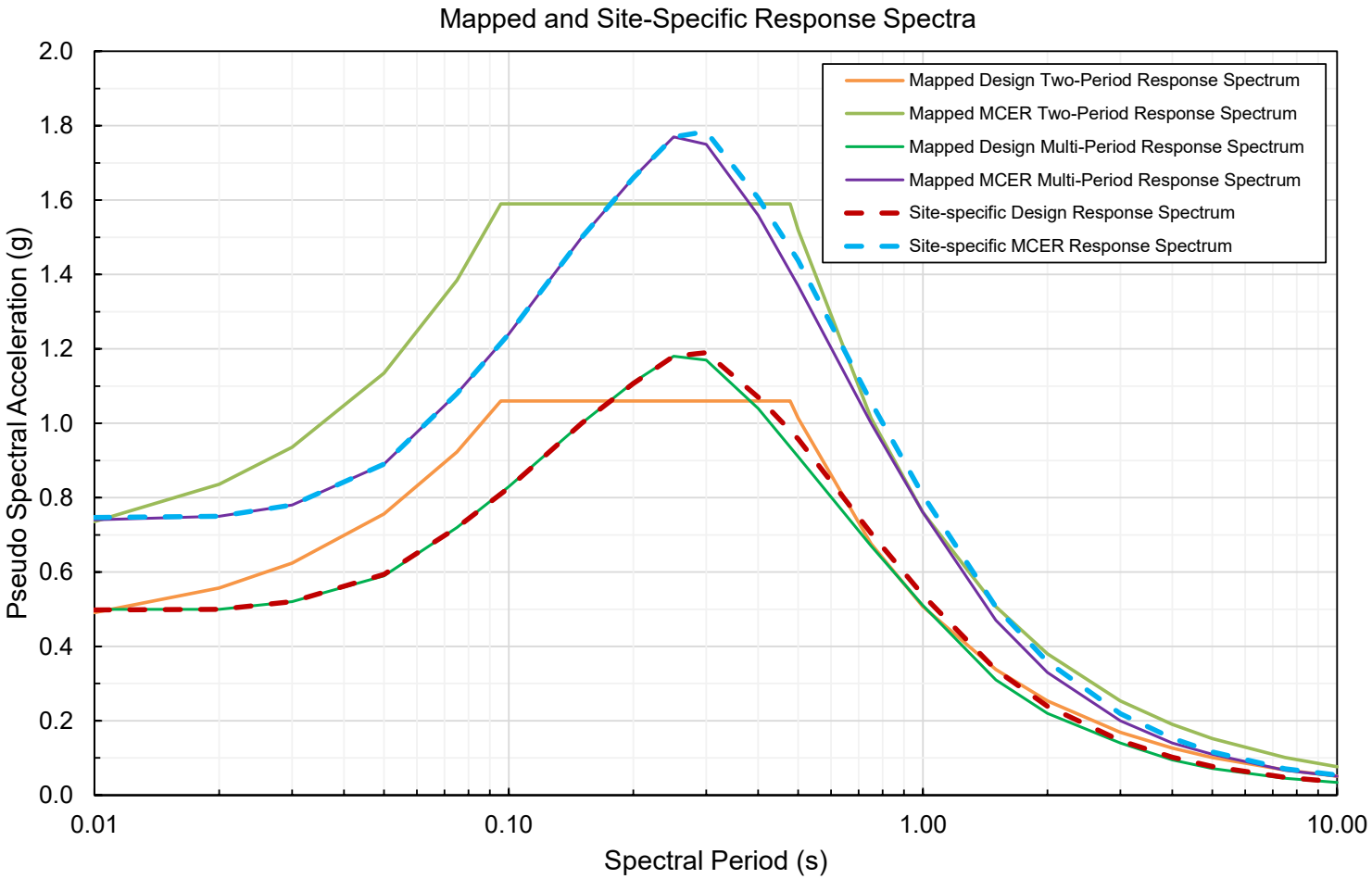
Site-specific Spectral Acceleration Parameters				
PGA_M	S_{MS}	S_{M1}	S_{DS}	S_{D1}
0.560	1.606	0.807	1.070	0.538

ATLAS

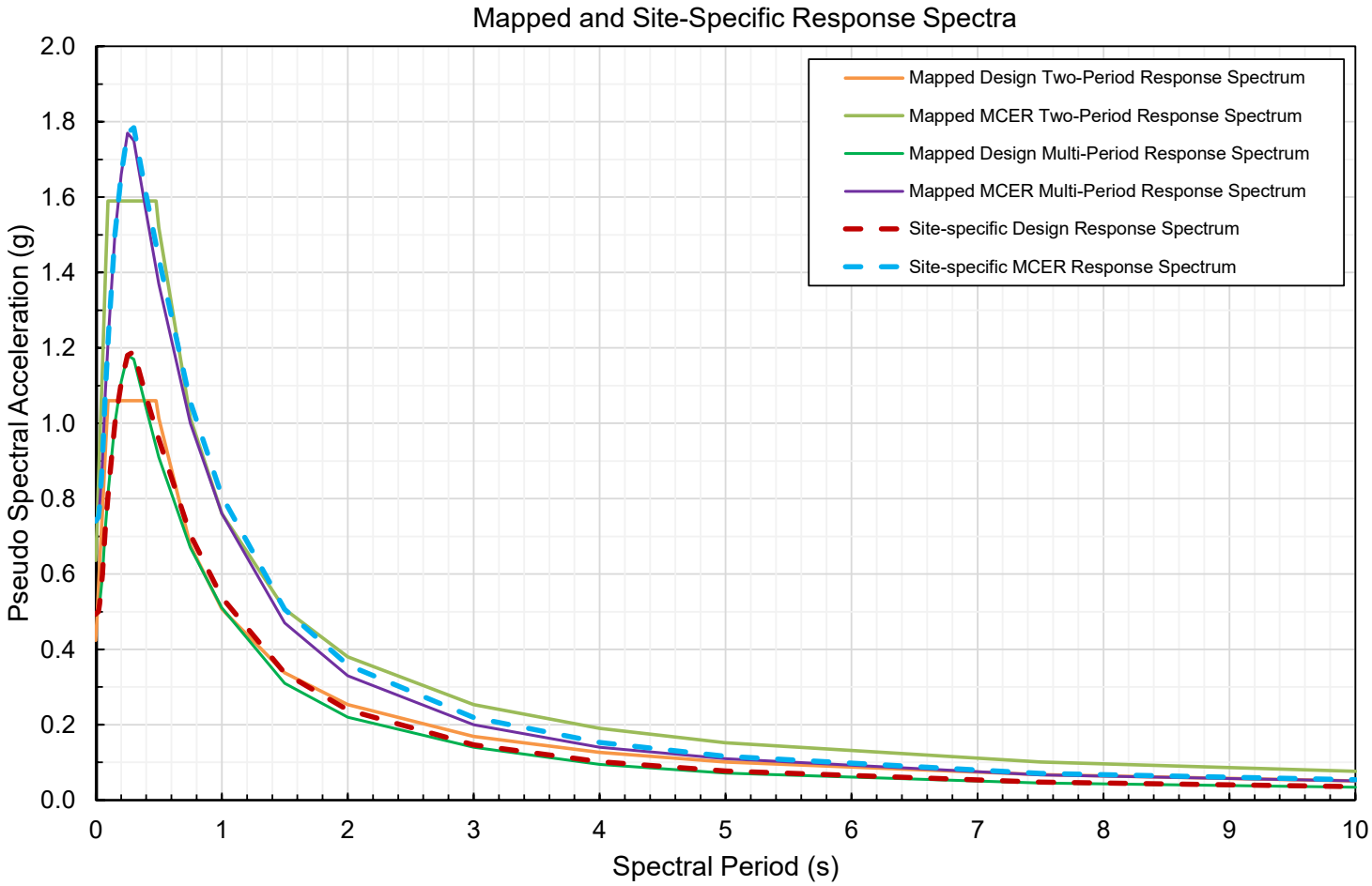
Quincy Courthouse 253, 287, 295, Lawrence Street, Quincy, CA			
By:	SD	Date:	October-25
Job Number:	18077.00	Figure:	1



ATLAS	Quincy Courthouse 253, 287, 295, Lawrence Street, Quincy, CA		
By:	SD	Date:	October-25
Job Number:	18077.00	Figure:	2

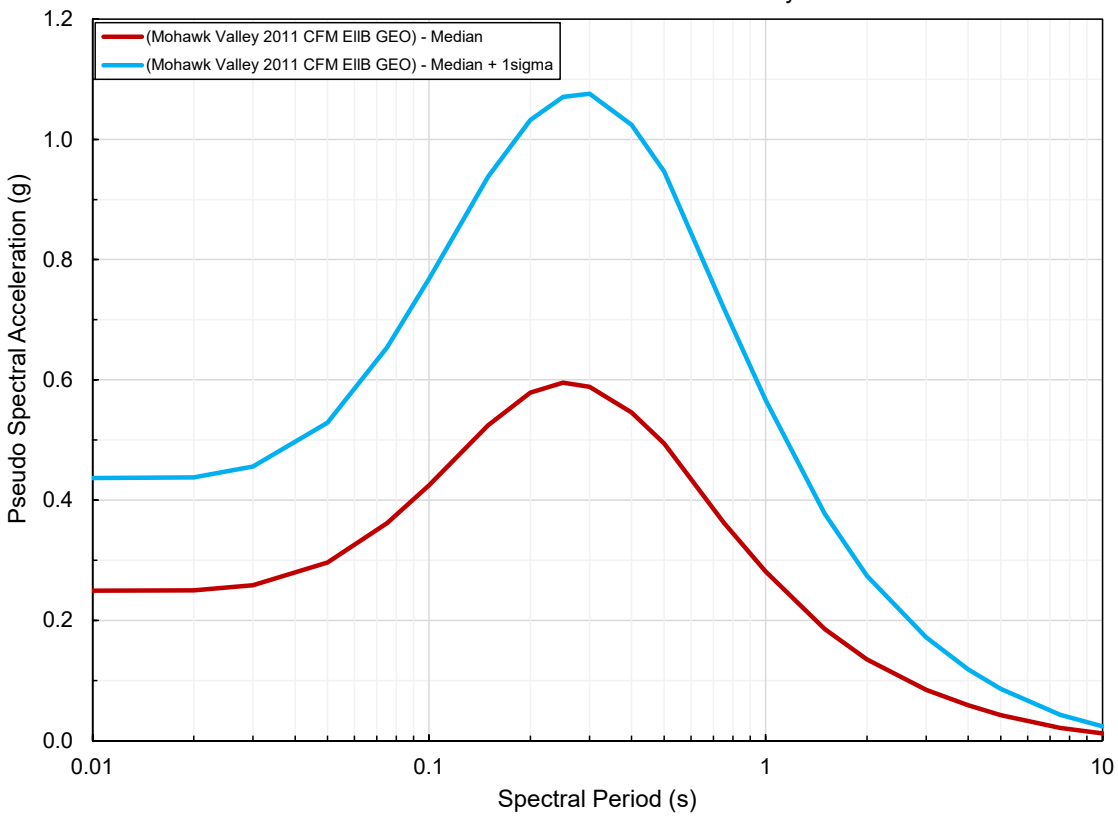


Quincy Courthouse 253, 287, 295, Lawrence Street, Quincy, CA			
By:	SD	Date:	October-25
Job Number:	18077.00	Figure:	3A



Quincy Courthouse 253, 287, 295, Lawrence Street, Quincy, CA			
By:	SD	Date:	October-25
Job Number:	18077.00	Figure:	3B

Deterministic Seismic Hazard Analysis



Period (sec)	Median	Deterministic 84th Percentile Spectral Accelaration (Median + 1std)
PGA	0.248	0.434
0.01	0.250	0.437
0.02	0.250	0.438
0.03	0.259	0.456
0.05	0.296	0.529
0.08	0.362	0.654
0.10	0.424	0.768
0.15	0.525	0.938
0.20	0.579	1.032
0.25	0.596	1.071
0.30	0.588	1.076
0.40	0.546	1.024
0.50	0.494	0.947
0.75	0.363	0.720
1.00	0.281	0.566
1.50	0.186	0.377
2.00	0.135	0.274
3.00	0.084	0.172
4.00	0.059	0.119
5.00	0.042	0.086
7.50	0.021	0.043
10.00	0.012	0.024

No	FaultName	Mag[1]	Dip °	Mech	R_{RUP} km	R_{JB} km	R_X km	Z_{TOR} km	RupWidth km	Z_{Hypo} km
1	Mohawk Valley 2011 CFM	7.13	90	SS	16.6	16.6	16.3	1.47	13.2	8.1

[1]Magnitude was taken from Building the Seismic Safety Council 2014 (BSSC2014) - UCERF3 Event Set.

ATLAS

Quincy Courthouse
253, 287, 295, Lawrence Street, Quincy, CA

By:	SD	Date:	October-25
Job Number:	18077.00	Figure:	4

APPENDIX V
LIQUEFACTION ANALYSIS RESULTS

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San Diego, CA, 92123
(619) 280-4321

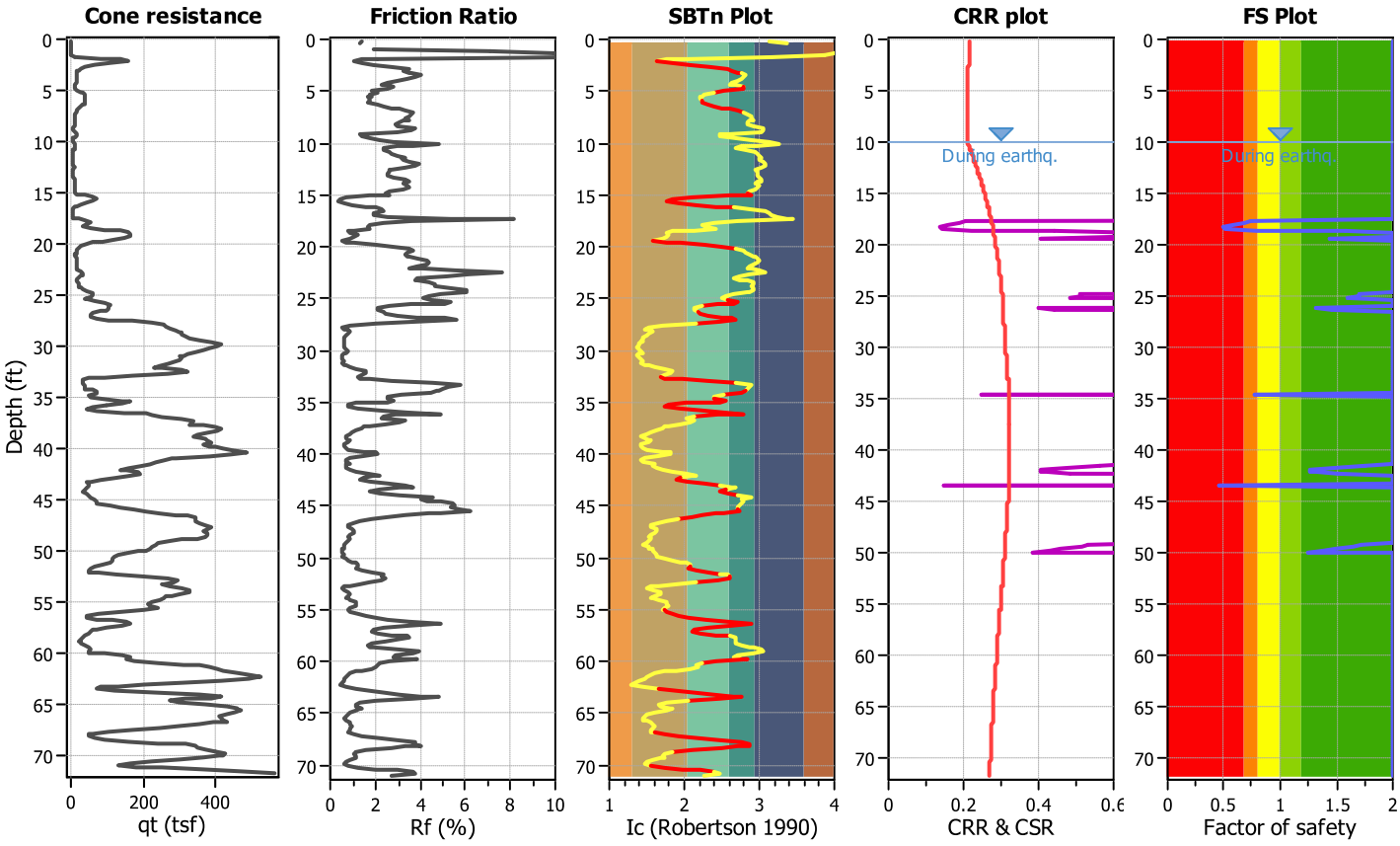
LIQUEFACTION ANALYSIS REPORT

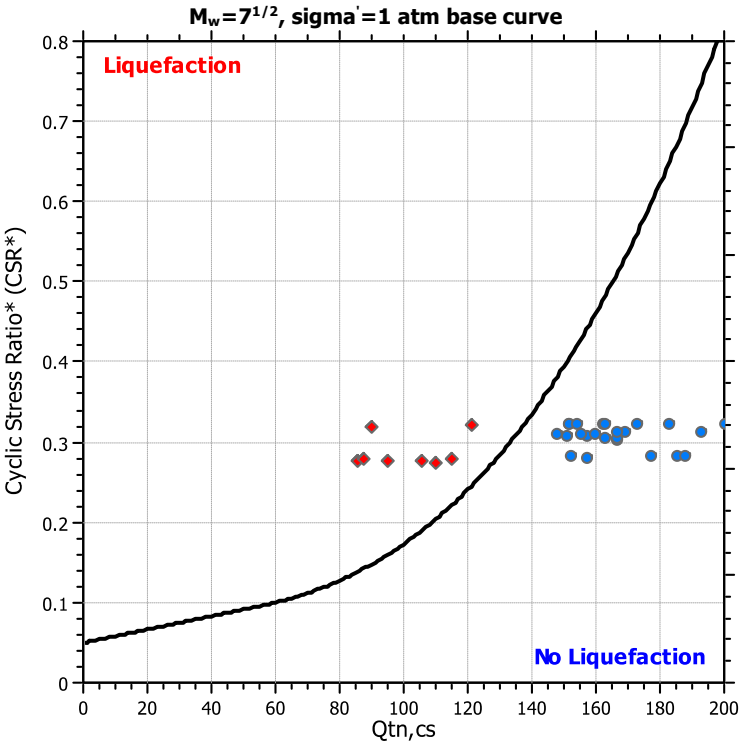
Project title : Quincy Courthouse **Location : Quincy, CA**

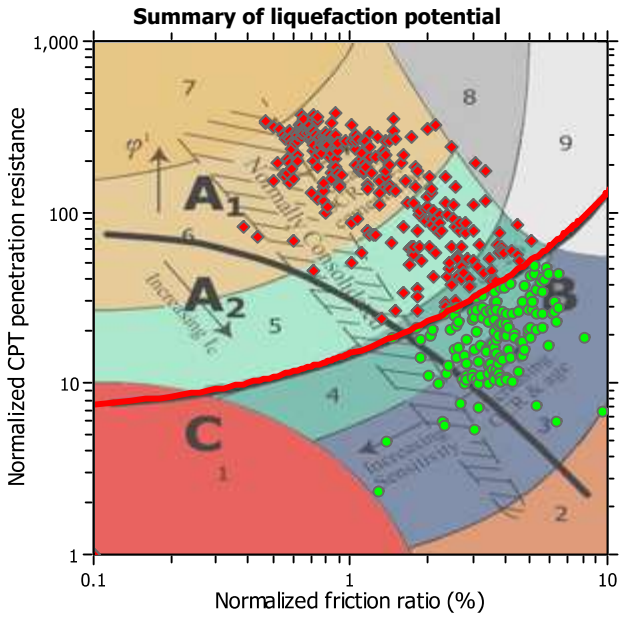
CPT file : CPT-01

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.50 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	10.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	5.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.56	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

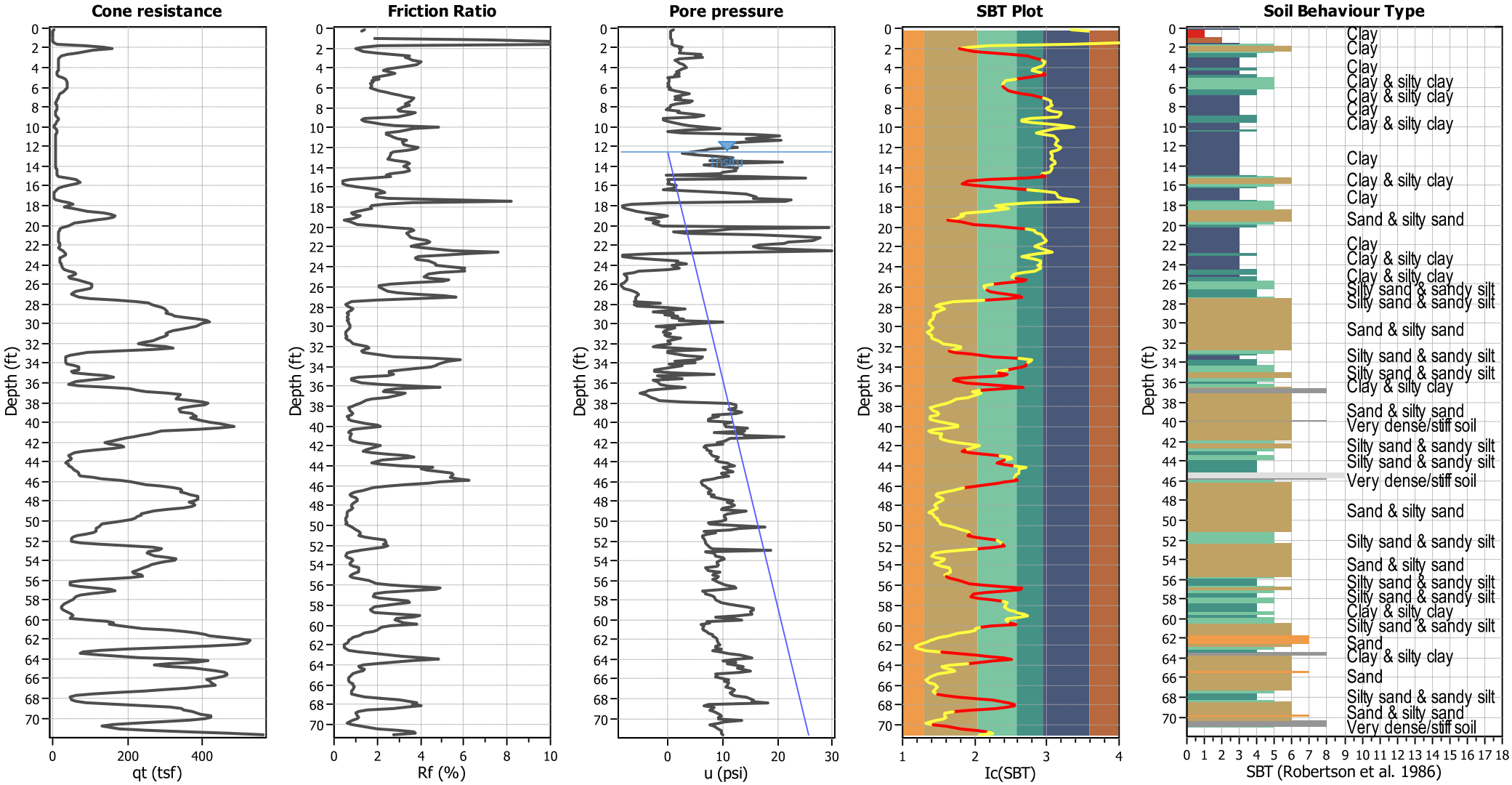






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



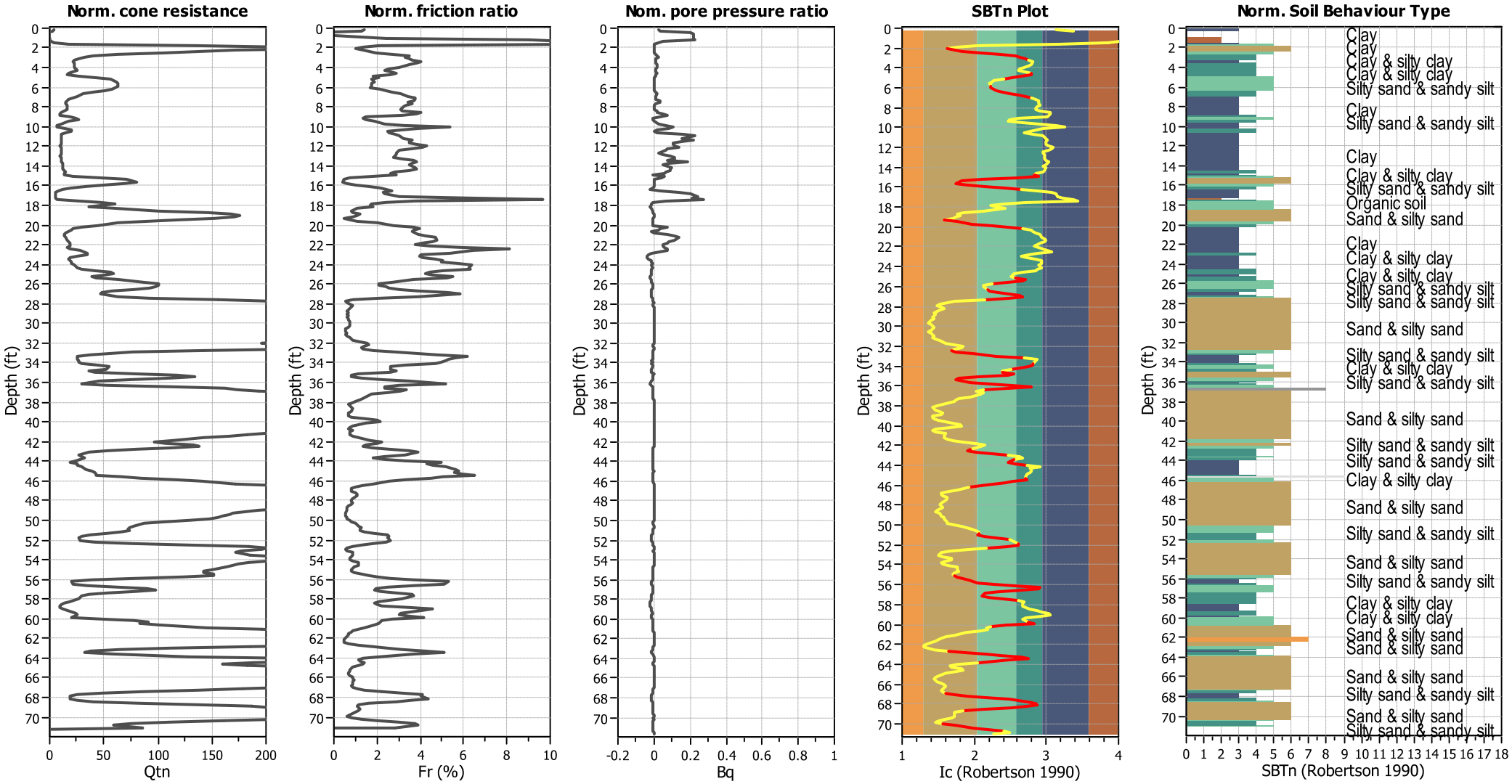
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



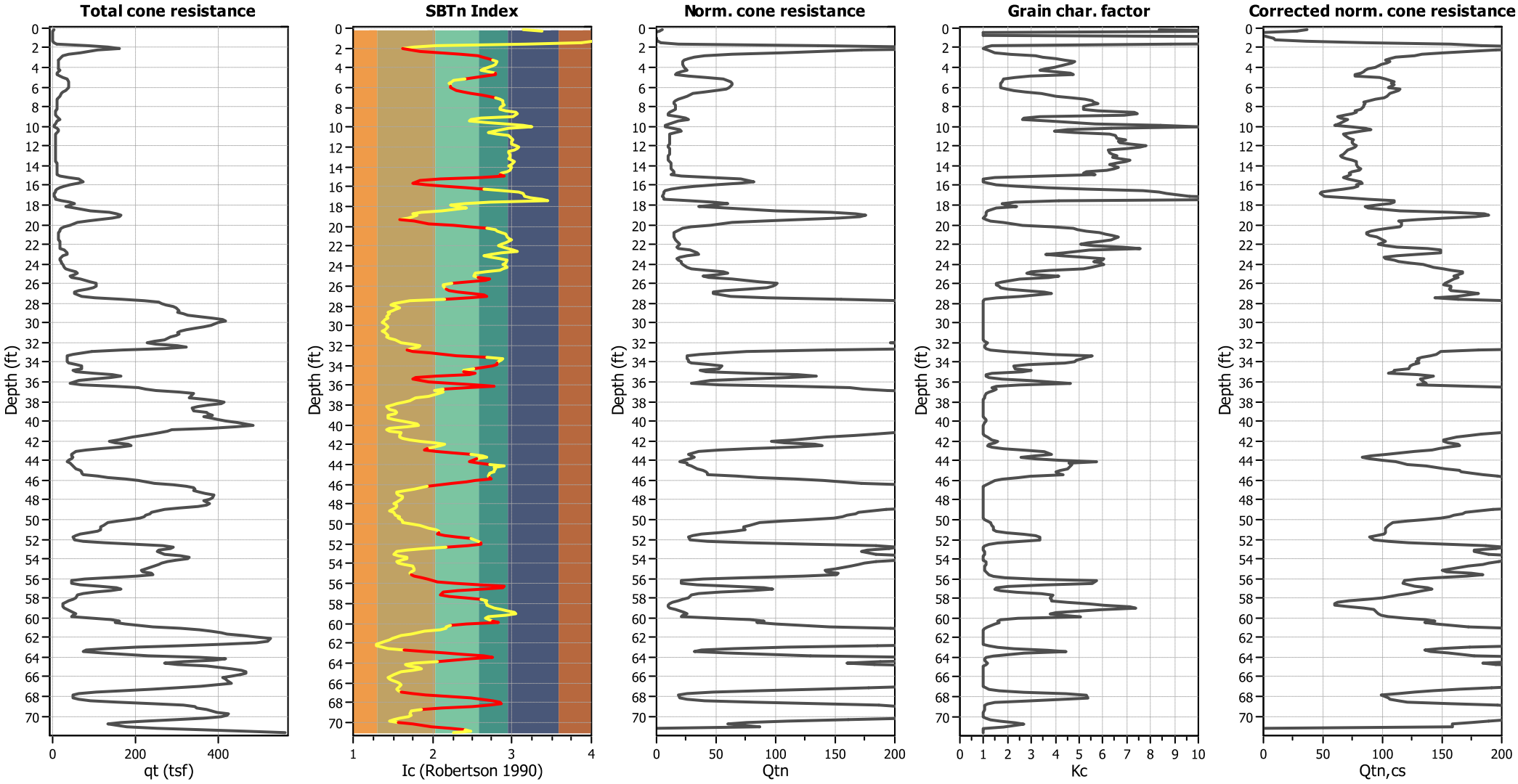
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

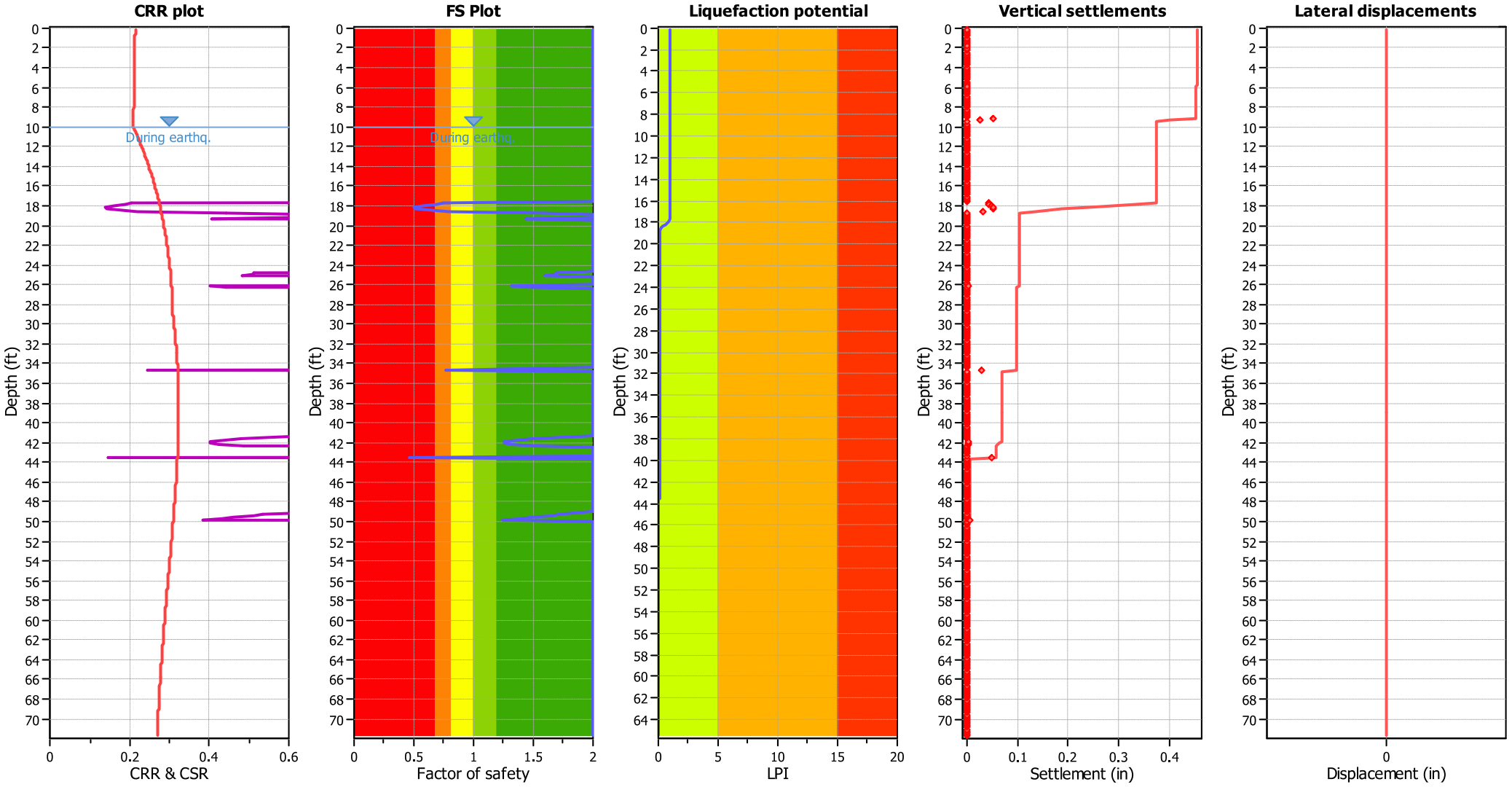
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

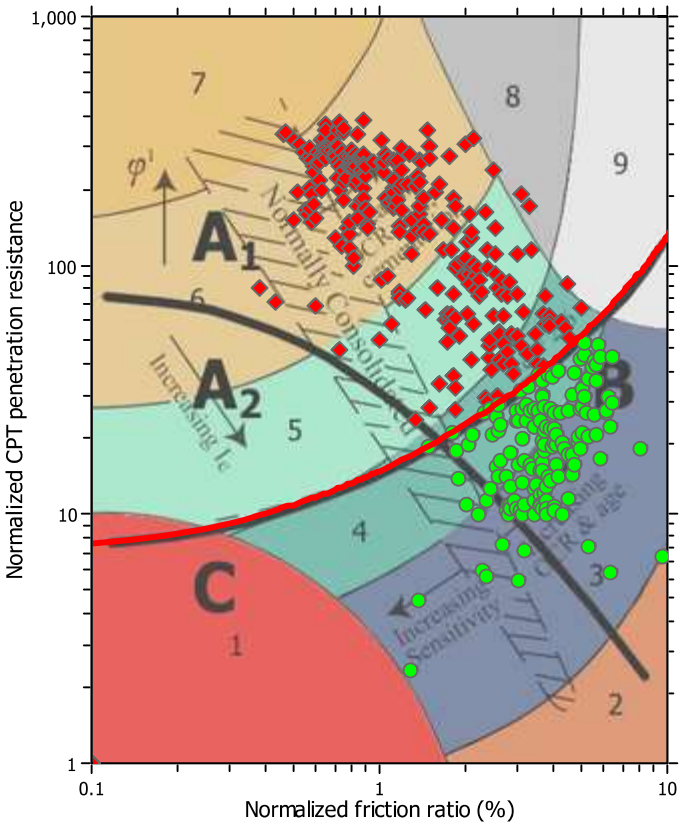
F.S. color scheme

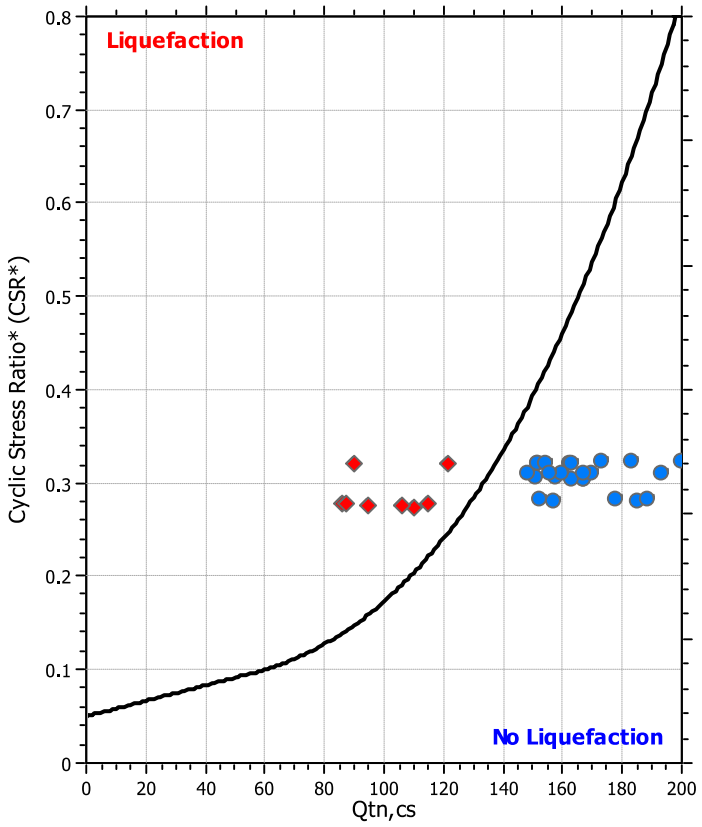
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

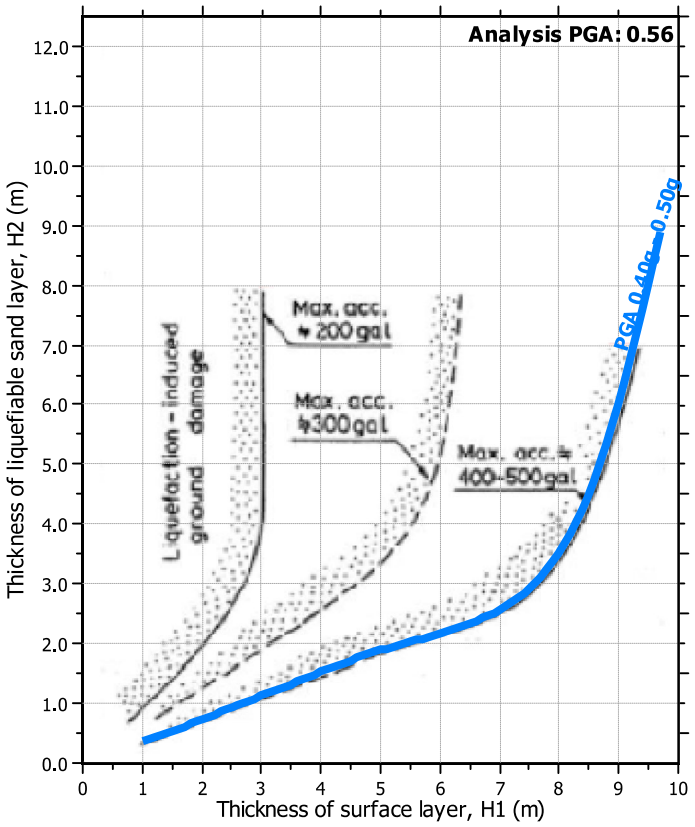
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



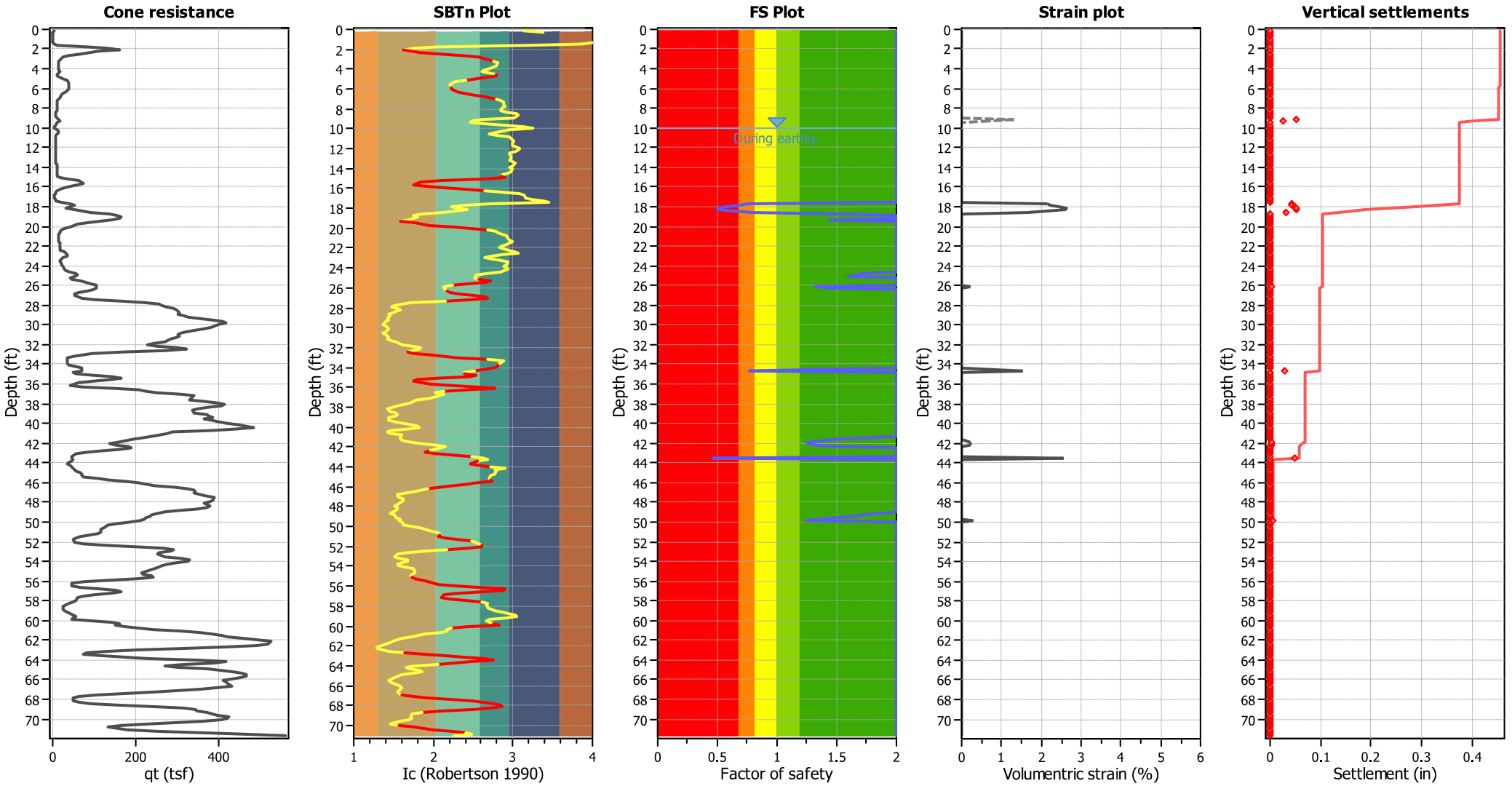




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement of dry sands ::

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
0.16	3.13	4.45	8.34	37.14	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.33	3.38	2.33	11.92	27.77	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.49	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.66	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.82	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.98	4.06	0.31	26.61	8.28	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.15	4.06	0.35	26.61	9.29	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.31	4.01	1.41	25.33	35.74	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.48	3.87	3.96	21.75	86.22	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.64	3.17	17.74	8.83	156.71	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.80	2.04	135.10	1.36	183.10	39	1002	0.21	0.004	0.00	2.41	0.00	0.000
1.97	1.77	216.83	1.08	234.94	45	1139	0.21	0.004	0.00	2.41	0.00	0.000
2.13	1.63	258.28	1.00	258.28	47	1136	0.21	0.004	0.00	2.41	0.00	0.000
2.30	1.83	172.06	1.13	194.80	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.46	2.09	104.98	1.44	151.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.62	2.35	62.82	2.12	133.32	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.79	2.57	40.22	3.14	126.34	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.95	2.62	32.23	3.46	111.58	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.12	2.70	26.36	4.03	106.17	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.28	2.76	23.32	4.42	103.04	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.44	2.81	21.92	4.84	106.01	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.61	2.79	22.29	4.67	104.08	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.77	2.76	22.38	4.44	99.39	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.94	2.70	23.44	3.99	93.53	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.10	2.64	24.63	3.57	88.05	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.27	2.61	25.31	3.37	85.31	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.43	2.70	21.28	3.98	84.61	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.59	2.78	17.65	4.65	82.11	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.76	2.79	16.13	4.74	76.47	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.92	2.53	26.27	2.93	76.97	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.09	2.40	42.04	2.33	98.06	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.25	2.26	56.32	1.82	102.75	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.41	2.24	62.05	1.77	110.10	25	594	0.21	0.042	0.03	2.41	0.01	0.001
5.58	2.21	63.40	1.70	107.91	24	586	0.21	0.046	0.04	2.41	0.02	0.001
5.74	2.22	63.56	1.72	109.33	25	593	0.21	0.047	0.04	2.41	0.02	0.001
5.91	2.22	62.46	1.73	107.87	25	585	0.21	0.051	0.04	2.41	0.02	0.001
6.07	2.23	60.39	1.74	104.85	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.23	2.30	58.29	1.96	114.21	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.40	2.39	50.59	2.25	113.97	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.56	2.49	40.52	2.72	110.30	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.73	2.62	30.81	3.44	105.95	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.89	2.70	25.71	4.02	103.33	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.05	2.79	21.57	4.72	101.82	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.22	2.85	17.86	5.26	93.98	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.38	2.88	16.02	5.55	88.94	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.55	2.89	15.06	5.58	84.02	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.71	2.91	14.81	5.78	85.69	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.87	2.87	15.63	5.42	84.68	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.04	2.84	16.36	5.16	84.40	0	0	0.21	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
8.20	2.84	15.69	5.17	81.12	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.37	2.91	13.26	5.82	77.15	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.53	3.05	10.61	7.34	77.95	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.69	3.06	9.97	7.44	74.18	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.86	3.01	9.90	6.91	68.38	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.02	2.61	18.46	3.36	62.10	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.19	2.48	24.06	2.69	64.68	17	313	0.21	2.368	2.97	2.41	1.31	0.051
9.35	2.47	26.89	2.62	70.48	18	344	0.21	1.376	1.57	2.41	0.69	0.027
9.51	2.67	17.91	3.81	68.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.68	2.90	11.29	5.66	63.86	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.84	3.14	7.05	8.41	59.28	0	0	0.21	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.08

Abbreviations

Q_{tn}: Equivalent clean sand normalized cone resistance
K_c: Fines correction factor
$Q_{tn,cs}$: Post-liquefaction volumentric strain
G_{max}: Small strain shear modulus
CSR: Soil cyclic stress ratio
γ: Cyclic shear strain
$e_{vol(15)}$: Volumetric strain after 15 cycles
N_c: Equivalent number of cycles
e_v: Volumetric strain
Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.01	73.34	2.00	0.00	1.00	0.00	10.17	85.71	2.00	0.00	1.00	0.00
10.33	90.08	2.00	0.00	1.00	0.00	10.50	81.50	2.00	0.00	1.00	0.00
10.66	73.97	2.00	0.00	1.00	0.00	10.83	67.63	2.00	0.00	1.00	0.00
10.99	68.67	2.00	0.00	1.00	0.00	11.15	71.46	2.00	0.00	1.00	0.00
11.32	75.08	2.00	0.00	1.00	0.00	11.48	74.61	2.00	0.00	1.00	0.00
11.65	74.99	2.00	0.00	1.00	0.00	11.81	75.90	2.00	0.00	1.00	0.00
11.98	77.80	2.00	0.00	1.00	0.00	12.14	77.17	2.00	0.00	1.00	0.00
12.30	74.75	2.00	0.00	1.00	0.00	12.47	70.46	2.00	0.00	1.00	0.00
12.63	67.90	2.00	0.00	1.00	0.00	12.80	67.09	2.00	0.00	1.00	0.00
12.96	65.14	2.00	0.00	1.00	0.00	13.12	65.67	2.00	0.00	1.00	0.00
13.29	69.05	2.00	0.00	1.00	0.00	13.45	74.14	2.00	0.00	1.00	0.00
13.62	77.87	2.00	0.00	1.00	0.00	13.78	77.87	2.00	0.00	1.00	0.00
13.94	78.33	2.00	0.00	1.00	0.00	14.11	79.39	2.00	0.00	1.00	0.00
14.27	81.97	2.00	0.00	1.00	0.00	14.44	80.00	2.00	0.00	1.00	0.00
14.60	74.73	2.00	0.00	1.00	0.00	14.76	72.51	2.00	0.00	1.00	0.00
14.93	72.65	2.00	0.00	1.00	0.00	15.09	70.75	2.00	0.00	1.00	0.00
15.26	67.16	2.00	0.00	1.00	0.00	15.42	71.16	2.00	0.00	1.00	0.00
15.58	81.17	2.00	0.00	1.00	0.00	15.75	82.84	2.00	0.00	1.00	0.00
15.91	77.80	2.00	0.00	1.00	0.00	16.08	79.30	2.00	0.00	1.00	0.00
16.24	75.42	2.00	0.00	1.00	0.00	16.40	67.25	2.00	0.00	1.00	0.00
16.57	57.01	2.00	0.00	1.00	0.00	16.73	48.78	2.00	0.00	1.00	0.00
16.90	48.15	2.00	0.00	1.00	0.00	17.06	51.69	2.00	0.00	1.00	0.00
17.22	69.78	2.00	0.00	1.00	0.00	17.39	87.46	2.00	0.00	1.00	0.00
17.55	110.36	2.00	0.00	1.00	0.00	17.72	110.26	0.75	2.14	1.00	0.04

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
17.88	105.73	0.69	2.23	1.00	0.04	18.04	94.96	0.58	2.44	1.00	0.05
18.21	85.71	0.50	2.65	1.00	0.05	18.37	87.36	0.51	2.61	1.00	0.05
18.54	114.71	0.79	1.66	1.00	0.03	18.70	157.31	1.58	0.00	1.00	0.00
18.86	185.36	2.00	0.00	1.00	0.00	19.03	188.43	2.00	0.00	1.00	0.00
19.19	177.57	2.00	0.00	1.00	0.00	19.36	152.19	1.44	0.00	1.00	0.00
19.52	129.74	2.00	0.00	1.00	0.00	19.69	113.16	2.00	0.00	1.00	0.00
19.85	115.83	2.00	0.00	1.00	0.00	20.01	115.86	2.00	0.00	1.00	0.00
20.18	114.66	2.00	0.00	1.00	0.00	20.34	104.50	2.00	0.00	1.00	0.00
20.51	96.57	2.00	0.00	1.00	0.00	20.67	90.51	2.00	0.00	1.00	0.00
20.83	86.78	2.00	0.00	1.00	0.00	21.00	86.15	2.00	0.00	1.00	0.00
21.16	89.61	2.00	0.00	1.00	0.00	21.33	94.77	2.00	0.00	1.00	0.00
21.49	99.57	2.00	0.00	1.00	0.00	21.65	101.86	2.00	0.00	1.00	0.00
21.82	99.97	2.00	0.00	1.00	0.00	21.98	96.30	2.00	0.00	1.00	0.00
22.15	102.09	2.00	0.00	1.00	0.00	22.31	112.75	2.00	0.00	1.00	0.00
22.47	137.39	2.00	0.00	1.00	0.00	22.64	149.22	2.00	0.00	1.00	0.00
22.80	149.23	2.00	0.00	1.00	0.00	22.97	128.91	2.00	0.00	1.00	0.00
23.13	112.49	2.00	0.00	1.00	0.00	23.29	101.40	2.00	0.00	1.00	0.00
23.46	102.80	2.00	0.00	1.00	0.00	23.62	109.18	2.00	0.00	1.00	0.00
23.79	113.38	2.00	0.00	1.00	0.00	23.95	122.72	2.00	0.00	1.00	0.00
24.11	134.74	2.00	0.00	1.00	0.00	24.28	142.20	2.00	0.00	1.00	0.00
24.44	151.76	2.00	0.00	1.00	0.00	24.61	157.05	2.00	0.00	1.00	0.00
24.77	166.92	1.69	0.00	1.00	0.00	24.93	167.08	1.70	0.00	1.00	0.00
25.10	163.03	1.59	0.00	1.00	0.00	25.26	160.04	2.00	0.00	1.00	0.00
25.43	163.35	2.00	0.00	1.00	0.00	25.59	159.63	2.00	0.00	1.00	0.00
25.75	155.45	2.00	0.00	1.00	0.00	25.92	152.45	2.00	0.00	1.00	0.00
26.08	151.28	1.32	0.22	1.00	0.00	26.25	157.57	1.45	0.00	1.00	0.00
26.41	156.89	2.00	0.00	1.00	0.00	26.57	156.27	2.00	0.00	1.00	0.00
26.74	156.75	2.00	0.00	1.00	0.00	26.90	170.91	2.00	0.00	1.00	0.00
27.07	180.68	2.00	0.00	1.00	0.00	27.23	162.11	2.00	0.00	1.00	0.00
27.40	143.37	2.00	0.00	1.00	0.00	27.56	162.95	2.00	0.00	1.00	0.00
27.72	204.31	2.00	0.00	1.00	0.00	27.89	236.91	2.00	0.00	1.00	0.00
28.05	242.44	2.00	0.00	1.00	0.00	28.22	251.98	2.00	0.00	1.00	0.00
28.38	266.36	2.00	0.00	1.00	0.00	28.54	272.52	2.00	0.00	1.00	0.00
28.71	279.83	2.00	0.00	1.00	0.00	28.87	276.07	2.00	0.00	1.00	0.00
29.04	287.27	2.00	0.00	1.00	0.00	29.20	294.28	2.00	0.00	1.00	0.00
29.36	319.50	2.00	0.00	1.00	0.00	29.53	348.91	2.00	0.00	1.00	0.00
29.69	370.32	2.00	0.00	1.00	0.00	29.86	374.09	2.00	0.00	1.00	0.00
30.02	358.63	2.00	0.00	1.00	0.00	30.18	342.75	2.00	0.00	1.00	0.00
30.35	324.96	2.00	0.00	1.00	0.00	30.51	305.28	2.00	0.00	1.00	0.00
30.68	286.04	2.00	0.00	1.00	0.00	30.84	273.70	2.00	0.00	1.00	0.00
31.00	265.25	2.00	0.00	1.00	0.00	31.17	269.16	2.00	0.00	1.00	0.00
31.33	261.04	2.00	0.00	1.00	0.00	31.50	249.42	2.00	0.00	1.00	0.00
31.66	234.59	2.00	0.00	1.00	0.00	31.82	224.16	2.00	0.00	1.00	0.00
31.99	223.31	2.00	0.00	1.00	0.00	32.15	241.11	2.00	0.00	1.00	0.00
32.32	275.07	2.00	0.00	1.00	0.00	32.48	283.79	2.00	0.00	1.00	0.00
32.64	246.03	2.00	0.00	1.00	0.00	32.81	180.82	2.00	0.00	1.00	0.00
32.97	148.85	2.00	0.00	1.00	0.00	33.14	144.77	2.00	0.00	1.00	0.00
33.30	139.99	2.00	0.00	1.00	0.00	33.46	132.87	2.00	0.00	1.00	0.00
33.63	129.66	2.00	0.00	1.00	0.00	33.79	130.57	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
33.96	127.76	2.00	0.00	1.00	0.00	34.12	130.47	2.00	0.00	1.00	0.00
34.28	126.22	2.00	0.00	1.00	0.00	34.45	122.81	2.00	0.00	1.00	0.00
34.61	121.36	0.77	1.53	1.00	0.03	34.78	109.65	2.00	0.00	1.00	0.00
34.94	109.62	2.00	0.00	1.00	0.00	35.10	104.61	2.00	0.00	1.00	0.00
35.27	129.69	2.00	0.00	1.00	0.00	35.43	143.25	2.00	0.00	1.00	0.00
35.60	137.81	2.00	0.00	1.00	0.00	35.76	132.25	2.00	0.00	1.00	0.00
35.93	133.19	2.00	0.00	1.00	0.00	36.09	136.72	2.00	0.00	1.00	0.00
36.25	129.22	2.00	0.00	1.00	0.00	36.42	172.56	2.00	0.00	1.00	0.00
36.58	216.94	2.00	0.00	1.00	0.00	36.75	262.96	2.00	0.00	1.00	0.00
36.91	274.81	2.00	0.00	1.00	0.00	37.07	297.64	2.00	0.00	1.00	0.00
37.24	298.99	2.00	0.00	1.00	0.00	37.40	285.67	2.00	0.00	1.00	0.00
37.57	276.71	2.00	0.00	1.00	0.00	37.73	294.30	2.00	0.00	1.00	0.00
37.89	320.76	2.00	0.00	1.00	0.00	38.06	333.25	2.00	0.00	1.00	0.00
38.22	326.26	2.00	0.00	1.00	0.00	38.39	301.12	2.00	0.00	1.00	0.00
38.55	280.44	2.00	0.00	1.00	0.00	38.71	269.92	2.00	0.00	1.00	0.00
38.88	271.41	2.00	0.00	1.00	0.00	39.04	296.43	2.00	0.00	1.00	0.00
39.21	299.55	2.00	0.00	1.00	0.00	39.37	305.18	2.00	0.00	1.00	0.00
39.53	289.86	2.00	0.00	1.00	0.00	39.70	311.87	2.00	0.00	1.00	0.00
39.86	343.45	2.00	0.00	1.00	0.00	40.03	361.88	2.00	0.00	1.00	0.00
40.19	354.64	2.00	0.00	1.00	0.00	40.35	380.87	2.00	0.00	1.00	0.00
40.52	346.40	2.00	0.00	1.00	0.00	40.68	298.89	2.00	0.00	1.00	0.00
40.85	225.09	2.00	0.00	1.00	0.00	41.01	214.32	2.00	0.00	1.00	0.00
41.17	200.32	2.00	0.00	1.00	0.00	41.34	182.99	2.00	0.00	1.00	0.00
41.50	173.40	1.75	0.00	1.00	0.00	41.67	162.47	1.49	0.00	1.00	0.00
41.83	151.57	1.25	0.22	1.00	0.00	41.99	151.57	1.26	0.22	1.00	0.00
42.16	154.45	1.31	0.21	1.00	0.00	42.32	163.36	1.51	0.00	1.00	0.00
42.49	164.59	2.00	0.00	1.00	0.00	42.65	154.51	2.00	0.00	1.00	0.00
42.81	147.27	2.00	0.00	1.00	0.00	42.98	141.20	2.00	0.00	1.00	0.00
43.14	126.59	2.00	0.00	1.00	0.00	43.31	103.92	2.00	0.00	1.00	0.00
43.47	90.14	0.46	2.54	1.00	0.05	43.64	82.68	2.00	0.00	1.00	0.00
43.80	89.37	2.00	0.00	1.00	0.00	43.96	98.46	2.00	0.00	1.00	0.00
44.13	110.88	2.00	0.00	1.00	0.00	44.29	116.08	2.00	0.00	1.00	0.00
44.46	120.25	2.00	0.00	1.00	0.00	44.62	136.88	2.00	0.00	1.00	0.00
44.78	152.68	2.00	0.00	1.00	0.00	44.95	164.73	2.00	0.00	1.00	0.00
45.11	165.99	2.00	0.00	1.00	0.00	45.28	174.37	2.00	0.00	1.00	0.00
45.44	184.28	2.00	0.00	1.00	0.00	45.60	196.46	2.00	0.00	1.00	0.00
45.77	204.85	2.00	0.00	1.00	0.00	45.93	206.00	2.00	0.00	1.00	0.00
46.10	203.27	2.00	0.00	1.00	0.00	46.26	209.43	2.00	0.00	1.00	0.00
46.42	225.98	2.00	0.00	1.00	0.00	46.59	236.38	2.00	0.00	1.00	0.00
46.75	250.52	2.00	0.00	1.00	0.00	46.92	252.13	2.00	0.00	1.00	0.00
47.08	249.79	2.00	0.00	1.00	0.00	47.24	258.42	2.00	0.00	1.00	0.00
47.41	268.35	2.00	0.00	1.00	0.00	47.57	281.97	2.00	0.00	1.00	0.00
47.74	280.21	2.00	0.00	1.00	0.00	47.90	273.81	2.00	0.00	1.00	0.00
48.06	263.29	2.00	0.00	1.00	0.00	48.23	269.85	2.00	0.00	1.00	0.00
48.39	272.50	2.00	0.00	1.00	0.00	48.56	268.48	2.00	0.00	1.00	0.00
48.72	251.59	2.00	0.00	1.00	0.00	48.88	218.31	2.00	0.00	1.00	0.00
49.05	193.19	2.00	0.00	1.00	0.00	49.21	169.47	1.71	0.00	1.00	0.00
49.38	167.02	1.65	0.00	1.00	0.00	49.54	159.91	1.48	0.00	1.00	0.00
49.70	155.58	1.39	0.00	1.00	0.00	49.87	148.32	1.24	0.31	1.00	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 0.37

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

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9085 Aero Drive, Suite B
San Diego, CA, 92123
(619) 280-4321

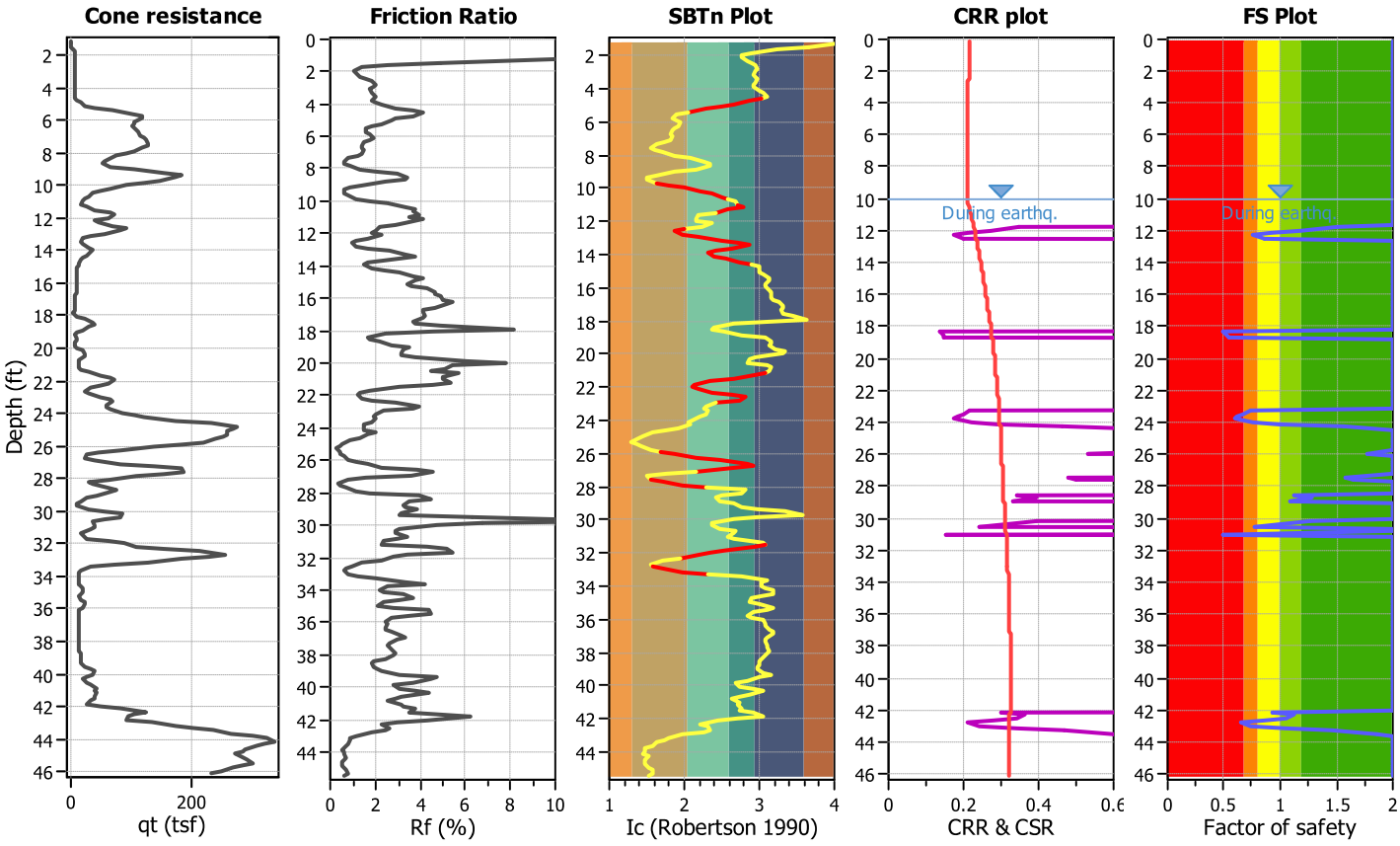
LIQUEFACTION ANALYSIS REPORT

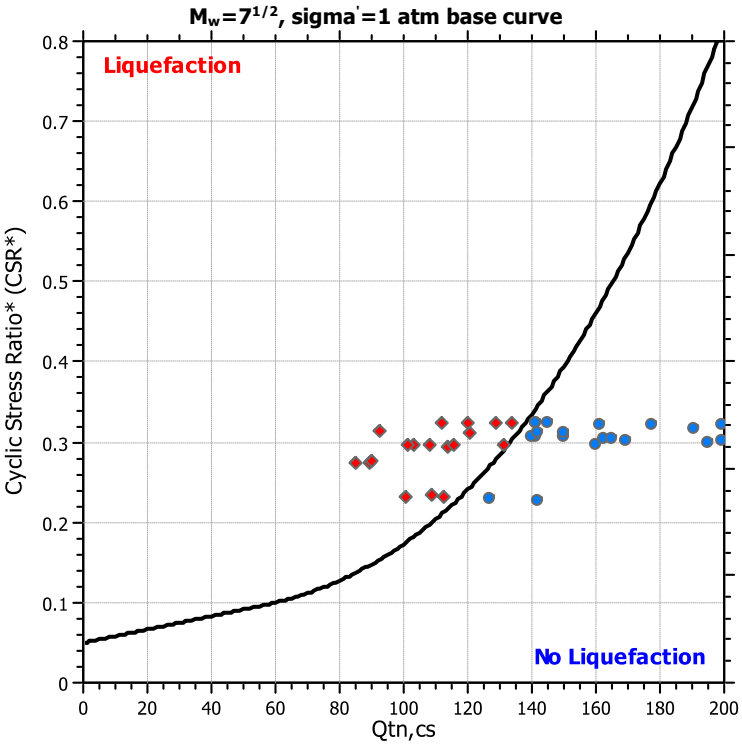
Project title : Quincy Courthouse **Location : Quincy, CA**

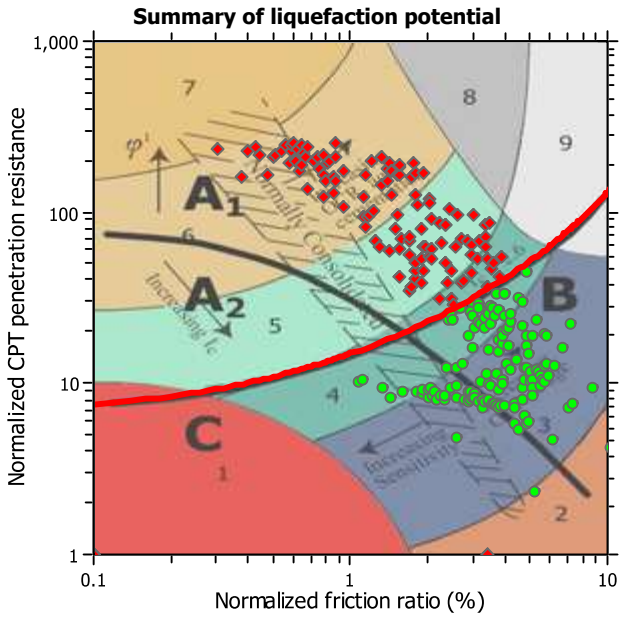
CPT file : CPT-02

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	15.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	10.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	5.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.56	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

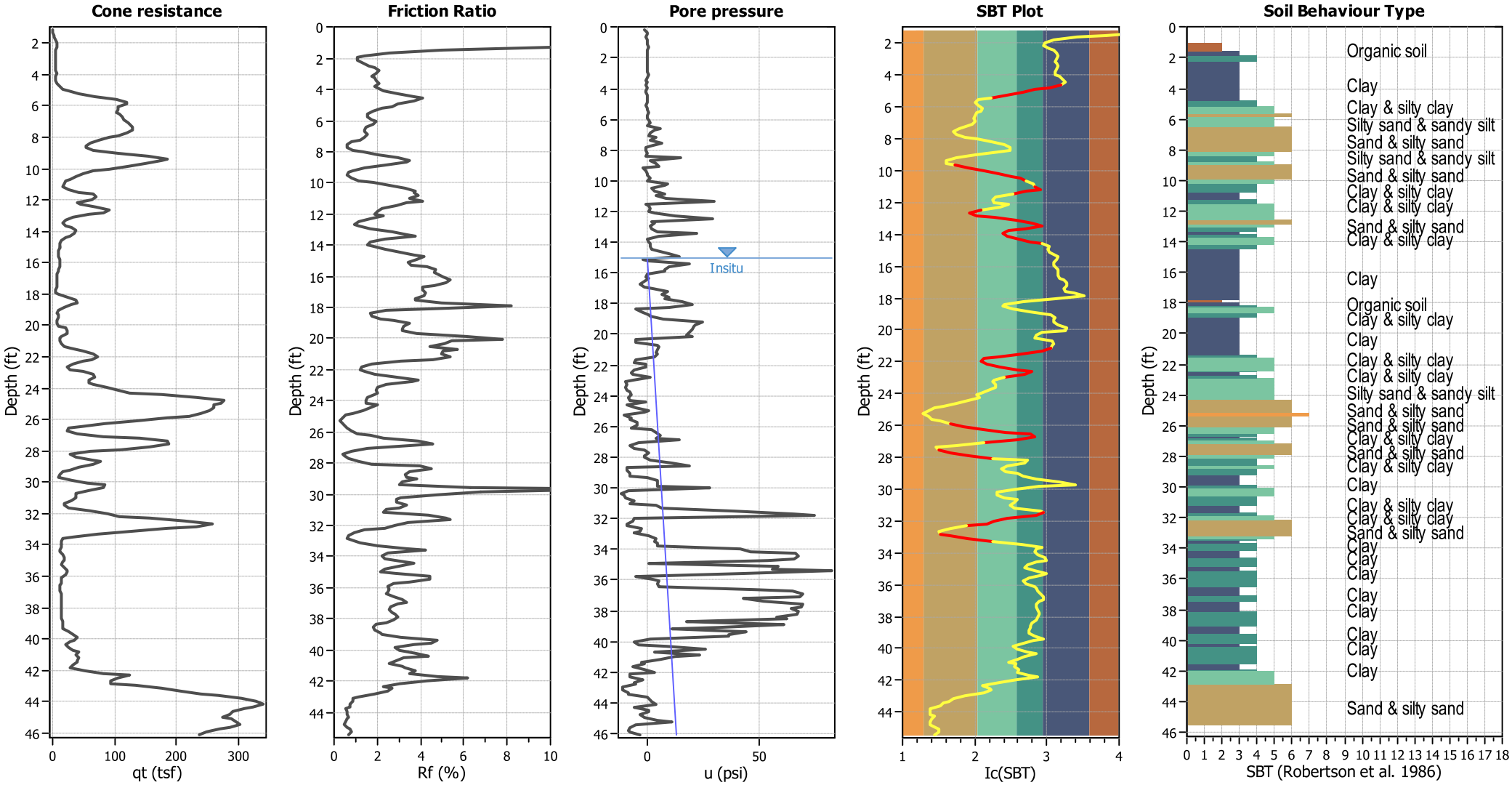






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



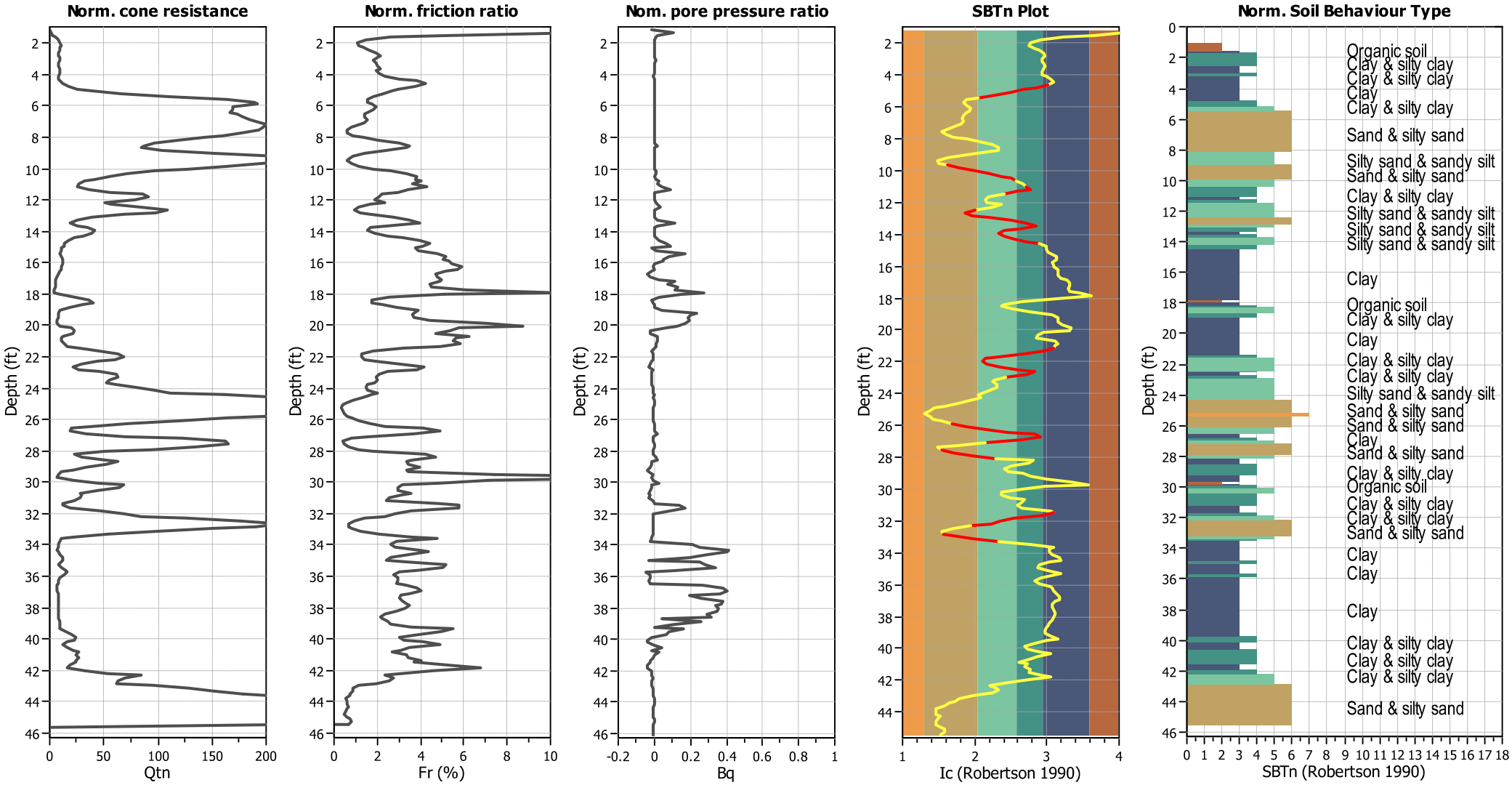
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	15.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



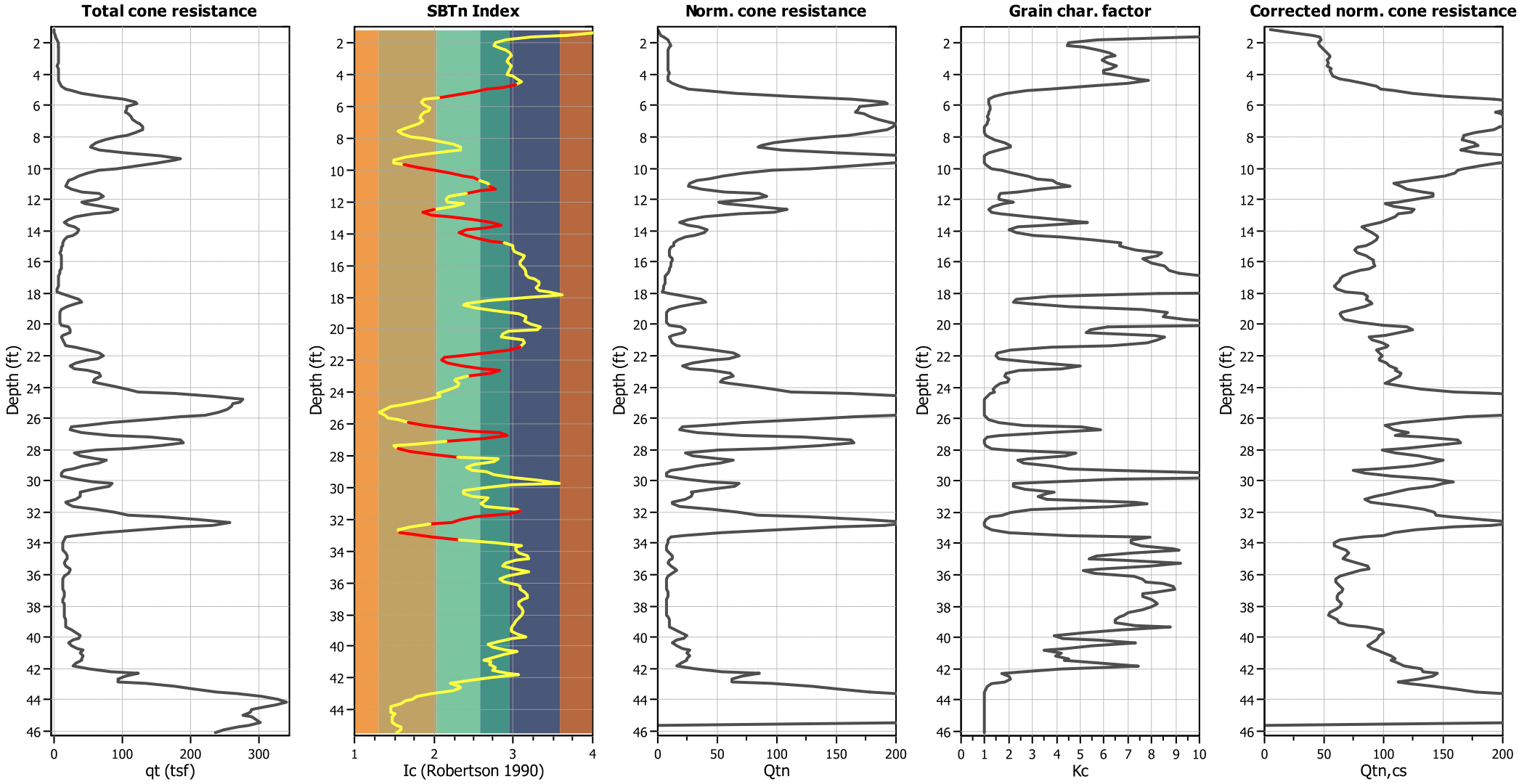
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	15.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

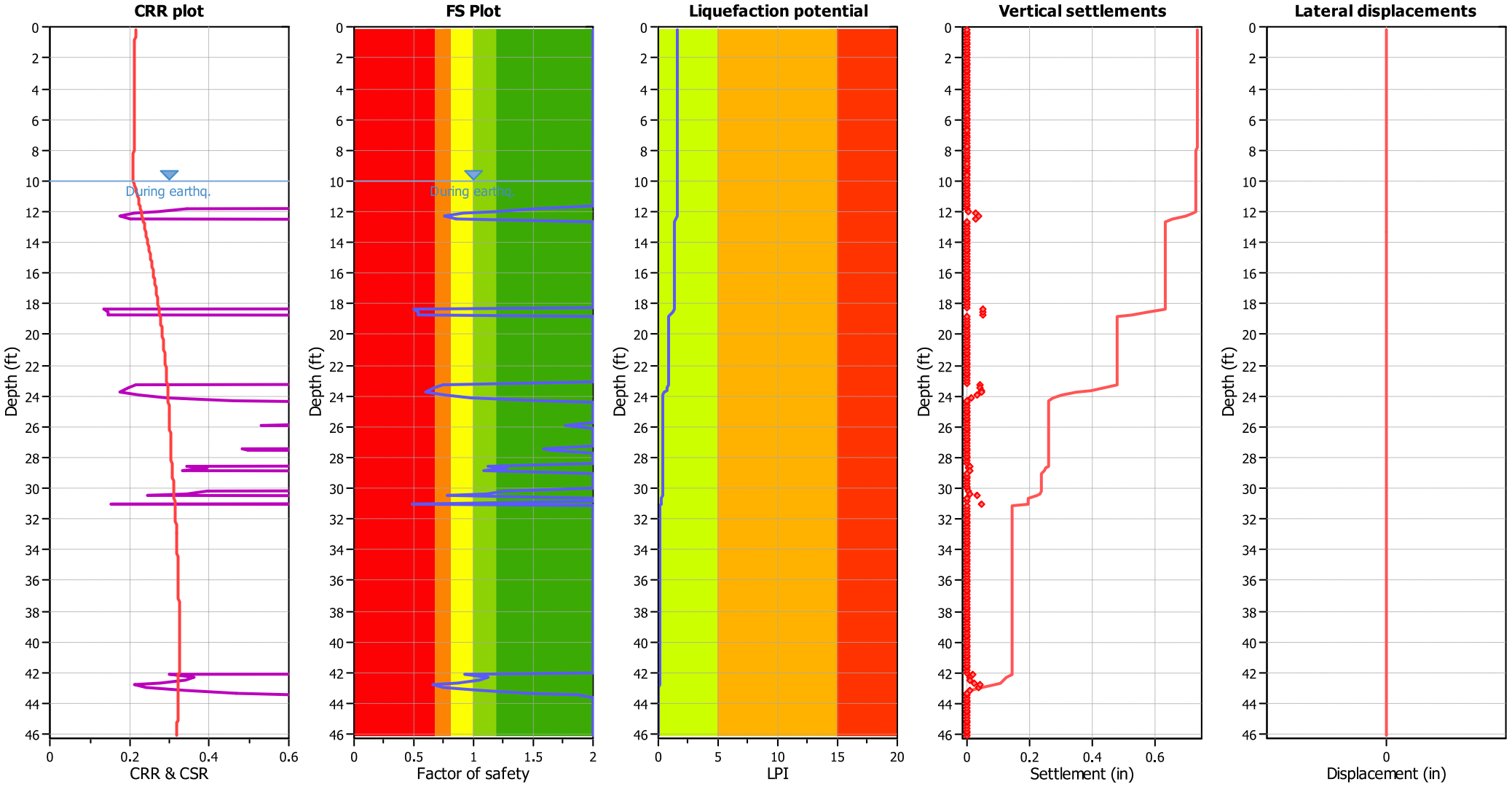
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	15.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	15.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

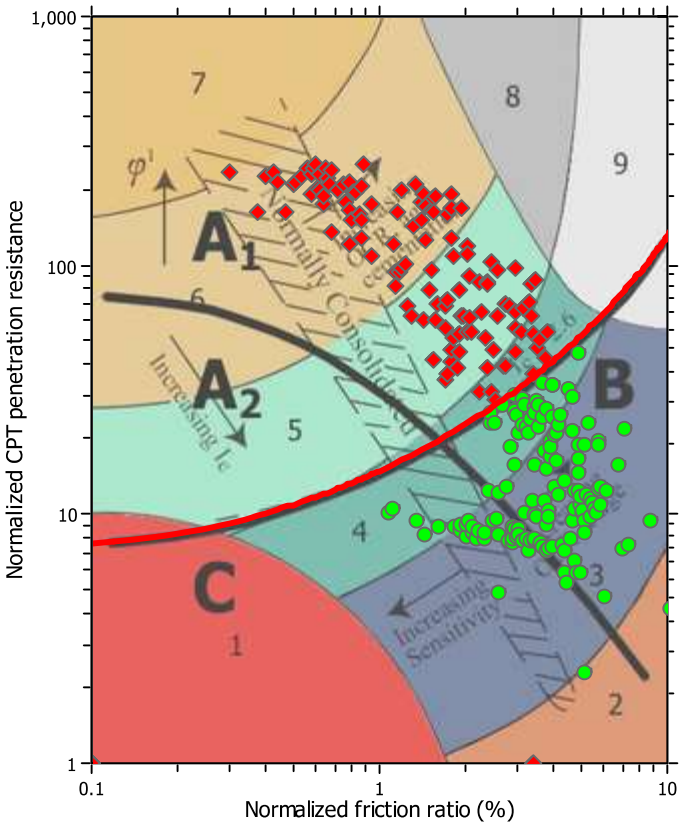
F.S. color scheme

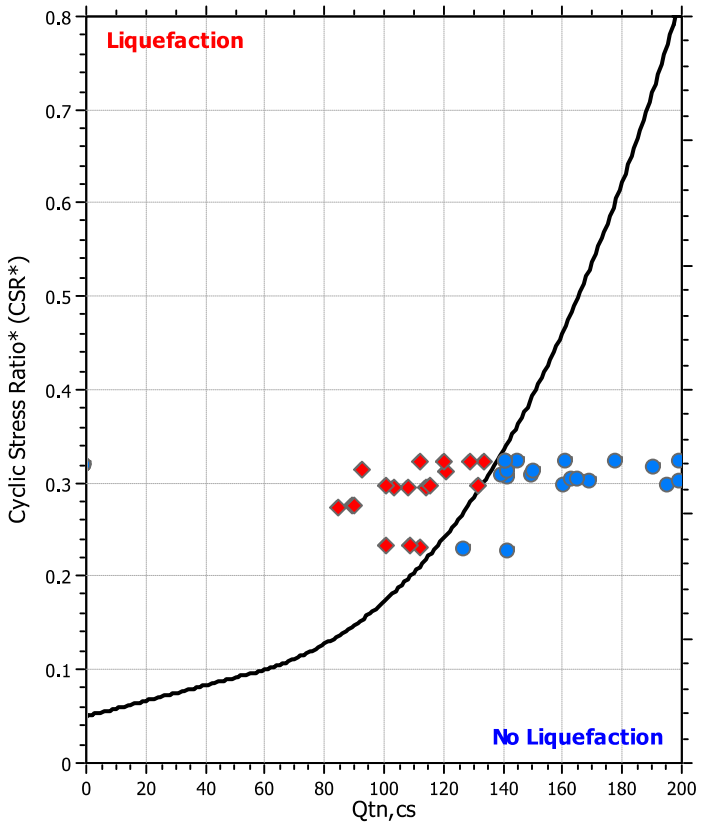
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

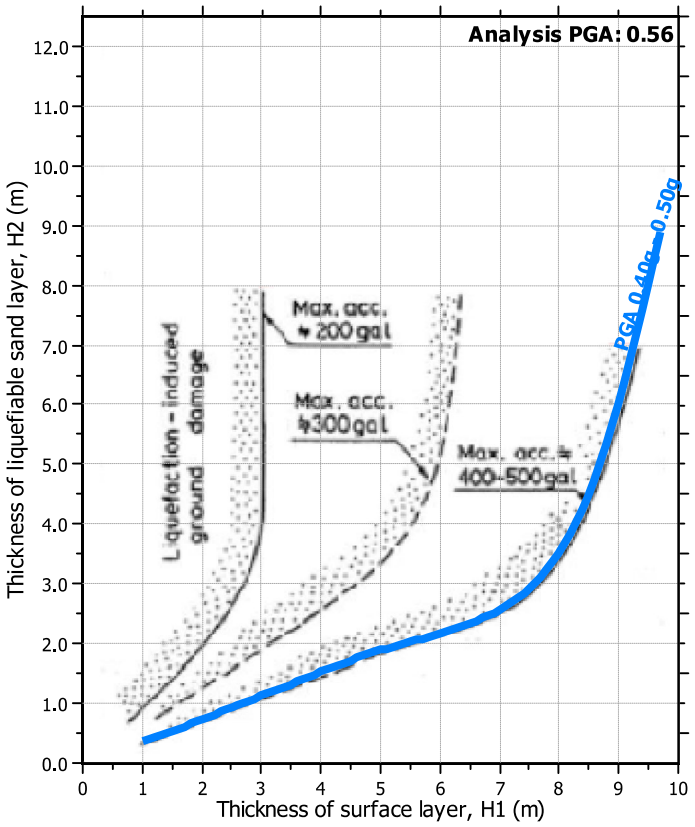
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



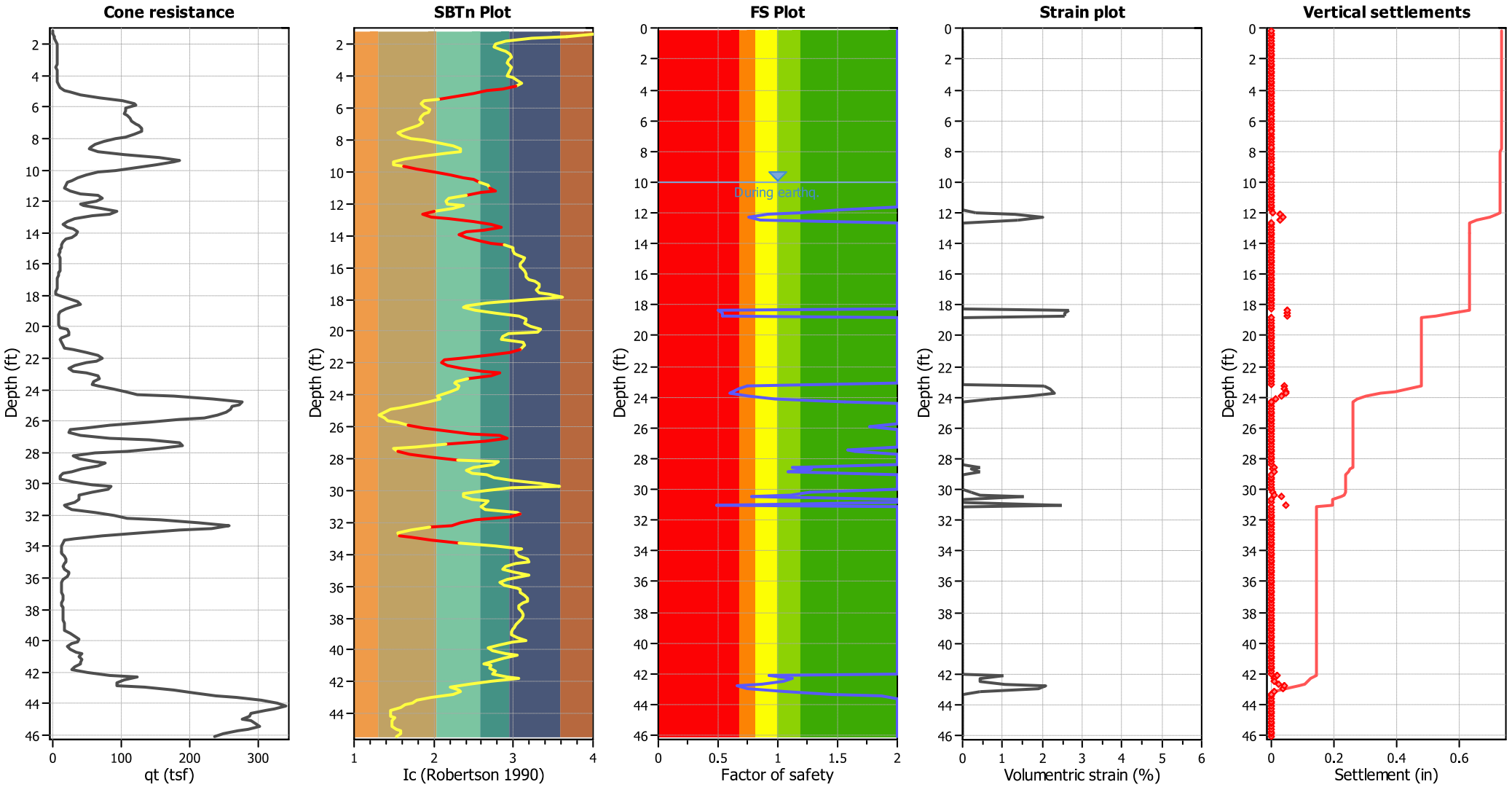




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	15.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement of dry sands ::

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
0.16	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.33	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.49	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.66	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.82	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.98	-1.00	-1.00	1.00	-1.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.15	4.06	0.17	26.61	4.61	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.31	4.06	0.83	26.61	22.17	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.48	3.66	2.30	17.28	39.69	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.64	3.23	4.78	9.73	46.53	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.80	2.90	8.20	5.74	47.10	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.97	2.77	10.01	4.54	45.44	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.13	2.76	10.46	4.45	46.50	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.30	2.84	9.31	5.15	47.94	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.46	2.90	8.82	5.71	50.37	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.62	2.95	8.48	6.24	52.93	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.79	2.98	8.43	6.49	54.70	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.95	2.94	9.00	6.12	55.07	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.12	2.92	8.90	5.94	52.85	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.28	2.95	8.63	6.16	53.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.44	2.98	8.09	6.53	52.86	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.61	2.96	8.90	6.28	55.93	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.77	2.93	9.05	6.00	54.32	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.94	2.93	9.40	5.99	56.32	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.10	3.00	8.41	6.76	56.86	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.27	3.05	8.61	7.36	63.41	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.43	3.10	8.97	7.87	70.59	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.59	3.02	11.91	7.01	83.43	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.76	2.86	17.78	5.29	94.04	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.92	2.66	25.90	3.74	96.95	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.09	2.50	39.15	2.77	108.58	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.25	2.28	65.51	1.90	124.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.41	2.06	109.71	1.38	151.51	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.58	1.89	163.98	1.18	192.97	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.74	1.85	189.82	1.14	217.14	43	1105	0.21	0.013	0.01	2.41	0.00	0.000
5.91	1.89	192.61	1.18	226.55	45	1176	0.21	0.013	0.00	2.41	0.00	0.000
6.07	1.95	169.41	1.24	210.38	43	1124	0.21	0.014	0.01	2.41	0.00	0.000
6.23	1.93	168.66	1.22	205.01	42	1084	0.21	0.015	0.01	2.41	0.00	0.000
6.40	1.88	166.11	1.17	193.94	39	1002	0.21	0.018	0.01	2.41	0.00	0.000
6.56	1.85	173.35	1.14	198.31	39	1009	0.21	0.018	0.01	2.41	0.00	0.000
6.73	1.83	178.38	1.13	201.21	39	1012	0.21	0.019	0.01	2.41	0.00	0.000
6.89	1.85	184.86	1.15	211.89	42	1080	0.21	0.018	0.01	2.41	0.00	0.000
7.05	1.81	194.76	1.12	217.19	42	1082	0.21	0.018	0.01	2.41	0.00	0.000
7.22	1.75	200.06	1.07	214.06	41	1025	0.21	0.020	0.01	2.41	0.00	0.000
7.38	1.64	197.38	1.00	197.38	36	925	0.21	0.025	0.01	2.41	0.01	0.000
7.55	1.54	193.20	1.00	193.20	34	811	0.21	0.034	0.02	2.41	0.01	0.000
7.71	1.59	176.63	1.00	176.63	32	803	0.21	0.036	0.02	2.41	0.01	0.000
7.87	1.71	160.15	1.05	167.45	31	833	0.21	0.034	0.02	2.41	0.01	0.000
8.04	1.88	143.23	1.17	167.17	33	880	0.21	0.031	0.02	2.41	0.01	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
8.20	2.07	118.84	1.40	166.04	35	912	0.21	0.030	0.02	2.41	0.01	0.000
8.37	2.25	97.30	1.80	175.48	40	944	0.21	0.029	0.01	2.41	0.01	0.000
8.53	2.34	86.64	2.07	179.15	43	934	0.21	0.031	0.01	2.41	0.01	0.000
8.69	2.33	84.00	2.06	173.26	41	904	0.21	0.034	0.01	2.41	0.01	0.000
8.86	2.17	103.65	1.59	164.67	37	902	0.21	0.035	0.02	2.41	0.01	0.000
9.02	1.88	152.17	1.17	177.89	35	1011	0.21	0.029	0.01	2.41	0.01	0.000
9.19	1.63	209.34	1.00	209.34	38	1102	0.21	0.026	0.01	2.41	0.01	0.000
9.35	1.49	245.30	1.00	245.30	43	1091	0.21	0.027	0.01	2.41	0.00	0.000
9.51	1.50	232.73	1.00	232.73	41	1053	0.21	0.029	0.01	2.41	0.01	0.000
9.68	1.63	196.02	1.00	196.02	36	1057	0.21	0.030	0.01	2.41	0.01	0.000
9.84	1.79	163.71	1.10	180.50	0	0	0.21	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.01

Abbreviations

Q_{tn}: Equivalent clean sand normalized cone resistance
K_c: Fines correction factor
$Q_{tn,cs}$: Post-liquefaction volumentric strain
G_{max}: Small strain shear modulus
CSR: Soil cyclic stress ratio
γ: Cyclic shear strain
$e_{vol(15)}$: Volumetric strain after 15 cycles
N_c: Equivalent number of cycles
e_v: Volumetric strain
Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.01	167.34	2.00	0.00	1.00	0.00	10.17	162.15	2.00	0.00	1.00	0.00
10.33	159.17	2.00	0.00	1.00	0.00	10.50	151.41	2.00	0.00	1.00	0.00
10.66	134.33	2.00	0.00	1.00	0.00	10.83	124.42	2.00	0.00	1.00	0.00
10.99	108.95	2.00	0.00	1.00	0.00	11.15	115.01	2.00	0.00	1.00	0.00
11.32	119.41	2.00	0.00	1.00	0.00	11.48	132.73	2.00	0.00	1.00	0.00
11.65	141.85	2.00	0.00	1.00	0.00	11.81	141.82	1.52	0.00	1.00	0.00
11.98	127.16	1.18	0.34	1.00	0.01	12.14	112.24	0.92	1.32	1.00	0.03
12.30	100.71	0.75	2.01	1.00	0.04	12.47	109.03	0.86	1.38	1.00	0.03
12.63	125.13	2.00	0.00	1.00	0.00	12.80	122.81	2.00	0.00	1.00	0.00
12.96	111.85	2.00	0.00	1.00	0.00	13.12	109.20	2.00	0.00	1.00	0.00
13.29	103.55	2.00	0.00	1.00	0.00	13.45	97.92	2.00	0.00	1.00	0.00
13.62	87.16	2.00	0.00	1.00	0.00	13.78	82.06	2.00	0.00	1.00	0.00
13.94	84.99	2.00	0.00	1.00	0.00	14.11	90.07	2.00	0.00	1.00	0.00
14.27	94.15	2.00	0.00	1.00	0.00	14.44	95.01	2.00	0.00	1.00	0.00
14.60	93.96	2.00	0.00	1.00	0.00	14.76	89.89	2.00	0.00	1.00	0.00
14.93	85.03	2.00	0.00	1.00	0.00	15.09	77.62	2.00	0.00	1.00	0.00
15.26	75.75	2.00	0.00	1.00	0.00	15.42	78.31	2.00	0.00	1.00	0.00
15.58	84.90	2.00	0.00	1.00	0.00	15.75	89.36	2.00	0.00	1.00	0.00
15.91	91.78	2.00	0.00	1.00	0.00	16.08	91.98	2.00	0.00	1.00	0.00
16.24	92.24	2.00	0.00	1.00	0.00	16.40	88.15	2.00	0.00	1.00	0.00
16.57	81.08	2.00	0.00	1.00	0.00	16.73	72.30	2.00	0.00	1.00	0.00
16.90	66.06	2.00	0.00	1.00	0.00	17.06	63.91	2.00	0.00	1.00	0.00
17.22	63.06	2.00	0.00	1.00	0.00	17.39	61.05	2.00	0.00	1.00	0.00
17.55	58.77	2.00	0.00	1.00	0.00	17.72	60.90	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
17.88	68.11	2.00	0.00	1.00	0.00	18.04	83.49	2.00	0.00	1.00	0.00
18.21	86.00	2.00	0.00	1.00	0.00	18.37	84.87	0.50	2.67	1.00	0.05
18.54	89.32	0.53	2.56	1.00	0.05	18.70	90.06	0.54	2.55	1.00	0.05
18.86	84.25	2.00	0.00	1.00	0.00	19.03	73.80	2.00	0.00	1.00	0.00
19.19	64.14	2.00	0.00	1.00	0.00	19.36	63.66	2.00	0.00	1.00	0.00
19.52	64.53	2.00	0.00	1.00	0.00	19.69	67.35	2.00	0.00	1.00	0.00
19.85	80.56	2.00	0.00	1.00	0.00	20.01	100.61	2.00	0.00	1.00	0.00
20.18	120.03	2.00	0.00	1.00	0.00	20.34	124.30	2.00	0.00	1.00	0.00
20.51	113.34	2.00	0.00	1.00	0.00	20.67	100.79	2.00	0.00	1.00	0.00
20.83	88.38	2.00	0.00	1.00	0.00	21.00	89.94	2.00	0.00	1.00	0.00
21.16	99.34	2.00	0.00	1.00	0.00	21.33	103.07	2.00	0.00	1.00	0.00
21.49	102.74	2.00	0.00	1.00	0.00	21.65	94.32	2.00	0.00	1.00	0.00
21.82	96.02	2.00	0.00	1.00	0.00	21.98	99.34	2.00	0.00	1.00	0.00
22.15	96.90	2.00	0.00	1.00	0.00	22.31	96.42	2.00	0.00	1.00	0.00
22.47	102.65	2.00	0.00	1.00	0.00	22.64	105.36	2.00	0.00	1.00	0.00
22.80	110.89	2.00	0.00	1.00	0.00	22.97	110.20	2.00	0.00	1.00	0.00
23.13	115.14	2.00	0.00	1.00	0.00	23.29	113.97	0.74	2.04	1.00	0.04
23.46	108.08	0.67	2.19	1.00	0.04	23.62	103.21	0.62	2.28	1.00	0.04
23.79	100.98	0.59	2.32	1.00	0.05	23.95	115.38	0.75	1.65	1.00	0.03
24.11	131.43	0.98	0.69	1.00	0.01	24.28	160.25	1.56	0.00	1.00	0.00
24.44	195.12	2.00	0.00	1.00	0.00	24.61	229.95	2.00	0.00	1.00	0.00
24.77	252.62	2.00	0.00	1.00	0.00	24.93	246.94	2.00	0.00	1.00	0.00
25.10	237.50	2.00	0.00	1.00	0.00	25.26	235.73	2.00	0.00	1.00	0.00
25.43	228.62	2.00	0.00	1.00	0.00	25.59	216.35	2.00	0.00	1.00	0.00
25.75	199.21	2.00	0.00	1.00	0.00	25.92	169.36	1.77	0.00	1.00	0.00
26.08	142.24	2.00	0.00	1.00	0.00	26.25	115.48	2.00	0.00	1.00	0.00
26.41	100.79	2.00	0.00	1.00	0.00	26.57	103.93	2.00	0.00	1.00	0.00
26.74	108.97	2.00	0.00	1.00	0.00	26.90	120.17	2.00	0.00	1.00	0.00
27.07	110.25	2.00	0.00	1.00	0.00	27.23	133.23	2.00	0.00	1.00	0.00
27.40	162.78	1.58	0.00	1.00	0.00	27.56	165.16	1.64	0.00	1.00	0.00
27.72	141.36	2.00	0.00	1.00	0.00	27.89	117.63	2.00	0.00	1.00	0.00
28.05	99.12	2.00	0.00	1.00	0.00	28.22	109.49	2.00	0.00	1.00	0.00
28.38	129.44	2.00	0.00	1.00	0.00	28.54	141.50	1.12	0.44	1.00	0.01
28.71	149.91	1.28	0.22	1.00	0.00	28.87	139.76	1.09	0.44	1.00	0.01
29.04	124.73	2.00	0.00	1.00	0.00	29.20	94.69	2.00	0.00	1.00	0.00
29.36	74.32	2.00	0.00	1.00	0.00	29.53	84.15	2.00	0.00	1.00	0.00
29.69	106.14	2.00	0.00	1.00	0.00	29.86	141.18	2.00	0.00	1.00	0.00
30.02	158.28	2.00	0.00	1.00	0.00	30.18	150.29	1.27	0.22	1.00	0.00
30.35	141.84	1.11	0.44	1.00	0.01	30.51	120.72	0.78	1.54	1.00	0.03
30.68	109.80	2.00	0.00	1.00	0.00	30.84	104.44	2.00	0.00	1.00	0.00
31.00	92.79	0.49	2.48	1.00	0.05	31.17	84.41	2.00	0.00	1.00	0.00
31.33	89.52	2.00	0.00	1.00	0.00	31.50	97.93	2.00	0.00	1.00	0.00
31.66	118.36	2.00	0.00	1.00	0.00	31.82	134.61	2.00	0.00	1.00	0.00
31.99	142.62	2.00	0.00	1.00	0.00	32.15	144.48	2.00	0.00	1.00	0.00
32.32	155.20	2.00	0.00	1.00	0.00	32.48	183.47	2.00	0.00	1.00	0.00
32.64	213.03	2.00	0.00	1.00	0.00	32.81	190.84	2.00	0.00	1.00	0.00
32.97	158.13	2.00	0.00	1.00	0.00	33.14	127.30	2.00	0.00	1.00	0.00
33.30	108.66	2.00	0.00	1.00	0.00	33.46	99.94	2.00	0.00	1.00	0.00
33.63	83.12	2.00	0.00	1.00	0.00	33.79	62.87	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
33.96	58.66	2.00	0.00	1.00	0.00	34.12	59.07	2.00	0.00	1.00	0.00
34.28	64.65	2.00	0.00	1.00	0.00	34.45	68.63	2.00	0.00	1.00	0.00
34.61	71.13	2.00	0.00	1.00	0.00	34.78	68.35	2.00	0.00	1.00	0.00
34.94	66.19	2.00	0.00	1.00	0.00	35.10	69.44	2.00	0.00	1.00	0.00
35.27	77.48	2.00	0.00	1.00	0.00	35.43	86.30	2.00	0.00	1.00	0.00
35.60	88.26	2.00	0.00	1.00	0.00	35.76	80.20	2.00	0.00	1.00	0.00
35.93	71.49	2.00	0.00	1.00	0.00	36.09	63.31	2.00	0.00	1.00	0.00
36.25	60.30	2.00	0.00	1.00	0.00	36.42	59.22	2.00	0.00	1.00	0.00
36.58	60.39	2.00	0.00	1.00	0.00	36.75	63.70	2.00	0.00	1.00	0.00
36.91	65.51	2.00	0.00	1.00	0.00	37.07	64.74	2.00	0.00	1.00	0.00
37.24	62.37	2.00	0.00	1.00	0.00	37.40	61.45	2.00	0.00	1.00	0.00
37.57	61.54	2.00	0.00	1.00	0.00	37.73	62.85	2.00	0.00	1.00	0.00
37.89	64.04	2.00	0.00	1.00	0.00	38.06	63.04	2.00	0.00	1.00	0.00
38.22	59.96	2.00	0.00	1.00	0.00	38.39	55.21	2.00	0.00	1.00	0.00
38.55	53.95	2.00	0.00	1.00	0.00	38.71	55.97	2.00	0.00	1.00	0.00
38.88	60.62	2.00	0.00	1.00	0.00	39.04	62.16	2.00	0.00	1.00	0.00
39.21	70.73	2.00	0.00	1.00	0.00	39.37	84.77	2.00	0.00	1.00	0.00
39.53	98.34	2.00	0.00	1.00	0.00	39.70	100.17	2.00	0.00	1.00	0.00
39.86	95.92	2.00	0.00	1.00	0.00	40.03	95.39	2.00	0.00	1.00	0.00
40.19	94.48	2.00	0.00	1.00	0.00	40.35	90.36	2.00	0.00	1.00	0.00
40.52	86.02	2.00	0.00	1.00	0.00	40.68	90.85	2.00	0.00	1.00	0.00
40.85	93.97	2.00	0.00	1.00	0.00	41.01	99.95	2.00	0.00	1.00	0.00
41.17	105.67	2.00	0.00	1.00	0.00	41.34	110.06	2.00	0.00	1.00	0.00
41.50	105.75	2.00	0.00	1.00	0.00	41.67	112.36	2.00	0.00	1.00	0.00
41.83	117.64	2.00	0.00	1.00	0.00	41.99	131.25	2.00	0.00	1.00	0.00
42.16	133.49	0.93	1.02	1.00	0.02	42.32	144.97	1.12	0.43	1.00	0.01
42.49	141.09	1.05	0.44	1.00	0.01	42.65	129.04	0.87	1.08	1.00	0.02
42.81	112.06	0.65	2.09	1.00	0.04	42.98	119.94	0.74	1.90	1.00	0.04
43.14	141.22	1.06	0.44	1.00	0.01	43.31	161.07	1.45	0.00	1.00	0.00
43.47	177.76	1.87	0.00	1.00	0.00	43.64	199.52	2.00	0.00	1.00	0.00
43.80	227.12	2.00	0.00	1.00	0.00	43.96	245.13	2.00	0.00	1.00	0.00
44.13	253.57	2.00	0.00	1.00	0.00	44.29	240.25	2.00	0.00	1.00	0.00
44.46	230.40	2.00	0.00	1.00	0.00	44.62	214.68	2.00	0.00	1.00	0.00
44.78	212.51	2.00	0.00	1.00	0.00	44.95	203.22	2.00	0.00	1.00	0.00
45.11	212.54	2.00	0.00	1.00	0.00	45.28	217.52	2.00	0.00	1.00	0.00
45.44	222.24	2.00	0.00	1.00	0.00	45.60	-1.00	2.00	0.00	1.00	0.00
45.77	-1.00	2.00	0.00	1.00	0.00	45.93	-1.00	2.00	0.00	1.00	0.00
46.10	-1.00	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.73

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

Atlas Technical Consultants
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San Diego, CA, 92123
(619) 280-4321

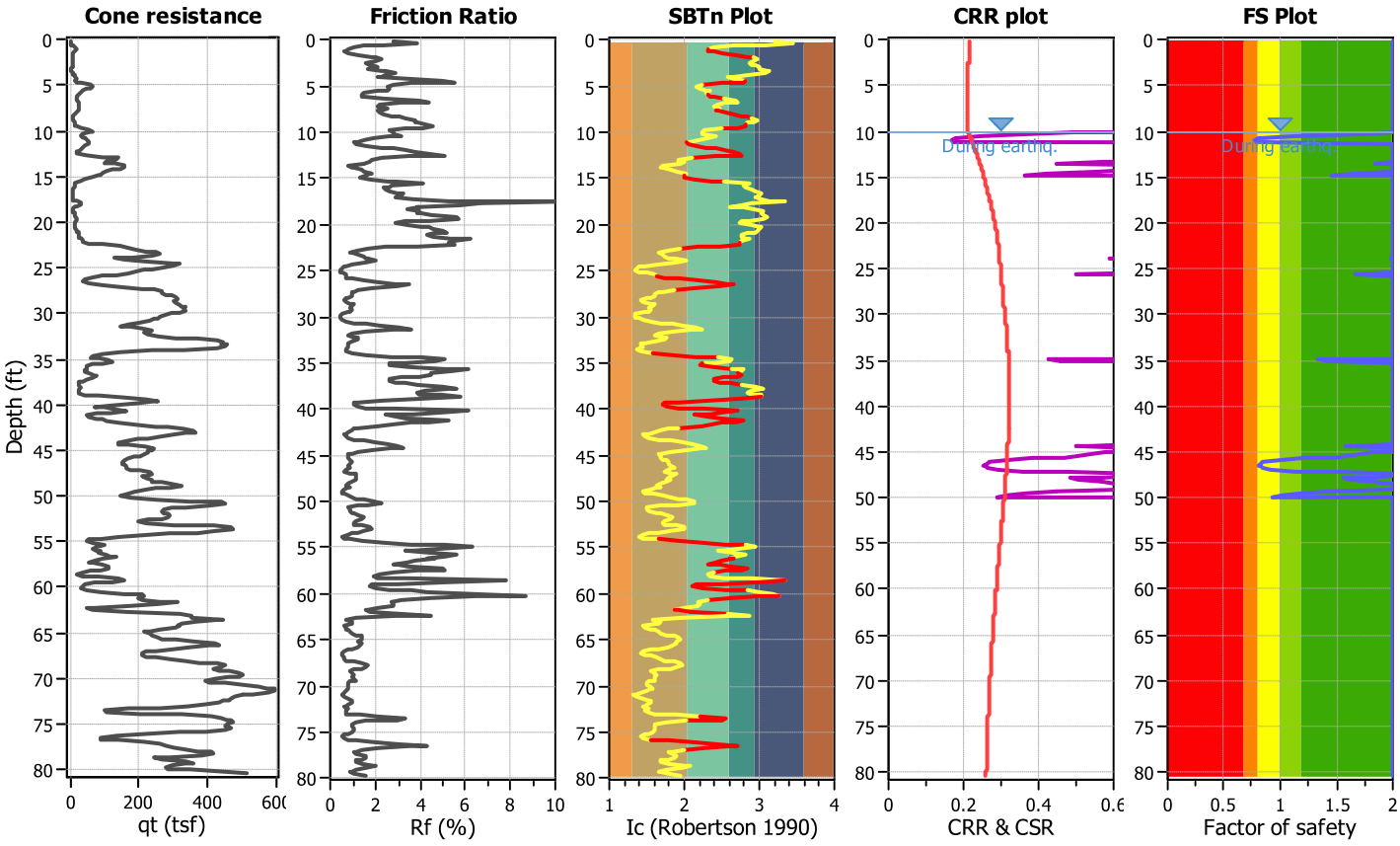
LIQUEFACTION ANALYSIS REPORT

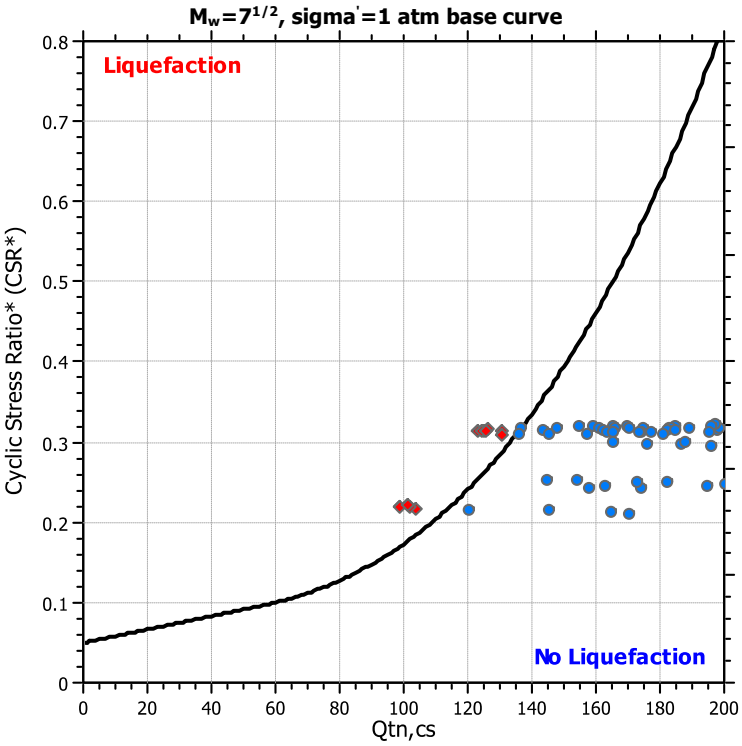
Project title : Quincy Courthouse **Location : Quincy, CA**

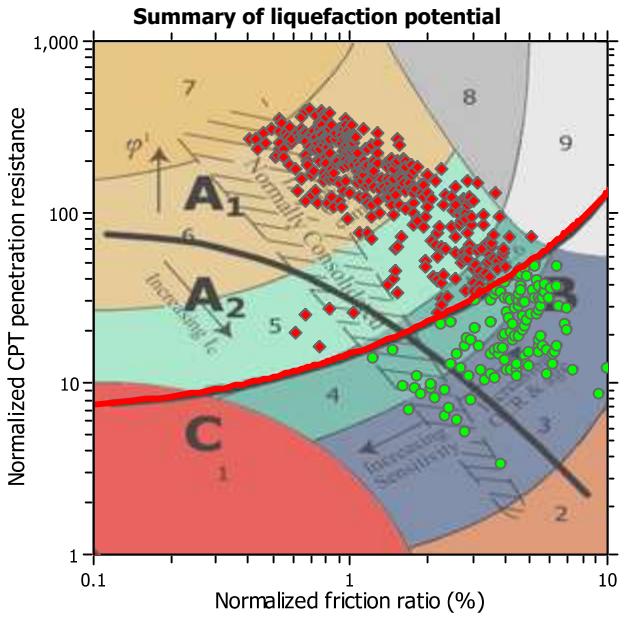
CPT file : CPT-03

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	10.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	10.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	5.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.56	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

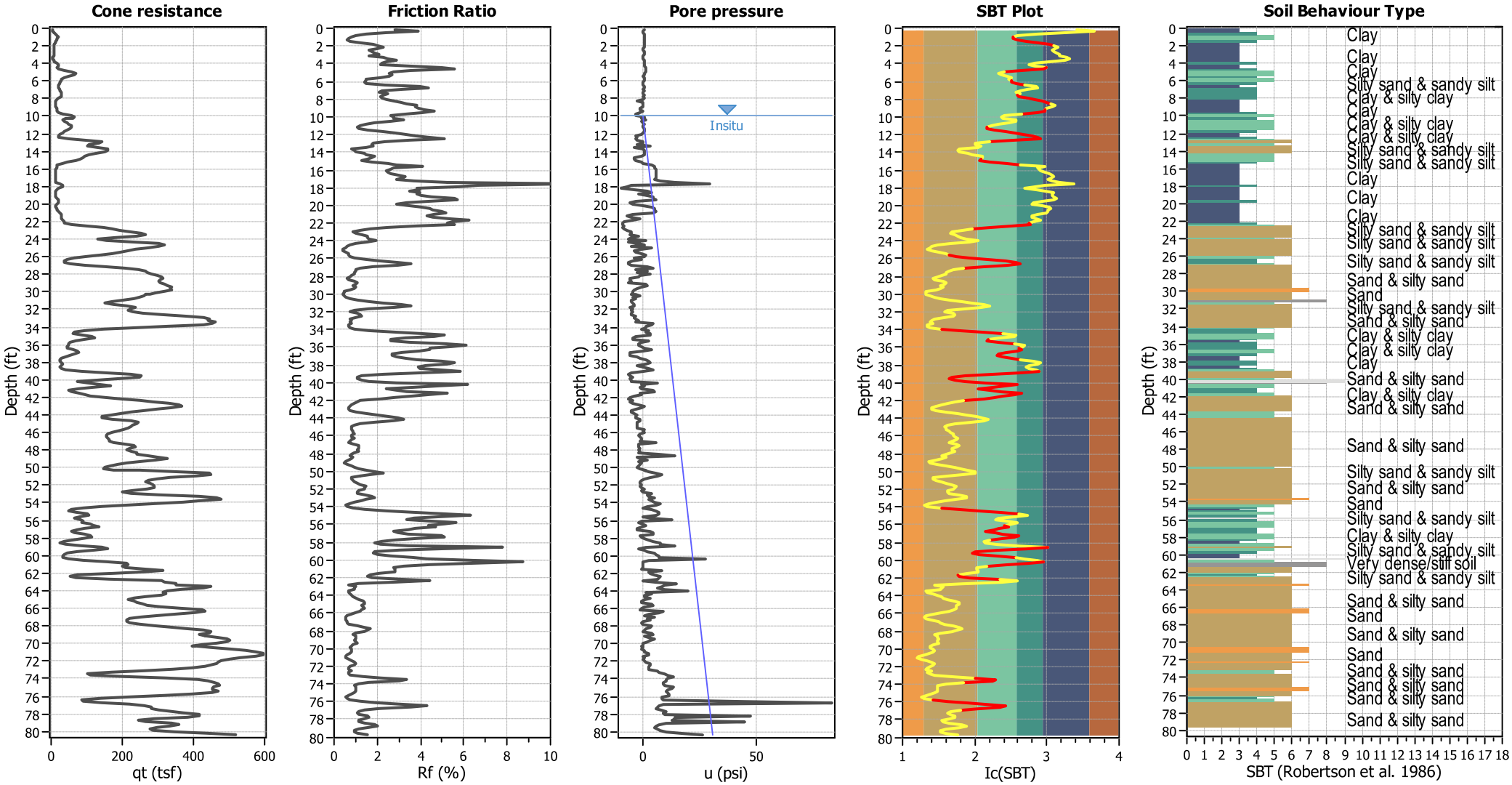






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



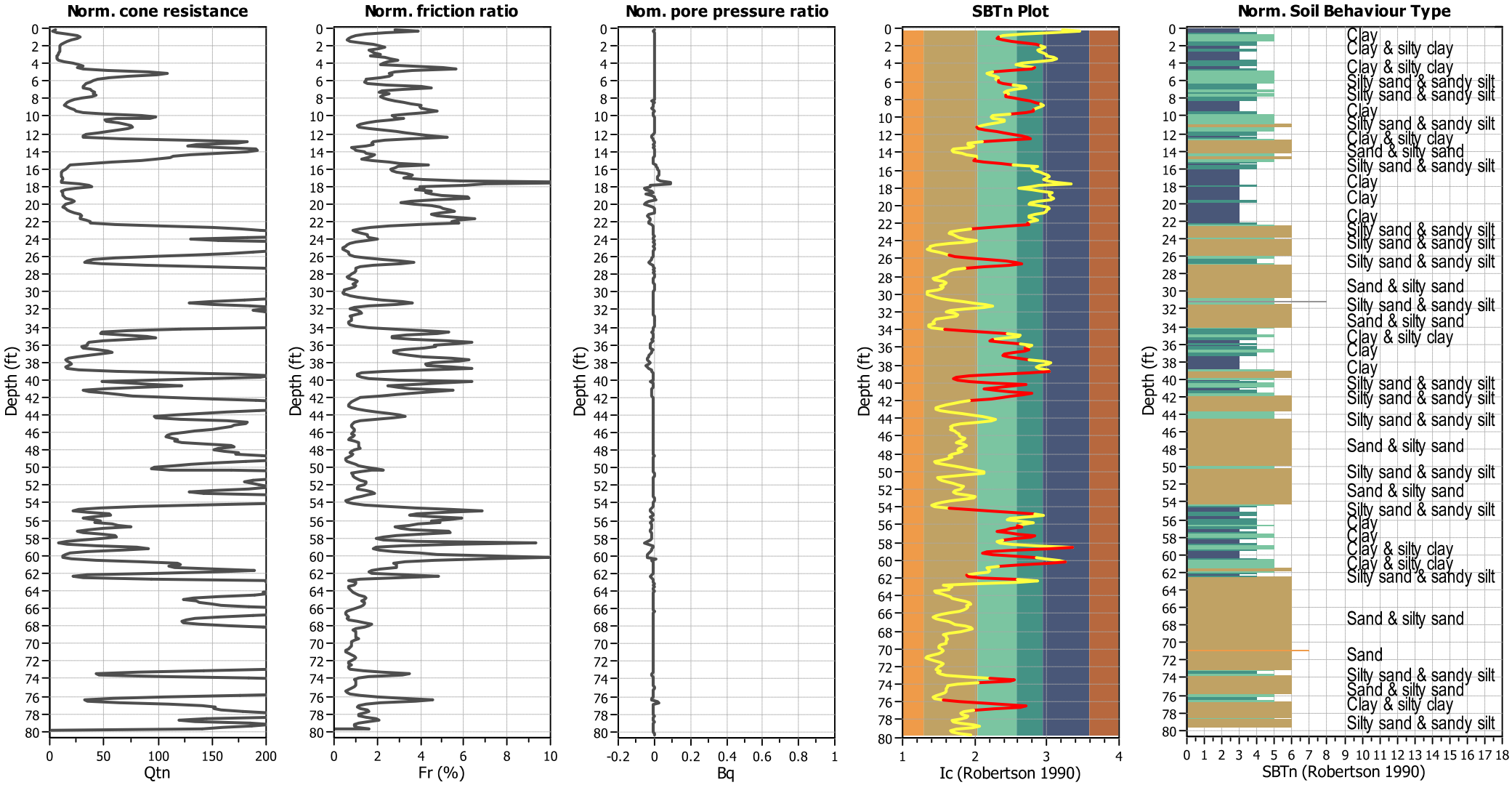
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	10.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



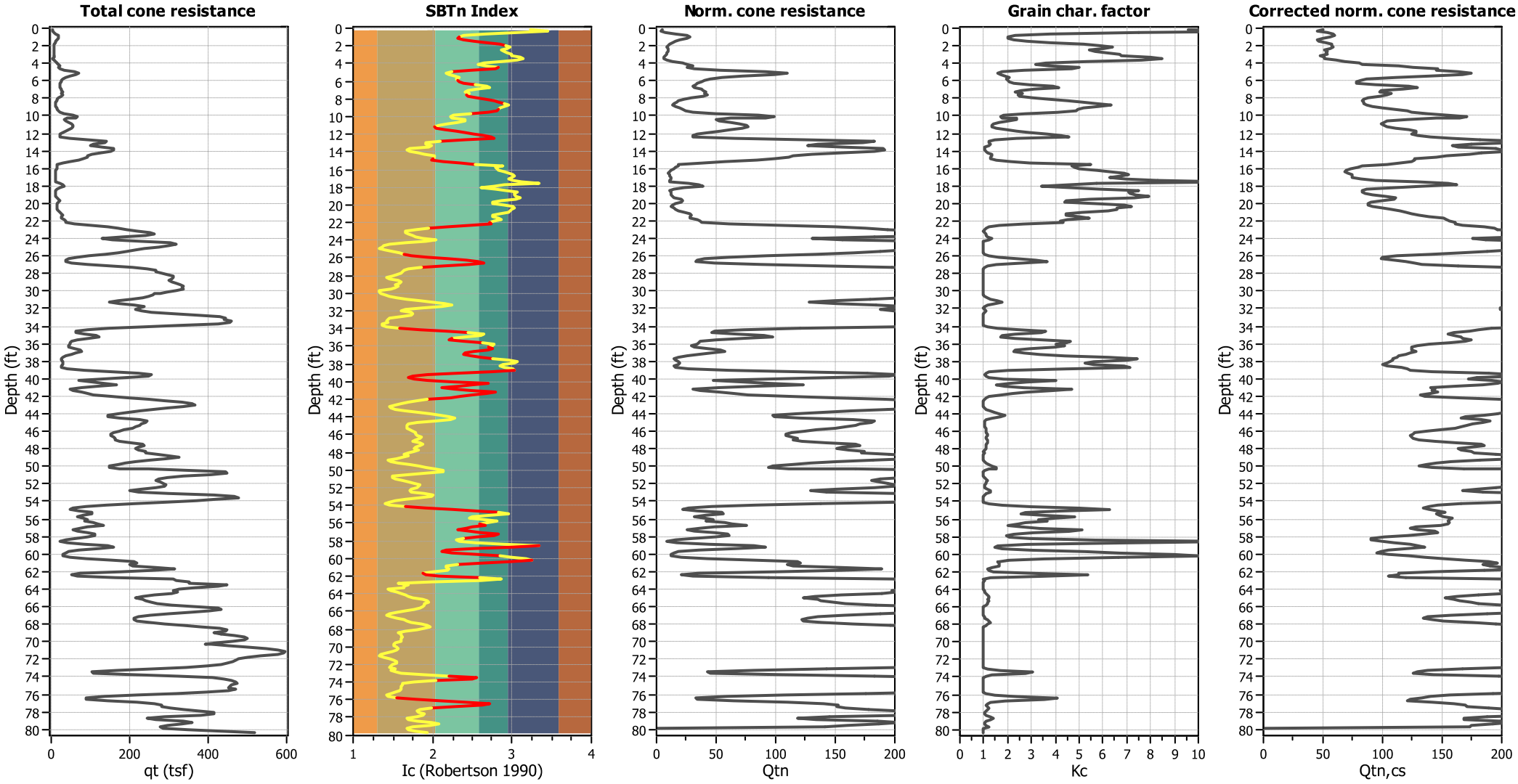
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	10.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

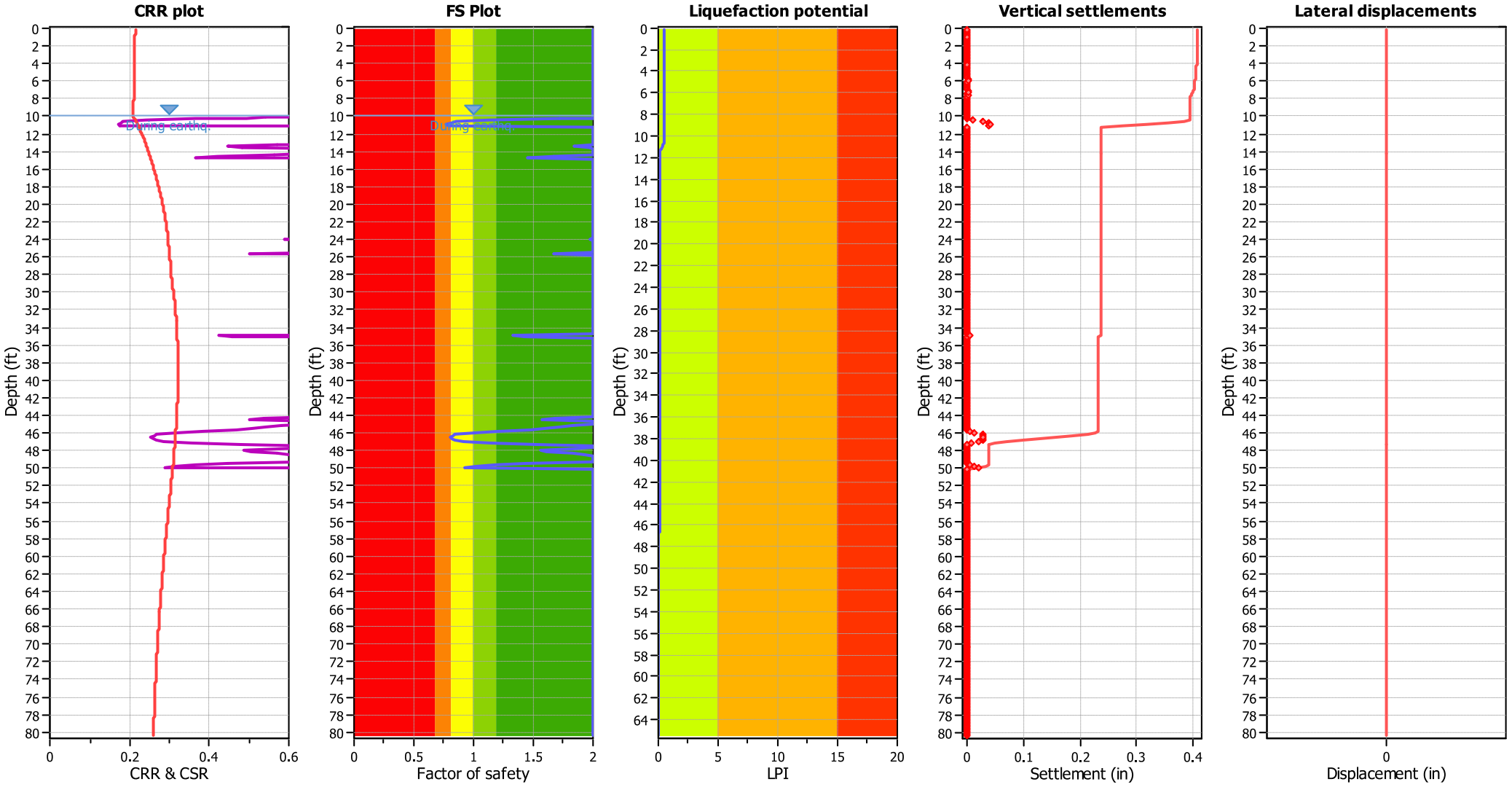
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	10.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	10.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

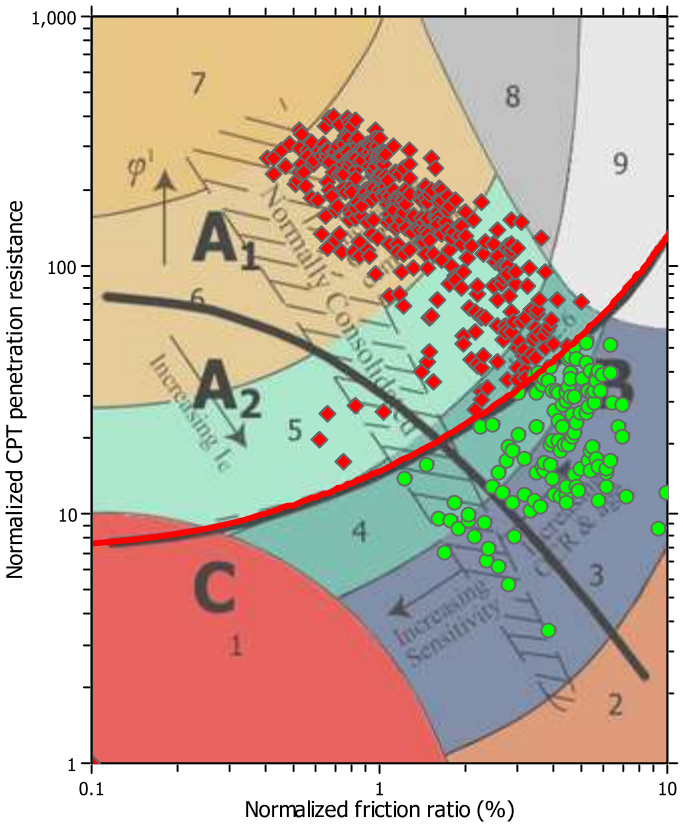
F.S. color scheme

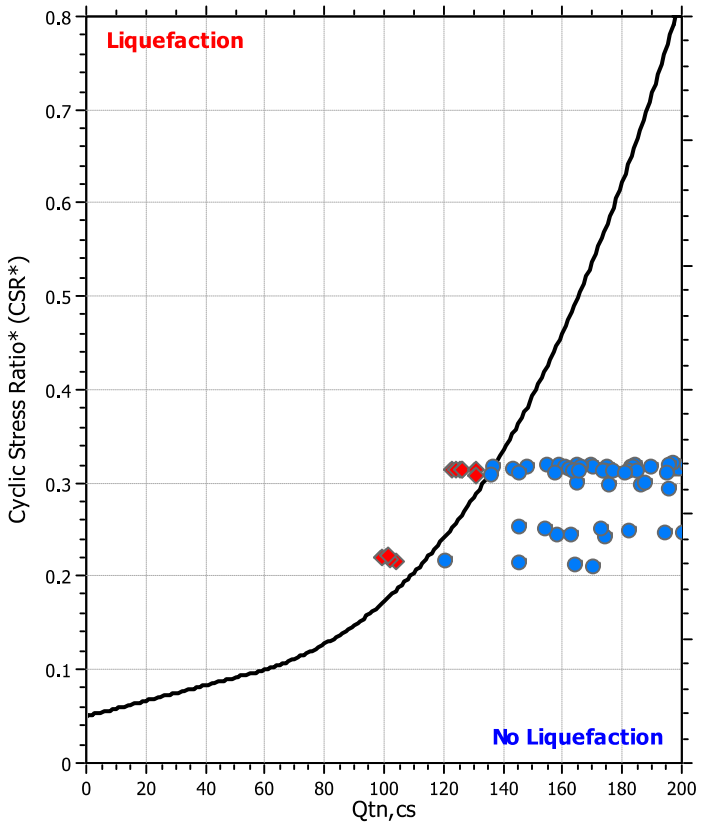
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

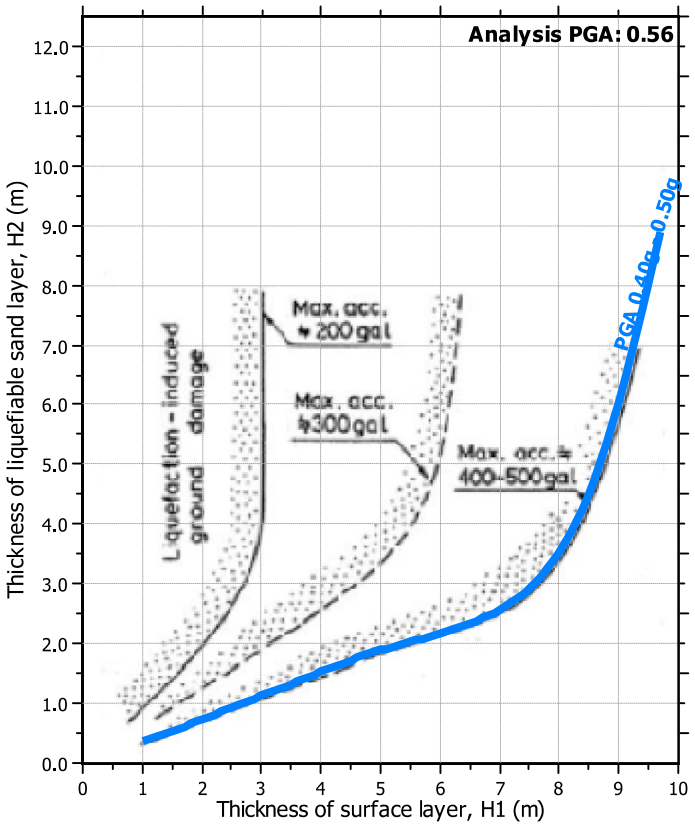
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



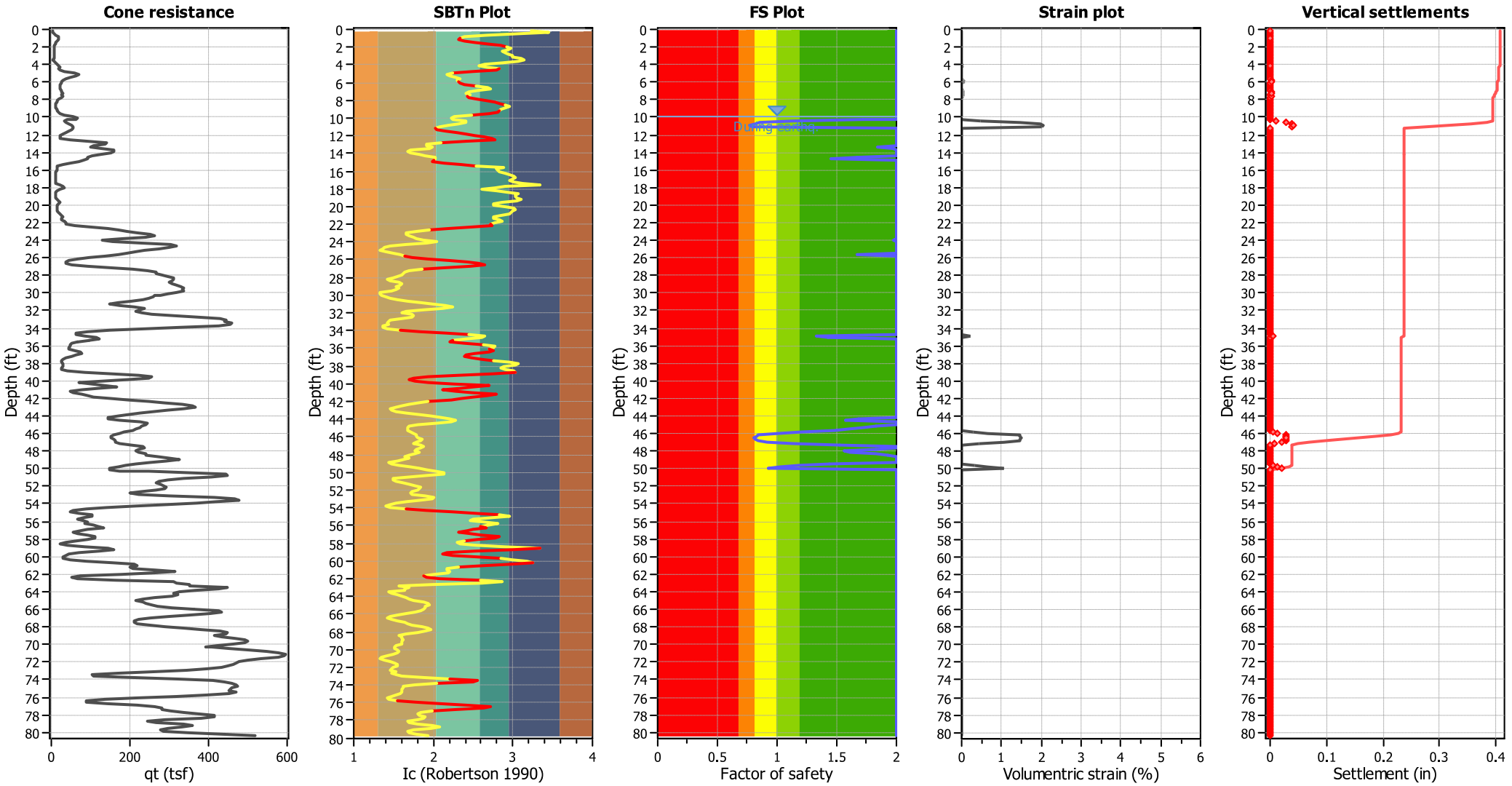




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	10.00 ft	Fill height:	N/A	Limit depth:	50.00 ft

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement of dry sands ::

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
0.16	3.22	5.17	9.58	49.48	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.33	3.46	3.35	13.31	44.63	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.49	3.07	7.18	7.51	53.95	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.66	2.67	15.68	3.75	58.85	0	0	0.21	0.000	0.00	0.00	0.00	0.000
0.82	2.40	25.96	2.30	59.84	15	303	0.21	0.009	0.01	2.41	0.01	0.000
0.98	2.33	27.52	2.04	56.08	13	294	0.21	0.013	0.02	2.41	0.01	0.000
1.15	2.32	25.19	2.00	50.43	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.31	2.39	20.02	2.28	45.63	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.48	2.51	16.28	2.82	45.96	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.64	2.67	13.76	3.81	52.45	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.80	2.84	11.05	5.16	57.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
1.97	2.91	9.82	5.84	57.35	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.13	2.97	9.14	6.40	58.51	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.30	2.93	9.28	6.04	56.03	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.46	2.87	9.45	5.45	51.46	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.62	2.90	9.34	5.70	53.20	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.79	2.95	8.60	6.16	53.00	0	0	0.21	0.000	0.00	0.00	0.00	0.000
2.95	3.00	8.04	6.73	54.12	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.12	3.00	6.98	6.74	47.04	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.28	3.10	6.40	7.97	51.03	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.44	3.14	6.08	8.49	51.66	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.61	3.07	8.01	7.60	60.89	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.77	2.86	12.89	5.30	68.35	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.94	2.65	22.11	3.62	80.12	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.10	2.57	26.18	3.18	83.12	22	382	0.21	0.079	0.07	2.41	0.03	0.001
4.27	2.66	30.36	3.73	113.20	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.43	2.82	25.11	5.00	125.45	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.59	2.79	31.33	4.68	146.71	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.76	2.49	53.69	2.71	145.25	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.92	2.25	91.18	1.79	163.46	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.09	2.17	109.35	1.59	174.29	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.25	2.21	99.13	1.69	167.51	38	911	0.21	0.016	0.01	2.41	0.00	0.000
5.41	2.29	72.56	1.91	138.76	32	737	0.21	0.024	0.01	2.41	0.01	0.000
5.58	2.33	54.46	2.05	111.49	27	583	0.21	0.042	0.03	2.41	0.01	0.001
5.74	2.29	44.92	1.92	86.34	20	458	0.21	0.091	0.09	2.41	0.04	0.002
5.91	2.32	40.69	2.01	81.90	19	430	0.21	0.123	0.13	2.41	0.06	0.002
6.07	2.34	37.53	2.07	77.65	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.23	2.39	34.12	2.28	77.90	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.40	2.53	32.37	2.92	94.38	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.56	2.69	30.93	3.93	121.44	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.73	2.72	31.27	4.14	129.60	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.89	2.56	37.84	3.09	116.94	31	542	0.21	0.076	0.05	2.41	0.02	0.001
7.05	2.45	38.76	2.54	98.27	25	484	0.21	0.117	0.09	2.41	0.04	0.002
7.22	2.41	41.75	2.34	97.89	24	493	0.21	0.115	0.09	2.41	0.04	0.002
7.38	2.47	40.76	2.62	106.96	27	522	0.21	0.100	0.07	2.41	0.03	0.001
7.55	2.43	43.04	2.42	104.09	26	520	0.21	0.106	0.08	2.41	0.03	0.001
7.71	2.44	39.28	2.47	97.17	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.87	2.55	29.08	3.04	88.40	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.04	2.66	22.69	3.71	84.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
8.20	2.77	18.46	4.51	83.24	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.37	2.84	16.56	5.09	84.33	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.53	2.91	14.65	5.75	84.21	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.69	2.96	13.70	6.32	86.53	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.86	2.91	15.81	5.79	91.62	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.02	2.84	19.42	5.17	100.37	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.19	2.82	22.20	4.97	110.27	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.35	2.81	24.71	4.89	120.92	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.51	2.71	30.59	4.07	124.54	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.68	2.49	50.55	2.72	137.25	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.84	2.25	84.93	1.81	153.61	0	0	0.21	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.01

Abbreviations

Q_{tn}: Equivalent clean sand normalized cone resistance
K_c: Fines correction factor
$Q_{tn,cs}$: Post-liquefaction volumentric strain
G_{max}: Small strain shear modulus
CSR: Soil cyclic stress ratio
γ: Cyclic shear strain
$e_{vol(15)}$: Volumetric strain after 15 cycles
N_c: Equivalent number of cycles
e_v: Volumetric strain
Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.01	170.78	2.00	0.00	1.00	0.00	10.17	164.71	2.00	0.00	1.00	0.00
10.33	145.46	1.72	0.00	1.00	0.00	10.50	120.64	1.13	0.49	1.00	0.01
10.66	103.95	0.85	1.48	1.00	0.03	10.83	101.72	0.81	1.98	1.00	0.04
10.99	99.01	0.77	2.06	1.00	0.04	11.15	101.15	0.79	2.00	1.00	0.04
11.32	104.16	2.00	0.00	1.00	0.00	11.48	111.58	2.00	0.00	1.00	0.00
11.65	121.61	2.00	0.00	1.00	0.00	11.81	128.02	2.00	0.00	1.00	0.00
11.98	128.42	2.00	0.00	1.00	0.00	12.14	124.04	2.00	0.00	1.00	0.00
12.30	129.00	2.00	0.00	1.00	0.00	12.47	140.45	2.00	0.00	1.00	0.00
12.63	158.17	2.00	0.00	1.00	0.00	12.80	181.63	2.00	0.00	1.00	0.00
12.96	218.82	2.00	0.00	1.00	0.00	13.12	208.30	2.00	0.00	1.00	0.00
13.29	174.25	2.00	0.00	1.00	0.00	13.45	158.06	1.84	0.00	1.00	0.00
13.62	162.95	1.98	0.00	1.00	0.00	13.78	194.92	2.00	0.00	1.00	0.00
13.94	200.37	2.00	0.00	1.00	0.00	14.11	205.59	2.00	0.00	1.00	0.00
14.27	182.75	2.00	0.00	1.00	0.00	14.44	173.02	2.00	0.00	1.00	0.00
14.60	154.18	1.67	0.00	1.00	0.00	14.76	145.31	1.45	0.00	1.00	0.00
14.93	126.85	2.00	0.00	1.00	0.00	15.09	126.89	2.00	0.00	1.00	0.00
15.26	124.15	2.00	0.00	1.00	0.00	15.42	114.05	2.00	0.00	1.00	0.00
15.58	103.57	2.00	0.00	1.00	0.00	15.75	83.25	2.00	0.00	1.00	0.00
15.91	78.82	2.00	0.00	1.00	0.00	16.08	73.14	2.00	0.00	1.00	0.00
16.24	69.40	2.00	0.00	1.00	0.00	16.40	68.71	2.00	0.00	1.00	0.00
16.57	70.91	2.00	0.00	1.00	0.00	16.73	74.48	2.00	0.00	1.00	0.00
16.90	74.92	2.00	0.00	1.00	0.00	17.06	73.80	2.00	0.00	1.00	0.00
17.22	82.26	2.00	0.00	1.00	0.00	17.39	93.65	2.00	0.00	1.00	0.00
17.55	128.71	2.00	0.00	1.00	0.00	17.72	154.41	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
17.88	162.33	2.00	0.00	1.00	0.00	18.04	133.28	2.00	0.00	1.00	0.00
18.21	111.41	2.00	0.00	1.00	0.00	18.37	87.18	2.00	0.00	1.00	0.00
18.54	82.62	2.00	0.00	1.00	0.00	18.70	83.20	2.00	0.00	1.00	0.00
18.86	85.55	2.00	0.00	1.00	0.00	19.03	91.12	2.00	0.00	1.00	0.00
19.19	102.03	2.00	0.00	1.00	0.00	19.36	110.84	2.00	0.00	1.00	0.00
19.52	110.25	2.00	0.00	1.00	0.00	19.69	99.84	2.00	0.00	1.00	0.00
19.85	90.51	2.00	0.00	1.00	0.00	20.01	87.53	2.00	0.00	1.00	0.00
20.18	88.27	2.00	0.00	1.00	0.00	20.34	91.52	2.00	0.00	1.00	0.00
20.51	100.15	2.00	0.00	1.00	0.00	20.67	107.18	2.00	0.00	1.00	0.00
20.83	115.13	2.00	0.00	1.00	0.00	21.00	119.64	2.00	0.00	1.00	0.00
21.16	124.45	2.00	0.00	1.00	0.00	21.33	130.41	2.00	0.00	1.00	0.00
21.49	138.76	2.00	0.00	1.00	0.00	21.65	150.65	2.00	0.00	1.00	0.00
21.82	153.82	2.00	0.00	1.00	0.00	21.98	155.74	2.00	0.00	1.00	0.00
22.15	161.35	2.00	0.00	1.00	0.00	22.31	161.22	2.00	0.00	1.00	0.00
22.47	166.69	2.00	0.00	1.00	0.00	22.64	185.18	2.00	0.00	1.00	0.00
22.80	193.93	2.00	0.00	1.00	0.00	22.97	195.98	2.00	0.00	1.00	0.00
23.13	223.28	2.00	0.00	1.00	0.00	23.29	263.54	2.00	0.00	1.00	0.00
23.46	286.63	2.00	0.00	1.00	0.00	23.62	266.43	2.00	0.00	1.00	0.00
23.79	212.98	2.00	0.00	1.00	0.00	23.95	176.04	1.98	0.00	1.00	0.00
24.11	186.82	2.00	0.00	1.00	0.00	24.28	228.90	2.00	0.00	1.00	0.00
24.44	299.50	2.00	0.00	1.00	0.00	24.61	314.20	2.00	0.00	1.00	0.00
24.77	296.10	2.00	0.00	1.00	0.00	24.93	267.29	2.00	0.00	1.00	0.00
25.10	231.80	2.00	0.00	1.00	0.00	25.26	208.62	2.00	0.00	1.00	0.00
25.43	188.24	2.00	0.00	1.00	0.00	25.59	165.38	1.67	0.00	1.00	0.00
25.75	140.07	2.00	0.00	1.00	0.00	25.92	112.23	2.00	0.00	1.00	0.00
26.08	99.86	2.00	0.00	1.00	0.00	26.25	98.56	2.00	0.00	1.00	0.00
26.41	109.23	2.00	0.00	1.00	0.00	26.57	119.07	2.00	0.00	1.00	0.00
26.74	127.44	2.00	0.00	1.00	0.00	26.90	132.73	2.00	0.00	1.00	0.00
27.07	163.54	2.00	0.00	1.00	0.00	27.23	205.16	2.00	0.00	1.00	0.00
27.40	230.66	2.00	0.00	1.00	0.00	27.56	250.11	2.00	0.00	1.00	0.00
27.72	251.27	2.00	0.00	1.00	0.00	27.89	262.52	2.00	0.00	1.00	0.00
28.05	276.87	2.00	0.00	1.00	0.00	28.22	290.36	2.00	0.00	1.00	0.00
28.38	291.01	2.00	0.00	1.00	0.00	28.54	285.98	2.00	0.00	1.00	0.00
28.71	278.73	2.00	0.00	1.00	0.00	28.87	283.95	2.00	0.00	1.00	0.00
29.04	294.20	2.00	0.00	1.00	0.00	29.20	301.26	2.00	0.00	1.00	0.00
29.36	308.87	2.00	0.00	1.00	0.00	29.53	305.42	2.00	0.00	1.00	0.00
29.69	308.46	2.00	0.00	1.00	0.00	29.86	291.11	2.00	0.00	1.00	0.00
30.02	267.12	2.00	0.00	1.00	0.00	30.18	250.84	2.00	0.00	1.00	0.00
30.35	237.33	2.00	0.00	1.00	0.00	30.51	233.39	2.00	0.00	1.00	0.00
30.68	227.04	2.00	0.00	1.00	0.00	30.84	233.41	2.00	0.00	1.00	0.00
31.00	230.77	2.00	0.00	1.00	0.00	31.17	231.22	2.00	0.00	1.00	0.00
31.33	227.77	2.00	0.00	1.00	0.00	31.50	224.25	2.00	0.00	1.00	0.00
31.66	214.69	2.00	0.00	1.00	0.00	31.82	210.47	2.00	0.00	1.00	0.00
31.99	198.27	2.00	0.00	1.00	0.00	32.15	199.05	2.00	0.00	1.00	0.00
32.32	214.05	2.00	0.00	1.00	0.00	32.48	236.17	2.00	0.00	1.00	0.00
32.64	271.48	2.00	0.00	1.00	0.00	32.81	326.42	2.00	0.00	1.00	0.00
32.97	374.10	2.00	0.00	1.00	0.00	33.14	386.90	2.00	0.00	1.00	0.00
33.30	381.25	2.00	0.00	1.00	0.00	33.46	398.36	2.00	0.00	1.00	0.00
33.63	391.96	2.00	0.00	1.00	0.00	33.79	367.39	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
33.96	282.97	2.00	0.00	1.00	0.00	34.12	228.81	2.00	0.00	1.00	0.00
34.28	190.93	2.00	0.00	1.00	0.00	34.45	180.81	2.00	0.00	1.00	0.00
34.61	172.69	2.00	0.00	1.00	0.00	34.78	160.01	2.00	0.00	1.00	0.00
34.94	154.88	1.33	0.21	1.00	0.00	35.10	159.29	1.43	0.00	1.00	0.00
35.27	166.17	2.00	0.00	1.00	0.00	35.43	167.46	2.00	0.00	1.00	0.00
35.60	174.17	2.00	0.00	1.00	0.00	35.76	168.96	2.00	0.00	1.00	0.00
35.93	156.00	2.00	0.00	1.00	0.00	36.09	138.47	2.00	0.00	1.00	0.00
36.25	129.70	2.00	0.00	1.00	0.00	36.42	124.80	2.00	0.00	1.00	0.00
36.58	124.65	2.00	0.00	1.00	0.00	36.75	124.99	2.00	0.00	1.00	0.00
36.91	128.21	2.00	0.00	1.00	0.00	37.07	123.40	2.00	0.00	1.00	0.00
37.24	119.46	2.00	0.00	1.00	0.00	37.40	113.74	2.00	0.00	1.00	0.00
37.57	112.01	2.00	0.00	1.00	0.00	37.73	108.94	2.00	0.00	1.00	0.00
37.89	108.10	2.00	0.00	1.00	0.00	38.06	105.70	2.00	0.00	1.00	0.00
38.22	103.11	2.00	0.00	1.00	0.00	38.39	99.64	2.00	0.00	1.00	0.00
38.55	103.42	2.00	0.00	1.00	0.00	38.71	115.84	2.00	0.00	1.00	0.00
38.88	120.44	2.00	0.00	1.00	0.00	39.04	122.59	2.00	0.00	1.00	0.00
39.21	141.44	2.00	0.00	1.00	0.00	39.37	188.56	2.00	0.00	1.00	0.00
39.53	210.24	2.00	0.00	1.00	0.00	39.70	211.60	2.00	0.00	1.00	0.00
39.86	179.34	2.00	0.00	1.00	0.00	40.03	171.97	2.00	0.00	1.00	0.00
40.19	192.07	2.00	0.00	1.00	0.00	40.35	201.77	2.00	0.00	1.00	0.00
40.52	195.99	2.00	0.00	1.00	0.00	40.68	184.26	2.00	0.00	1.00	0.00
40.85	161.31	2.00	0.00	1.00	0.00	41.01	140.22	2.00	0.00	1.00	0.00
41.17	143.93	2.00	0.00	1.00	0.00	41.34	141.81	2.00	0.00	1.00	0.00
41.50	146.12	2.00	0.00	1.00	0.00	41.67	139.66	2.00	0.00	1.00	0.00
41.83	131.88	2.00	0.00	1.00	0.00	41.99	135.07	2.00	0.00	1.00	0.00
42.16	164.74	2.00	0.00	1.00	0.00	42.32	197.49	2.00	0.00	1.00	0.00
42.49	222.44	2.00	0.00	1.00	0.00	42.65	256.91	2.00	0.00	1.00	0.00
42.81	278.81	2.00	0.00	1.00	0.00	42.98	282.90	2.00	0.00	1.00	0.00
43.14	260.27	2.00	0.00	1.00	0.00	43.31	230.64	2.00	0.00	1.00	0.00
43.47	218.27	2.00	0.00	1.00	0.00	43.64	206.25	2.00	0.00	1.00	0.00
43.80	202.23	2.00	0.00	1.00	0.00	43.96	196.29	2.00	0.00	1.00	0.00
44.13	184.87	2.00	0.00	1.00	0.00	44.29	169.93	1.69	0.00	1.00	0.00
44.46	165.34	1.57	0.00	1.00	0.00	44.62	182.98	2.00	0.00	1.00	0.00
44.78	189.66	2.00	0.00	1.00	0.00	44.95	183.83	2.00	0.00	1.00	0.00
45.11	175.23	1.83	0.00	1.00	0.00	45.28	170.72	1.71	0.00	1.00	0.00
45.44	166.21	1.60	0.00	1.00	0.00	45.60	160.95	1.48	0.00	1.00	0.00
45.77	148.20	1.21	0.31	1.00	0.01	45.93	136.92	1.01	0.66	1.00	0.01
46.10	126.23	0.85	1.45	1.00	0.03	46.26	125.18	0.83	1.46	1.00	0.03
46.42	122.82	0.80	1.51	1.00	0.03	46.59	124.24	0.82	1.48	1.00	0.03
46.75	125.93	0.85	1.45	1.00	0.03	46.92	130.59	0.91	1.06	1.00	0.02
47.08	143.74	1.13	0.44	1.00	0.01	47.24	162.44	1.53	0.00	1.00	0.00
47.41	182.70	2.00	0.00	1.00	0.00	47.57	185.04	2.00	0.00	1.00	0.00
47.74	174.35	1.83	0.00	1.00	0.00	47.90	163.46	1.56	0.00	1.00	0.00
48.06	165.71	1.61	0.00	1.00	0.00	48.29	173.91	1.83	0.00	1.00	0.00
48.39	177.31	1.92	0.00	1.00	0.00	48.56	195.51	2.00	0.00	1.00	0.00
48.72	216.75	2.00	0.00	1.00	0.00	48.88	236.12	2.00	0.00	1.00	0.00
49.05	212.69	2.00	0.00	1.00	0.00	49.21	181.19	2.00	0.00	1.00	0.00
49.38	157.70	1.44	0.00	1.00	0.00	49.54	145.37	1.18	0.31	1.00	0.01
49.70	136.19	1.02	0.66	1.00	0.01	49.87	130.75	0.93	1.05	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 0.39

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

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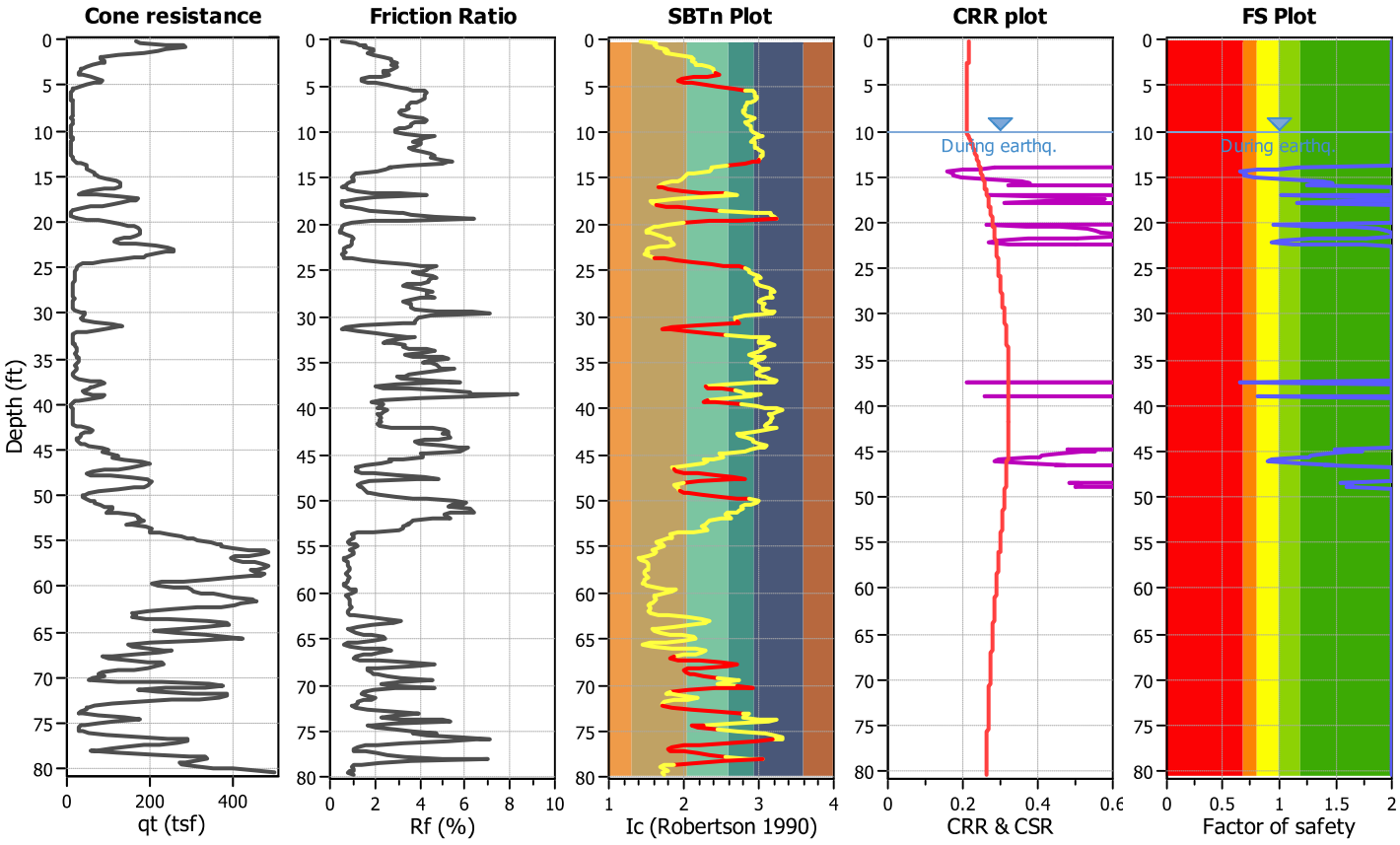
LIQUEFACTION ANALYSIS REPORT

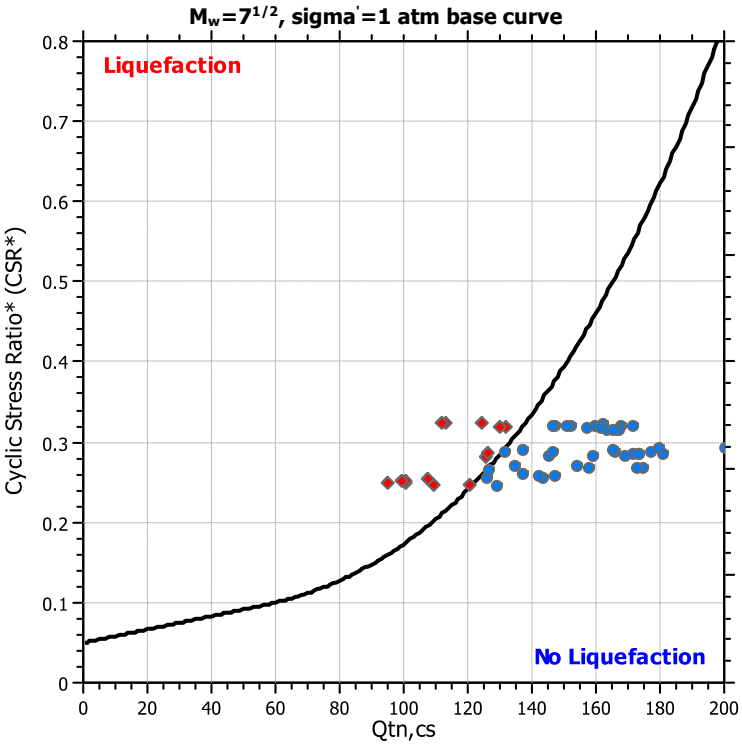
Project title : Quincy Courthouse **Location : Quincy, CA**

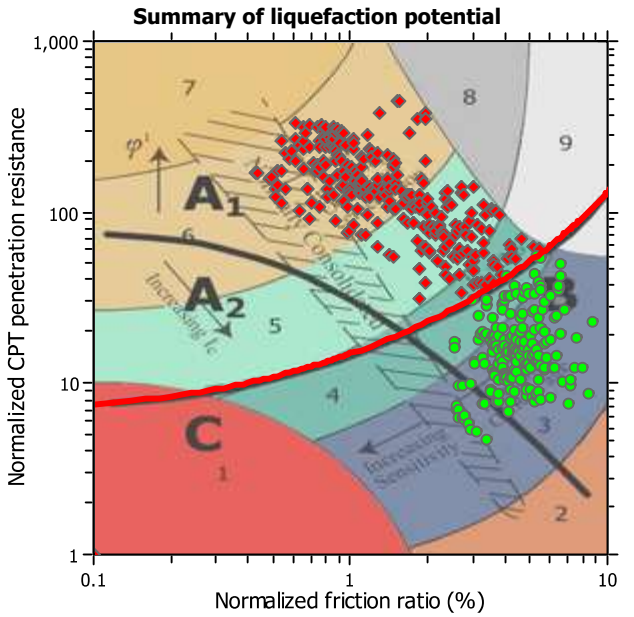
CPT file : CPT-04

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	12.50 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	10.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	50.00 ft
Earthquake magnitude M_w:	5.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.56	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

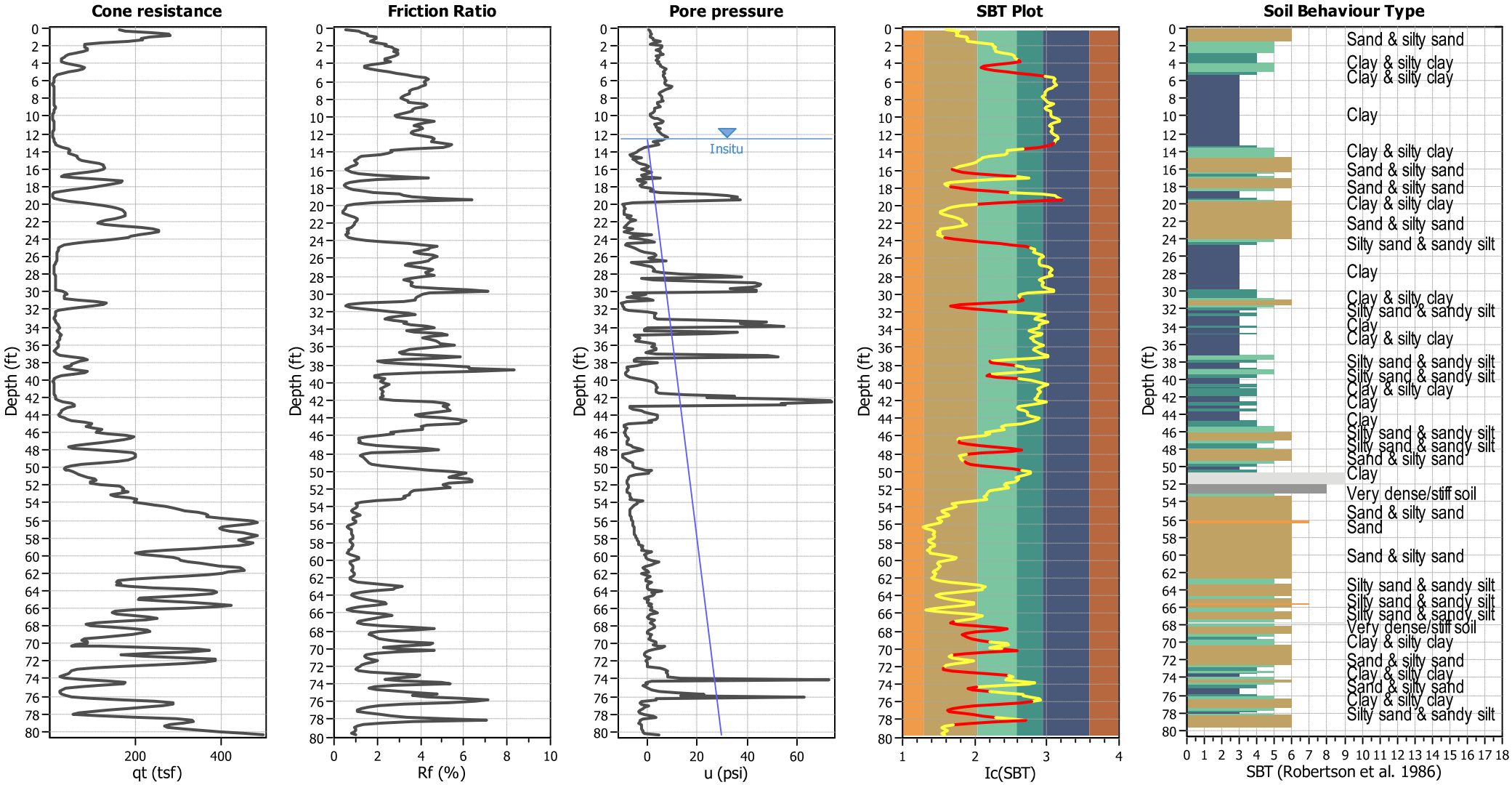






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



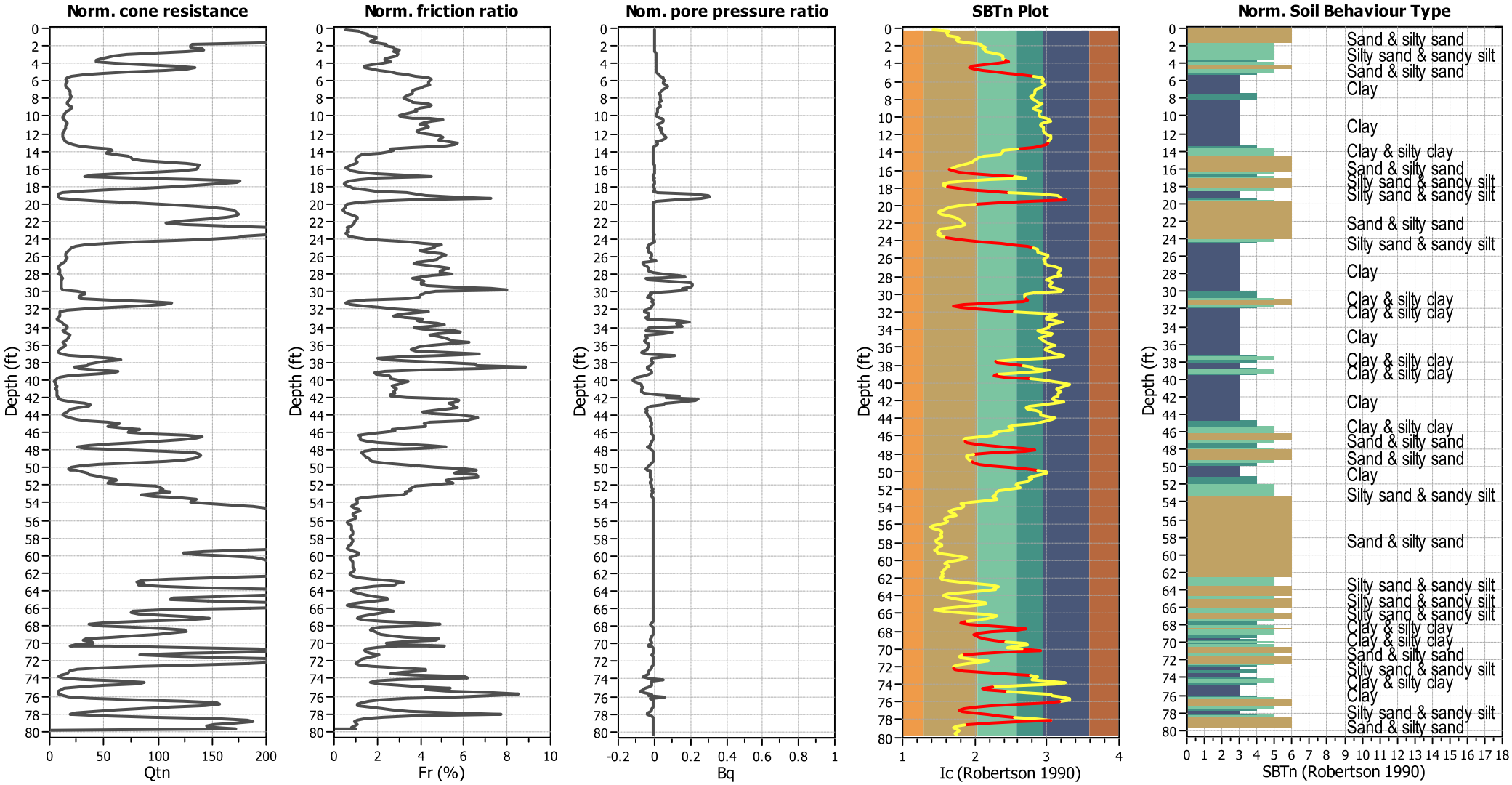
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



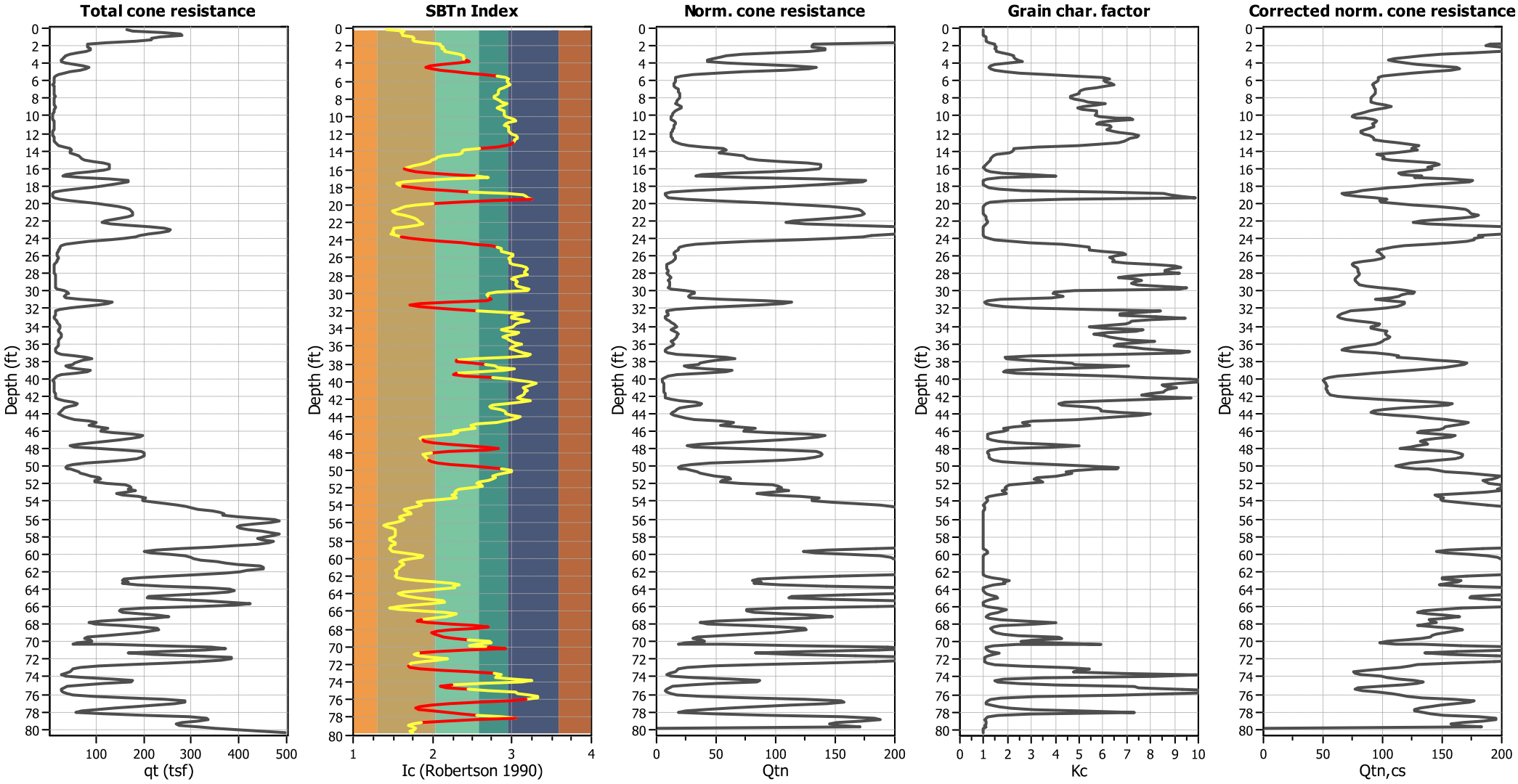
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

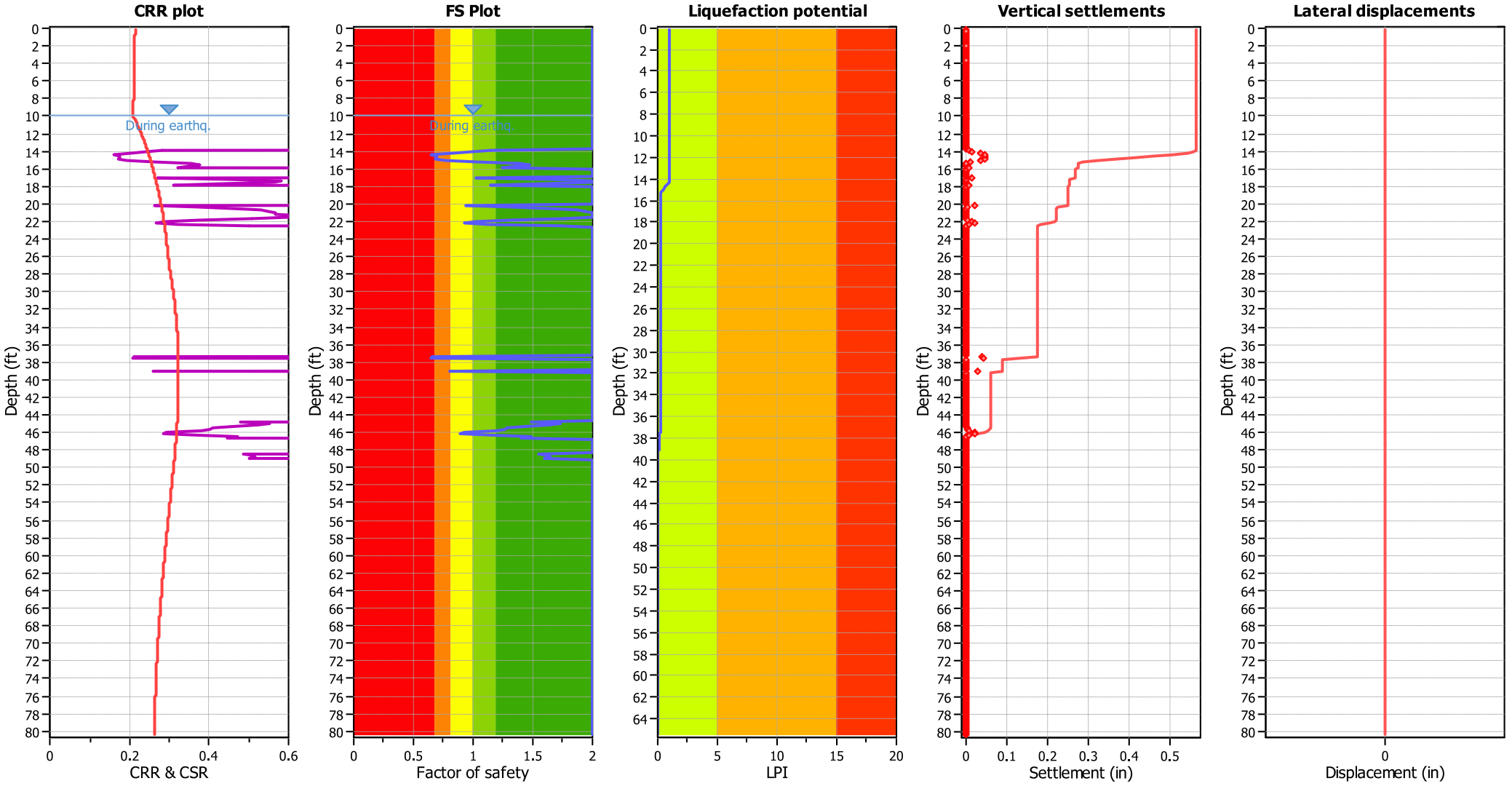
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

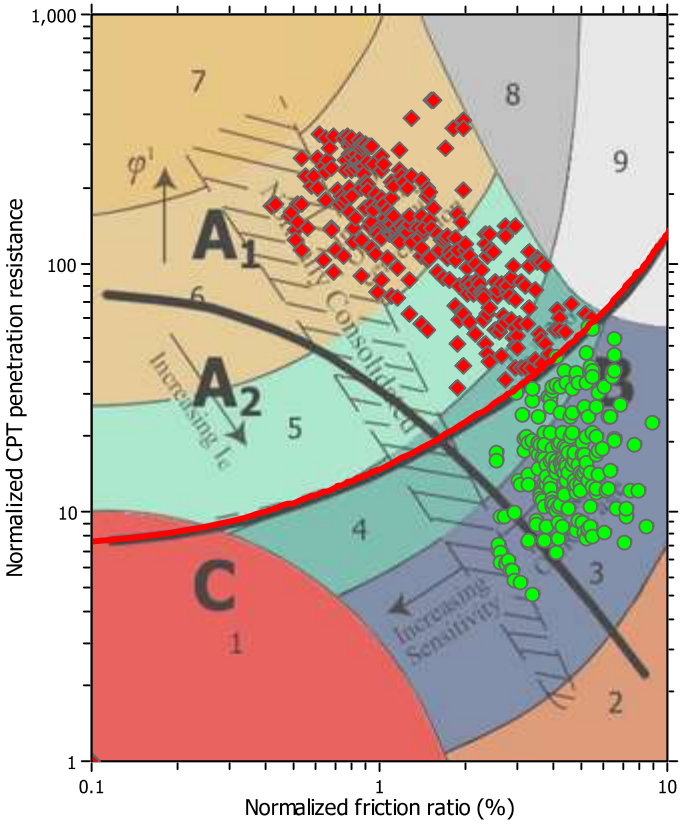
F.S. color scheme

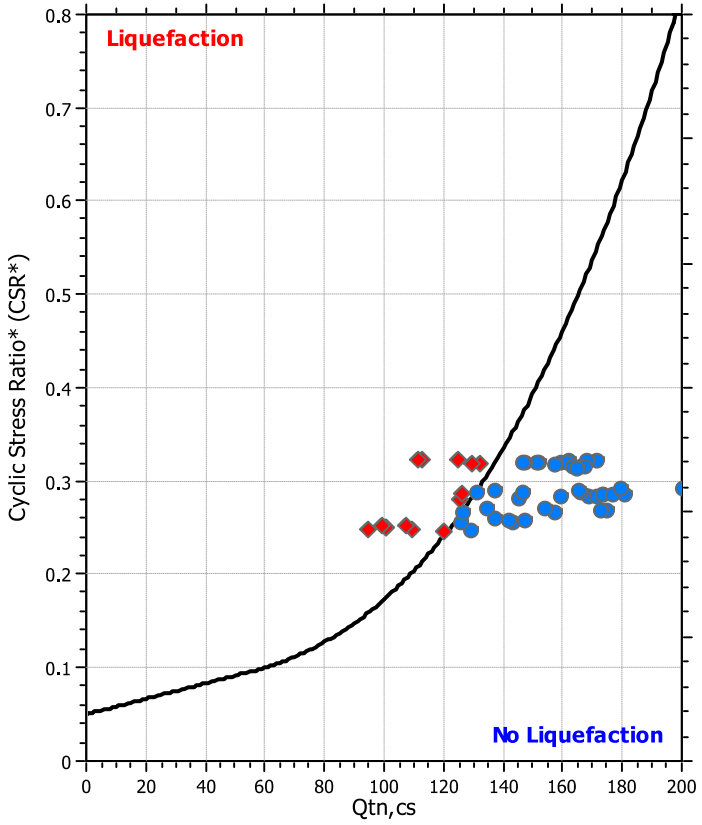
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

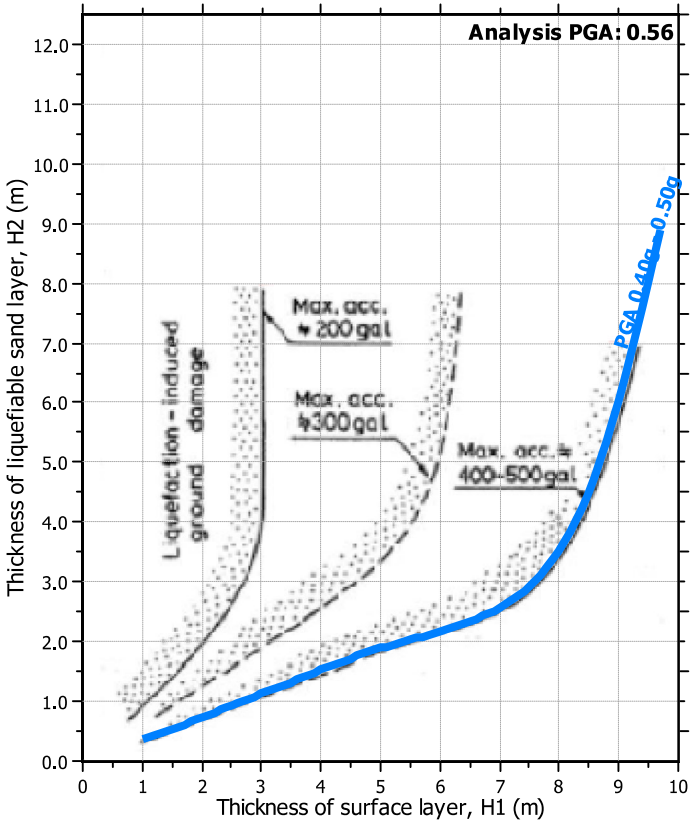
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



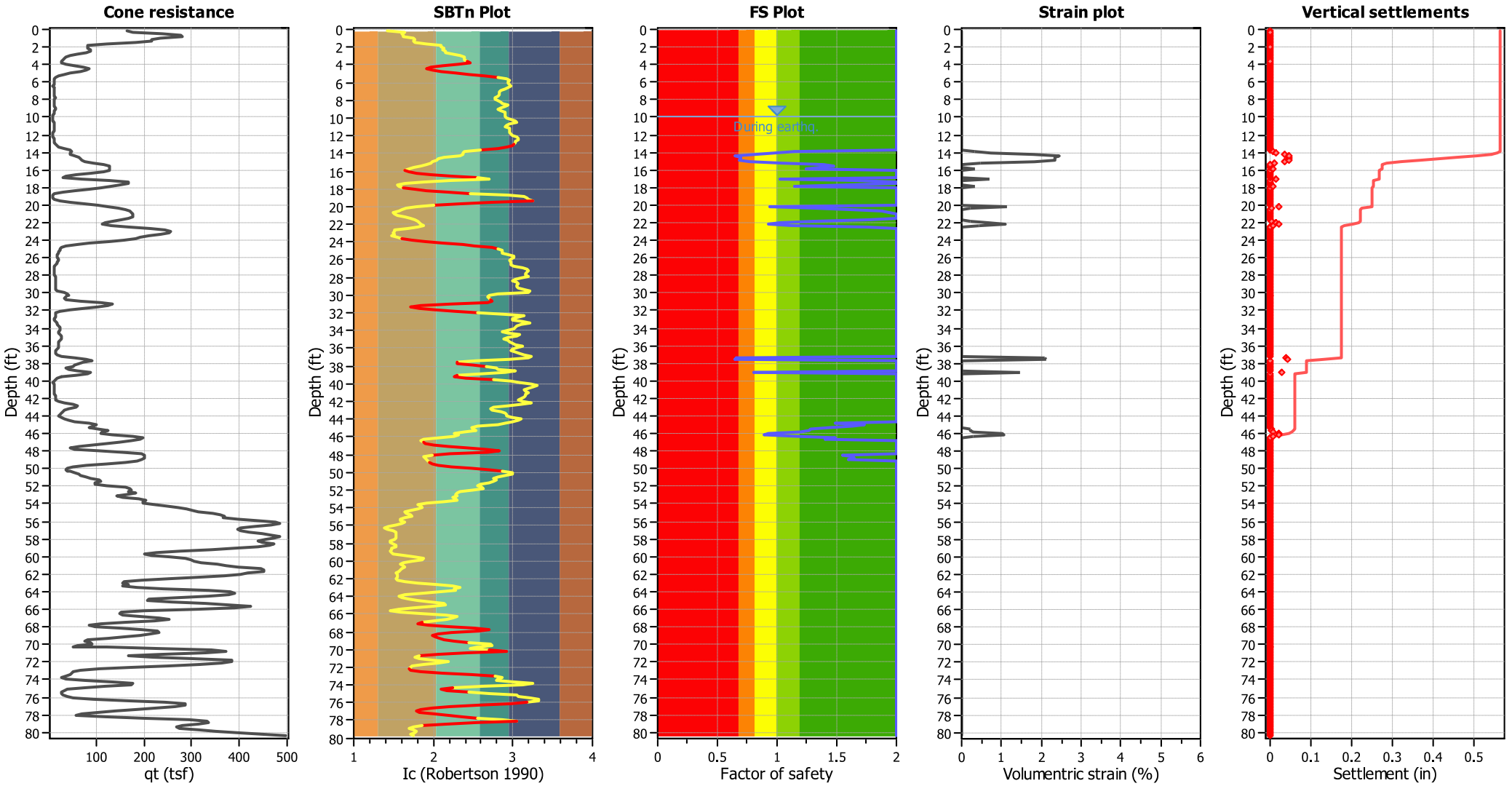




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	10.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	5.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.56	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	12.50 ft	Fill height:	N/A	Limit depth:	50.00 ft

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement of dry sands ::

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
0.16	1.42	262.93	1.00	262.93	45	886	0.21	0.000	0.00	2.41	0.00	0.000
0.33	1.64	283.57	1.00	282.48	52	1267	0.21	0.001	0.00	2.41	0.00	0.000
0.49	1.60	380.23	1.00	380.23	69	1614	0.21	0.001	0.00	2.41	0.00	0.000
0.66	1.63	448.17	1.00	448.17	82	1980	0.21	0.001	0.00	2.41	0.00	0.000
0.82	1.62	452.50	1.00	452.50	82	1975	0.21	0.001	0.00	2.41	0.00	0.000
0.98	1.75	376.69	1.07	404.69	77	1945	0.21	0.001	0.00	2.41	0.00	0.000
1.15	1.78	346.50	1.09	377.83	72	1843	0.21	0.002	0.00	2.41	0.00	0.000
1.31	1.75	347.18	1.07	371.30	70	1777	0.21	0.002	0.00	2.41	0.00	0.000
1.48	1.76	292.66	1.08	316.49	60	1531	0.21	0.003	0.00	2.41	0.00	0.000
1.64	1.91	197.05	1.20	236.61	48	1243	0.21	0.004	0.00	2.41	0.00	0.000
1.80	2.09	131.67	1.44	189.96	41	1045	0.21	0.005	0.00	2.41	0.00	0.000
1.97	2.09	130.01	1.43	186.57	40	1026	0.21	0.005	0.00	2.41	0.00	0.000
2.13	2.14	129.98	1.53	198.92	44	1093	0.21	0.006	0.00	2.41	0.00	0.000
2.30	2.12	141.20	1.49	209.92	46	1155	0.21	0.006	0.00	2.41	0.00	0.000
2.46	2.15	141.88	1.55	219.56	48	1206	0.21	0.006	0.00	2.41	0.00	0.000
2.62	2.15	127.80	1.55	197.52	44	1085	0.21	0.007	0.00	2.41	0.00	0.000
2.79	2.24	98.43	1.78	175.01	40	944	0.21	0.009	0.00	2.41	0.00	0.000
2.95	2.34	71.40	2.08	148.65	36	774	0.21	0.013	0.01	2.41	0.00	0.000
3.12	2.39	59.13	2.25	133.33	33	679	0.21	0.017	0.01	2.41	0.00	0.000
3.28	2.39	53.51	2.27	121.68	30	619	0.21	0.022	0.01	2.41	0.01	0.000
3.44	2.40	47.53	2.30	109.37	27	554	0.21	0.030	0.02	2.41	0.01	0.000
3.61	2.43	42.97	2.44	105.01	26	523	0.21	0.037	0.03	2.41	0.01	0.000
3.77	2.46	42.83	2.60	111.13	0	0	0.21	0.000	0.00	0.00	0.00	0.000
3.94	2.32	59.01	2.02	119.42	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.10	2.12	86.44	1.49	128.87	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.27	1.96	115.18	1.26	144.68	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.43	1.92	134.55	1.21	162.49	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.59	1.99	127.53	1.29	164.80	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.76	2.10	107.28	1.46	156.73	0	0	0.21	0.000	0.00	0.00	0.00	0.000
4.92	2.29	73.60	1.91	140.62	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.09	2.44	49.72	2.50	124.46	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.25	2.65	30.77	3.64	111.85	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.41	2.80	20.74	4.81	99.85	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.58	2.93	16.12	5.98	96.39	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.74	2.95	15.32	6.25	95.79	0	0	0.21	0.000	0.00	0.00	0.00	0.000
5.91	2.94	15.89	6.07	96.37	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.07	2.94	15.59	6.10	95.02	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.23	2.96	14.70	6.32	92.93	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.40	2.98	14.16	6.47	91.69	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.56	2.94	15.16	6.08	92.13	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.73	2.91	16.21	5.75	93.24	0	0	0.21	0.000	0.00	0.00	0.00	0.000
6.89	2.85	17.78	5.27	93.65	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.05	2.83	18.58	5.06	94.11	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.22	2.82	18.88	4.98	93.96	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.38	2.82	18.93	4.98	94.26	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.55	2.80	19.27	4.82	92.83	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.71	2.78	19.78	4.62	91.46	0	0	0.21	0.000	0.00	0.00	0.00	0.000
7.87	2.78	19.41	4.65	90.17	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.04	2.80	18.71	4.82	90.19	0	0	0.21	0.000	0.00	0.00	0.00	0.000

:: Post-earthquake settlement of dry sands :: (continued)

Depth (ft)	Ic	Q_{tn}	Kc	$Q_{tn,cs}$	$N_{1,60}$ (blows)	G_{max} (tsf)	CSR	Shear, γ (%)	$e_{vol(15)}$ (%)	N_c	e_v (%)	Settle. (in)
8.20	2.84	17.53	5.18	90.79	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.37	2.86	16.75	5.36	89.80	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.53	2.94	15.76	6.07	95.68	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.69	2.90	17.84	5.71	101.90	0	0	0.21	0.000	0.00	0.00	0.00	0.000
8.86	2.85	20.50	5.21	106.80	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.02	2.82	20.58	4.95	101.93	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.19	2.84	18.62	5.14	95.72	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.35	2.90	15.52	5.75	89.16	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.51	2.90	14.92	5.71	85.24	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.68	2.90	14.02	5.72	80.13	0	0	0.21	0.000	0.00	0.00	0.00	0.000
9.84	2.90	13.35	5.68	75.87	0	0	0.21	0.000	0.00	0.00	0.00	0.000

Total estimated settlement: 0.00

Abbreviations

Q_{tn}: Equivalent clean sand normalized cone resistance
K_c: Fines correction factor
$Q_{tn,cs}$: Post-liquefaction volumentric strain
G_{max}: Small strain shear modulus
CSR: Soil cyclic stress ratio
γ: Cyclic shear strain
$e_{vol(15)}$: Volumetric strain after 15 cycles
N_c: Equivalent number of cycles
e_v: Volumetric strain
Settle.: Calculated settlement

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
10.01	74.90	2.00	0.00	1.00	0.00	10.17	77.95	2.00	0.00	1.00	0.00
10.33	85.07	2.00	0.00	1.00	0.00	10.50	92.67	2.00	0.00	1.00	0.00
10.66	95.71	2.00	0.00	1.00	0.00	10.83	93.84	2.00	0.00	1.00	0.00
10.99	91.97	2.00	0.00	1.00	0.00	11.15	92.61	2.00	0.00	1.00	0.00
11.32	92.56	2.00	0.00	1.00	0.00	11.48	89.36	2.00	0.00	1.00	0.00
11.65	85.39	2.00	0.00	1.00	0.00	11.81	82.24	2.00	0.00	1.00	0.00
11.98	82.08	2.00	0.00	1.00	0.00	12.14	84.46	2.00	0.00	1.00	0.00
12.30	88.65	2.00	0.00	1.00	0.00	12.47	91.08	2.00	0.00	1.00	0.00
12.63	92.18	2.00	0.00	1.00	0.00	12.80	92.48	2.00	0.00	1.00	0.00
12.96	101.38	2.00	0.00	1.00	0.00	13.12	112.14	2.00	0.00	1.00	0.00
13.29	121.52	2.00	0.00	1.00	0.00	13.45	130.72	2.00	0.00	1.00	0.00
13.62	127.17	2.00	0.00	1.00	0.00	13.78	124.60	2.00	0.00	1.00	0.00
13.94	129.51	1.15	0.34	1.00	0.01	14.11	120.44	0.98	0.74	1.00	0.01
14.27	109.40	0.82	1.78	1.00	0.04	14.44	94.96	0.64	2.44	1.00	0.05
14.60	100.53	0.70	2.33	1.00	0.05	14.76	100.71	0.70	2.32	1.00	0.05
14.93	99.44	0.68	2.35	1.00	0.05	15.09	107.50	0.77	1.83	1.00	0.04
15.26	126.45	1.05	0.47	1.00	0.01	15.42	143.61	1.39	0.00	1.00	0.00
15.58	147.48	1.48	0.00	1.00	0.00	15.75	142.30	1.35	0.00	1.00	0.00
15.91	137.59	1.25	0.32	1.00	0.01	16.08	141.44	2.00	0.00	1.00	0.00
16.24	134.37	2.00	0.00	1.00	0.00	16.40	121.03	2.00	0.00	1.00	0.00
16.57	112.85	2.00	0.00	1.00	0.00	16.73	116.06	2.00	0.00	1.00	0.00
16.90	132.34	2.00	0.00	1.00	0.00	17.06	127.00	1.02	0.71	1.00	0.01
17.22	157.85	1.68	0.00	1.00	0.00	17.39	175.19	2.00	0.00	1.00	0.00
17.55	173.37	2.00	0.00	1.00	0.00	17.72	154.50	1.58	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
17.88	135.19	1.15	0.33	1.00	0.01	18.04	123.62	2.00	0.00	1.00	0.00
18.21	106.22	2.00	0.00	1.00	0.00	18.37	94.04	2.00	0.00	1.00	0.00
18.54	82.78	2.00	0.00	1.00	0.00	18.70	77.37	2.00	0.00	1.00	0.00
18.86	65.58	2.00	0.00	1.00	0.00	19.03	68.83	2.00	0.00	1.00	0.00
19.19	78.75	2.00	0.00	1.00	0.00	19.36	94.01	2.00	0.00	1.00	0.00
19.52	103.62	2.00	0.00	1.00	0.00	19.69	97.48	2.00	0.00	1.00	0.00
19.85	98.83	2.00	0.00	1.00	0.00	20.01	112.13	2.00	0.00	1.00	0.00
20.18	125.46	0.94	1.12	1.00	0.02	20.34	145.71	1.31	0.22	1.00	0.00
20.51	159.57	1.62	0.00	1.00	0.00	20.67	169.26	1.88	0.00	1.00	0.00
20.83	171.61	1.94	0.00	1.00	0.00	21.00	173.76	2.00	0.00	1.00	0.00
21.16	173.83	2.00	0.00	1.00	0.00	21.33	180.96	2.00	0.00	1.00	0.00
21.49	177.44	2.00	0.00	1.00	0.00	21.65	166.23	1.77	0.00	1.00	0.00
21.82	146.80	1.31	0.22	1.00	0.00	21.98	131.70	1.02	0.68	1.00	0.01
22.15	126.05	0.93	1.11	1.00	0.02	22.31	137.59	1.12	0.45	1.00	0.01
22.47	165.58	1.74	0.00	1.00	0.00	22.64	205.22	2.00	0.00	1.00	0.00
22.80	232.61	2.00	0.00	1.00	0.00	22.97	244.45	2.00	0.00	1.00	0.00
23.13	241.72	2.00	0.00	1.00	0.00	23.29	224.21	2.00	0.00	1.00	0.00
23.46	200.72	2.00	0.00	1.00	0.00	23.62	180.08	2.00	0.00	1.00	0.00
23.79	184.01	2.00	0.00	1.00	0.00	23.95	177.14	2.00	0.00	1.00	0.00
24.11	176.72	2.00	0.00	1.00	0.00	24.28	170.52	2.00	0.00	1.00	0.00
24.44	156.97	2.00	0.00	1.00	0.00	24.61	139.16	2.00	0.00	1.00	0.00
24.77	117.83	2.00	0.00	1.00	0.00	24.93	108.99	2.00	0.00	1.00	0.00
25.10	102.32	2.00	0.00	1.00	0.00	25.26	96.28	2.00	0.00	1.00	0.00
25.43	95.12	2.00	0.00	1.00	0.00	25.59	97.19	2.00	0.00	1.00	0.00
25.75	99.15	2.00	0.00	1.00	0.00	25.92	100.30	2.00	0.00	1.00	0.00
26.08	100.66	2.00	0.00	1.00	0.00	26.25	98.35	2.00	0.00	1.00	0.00
26.41	92.12	2.00	0.00	1.00	0.00	26.57	82.46	2.00	0.00	1.00	0.00
26.74	75.90	2.00	0.00	1.00	0.00	26.90	73.91	2.00	0.00	1.00	0.00
27.07	75.23	2.00	0.00	1.00	0.00	27.23	78.34	2.00	0.00	1.00	0.00
27.40	79.54	2.00	0.00	1.00	0.00	27.56	79.11	2.00	0.00	1.00	0.00
27.72	79.02	2.00	0.00	1.00	0.00	27.89	80.15	2.00	0.00	1.00	0.00
28.05	80.92	2.00	0.00	1.00	0.00	28.22	79.66	2.00	0.00	1.00	0.00
28.38	77.49	2.00	0.00	1.00	0.00	28.54	76.72	2.00	0.00	1.00	0.00
28.71	77.07	2.00	0.00	1.00	0.00	28.87	77.85	2.00	0.00	1.00	0.00
29.04	78.84	2.00	0.00	1.00	0.00	29.20	80.06	2.00	0.00	1.00	0.00
29.36	87.12	2.00	0.00	1.00	0.00	29.53	97.94	2.00	0.00	1.00	0.00
29.69	110.88	2.00	0.00	1.00	0.00	29.86	120.50	2.00	0.00	1.00	0.00
30.02	127.30	2.00	0.00	1.00	0.00	30.18	125.43	2.00	0.00	1.00	0.00
30.35	120.93	2.00	0.00	1.00	0.00	30.51	115.74	2.00	0.00	1.00	0.00
30.68	112.93	2.00	0.00	1.00	0.00	30.84	107.25	2.00	0.00	1.00	0.00
31.00	93.35	2.00	0.00	1.00	0.00	31.17	104.48	2.00	0.00	1.00	0.00
31.33	118.02	2.00	0.00	1.00	0.00	31.50	118.68	2.00	0.00	1.00	0.00
31.66	115.26	2.00	0.00	1.00	0.00	31.82	112.34	2.00	0.00	1.00	0.00
31.99	103.10	2.00	0.00	1.00	0.00	32.15	90.40	2.00	0.00	1.00	0.00
32.32	73.59	2.00	0.00	1.00	0.00	32.48	68.91	2.00	0.00	1.00	0.00
32.64	66.17	2.00	0.00	1.00	0.00	32.81	63.23	2.00	0.00	1.00	0.00
32.97	61.93	2.00	0.00	1.00	0.00	33.14	64.07	2.00	0.00	1.00	0.00
33.30	69.35	2.00	0.00	1.00	0.00	33.46	78.79	2.00	0.00	1.00	0.00
33.63	90.41	2.00	0.00	1.00	0.00	33.79	97.81	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
33.96	96.72	2.00	0.00	1.00	0.00	34.12	90.19	2.00	0.00	1.00	0.00
34.28	90.48	2.00	0.00	1.00	0.00	34.45	96.76	2.00	0.00	1.00	0.00
34.61	103.60	2.00	0.00	1.00	0.00	34.78	102.13	2.00	0.00	1.00	0.00
34.94	102.96	2.00	0.00	1.00	0.00	35.10	104.11	2.00	0.00	1.00	0.00
35.27	106.63	2.00	0.00	1.00	0.00	35.43	104.46	2.00	0.00	1.00	0.00
35.60	101.49	2.00	0.00	1.00	0.00	35.76	100.46	2.00	0.00	1.00	0.00
35.93	97.96	2.00	0.00	1.00	0.00	36.09	93.48	2.00	0.00	1.00	0.00
36.25	84.11	2.00	0.00	1.00	0.00	36.42	75.09	2.00	0.00	1.00	0.00
36.58	68.22	2.00	0.00	1.00	0.00	36.75	65.86	2.00	0.00	1.00	0.00
36.91	75.00	2.00	0.00	1.00	0.00	37.07	94.37	2.00	0.00	1.00	0.00
37.24	106.66	2.00	0.00	1.00	0.00	37.40	112.88	0.66	2.07	1.00	0.04
37.57	111.65	0.65	2.13	1.00	0.04	37.73	128.89	2.00	0.00	1.00	0.00
37.89	142.57	2.00	0.00	1.00	0.00	38.06	164.00	2.00	0.00	1.00	0.00
38.22	170.40	2.00	0.00	1.00	0.00	38.39	168.01	2.00	0.00	1.00	0.00
38.55	160.56	2.00	0.00	1.00	0.00	38.71	152.59	2.00	0.00	1.00	0.00
38.88	139.81	2.00	0.00	1.00	0.00	39.04	124.69	0.80	1.47	1.00	0.03
39.21	108.81	2.00	0.00	1.00	0.00	39.37	92.07	2.00	0.00	1.00	0.00
39.53	77.71	2.00	0.00	1.00	0.00	39.70	62.62	2.00	0.00	1.00	0.00
39.86	54.77	2.00	0.00	1.00	0.00	40.03	50.71	2.00	0.00	1.00	0.00
40.19	50.24	2.00	0.00	1.00	0.00	40.35	51.16	2.00	0.00	1.00	0.00
40.52	52.58	2.00	0.00	1.00	0.00	40.68	52.49	2.00	0.00	1.00	0.00
40.85	53.14	2.00	0.00	1.00	0.00	41.01	52.24	2.00	0.00	1.00	0.00
41.17	52.99	2.00	0.00	1.00	0.00	41.34	53.46	2.00	0.00	1.00	0.00
41.50	54.24	2.00	0.00	1.00	0.00	41.67	54.72	2.00	0.00	1.00	0.00
41.83	56.26	2.00	0.00	1.00	0.00	41.99	62.30	2.00	0.00	1.00	0.00
42.16	76.92	2.00	0.00	1.00	0.00	42.32	96.80	2.00	0.00	1.00	0.00
42.49	120.82	2.00	0.00	1.00	0.00	42.65	144.94	2.00	0.00	1.00	0.00
42.81	158.60	2.00	0.00	1.00	0.00	42.98	155.32	2.00	0.00	1.00	0.00
43.14	136.41	2.00	0.00	1.00	0.00	43.31	116.03	2.00	0.00	1.00	0.00
43.47	101.66	2.00	0.00	1.00	0.00	43.64	92.93	2.00	0.00	1.00	0.00
43.80	89.73	2.00	0.00	1.00	0.00	43.96	95.09	2.00	0.00	1.00	0.00
44.13	109.39	2.00	0.00	1.00	0.00	44.29	128.11	2.00	0.00	1.00	0.00
44.46	139.09	2.00	0.00	1.00	0.00	44.62	154.23	2.00	0.00	1.00	0.00
44.78	162.38	1.49	0.00	1.00	0.00	44.95	172.06	1.73	0.00	1.00	0.00
45.11	168.21	1.63	0.00	1.00	0.00	45.28	159.99	1.44	0.00	1.00	0.00
45.44	152.46	1.28	0.21	1.00	0.00	45.60	151.51	1.26	0.22	1.00	0.00
45.77	147.72	1.19	0.31	1.00	0.01	45.93	131.93	0.92	1.04	1.00	0.02
46.10	129.84	0.89	1.07	1.00	0.02	46.26	146.75	1.18	0.31	1.00	0.01
46.42	161.56	1.49	0.00	1.00	0.00	46.59	157.71	1.40	0.00	1.00	0.00
46.75	144.85	2.00	0.00	1.00	0.00	46.92	135.53	2.00	0.00	1.00	0.00
47.08	131.59	2.00	0.00	1.00	0.00	47.24	136.10	2.00	0.00	1.00	0.00
47.41	137.41	2.00	0.00	1.00	0.00	47.57	128.98	2.00	0.00	1.00	0.00
47.74	123.47	2.00	0.00	1.00	0.00	47.90	114.50	2.00	0.00	1.00	0.00
48.06	136.51	2.00	0.00	1.00	0.00	48.23	157.38	2.00	0.00	1.00	0.00
48.39	163.46	1.55	0.00	1.00	0.00	48.56	166.73	1.63	0.00	1.00	0.00
48.72	167.49	1.65	0.00	1.00	0.00	48.88	165.32	1.60	0.00	1.00	0.00
49.05	160.53	2.00	0.00	1.00	0.00	49.21	147.94	2.00	0.00	1.00	0.00
49.38	134.26	2.00	0.00	1.00	0.00	49.54	122.69	2.00	0.00	1.00	0.00
49.70	116.48	2.00	0.00	1.00	0.00	49.87	111.16	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 0.56

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

APPENDIX VI
ENVIRONMENTAL LABORATORY TESTING

Enthalpy Analytical
931 West Barkley Ave
Orange, CA 92868
(714) 771-6900

enthalpy.com

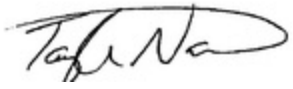
Lab Job Number : 542509
Report Level : II
Report Date : 09/30/2025

Analytical Report *prepared for:*

Jalal Fatemi
Atlas Technical Consultants
9085 Aero Dr
Suite B
San Diego, CA 92123

Location: Quincy Courthouse

Authorized for release by:



Taylor Nasu, Project Manager
Taylor.Nasu@enthalpy.com

This data package has been reviewed for technical correctness and completeness. Release of this data has been authorized by the Laboratory Manager or the Manager's designee, as verified by the above signature which applies to this PDF file as well as any associated electronic data deliverable files. The results contained in this report meet all requirements of NELAP and pertain only to those samples which were submitted for analysis. This report may be reproduced only in its entirety.

CA ELAP# 1338, CA ELAP #1338-S1, NELAP# 4038, SCAQMD LAP# 18LA0518, LACSD ID# 10105, ORELAP# 4197

ENTHALPY ANALYTICAL

Sample Summary

Jalal Fatemi
Atlas Technical Consultants
9085 Aero Dr
Suite B
San Diego, CA 92123

Lab Job #: 542509
Location: Quincy Courthouse
Date Received: 09/18/25

Sample ID	Lab ID	Collected	Matrix
B-7 @1-2.5'	542509-001	09/17/25 10:13	Soil
B-7 @ 5'	542509-002	09/17/25 10:19	Soil
B-8 @1-5'	542509-003	09/17/25 07:30	Soil
B-10 @2.5'	542509-004	09/17/25 12:27	Soil
B-9 @ 1-5'	542509-005	09/17/25 13:23	Soil
B-11 @ 3'	542509-006	09/17/25 13:54	Soil

Case Narrative

Atlas Technical Consultants
9085 Aero Dr
Suite B
San Diego, CA 92123
Jalal Fatemi

Lab Job Number: 542509
Location: Quincy Courthouse
Date Received: 09/18/25

This data package contains sample and QC results for three soil samples, requested for the above referenced project on 09/19/25. The samples were received in good condition.

TPH-Extractables by GC (EPA 8015M):
No analytical problems were encountered.

Metals (EPA 6010B and EPA 7471A):

- Low recoveries were observed for antimony in the MS/MSD for batch 382723; the parent sample was not a project sample, the LCS was within limits, and the associated RPD was within limits. High recovery was observed for barium in the MSD for batch 382723; the LCS was within limits, and the associated RPD was within limits.
- No other analytical problems were encountered.

Asbestos by PLM (EPA 600/R-93-116):
AmeriSci Los Angeles in Carson, CA performed the analysis (see sublab report section for certifications). Please see the AmeriSci Los Angeles case narrative.

ENTHALPY ANALYTICAL

Login 542509

Chain of Custody Record

Lab No: 542509

Page: of

Turn Around Time (rush by advanced notice only)

Standard:	X	5 Day:		3 Day:	
2 Day:		1 Day:		Custom TAT:	

Matrix: A = Air, S = Soil/Solid, W = Water, DW = Drinking Water, P = Product, O = Oil, SD = Sediment, T = Tissue, WP = Wipe, WW = Wastewater, X = Other

Sample Type: C = Composite, G = Grab or Discrete, B = Blank, O = Other

Preservatives: 0 = none, 1 = $Na_2S_2O_3$, 2 = HCl, 3 = HNO_3, 4 = H_2SO_4, 5 = NaOH, 6 = Other

Sample Receipt Temp and Notes: (lab use only)

CUSTOMER INFORMATION

Company:	Atlas Technical Consultants
Report To:	Jalal Fatemi
Email:	jalaleddin.fatemi@oneatlas.com
Address:	9085 Aero Drive, Suite B
	San Diego, CA 92123
Phone:	858.868.0096
Fax:	

PROJECT INFORMATION

Name:	Quincy Courthouse
Number:	91-65859-PW
P.O. #:	
Address:	257 Lawrence Street
	Quincy, California
Global ID:	
Sampled By:	KBH

	Sample ID	Sampling Date	Sampling Time (24 hr)	Matrix	Sample Type	Pres.	Cont. No.	Cont. Size	Initials	CAM17 Metals (6010B)	TPH (C6-C44) (8015M)	PLM Asbestos epa/600/R-93/116	Test Instructions / Comments
1	B-7 @ 1-2.5'	9/17/25	1013	S	G	0	1	8oz	KH	X	X	X	
2	B-7 @ 5'	9/17/25	1019	S	G	0	1	8oz	KH	X	X	X	
3	B-8 @ 1-5'	9/17/25	0730	S	G	0	1	8oz	KH	X	X	X	
4	B-10 @ 2.5'	9/17/25	1227	S	G	0	1	8oz	KH	X	X	X	
5	B-9 at 1-5	9/17/25	1323	S	G	0	1	8oz	KH	X	X	X	
6	B-11 @ 3'	9/17/25	1354	S	G	0	1	8oz	KH	X	X	X	
7													
8													
9													
10													

	Signature	Print Name	Company / Title	Date / Time
1 Relinquished By:		Kyle Hahn	Atlas / PG	9/18/25 / 1439
1 Received By:	Brenda Hamilton	Brenda Hamilton	EA / SCM	9/18/25 1429
2 Relinquished By:	Brenda Hamilton	Brenda Hamilton	EA / SCM	9/18/25 1800
2 Received By:		JXR	EA	9/19/25 0830
3 Relinquished By:				
3 Received By:				

SAMPLE RECEIPT CHECKLIST

Section 1: General Info
Date Received: 9/18/25 WO# 542509 Client: Atlas

Section 2: Shipping / Custody **Are custody seals present?** ☐ Yes ☑ No
Custody seals intact on arrival? ☑ N/A ☐ Yes ☐ No ☐ On cooler / box ☐ On samples
☐ Courier ☒ Walk-In ☐ Field Sampling ☐ Shipping Info: _____

Section 3a: Condition / Packaging ☐ **Outside 0.0 - 6.0°C (0.0 - 10.0°C for microbiology) (PM notified)**
Date Opened 9/18/25 By (initials) KM Type of ice used: ☒ Wet ☐ Blue/Gel ☐ None
☐ Samples received on ice directly from the field; cooling process had begun. (if checked, skip temperatures)
☐ Sample matrix doesn't require cooling (e.g. air, bulk PCB). (if checked, skip temperatures)
If no cooler: Observed/Adjusted Temp (°C): _____ / _____ Thermometer/IR Gun: IR16 CF: +0.1 °C
Cooler Temp (°C) #1: 4.6 / 4.7 #2: ____/____ #3: ____/____ #4: ____/____ #5: ____/____ #6: ____/____

Section 3b: Microbiology Samples ☒ **No microbiology samples submitted (skip 3b)**
☐ Within temp range 0.0 - 10.0°C or received on ice directly from field.
☐ Adequate headspace for microbiology analysis.

Section 3c: Air Samples ☒ **No air samples submitted (skip 3c)**
☐ 1.4L Canisters ☐ 6L Canisters ☐ Tedlar Bags ☐ MCE Cassettes ☐ Sorbent Tubes ☐ Other_____

Section 4: Containers / Labels / Samples	YES	NO	N/A
1) Were custody papers present, filled properly, and legible?	X		
2) Is the sampler's name present on the CoC?	X		
3) Were containers received in good condition (unbroken / unopened / uncompromised)?	X		
4) Were the samples bagged? (required for microbiology samples; recommended for soil samples)	X		
5) Were all of, and only, the correct samples received?	X		
6) Are sample labels present, legible, and in agreement with the CoC?	X		
7) Does the container count match the CoC?	X		
8) Was sufficient sample volume / mass received for the analyses requested?	X		
9) Were samples received in proper containers for the analyses requested?	X		
10) Were samples received with > 1/2 holding time remaining?	X		
11) Are samples properly preserved as indicated by CoC / labels?	X		
12) Unpreserved VOAs received - If necessary, was the hold time changed in LIMS?			X
13) Are VOA vials free from headspace/bubbles > 6mm?			

Section 5: Explanations / Comments
(If no comments are made, then no discrepancies noted.)

☐ **No additional discrepancies**

Date Logged 9/18/25 **By (print)** Brenda Hamilton **(sign)** Brenda Hamilton
Date Labeled 9/18/25 **By (print)** Brenda Hamilton **(sign)** Brenda Hamilton

SAMPLE RECEIPT CHECKLIST

Section 1: General Info

Date Received: 9/19/25 WO# 542509 Client: Atlas

Section 2: Shipping / Custody **Are custody seals present?** ☒ **Yes** ☐ **No**

Custody seals intact on arrival? ☐ N/A ■ Yes ☐ No ■ On cooler / box ☐ On samples

☐ Courier ☐ Walk-In ☐ Field Sampling ■ Shipping Info: INTRASTATE

Section 3a: Condition / Packaging ☐ **Outside 0.0 - 6.0°C (0.0 - 10.0°C for microbiology) (PM notified)**

Date Opened 9/19/25 By (initials) JXR Type of ice used: ■ Wet ☐ Blue/Gel ☐ None

☐ Samples received on ice directly from the field; cooling process had begun. (if checked, skip temperatures)

☐ Sample matrix doesn't require cooling (e.g. air, bulk PCB). (if checked, skip temperatures)

If no cooler: Observed/Adjusted Temp (°C): _____ / _____ Thermometer/IR Gun: IR13 CF: +0.0

Cooler Temp (°C) #1: 2.0 / 2.0 #2: ____/____ #3: ____/____ #4: ____/____ #5: ____/____ #6: ____/____

Section 3b: Microbiology Samples ■ **No microbiology samples submitted (skip 3b)**

☐ Within temp range 0.0 - 10.0°C or received on ice directly from field.

☐ Adequate headspace for microbiology analysis.

Section 3c: Air Samples ■ **No air samples submitted (skip 3c)**

☐ 1.4L Canisters ☐ 6L Canisters ☐ Tedlar Bags ☐ MCE Cassettes ☐ Sorbent Tubes ☐ Other _____

Section 4: Containers / Labels / Samples	YES	NO	N/A
1) Were custody papers present, filled properly, and legible?	X		
2) Is the sampler's name present on the CoC?	X		
3) Were containers received in good condition (unbroken / unopened / uncompromised)?	X		
4) Were the samples bagged? (required for microbiology samples; recommended for soil samples)	X		
5) Were all of, and only, the correct samples received?	X		
6) Are sample labels present, legible, and in agreement with the CoC?	X		
7) Does the container count match the CoC?	X		
8) Was sufficient sample volume / mass received for the analyses requested?	X		
9) Were samples received in proper containers for the analyses requested?	X		
10) Were samples received with > 1/2 holding time remaining?	X		
11) Are samples properly preserved as indicated by CoC / labels?	X		
12) Unpreserved VOAs received - If necessary, was the hold time changed in LIMS?			X
13) Are VOA vials free from headspace/bubbles > 6mm?			X

Section 5: Explanations / Comments

(If no comments are made, then no discrepancies noted.)

☐ **No additional discrepancies**

Date Logged 9/18/25 **By (print)** SAC **(sign)** _____

Date Labeled 9/18/25 **By (print)** SAC **(sign)** _____

ENTHALPY ANALYTICAL

Analysis Results for 542509

Jalal Fatemi
Atlas Technical Consultants
9085 Aero Dr
Suite B
San Diego, CA 92123

Lab Job #: 542509
Location: Quincy Courthouse
Date Received: 09/18/25

Sample ID: B-7 @ 5' **Lab ID: 542509-002** **Collected: 09/17/25 10:19**
Matrix: Soil

542509-002 Analyte	Result	Qual	Units	RL	DF	Batch	Prepared	Analyzed	Chemist
Method: EPA 6010B Prep Method: EPA 3050B									
Antimony	ND		mg/Kg	2.9	0.97	382723	09/23/25	09/24/25	TWJ
Arsenic	**19**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Barium	**100**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Beryllium	ND		mg/Kg	0.49	0.97	382723	09/23/25	09/24/25	TWJ
Cadmium	ND		mg/Kg	0.49	0.97	382723	09/23/25	09/24/25	TWJ
Chromium	**36**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Cobalt	**19**		mg/Kg	0.49	0.97	382723	09/23/25	09/24/25	TWJ
Copper	**36**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Lead	**14**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Molybdenum	**1.0**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Nickel	**29**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Selenium	ND		mg/Kg	2.9	0.97	382723	09/23/25	09/24/25	TWJ
Silver	**0.79**		mg/Kg	0.49	0.97	382723	09/23/25	09/24/25	TWJ
Thallium	ND		mg/Kg	2.9	0.97	382723	09/23/25	09/24/25	TWJ
Vanadium	**52**		mg/Kg	0.97	0.97	382723	09/23/25	09/24/25	TWJ
Zinc	**59**		mg/Kg	4.9	0.97	382723	09/23/25	09/24/25	TWJ
Method: EPA 7471A Prep Method: EPA 7471A									
Mercury	ND		mg/Kg	0.14	1	382738	09/24/25	09/24/25	MLL
Method: EPA 8015M Prep Method: EPA 3580M									
GRO C8-C10	ND		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
DRO C10-C28	ND		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
ORO C28-C44	ND		mg/Kg	20	0.99	382785	09/24/25	09/25/25	DIB
Surrogates				**Limits**					
n-Triacontane	92%		%REC	59-136	0.99	382785	09/24/25	09/25/25	DIB

Results for any subcontracted analyses are not included in this section.

ENTHALPY ANALYTICAL

Analysis Results for 542509

Sample ID: B-8 @1-5'	Lab ID: 542509-003	Collected: 09/17/25 07:30
	Matrix: Soil	

542509-003 Analyte	Result	Qual	Units	RL	DF	Batch	Prepared	Analyzed	Chemist
Method: EPA 6010B Prep Method: EPA 3050B									
Antimony	ND		mg/Kg	2.9	0.96	382723	09/23/25	09/24/25	TWJ
Arsenic	**16**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Barium	**82**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Beryllium	ND		mg/Kg	0.48	0.96	382723	09/23/25	09/24/25	TWJ
Cadmium	ND		mg/Kg	0.48	0.96	382723	09/23/25	09/24/25	TWJ
Chromium	**47**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Cobalt	**14**		mg/Kg	0.48	0.96	382723	09/23/25	09/24/25	TWJ
Copper	**33**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Lead	**14**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Molybdenum	ND		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Nickel	**29**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Selenium	ND		mg/Kg	2.9	0.96	382723	09/23/25	09/24/25	TWJ
Silver	**0.78**		mg/Kg	0.48	0.96	382723	09/23/25	09/24/25	TWJ
Thallium	ND		mg/Kg	2.9	0.96	382723	09/23/25	09/24/25	TWJ
Vanadium	**43**		mg/Kg	0.96	0.96	382723	09/23/25	09/24/25	TWJ
Zinc	**56**		mg/Kg	4.8	0.96	382723	09/23/25	09/24/25	TWJ
Method: EPA 7471A Prep Method: EPA 7471A									
Mercury	ND		mg/Kg	0.14	1	382738	09/24/25	09/24/25	MLL
Method: EPA 8015M Prep Method: EPA 3580M									
GRO C8-C10	ND		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
DRO C10-C28	ND		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
ORO C28-C44	ND		mg/Kg	20	0.99	382785	09/24/25	09/25/25	DIB
Surrogates				**Limits**					
n-Triacontane	79%		%REC	59-136	0.99	382785	09/24/25	09/25/25	DIB

Results for any subcontracted analyses are not included in this section.

ENTHALPY ANALYTICAL

Analysis Results for 542509

Sample ID: B-9 @ 1-5'	Lab ID: 542509-005	Collected: 09/17/25 13:23
	Matrix: Soil	

542509-005 Analyte	Result	Qual	Units	RL	DF	Batch	Prepared	Analyzed	Chemist
Method: EPA 6010B Prep Method: EPA 3050B									
Antimony	ND		mg/Kg	3.0	0.99	382723	09/23/25	09/24/25	TWJ
Arsenic	**19**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Barium	**120**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Beryllium	ND		mg/Kg	0.50	0.99	382723	09/23/25	09/24/25	TWJ
Cadmium	ND		mg/Kg	0.50	0.99	382723	09/23/25	09/24/25	TWJ
Chromium	**54**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Cobalt	**13**		mg/Kg	0.50	0.99	382723	09/23/25	09/24/25	TWJ
Copper	**32**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Lead	**28**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Molybdenum	**1.2**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Nickel	**36**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Selenium	ND		mg/Kg	3.0	0.99	382723	09/23/25	09/24/25	TWJ
Silver	**0.79**		mg/Kg	0.50	0.99	382723	09/23/25	09/24/25	TWJ
Thallium	ND		mg/Kg	3.0	0.99	382723	09/23/25	09/24/25	TWJ
Vanadium	**51**		mg/Kg	0.99	0.99	382723	09/23/25	09/24/25	TWJ
Zinc	**76**		mg/Kg	5.0	0.99	382723	09/23/25	09/24/25	TWJ
Method: EPA 7471A Prep Method: EPA 7471A									
Mercury	ND		mg/Kg	0.16	1.2	382738	09/24/25	09/24/25	MLL
Method: EPA 8015M Prep Method: EPA 3580M									
GRO C8-C10	ND		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
DRO C10-C28	**20**		mg/Kg	9.9	0.99	382785	09/24/25	09/25/25	DIB
ORO C28-C44	**84**		mg/Kg	20	0.99	382785	09/24/25	09/25/25	DIB
Surrogates				**Limits**					
n-Triacontane	90%		%REC	59-136	0.99	382785	09/24/25	09/25/25	DIB

ND Not Detected

Results for any subcontracted analyses are not included in this section.

ENTHALPY ANALYTICAL

Batch QC

Type:	**Blank**	**Lab ID:**	**QC1296393**	**Batch:**	**382723**
Matrix:	**Soil**	**Method:**	**EPA 6010B**	**Prep Method:**	**EPA 3050B**

QC1296393 Analyte	Result	Qual	Units	RL	Prepared	Analyzed
Antimony	ND		mg/Kg	3.0	09/23/25	09/24/25
Arsenic	ND		mg/Kg	1.0	09/23/25	09/24/25
Barium	ND		mg/Kg	1.0	09/23/25	09/24/25
Beryllium	ND		mg/Kg	0.50	09/23/25	09/24/25
Cadmium	ND		mg/Kg	0.50	09/23/25	09/24/25
Chromium	ND		mg/Kg	1.0	09/23/25	09/24/25
Cobalt	ND		mg/Kg	0.50	09/23/25	09/24/25
Copper	ND		mg/Kg	1.0	09/23/25	09/24/25
Lead	ND		mg/Kg	1.0	09/23/25	09/24/25
Molybdenum	ND		mg/Kg	1.0	09/23/25	09/24/25
Nickel	ND		mg/Kg	1.0	09/23/25	09/24/25
Selenium	ND		mg/Kg	3.0	09/23/25	09/24/25
Silver	ND		mg/Kg	0.50	09/23/25	09/24/25
Thallium	ND		mg/Kg	3.0	09/23/25	09/24/25
Vanadium	ND		mg/Kg	1.0	09/23/25	09/24/25
Zinc	ND		mg/Kg	5.0	09/23/25	09/24/25

Type:	**Lab Control Sample**	**Lab ID:**	**QC1296394**	**Batch:**	**382723**
Matrix:	**Soil**	**Method:**	**EPA 6010B**	**Prep Method:**	**EPA 3050B**

QC1296394 Analyte	Result	Spiked	Units	Recovery	Qual	Limits
Antimony	106.8	100.0	mg/Kg	107%		80-120
Arsenic	106.1	100.0	mg/Kg	106%		80-120
Barium	109.3	100.0	mg/Kg	109%		80-120
Beryllium	109.2	100.0	mg/Kg	109%		80-120
Cadmium	109.4	100.0	mg/Kg	109%		80-120
Chromium	106.5	100.0	mg/Kg	106%		80-120
Cobalt	110.5	100.0	mg/Kg	110%		80-120
Copper	100.7	100.0	mg/Kg	101%		80-120
Lead	112.2	100.0	mg/Kg	112%		80-120
Molybdenum	103.6	100.0	mg/Kg	104%		80-120
Nickel	111.7	100.0	mg/Kg	112%		80-120
Selenium	103.5	100.0	mg/Kg	104%		80-120
Silver	50.57	50.00	mg/Kg	101%		80-120
Thallium	110.5	100.0	mg/Kg	110%		80-120
Vanadium	106.1	100.0	mg/Kg	106%		80-120
Zinc	112.3	100.0	mg/Kg	112%		80-120

ENTHALPY ANALYTICAL

Batch QC

Type:	Matrix Spike	Lab ID:	QC1296395	Batch:	382723
Matrix (Source ID):	Soil (541938-024)	Method:	EPA 6010B	Prep Method:	EPA 3050B

QC1296395 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	DF
Antimony	49.82	ND	97.09	mg/Kg	51%	*	75-125	0.97
Arsenic	116.7	18.12	97.09	mg/Kg	102%		75-125	0.97
Barium	301.8	180.9	97.09	mg/Kg	125%		75-125	0.97
Beryllium	102.2	0.5298	97.09	mg/Kg	105%		75-125	0.97
Cadmium	100.2	0.3454	97.09	mg/Kg	103%		75-125	0.97
Chromium	148.7	44.88	97.09	mg/Kg	107%		75-125	0.97
Cobalt	112.5	10.85	97.09	mg/Kg	105%		75-125	0.97
Copper	132.7	29.80	97.09	mg/Kg	106%		75-125	0.97
Lead	108.9	6.609	97.09	mg/Kg	105%		75-125	0.97
Molybdenum	93.15	0.8584	97.09	mg/Kg	95%		75-125	0.97
Nickel	157.0	50.97	97.09	mg/Kg	109%		75-125	0.97
Selenium	98.13	1.849	97.09	mg/Kg	99%		75-125	0.97
Silver	47.89	0.6145	48.54	mg/Kg	97%		75-125	0.97
Thallium	100.7	ND	97.09	mg/Kg	104%		75-125	0.97
Vanadium	175.6	65.72	97.09	mg/Kg	113%		75-125	0.97
Zinc	168.5	63.37	97.09	mg/Kg	108%		75-125	0.97

Type:	Matrix Spike Duplicate	Lab ID:	QC1296396	Batch:	382723
Matrix (Source ID):	Soil (541938-024)	Method:	EPA 6010B	Prep Method:	EPA 3050B

QC1296396 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	RPD	RPD Lim	DF
Antimony	50.84	ND	98.04	mg/Kg	52%	*	75-125	1	35	0.98
Arsenic	122.6	18.12	98.04	mg/Kg	107%		75-125	4	20	0.98
Barium	309.0	180.9	98.04	mg/Kg	131%	*	75-125	2	31	0.98
Beryllium	106.9	0.5298	98.04	mg/Kg	108%		75-125	4	20	0.98
Cadmium	105.2	0.3454	98.04	mg/Kg	107%		75-125	4	20	0.98
Chromium	157.0	44.88	98.04	mg/Kg	114%		75-125	5	25	0.98
Cobalt	116.2	10.85	98.04	mg/Kg	107%		75-125	2	20	0.98
Copper	138.3	29.80	98.04	mg/Kg	111%		75-125	3	25	0.98
Lead	114.0	6.609	98.04	mg/Kg	110%		75-125	4	28	0.98
Molybdenum	97.80	0.8584	98.04	mg/Kg	99%		75-125	4	20	0.98
Nickel	162.9	50.97	98.04	mg/Kg	114%		75-125	3	29	0.98
Selenium	103.2	1.849	98.04	mg/Kg	103%		75-125	4	20	0.98
Silver	50.00	0.6145	49.02	mg/Kg	101%		75-125	3	20	0.98
Thallium	105.6	ND	98.04	mg/Kg	108%		75-125	4	20	0.98
Vanadium	182.2	65.72	98.04	mg/Kg	119%		75-125	3	20	0.98
Zinc	174.6	63.37	98.04	mg/Kg	113%		75-125	3	31	0.98

ENTHALPY ANALYTICAL

Batch QC

Type:	Post Digest Spike	Lab ID:	QC1296397	Batch:	382723
Matrix (Source ID):	Soil (541938-024)	Method:	EPA 6010B	Prep Method:	EPA 3050B

QC1296397 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	DF
Antimony	93.71	ND	96.15	mg/Kg	97%		75-125	0.96
Arsenic	111.9	18.12	96.15	mg/Kg	98%		75-125	0.96
Barium	271.1	180.9	96.15	mg/Kg	94%		75-125	0.96
Beryllium	95.31	0.5298	96.15	mg/Kg	99%		75-125	0.96
Cadmium	93.63	0.3454	96.15	mg/Kg	97%		75-125	0.96
Chromium	135.2	44.88	96.15	mg/Kg	94%		75-125	0.96
Cobalt	103.5	10.85	96.15	mg/Kg	96%		75-125	0.96
Copper	122.9	29.80	96.15	mg/Kg	97%		75-125	0.96
Lead	101.7	6.609	96.15	mg/Kg	99%		75-125	0.96
Molybdenum	92.56	0.8584	96.15	mg/Kg	95%		75-125	0.96
Nickel	144.4	50.97	96.15	mg/Kg	97%		75-125	0.96
Selenium	93.44	1.849	96.15	mg/Kg	95%		75-125	0.96
Silver	45.42	0.6145	48.08	mg/Kg	93%		75-125	0.96
Thallium	95.11	ND	96.15	mg/Kg	99%		75-125	0.96
Vanadium	157.2	65.72	96.15	mg/Kg	95%		75-125	0.96
Zinc	156.7	63.37	96.15	mg/Kg	97%		75-125	0.96

Type:	Serial Dilution	Lab ID:	QC1296481	Batch:	382723
Matrix (Source ID):	Soil (541938-024)	Method:	EPA 6010B	Prep Method:	EPA 3050B

QC1296481 Analyte	Result	Source Sample Result	Units	Qual	RPD	RPD Lim	DF
Antimony	ND	ND	mg/Kg				4.8
Arsenic	20.61	18.12	mg/Kg				4.8
Barium	192.4	180.9	mg/Kg				4.8
Beryllium	0.4710	0.5298	mg/Kg	J			4.8
Cadmium	ND	0.3454	mg/Kg				4.8
Chromium	47.81	44.88	mg/Kg				4.8
Cobalt	12.57	10.85	mg/Kg				4.8
Copper	29.27	29.80	mg/Kg				4.8
Lead	5.886	6.609	mg/Kg				4.8
Molybdenum	ND	0.8584	mg/Kg				4.8
Nickel	53.71	50.97	mg/Kg				4.8
Selenium	ND	1.849	mg/Kg				4.8
Silver	ND	0.6145	mg/Kg				4.8
Thallium	ND	ND	mg/Kg				4.8
Vanadium	68.67	65.72	mg/Kg				4.8
Zinc	68.04	63.37	mg/Kg				4.8

Type:	Blank	Lab ID:	QC1296448	Batch:	382738
Matrix:	Soil	Method:	EPA 7471A	Prep Method:	EPA 7471A

QC1296448 Analyte	Result	Qual	Units	RL	Prepared	Analyzed
Mercury	ND		mg/Kg	0.14	09/24/25	09/24/25

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Batch QC

Type: Lab Control Sample	Lab ID: QC1296449	Batch: 382738
Matrix: Soil	Method: EPA 7471A	Prep Method: EPA 7471A

QC1296449 Analyte	Result	Spiked	Units	Recovery	Qual	Limits
Mercury	0.8255	0.8333	mg/Kg	99%		80-120

Type: Matrix Spike	Lab ID: QC1296450	Batch: 382738
Matrix (Source ID): Soil (542659-001)	Method: EPA 7471A	Prep Method: EPA 7471A

QC1296450 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	DF
Mercury	1.099	0.1592	0.9091	mg/Kg	103%		75-125	1.1

Type: Matrix Spike Duplicate	Lab ID: QC1296451	Batch: 382738
Matrix (Source ID): Soil (542659-001)	Method: EPA 7471A	Prep Method: EPA 7471A

QC1296451 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	RPD	RPD Lim	DF
Mercury	1.147	0.1592	1.000	mg/Kg	99%		75-125	4	20	1.2

Type: Blank	Lab ID: QC1296600	Batch: 382785
Matrix: Soil	Method: EPA 8015M	Prep Method: EPA 3580M

QC1296600 Analyte	Result	Qual	Units	RL	Prepared	Analyzed
GRO C8-C10	ND		mg/Kg	10	09/24/25	09/24/25
DRO C10-C28	ND		mg/Kg	10	09/24/25	09/24/25
ORO C28-C44	ND		mg/Kg	20	09/24/25	09/24/25
Surrogates				**Limits**		
n-Triacontane	89%		%REC	59-136	09/24/25	09/24/25

Type: Lab Control Sample	Lab ID: QC1296601	Batch: 382785
Matrix: Soil	Method: EPA 8015M	Prep Method: EPA 3580M

QC1296601 Analyte	Result	Spiked	Units	Recovery	Qual	Limits
Diesel C10-C28	216.0	247.5	mg/Kg	87%		61-120
Surrogates						
n-Triacontane	8.224	9.901	mg/Kg	83%		59-136

Type: Matrix Spike	Lab ID: QC1296602	Batch: 382785
Matrix (Source ID): Soil (542622-061)	Method: EPA 8015M	Prep Method: EPA 3580M

QC1296602 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	DF
Diesel C10-C28	226.0	3.466	248.9	mg/Kg	89%		47-127	1
Surrogates								
n-Triacontane	8.523		9.955	mg/Kg	86%		59-136	1

ENTHALPY ANALYTICAL

Batch QC

Type:	**Matrix Spike Duplicate**	**Lab ID:**	**QC1296603**	**Batch:**	**382785**
Matrix (Source ID):	**Soil (542622-061)**	**Method:**	**EPA 8015M**	**Prep Method:**	**EPA 3580M**

QC1296603 Analyte	Result	Source Sample Result	Spiked	Units	Recovery	Qual	Limits	RPD	RPD Lim	DF
Diesel C10-C28	240.0	3.466	249.9	mg/Kg	95%		47-127	6	48	1
Surrogates										
n-Triacontane	8.776		9.995	mg/Kg	88%		59-136			1

* Value is outside QC limits
J Estimated value
ND Not Detected

Laboratory Job Number 542509

Subcontracted Products

AmeriSci Los Angeles

Please Reply To:

AmeriSci Los Angeles
24416 S. Main Street, Ste 308
Carson, California 90745
TEL: (310) 834-4868 • FAX: (310) 834-4772

LABORATORY ELECTRONIC TRANSMITTAL

To: Project Manager
Enthalpy Analytical
Fax #:

Email: incomingreports@enthalpy.com

From: Thu M. Nguyen
AmeriSci Job #: 925091225
Subject: PLM-Bulk-Qualitative 5 day Resul
Client Project: EO-542509

Date: Monday, September 29, 2025
Time: 10:39:28
Comments:

Number of Pages: _____
(including cover sheet)

NOTE: Attached report is to be considered preliminary until final review with accompanying analysis summary letter is issued.

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AmeriSci Los Angeles
24416 S. Main Street, Ste 308
Carson, California 90745
TEL: (310) 834-4868 • FAX: (310) 834-4772

PLM Bulk Asbestos Report

Enthalpy Analytical
Attn: Project Manager
931 W. Barkley Ave.

Orange, CA 92868

Date Received 09/23/25
Date Examined 09/27/25

RE: EO-542509

AmeriSci Job # 925091225
P.O. #
Page 1 **of** 1

Client No. / HGA	Lab No.	Asbestos Present	Total % Asbestos
542509-002	925091225-01	***No***	NVA [1]
Location: B-7 @ 5'			by Thu M. Nguyen on 09/27/25
Analyst Description: Brown, Heterogeneous, Non-Fibrous, Soil **Asbestos Types:** **Other Material:** NVA NAD			
542509-003	925091225-02	***No***	NVA [1]
Location: B-8 @ 1-5"			by Thu M. Nguyen on 09/27/25
Analyst Description: Brown, Heterogeneous, Non-Fibrous, Soil **Asbestos Types:** **Other Material:** NVA NAD			
542509-005	925091225-03	***No***	NVA [1]
Location: B-9 @1-5"			by Thu M. Nguyen on 09/27/25
Analyst Description: Brown, Heterogeneous, Non-Fibrous, Soil **Asbestos Types:** **Other Material:** NVA 100%			

Reporting Notes:

(1) Qualitative PLM result may not be reliable for soil, tape, dust or debris samples due to high variability in particle and aggregate size.

Analyzed by: Thu M. Nguyen
Date: 9/27/2025

Thum nguyen

Reviewed by: Arturo A. Aldana

Art Aldana

*NAD = no asbestos detected; Detection Limit <1%; Reporting Limits: CVES = 1%, 400 Pt Ct = 0.25%, 1000 Pt Ct = 0.1%; NA = not analyzed; NA/PS = not analyzed / positive stop; NVA = No Visible Asbestos; PLM (polarized light microscopy) Bulk Asbestos Analysis by EPA 600/R-93/116, including requirements for EPA 600/M4-82-020 per 40 CFR 763 (NVLAP Lab #200346-0); Note: PLM is not consistently reliable in detecting asbestos in floor coverings and similar NOB materials. TEM is currently the only method that can be used to determine if this material can be considered or treated as non-asbestos-containing in New York State (also see EPA Advisory for floor tile, FR 59, 146, 38970, 8/1/94). NIST Accreditation requirements mandate that this report must not be reproduced except in full with the approval of the laboratory. This PLM report relates ONLY to the items tested.

ENTHALPY ANALYTICAL

931 West Barkley Ave
Orange, CA 92868
(714) 771-6900

Subcontract Laboratory:
AmeriSci Los Angeles
24416 S. Main Street
Suite 308
Carson, CA 90745
ATTN: Sample Control
PO #: Required, to be sent via email

Enthalpy Order: EO-542509
PM: Taylor Nasu
Email: Taylor.Nasu@enthalpy.com
CC: incomingreports@enthalpy.com
Phone: (714) 771-6900

~~925909~~
9250912225

Results Due: Standard TAT
Report Level: II
Report To: RL
EDDs:

Notes:

Sample ID	Collected	Lab ID	# Cont.	Matrix	Analysis Requested	Comment
B-7 @ 5'	17-SEP-2025 10:19	542509-002	1	Soil	Asbestos by PLM	
B-8 @1-5'	17-SEP-2025 07:30	542509-003	1	Soil	Asbestos by PLM	
B-9 @ 1-5'	17-SEP-2025 13:23	542509-005	1	Soil	Asbestos by PLM	

Notes:	Relinquished By:	Received By:
		Brittany Rolle
	Date: 9/23/25 1325	Date: 9/23/25 1520
	Date:	Date:
	Date:	Date: